

Specification

Title of the Invention: Portland Cement Clinker, Cement Composition, and Method for Producing Portland Cement Clinker

Field of the Invention

[0001]

The invention relates to a novel cement clinker and a cement composition. In more detail, the invention relates to a cement clinker and a cement composition that exhibit good long-term strength development and are adapted to be baked at a relatively low temperature.

Background Art

[0002]

The cement industry is a mass-production and mass-consumption type industry, and in recent years, resource saving and energy saving have become a top priority due to environmental issues such as CO₂ emissions. For example, Portland cement, the most mass-produced cement, needs a clinker made by baking the raw materials adjusted to a predetermined chemical composition at a temperature as high as 1450 degree Celsius to 1550 degree Celsius. The baking process is the most energy-consuming process. In other words, if the clinker baking temperature is reduced, the energy consumption is reduced. To reduce the baking temperature of clinker, a technology has been developed with increasing C₄AF (4CaO, Al₂O₃, Fe₂O₃), one of the main clinker minerals, as a low-temperature baking-type clinker (see Patent Document 1).

[0003]

Further, effective utilization of wastes and by-products have become an important issue from the viewpoint of resource recycling. Taking advantage of the characteristics of the cement industry and cement manufacturing facilities, the reuse of wastes or waste disposal as raw materials or heat energy sources during cement production is effective for the safe and mass disposal of wastes. Many wastes and by-products have high Al₂O₃ content. In the above system of increasing C₄AF, the Al₂O₃ content of the cement clinker is increased compared to conventional Portland cement clinkers, and thus more wastes and by-products are used than in conventional Portland cement clinkers. In this respect, the low-temperature baking-type clinker described in Patent Document 1 has superior characteristics.

[0004]

Clinker with more C₃A (3CaO-Al₂O₃) or C₄AF among clinker minerals is also advantageous since it contains more Al₂O₃ and Fe₂O₃, so that more wastes and by-products containing these components can be used (e.g., Patent Document 2).

[0005]

On the other hand, with utilizing wastes and by-products, the components contained in the wastes and by-products are brought into the cement clinker. Not only CaO, SiO₂, Al₂O₃, and Fe₂O₃, which are the major components of cement clinker, but also other small amounts of components are introduced and affect the easy baking characteristics, actual mineral composition of clinker, and the physical properties of cement. Therefore, appropriate control of the small amount components is required. Results have been disclosed on the influence of small amount

components on the physical properties of the low-temperature baking-type clinker (e.g., Non-Patent Document 1). According to the literature, increasing the MnO content in the low-temperature baking-type clinker increases the long-term compressive strength at day 28.

References of Prior Art

[0006]

Patent Document 1: Japanese Patent Publication 2012-224504

Patent Document 2: Japanese Patent Publication 2004-352515

Non-patent Document

[0007]

Non-Patent Document 1 Masami Ohta et al., Abstracts of the 75th Cement Technology Conference, p.p. 20-21 (2021)

Summary of the Invention

Problem to be solved by the invention

[0008]

The low-temperature baking-type clinker is baked at a relatively low temperature and can consume a large amount of wastes containing Al_2O_3 and Fe_2O_3 . However, the C_2S ($2\text{CaO} \cdot \text{SiO}_2$) content, which has been considered to contribute to long-term strength development, is reduced compared to conventional Portland cement clinkers, for example, having the total C_3A and C_4AF content of about 20 mass% or less. As a result, the long-term strength development has tended to be lower to some extent. It is possible to increase the long-term strength development by adjusting the MnO content in the low-temperature baking-type clinker, as shown in Non-Patent Document 1. However, regarding other small content components, the long-term strength development is not clear. Therefore, the object of the invention is to provide a novel clinker baked at a relatively low temperature and has good long-term strength development.

Means for Solving the Problem

[0009]

The present inventors have studied diligently to solve the above problem and have found that when the low-temperature baking-type clinker has an adjusted BaO content of 0.8 to 1.4 mass% the clinker has a good long-term strength development compared to conventional low-temperature baking-type clinker, which has a small or no BaO content (low-temperature baking-type clinker with small BaO content).

[0010]

According to the first aspect of the present invention, a novel Portland cement clinker having the total C_3A and C_4AF content of 22 mass% or more, the C_3S ($3\text{C}_3\text{S} \cdot \text{SiO}_2$) content of 60 mass% or more, the iron modulus (I.M.) of 1.3 or less, calculated according to the Bogue's formulae, is provided and the cement clinker has the BaO content of 0.8 to 1.4 mass%. Preferably, the cement clinker has a C_4AF content of 15 mass% or more. The total C_3S and C_2S content is preferably 69 mass% or more.

