

5

10

Grounded socket and method for insulation fault location in an ungrounded power supply system including insulation monitoring

15

The invention relates to a grounded socket for insulation fault location and to a method for insulation fault location in an ungrounded power supply system including insulation monitoring by a standard insulation monitoring device superimposing a measuring voltage on the ungrounded power supply system for determining an insulation resistance of the ungrounded power supply system.

The network type of an ungrounded power supply systems, which is also referred to as an insulated network or as an IT (French: *isolé terre*) network, is used to ensure high availability and operational safety of the electrical power supply.

In this type of power supply system, the active parts of the IT network are separated from the ground potential, i.e., insulated against ground, or connected to ground via a high impedance. The frames (conductive housings) of the loads connected to the IT network are connected to the

ground potential (grounded) individually or jointly by means of a protective conductor.

The advantage of the IT networks is that an insulation fault (first fault), such as a ground fault or a fault to frame, will not affect the function of the connected loads since the ideally infinitely large impedance value means that no closed fault circuit can form between an active conductor of the IT network and ground. This inherent safety thus allows a continuous power supply of the loads fed by the ungrounded power supply system to be ensured even if a first insulation fault occurs. Hence, this network type is employed in particular in medically used areas.

Therefore, the resistance of the ungrounded power supply system against ground has to be constantly monitored since a possible other fault on another active conductor (second fault) would lead to a fault loop, and—in connection with an overcurrent protection device—the current flowing in this case would cause the installation to be shut down and operation to come to a halt.

The ungrounded power supply system is monitored according to standard IEC61557-8 using an insulation monitoring device (IMD) which is connected between at least one of the active conductors of the ungrounded power supply system and ground and superimposes a measuring voltage on the ungrounded power supply system, causing a measuring current to form which corresponds to the insulation fault and whose magnitude is in the μA range.

On the condition that the insulation state of the ungrounded power supply system is therefore continuously monitored by the insulation monitoring device, the ungrounded power supply system can continue to be operated indefinitely even if a first fault has occurred; however, it is advisable for the first fault to be removed as fast as practically possible.

When the insulation fault monitoring device has detected an insulation fault in a first step, the insulation fault search starts in a second step with a test device or the insulation monitoring device feeding a test current into the IT network by means of a test current generator. This test current, which is typically greater than the measuring current with a view to reliable detection and can be several milliamperes, is detected by all measuring current transformers located in a faulty line output (branch) of the ungrounded power supply system and is evaluated in evaluating electronics of an insulation fault evaluating device and displayed in a signaling device. The fault position can be located based on which circuit or line output the measuring current transformer is assigned to.

However, this solution, which corresponds to the general state of the art, does have several disadvantages.

First, the measuring current transformers are only assigned to the respective line outputs of the ungrounded power supply system and not to the individual connection points (sockets) for the loads.

Second, too long a period of time often goes by until the faulty line output is signaled, said period of time being mainly composed of the measuring time of the insulation monitoring device, the measuring time of the insulation fault searching device subsequently put into operation, and the duration until an alarm signal is registered at a signaling device, which is typically located at some distance from a socket. So if a faulty load is put into operation by plugging the feed line of the load into a socket in an operating theater, it can take up to 60 seconds or longer in practice until the medical personnel is informed via an optical display or an acoustic signal that an insulation fault is present in the respective line output or in a load connected to this branch. In this situation, a quick assignment of the insulation fault to a specific load is often not possible anymore. Usually, an electrician will have to determine the faulty load by a time-consuming manual insulation fault search.

In unexamined patent publication DE 102011083792 A1, an insulation fault searching device is described which allows direct assignment to a load. However, aside from the measuring current induced by the insulation monitoring device for determining the insulation resistance (first step), subsequent feeding of a test current for insulation fault search (second step) is still required there. After the insulation resistance measurement, a test current which can be detected at a grounded socket by a measuring current transformer is fed into the ungrounded power supply network. In this case, the detection times for a faulty load are still in the range of about 10 seconds. A method which allows signaling nearly in real time, i.e., immediately when the load connector is plugged into the socket, is currently unknown.