[0011]

According to the second aspect of the present invention, the Portland cement clinker has the total C_3A and C_4AF content of 22 mass% or more, a C_3S modulus of 60 mass% or more, an iron modulus (I.M.) of 1.3 or less, respectively calculated according to the Bogue's formulae, and a BaO content of 0.8 to 1.4 mass%. To the Portland cement clinker, gypsum is added to produce a cement composition. The cement composition preferably contains one or more of the following admixtures selected from the group comprising blast furnace slag, siliceous admixture, fly ash, and limestone.

[0012]

Furthermore, according to the third aspect of the present invention, a novel low-temperature baking-type Portland cement clinker is produced by baking, at a temperature not less than 1300 degree Celsius and less than 1400 degree Celsius, the raw material comprising a CaO source, an SiO_2 source, an Al_2O_3 source, a Fe_2O_3 source, and a BaO source, having the total C_3A and C_4AF content after baking of 22 mass% or more, the C_3S content of 60 mass% or more, the iron modulus (I.M.) of 1.3 or less, respectively calculated according to the Bogue's formulae, and a BaO content of 0.8 to 1.4 mass%, in Portland cement clinker.

[0013]

Preferably, the Portland cement clinker has the total C_3A and C_4AF content of 22 mass% or more and 32 mass% or less, a C_3S content of 60% mass% or more and 70% mass% or less, and a C_2S content of 3 mass% or more and 18 mass% or less, and the total content of C_3A , C_4AF , C_3S , and C_2S is 100 mass% or less.

[0014]

The description of Portland cement clinker in this specification applies directly to both the cement composition and the method for producing Portland cement clinker. In principle, compositions are expressed as mass%, and when composition ranges are specified with upper and lower limits, the upper and lower limits are included, unless otherwise specified.

Advantageous Effects of the Invention

[0015]

According to the present invention, a novel cement clinker is provided such that it is producible by baking at a lower temperatures than conventional cement clinker, can consume an increased amount of waste materials, and has good long-term strength development (mortar compressive strength at day 28) compared to the ordinary low-temperature baking-type clinker with small BaO content.

Means for Solving the Problem

[0016]

The contents of C_3A , C_4AF , C_3S , and C_2S in Portland cement clinker (simply referred to as "cement clinker") according to the invention are determined according to the Bogue's formulae.

[0017]

The Bogue's formulae have been used in conjunction with the moduli and indices to calculate the approximate major compound composition using the major chemical analyses, and

have been well known to those skilled in the art. For the sake of clarity, the following is how to determine the amount of each mineral in cement clinker using the Bogue's formulae.

$$C_3S \text{ content} = (4.07 \times CaO) - (7.60 \times SiO_2) - (6.72 \times Al_2O_3) - (1.43 \times Fe_2O_3)$$

$$C_2S \text{ content} = (2.87 \times SiO_2) - (0.754 \times C_3S)$$

$$C_3A \text{ content} = (2.65 \times Al_2O_3) - (1.69 \times Fe_2O_3)$$

$$C_4AF \text{ content} = 3.04 \times Fe_2O_3$$

[0018]

The iron modulus (I.M.), hydraulic modulus (H.M.), silica modulus (S.M.), activity index (A.I.), and lime saturation degree (L.S.D.), are obtained using the major chemical compositions and are used as the characteristic values for cement clinker production control, and have been used and well known to those in the art. The calculation method of the iron modulus and so on are described below, as a precaution.

$$\text{Hydraulic Modulus (H.M.)} = CaO / (SiO_2 + Al_2O_3 + Fe_2O_3)$$

$$\text{Silica Modulus (S.M.)} = SiO_2 / (Al_2O_3 + Fe_2O_3)$$

$$\text{Iron Modulus (I.M.)} = Al_2O_3 / Fe_2O_3$$

$$\text{Activity Index (A.I.)} = SiO_2 / Al_2O_3$$

$$\text{Lime saturation Degree (L.S.D.)} = CaO / (2.8 \times SiO_2 + 1.2 \times Al_2O_3 + 0.65 \times Fe_2O_3)$$

[0019]

CaO, SiO₂, Al₂O₃, and Fe₂O₃ contents in the above can be measured according to the method in accordance with JIS R 5202 "Chemical Analysis Method for Portland Cement" and JIS R 5 204 "X-ray Fluorescence Analysis Method for Cement" respectively.

[0020]

As mentioned above, in the cement clinker according to the present invention, the contents of C₃A and C₄AF must total 22 mass% or more. If these contents are less than 22 mass%, it becomes difficult to obtain cement clinker with good physical properties such as strength development by baking at the low temperature. A more preferred total content is 24 mass% or more. As described below, 60 mass% or more of C₃S is required to obtain the high-strength development. Therefore, the total content of C₃A and C₄AF is limited up to 40 mass%. Preferably, it is 35 mass% or less, more preferably 32 mass% or less, and especially 28 mass% or less. Of these two components, C₄AF should be present alone at 15 mass% or more, because it can be sintered sufficiently even at low temperatures and the amount of f-CaO in the cement clinker can be reduced.

[0021]

The C₃S content is extremely important for the good strength development of cement compositions using the cement clinker according to the present invention (hereinafter simply "cement"). If this content is less than 60%, the good strength development cannot be obtained even if the total C₃A and C₄AF content and the iron modulus described below are within the specified range. The C₃S content is preferably 62 mas% or more and more preferably 63 mass% or more. Since the total C₃A and C₄AF content is at least 22 mass%, the upper limit of C₃S content is 78 mass%. In order to ensure some time from the start to the end of condensation, 70

mass% or less is preferred, and 65 mass% or less is further preferred.

[0022]

The cement clinker may further contain C_2S . The content should be not more than 18 mass%, preferably not more than 15 mass%, and not less than 3 mass%. From the viewpoint of obtaining long-term strength, the total content of C_3S and C_2S is especially preferred to be 69 mass% or more.

[0023]

The iron modulus (I.M.) of the cement clinker is not more than 1.3. If the iron modulus exceeds 1.3, sufficient good strength development (more specifically, for example, mortar strength development) cannot be obtained even if other requirements in the cement clinker according to the present invention are satisfied. Furthermore, if the iron modulus exceeds 1.3, the time from the start of setting to its termination tends to be too long. Therefore, the iron modulus should be not more than 1.3. A more preferred iron modulus range is 1.0 to 1.3, and especially preferred is 1.14 to 1.27.

[0024]

The hydraulic modulus and silica modulus are not particularly limited. However, in order to obtain an excellent balance of various properties, the hydraulic modulus is preferably 1.8 to 2.2, especially 1.9 to 2.1, and the silica modulus is preferably 1.0 to 2.0, especially 1.1 to 1.7.

[0025]

The most important point in the cement clinker according to the invention is to have a BaO content of 0.8 to 1.4 mass%. The BaO content in cement clinker can be measured using a general X-ray fluorescence analyzer, for example, by quantitative analysis such as a calibration curve method.

[0026]

When cement clinker with the above composition is prepared with usual raw materials, the cement clinker contains no or very small BaO. In contrast, by increasing the BaO content to 0.8 to 1.4 mass%, the cement clinker exhibits a good long-term strength development, compared to the low-temperature baking-type clinker with small BaO content. The reason for the good long-term strength development is assumed that C_2S in the low-temperature baking-type clinker is mainly in the β phase, but the Ba component stabilizes it to α or α' phase and improves the hydration reactivity. The more preferred BaO content is 0.8 to 1.3 mass%, and the particularly preferred BaO content is 0.9 to 1.2 mass%.

[0027]

The cement clinker according to the present invention containing BaO in the specific range has the characteristic of the good strength development compared to the low-temperature baking-type clinker with small BaO content.

[0028]

The cement clinker according to the present invention is producible by low-temperature baking, compared to conventional ordinary Portland cement clinker. Namely, while conventional ordinary Portland cement clinkers require a temperature of around 1450 degree Celsius for baking,

the cement clinker according to the present invention can be baked at a temperature between 1300-1400 degree Celsius.

[0029]

The method of producing cement clinker according to the present invention is not particularly limited, and the cement clinker is easily produced by preparing and mixing known cement (clinker) raw materials in a predetermined proportion to achieve of the needed mineral indices and moduli, and baking them in a known method (e.g. with SP kiln, NSP kiln, etc.).

[0030]

The preparation and mixing method of the cement raw materials can be made according to conventional methods. For example, the composition of wastes, by-products, and other raw materials (CaO sources such as limestone, quicklime, and slaked lime, SiO₂ sources such as silica stone, Al₂O₃ sources such as clay, Fe₂O₃ sources such as copper calamite and titanium calamite, etc.) are measured in advance, and the proportion of the materials is calculated from the proportion of the ingredients in the materials to mix the raw materials according to the proportion.

[0031]

The raw materials used in the manufacture of cement clinker are the same as those conventionally used in the manufacture of cement clinker, without any particular restrictions. It is also possible to use waste materials, by-products, etc.