Therefore, the object of the present invention is to design a device and a method which allow a load exhibiting an insulation fault to be detected and signaled as fast and reliably as possible directly at the connection point of the load.

According to the invention, this object is attained by a grounded socket for insulation fault location comprising a housing having electrical contacts, a signaling device for signaling an insulation state and a current measuring device for detecting and evaluating a differential current, the current measuring device having a measuring current transformer and evaluating electronics and being configured for high-resolution detection and evaluation of a measuring current driven by the measuring voltage as a differential measuring current.

The idea of the present invention is advantageously based on high-resolution detection and evaluation of the present measuring current effected by the insulation monitoring device, which is mandatory according to standards, for the purpose of insulation resistance determination—instead of a measuring current generated specifically therefor—as a differential measuring current directly in a socket for the purpose of insulation fault location.

According to standards, the mandatory insulation monitoring device—which is not part of the invention—has to meet requirements regarding its internal resistance and the height of the measuring voltage, resulting in a maximum measuring current whose magnitude is in the μA range (microampere range).

The fact that a highly sensitive current measuring device in the μA range consisting of a measuring current transformer and evaluating electronics is used according to the invention allows the measuring current of the insulation monitoring device to be constantly monitored.

10 The measuring current driven by the measuring voltage of the insulation monitoring device is detected by the measuring current transformer as a differential measuring current and, once evaluated and signaled, allows an immediate assessment of an insulation fault.

For example, an increase in the measuring current from $10\ \mu\text{A}$ to $50\ \mu\text{A}$ after a faulty load has been plugged in is detected in the preferably microprocessor-based evaluating electronics and leads to immediate signaling of a deteriorated insulation state through an optical and/or acoustic signal.

20 The immediate high-resolution detection and evaluation of the measuring current directly at the connection point (socket) of the load renders feeding of a separate test current after detection of an insulation fault unnecessary. A time-consuming insulation fault search using automatic or manual insulation fault searching devices is no longer required.

Moreover, electrical safety is increased since the absence of test currents in the mA range (milliampere range) reduces the risk of malfunctions of high-sensitivity sensors in the power supply system and therefore increases the acceptance of selective insulation monitoring even in a critical system environment.

Furthermore, this has the advantage that medical areas do not have to be kept completely empty for the duration of a common insulation fault search.

In another advantageous embodiment, the current measuring device is
5 configured to detect and evaluate a fault current flowing at the network frequency of the ungrounded power supply system as a differential fault current.

In addition to high-resolution detection and evaluation of the measuring
current driven by the measuring voltage as a differential measuring
10 current, the current measuring device is capable of detecting and evaluating a fault current caused by a network voltage at network frequency in an ungrounded alternating-voltage power supply system as a differential fault current.

Since a leakage current flows across the always present leakage capaci-
15 tances in the ungrounded power supply system in the event of an asymmetrical insulation fault, said fault current can be detected as a differential fault current by the measuring current transformer. A change in this differential fault current due to the connection of a faulty load can be detected very quickly (in less than a second) by the current measuring
20 device and can be displayed by the signaling device through an optical and/or acoustic signal.

Advantageously, the current measuring device is AC/DC-sensitive.

This configuration allows (smooth) direct fault currents, pulsated direct fault currents and alternating fault currents to be detected and evaluated
25 in particular in ungrounded direct-voltage power supply systems and inverter-operated ungrounded power supply systems.

Furthermore, the current measuring device has a test loop routed through the measuring current transformer for generating a test current.

A test current corresponding to the measuring current of the insulation monitoring device and used to test the correct function of the differential current detection is generated in the current measuring device.

Advantageously, the evaluating electronics are configured to assess the
5 differential measuring current curve in order to effect synchronous insulation fault signaling between the insulation monitoring device and the grounded socket for insulation fault location.