[0032]

In the manufacture of cement clinker, the use of one or more wastes, by-products, etc. is desirable from the viewpoint of promoting the effective use of wastes, by-products, etc. Usable examples of wastes and by-products include blast furnace slag, steelmaking slag, nonferrous tailings, coal ash, sewage sludge, water purification sludge, paper sludge, construction soil, foundry sand, soot, incinerated fly ash, molten fly ash, chlorine bypass dust, wood chips, waste white clay, bota, waste tires, shells, municipal waste, and its incinerated ash, etc. (Note Some of them may be used as the raw materials for cement as well as a source of heat energy.)

[0033]

In particular, the cement clinker according to the present invention contains the large total content of C₃A and C₄AF, which are minerals with Al₂O₃ as a constituent element. Therefore, it has the advantage over conventional cement clinker in that it can be produced using more Al₂O₃-rich wastes and by-products.

[0034]

When the compound compositions and moduli are adjusted according to the Bogue's formulae, using the natural raw materials, wastes, and by-products, as described above, the BaO content in the cement clinker after baking does not reach 0.7%. Therefore, the BaO content in the cement clinker is adjusted by analyzing respective BaO contents in the raw materials: the natural raw materials; the wastes; and the by-products, and the ratio between respective raw materials is adjusted to achieve the prescribed BaO content. From the viewpoint of promoting effective use of wastes and by-products, it is preferable to use more wastes and more by-products with high BaO contents in the production process than before. Barium sulfate, barium carbonate, barium

chloride, barium hydroxide, industrial wastes including these barium compounds and soil contaminated with barium are appropriate. Cathode-ray panel glass wastes and sewage sludge incineration ashes are particularly suitable.

[0035]

However, some discrepancies may occur depending on the clinker baking conditions, and therefore, the chemical composition of the clinker after baking needs to be analyzed to determine the chemical compositions of the raw materials.

[0036]

The cement clinker according to the present invention is made into cement by mixing it together with gypsum after grinding or grinding separately, as conventional cement clinkers. Ordinary Portland cement, early-strength Portland cement, and ultra-early-strength Portland cement are examples of such cements. In addition to Portland cement, it can also be used as a component of various mixed cements and solidifiers such as soil solidifiers.

[0037]

When gypsum is added to the cement composition, any gypsum known as a raw material for cement production, such as dihydrate gypsum, semi-hydrate gypsum, and anhydrate gypsum, can be used without any particular restrictions. In the case of Portland cement, it is preferable to add gypsum so that the SO_3 content in the Portland cement is 1.5 to 5.0 mass%, and 1.8 to 3 mass% is more preferable. For the method of grinding the above cement clinker and gypsum, known techniques can be used without any particular restrictions.

[0038]

Materials such as blast furnace slag, siliceous admixture, fly ash, calcium carbonate, limestone, and so on, and a grinding admixture may be added to the cement composition, and then, the resultant mixture may be ground. The cement clinker may be ground first and then, the materials may be mixed. Chlorine bypass dust, and so on, may also be mixed.

[0039]

The powder degree of the cement composition is not limited, but should be adjusted to 2800-4500 cm^2/g in terms of Blaine specific surface area.

[0040]

If necessary, blast furnace slag, fly ash, etc. can be mixed after grinding to make blast furnace slag cement, fly ash cement, etc.

Embodiments

[0041]

The following embodiments illustrate the solution and advantageous effects of the present invention, but the invention is not limited to these embodiments.

[0042]

Comparative Examples 1 and 2 and Embodiments 1 and 2

Cement clinker raw materials were prepared using industrial raw materials, including wastes, and a reagent class BaCO_3 , and baked at 1360 degree Celsius for 100 minutes to produce

cement clinkers. The chemical compositions of the clinkers obtained after calcination are shown in Table 1, and the mineral compositions, according to the Bogue's formulae, and the moduli and indices are shown in Table 2. To 100 mass parts of the cement clinkers, 2.2 mass parts of dihydrate gypsum and 1.8 mass parts of semi-hydrate gypsum were mixed and ground to produce the cements with a Blaine specific surface area of $3200 \pm 50 \text{ cm}^2/\text{g}$. The results of mortar compressive strength measurements for each cement are shown in Table 3.

[0043]

The measurement methods used were as follows.

- (1) Measurement of chemical composition of cement clinker raw materials and cement clinker other than BaO: Measured by X-ray fluorescence analysis method according to JIS R 5204.
- (2) Measurement of BaO content of cement clinker: Measured by quantitative analysis using a scanning X-ray fluorescence spectrometer (ZSX Primus IV, Rigaku Corporation) with a calibration curve.
- (3) Measurement of mortar compressive strength: Measured by the method according to JIS R 5201.

[0044]

Table1

	Chemical Composition (mass%)												
	BaO	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	SO ₃	Na ₂ O	K ₂ O	TiO ₂	P ₂ O ₅	SrO	Cl
Comp.Ex. 1	0.0	19.60	7.00	5.61	65.54	0.87	0.18	0.17	0.29	0.34	0.12	0.04	0
Comp.Ex. 2	0.59	19.70	7.06	5.58	65.40	0.89	0.15	0.16	0.31	0.35	0.12	0.04	0
Emb.1	0.89	19.81	7.04	5.59	65.21	0.90	0.16	0.18	0.33	0.37	0.13	0.04	0
Emb.2	1.15	19.75	7.01	5.56	65.34	0.90	0.15	0.18	0.35	0.36	0.12	0.04	0

[0045]

Table 2

	Mineral Composition according to Bogue's Formulae				Moduli· Indices		
	C ₃ S	C ₂ S	C ₃ A	C ₄ AF	H.M.	S.M.	I.M
Comp.Ex. 1	63	9	9	17	2.03	1.55	1.25
Comp.Ex. 2	61	11	9	17	2.02	1.56	1.27
Emb.1	60	12	9	17	2.01	1.57	1.26
Emb.2	61	11	9	17	2.02	1.57	1.26

[0046]

Table 3

	Day 28 Mortar Compressive Strength (N/mm ²)
Comp.Ex. 1	58.3
Comp.Ex. 2	58.0
Emb. 1	60.2
Emb. 2	60.0

[0047]

Comparative Example 1 is a low-temperature baking-type clinker that does not contain BaO. The results of the embodiments and the comparative examples shall be discussed based on the result of the Comparative Example 1.

[0048]

Comparative Example 2 has a BaO content of less than 0.7 mass%, and the mortar compressive strength at day 28 is equivalent to that of Comparative Example 1.

[0049]

The Embodiments 1 and 2 are of the present invention, and the mortar compressive strengths of the cements at day 28 are higher than that of Comparative Example 1.

Claims :

Claim 1. A Portland cement clinker having the total C_3A and C_4AF content of 22 mass% or more, a C_3S content of 60 mass% or more, an iron modulus (I.M.) of 1.3 or less, respectively calculated according to the Bogue's formulae, and a BaO content of 0.8 to 1.4 mass%,.

Claim 2. The Portland cement clinker according to claim 1, wherein the C_4AF content is 15 mass% or more.

Claim 3. The Portland cement clinker according to claim 1 or 2, characterized in that the total C_3S and C_2S content is 69 mass% or more.

Claim 4. The Portland cement clinker according to claim 1, characterized in that the total C_3A and C_4AF content is not less than 22 mass% and not more than 32 mass%, the C_3S content is not less than 60% mass and not more than 70% mass, a C_2S content is not less than 3% mass and not more than 18 mass%, and a sum of the total C_3A and C_4AF content, the C_3S content, and the C_2S content is not more than 100% mass%.

Claim 5. A cement composition comprising the Portland cement clinker according to one of claims 1 to 4, further comprising gypsum.

Claim 6. The cement composition according to claim 5, further comprising at least one admixture selected from the group comprising blast furnace slag, siliceous admixture, fly ash, and limestone.

Claim 7. A method for producing Portland cement clinker,
mixing a CaO source, an SiO_2 source, an Al_2O_3 source, a Fe_2O_3 source, and a BaO source to a mixture
such that the total C_3A and C_4AF content is 22 mass% or more, a C_3S content is 60 mass% or more an iron modulus (I.M.) is 1.3 or less, respectively calculated according to the Bogue's formulae, and
a BaO content is not less than 0.8 mass% and not more than 1.4 mass%, in
Portland cement clinker after baking, and
baking the mixture at a temperature not less than 1300 degree Celsius and less than 1400 degree Celsius.

Claim 8. The method for producing Portland cement clinker according to claim 7, characterized by

mixing the CaO source, the SiO₂ source, the Al₂O₃ source, the Fe₂O₃ source, and the BaO source to the mixture

such that the total C₃A and C₄AF content is 22 mass% or more and 32 mass% or less, the C₃S content is 60 mass% or more and 70 mass % or less, a C₂S content is 3 mass% or more and 18 mass% or less, and

a sum of the total C₃A and C₄AF content, the C₃S content, and the C₂S content is not more than 100% mass%.