The insulation monitoring device and the signaling device for signaling the insulation state disposed in the grounded socket for insulation fault
10 location according to the invention are typically installed at a distance from each other.

According to the state of the art, synchronization of the insulation fault display would require communication via a data interface, such as PowerLine, RS485 or MODBUS. Disadvantageously, this is very expensive and would necessitate additional installation measures.
15

Synchronous insulation fault signaling, on the other hand, allows an insulation fault to be displayed simultaneously in the grounded socket according to the invention and in the insulation monitoring device.

The differential measuring current curve for synchronous insulation fault
20 signaling is preferably assessed by detecting a change in amplitude of the differential measuring current.

Alternatively, the differential measuring current curve is assessed by detecting a change in pattern of the differential measuring current.

So by evaluating the curve over time of the measuring current detected
25 by the measuring current transformer as a differential measuring current in the evaluating electronics by means of threshold observation or correlation calculation, for example, the grounded socket according to

the invention receives information on whether an insulation fault is present from the insulation monitoring device.

Advantageously, the grounded socket according to the invention is realized as a permanently installed socket, as a mobile line coupler
5 (multiple socket) or as an adapter plug (adapter).

As the grounded socket for insulation fault location according to the invention is installed directly at the place where the load to be put into operation is connected, i.e., where the plug is plugged in, medical personnel immediately recognizes by means of the signaling device
10 whether an insulation fault is present on the load. The described increase in the measuring current of 10 μ A to 50 μ A, for example, after plugging in of the load supply line leads to immediate signaling of the insulation state at the socket in question.

The grounded socket can be realized as a permanently installed wall
15 socket or as an adapter plug in the form of an attachable adapter. Furthermore, a realization as a line coupler in the form of a multiple socket having multiple grounded sockets according to the invention for equipping an equipment cart, for example, is intended.

The described grounded socket according to the invention for insulation
20 fault location is based on the technical teaching described in independent method claim 7. In this respect, the technical effects mentioned above and the method-related advantages resulting therefrom also apply to the method features.

Other advantageous configuration features are apparent from the following
25 description and from the drawings, which illustrate preferred embodiments of the invention based on examples.

Fig. 1 shows a functional block diagram of a grounded socket according to the invention for insulation fault location;

Fig. 2 shows a grounded socket according to the invention as a permanently installed socket;

Fig. 3 shows a grounded socket according to the invention as an adapter plug;

5 **Fig. 4** shows a grounded socket according to the invention as a mobile line coupler;

Fig. 5 shows a grounded socket according to the invention having an omega symbol as an optical display;

10 **Fig. 6** shows a differential measuring current curve exhibiting a change in amplitude;

Fig. 7 shows a differential measuring current curve exhibiting a change in pattern; and

Fig. 8 shows a flow chart for synchronous insulation fault synchronization.

15 **Fig. 1** shows a grounded socket 10 according to the invention for insulation fault location in an ungrounded power supply system 2 (IT network) to which a load 6 is connected via active conductors L_1 , L_2 .

A standard insulation monitoring device 4 superimposing a measuring voltage U_m on the IT network is connected between active conductors L_1 , L_2 and ground PE for determining an insulation resistance R_f (insulation fault). A measuring circuit with a measuring current I_m driven by measuring voltage U_m forms via active conductors L_1 , L_2 , insulation resistance R_f and the protective conductor (protective conductor connection to ground PE) back to insulation monitoring device 4. Measuring current I_m is measured in insulation monitoring device 4 and allows an assessment of the magnitude of insulation resistance R_f .

20
25

As essential components, grounded socket 10 according to the invention comprises a current measuring device 12, a signaling device 14 and a housing 16 having contacts 17. Contacts 17 are realized as plug contacts for connecting a plug of a supply line of load 6.

- 5 Current measuring device 12 has a measuring current transformer 20, a toroidal core of which surrounds active conductors L_1 and L_2 as a primary “winding”, and evaluating electronics 22.

Measuring current transformer 20 detects measuring current I_m , which flows in the measuring circuit and continues as a differential measuring
 10 current I_{dm} in active conductors L_1 and L_2 , and transmits a differential current measurement result to evaluating electronics 22 via a secondary winding 24.

Evaluating electronics 22 are fed by a network voltage U_n of ungrounded power supply system 2.

- 15 Furthermore, current measuring device 12 comprises a test loop 15, by means of which a test current I_t is routed through measuring current transformer 20 to test the latter.

When an asymmetrical insulation fault R_f occurs, measuring current transformer 20 additionally detects a fault current I_f as a differential
 20 fault current I_{df} , which flows across always present leakage capacitances C_e of ungrounded power supply system 2.

Following **Figs. 2 to 5** show different embodiments of grounded socket 10 according to the invention. The outer dimensions of the respective
 25 embodiments correspond to the dimensions of a standard, grounding-compatible conventional socket.

In **Fig. 2**, grounded socket 10 according to the invention is realized as a permanently installed socket 32 in a wall outlet (wall socket) or for a cable duct installation, for example. At hand, signaling device 14 is

realized as an optical display 40 in the form of a lit LED ring. For example, the LED ring can light up green when no insulation fault has been located, and changes to yellow once an insulation fault has been located.

- 5 **Fig. 3** shows the configuration of grounded socket 10 according to the invention as an adapter plug 34 for a commercially available socket. This allows simple retrofitting of existing load connections with grounded socket 10 according to the invention for insulation fault location.

10 In another embodiment according to **Fig. 4**, grounded socket 10 according to the invention is realized as a mobile line coupler 36 (multiple socket). This embodiment permits an insulation fault location individual to the load since insulation fault location is integrated for one or more of the slots of the multiple socket 36.

15 As an example of the grounded socket 10 according to the invention realized as a permanently installed socket 32, **Fig. 5** shows a configuration of the signaling device 14 as an optical display 40 in the form of an omega symbol 42 for marking said socket as a grounded socket 10, 32 according to the invention including insulation fault location and therefor distinguishing it from conventional sockets without insulation fault
20 location.

Figs. 6 to 8 illustrate how the differential current measurement result is evaluated in evaluating electronics 22 by assessing differential measuring current curve I_{dm} to synchronize insulation fault signaling between insulation monitoring device 4 and grounded socket 10 according to the
25 invention.

Measuring current I_m driven by measuring voltage U_m continues at the location of measuring current transformer 20, i.e., in the socket, as differential measuring current I_{dm} and is constantly measured there in a phase T_1 . Evaluating electronics 22 test whether differential measuring

current I_{dm} exceeds a differential current threshold I_{dm1} (peak-peak amplitude) applying to the fault-free case. If differential current threshold I_{dm1} is not exceeded in said first phase T_1 , optical display 40 lights up green (**Fig. 8**).

- 5 If detected differential measuring current I_{dm} exceeds differential current threshold I_{dm1} , optical display 40 changes to a yellow-flashing display as a pre-warning (**Fig. 8**) in phase T_2 .

Once insulation monitoring device 4 detects an insulation fault in ungrounded power supply system 2—based on its longer evaluation time—,
 10 insulation monitoring device 4, which is to be programmed accordingly, reduces its internal resistance by an admissible value and thereby increases measuring current I_m . As detected differential measuring current I_{dm} , measuring current I_m thus exceeds a second differential current threshold I_{dm2} . This increase (amplitude modulation of the measuring
 15 currents) in phase T_3 is considered a criterion for an insulation fault report of insulation monitoring device 4, and yellow-flashing optical display 40 changes to a steady yellow display (**Fig. 8**).

Alternatively or additionally to the change in amplitude of measuring current I_m , a detected change in pattern of measuring current I_m (coding
 20 of the measuring current) can also cause the transition from second phase T_2 to third phase T_3 . Evaluating electronics 22 test whether the pattern of differential measuring current curve I_{dm} has changed from a pattern M_1 to a pattern M_2 by correlation calculation. If a change in pattern is detected, optical display 40 changes to a steady yellow display
 25 in phase T_3 (**Fig. 8**).

Claims

1. A grounded socket (10) for insulation fault location in an ungrounded power supply system (2) including insulation monitoring by a standard insulation monitoring device (4) superimposing a measuring voltage (U_m) on the ungrounded power supply system (2) for determining an insulation resistance (R_f) of the ungrounded power supply system (2),
the grounded socket (10) comprising
a housing (16) having electrical contacts (17),
a signaling device (14) for signaling an insulation state, and
a current measuring device (12) for detecting and evaluating a differential current (I_d , I_{dm} , I_{df}), the current measuring device (12) having a measuring current transformer (20) and evaluating electronics (22),
characterized in that
the current measuring device (12) is configured for high-resolution detection and evaluation of a measuring current (I_m) driven by the measuring voltage (U_m) as a differential measuring current (I_d , I_{dm}).
2. The grounded socket (10) for insulation fault location according to claim 1,
characterized in that
the current measuring device (12) is configured to detect and evaluate a fault current (I_f) flowing at a network frequency of the ungrounded power supply system (2) as a differential fault current (I_d , I_{df}).
3. The grounded socket (10) for insulation fault location according to claim 1 or 2,
characterized in that
the current measuring device (12) is AC/DC-sensitive.

4. The grounded socket (10) for insulation fault location according to any one of claims 1 to 3,
characterized in that
the current measuring device (12) has a test loop (15) routed through
the measuring current transformer (20) for generating a test current (I_t).
5
5. The grounded socket (10) for insulation fault location according to any one of claims 1 to 4,
characterized in that
10 the evaluating electronics (22) are configured to assess the differential measuring current curve (I_{dm}) in order to establish synchronous insulation fault signaling between the insulation monitoring device (4) and the device for insulation fault location (10).
6. The grounded socket (10) for insulation fault location according to any one of claims 1 to 5,
15 characterized by being realized as a permanently installed socket (32), as an adapter plug (34) or as a mobile line coupler (36).
7. A method for insulation fault location in an ungrounded power supply system (2) including insulation monitoring by a standard insulation monitoring device (4) superimposing a measuring voltage (U_m)
20 on the ungrounded power supply system (2) for determining an insulation resistance (R_f) of the ungrounded power supply system (2), the method comprising the method steps to be executed in a grounded socket according to any one of claims 1 to 6 of the invention:
25 detecting and evaluating a differential current (I_d , I_{dm} , I_{df}) by means of a current measuring device (12) having a measuring current transformer (20) and evaluating electronics (22),
signaling an insulation state by means of a signaling device (14),
characterized in that

a measuring current (I_m) driven by the measuring voltage (U_m) is detected and evaluated as a differential measuring current (I_d , I_{dm}) in high resolution by means of the current measuring device (12).

8. The method for insulation fault location according to claim 7,
5 characterized in that
a fault current (I_f) flowing at a network frequency of the ungrounded power supply system (2) is detected and evaluated as a differential fault current (I_d , I_{df}) by means of the current measuring device (12).
9. The method for insulation fault location according to claim 7 or 8,
10 characterized in that
the detection and evaluation by means of the current measuring device (12) is AC/DC-sensitive.
10. The method for insulation fault location according to any one of
claims 7 to 9,
15 characterized by the step of
generating a test current (I_t) which is routed through the measuring current transformer (20) of the current measuring device (12) by means of a test loop (15).
11. The method for insulation fault location according to any one of
20 claims 7 to 10,
characterized by the step of
assessing the differential measuring current curve (I_{dm}) by means of the evaluating electronics in order to synchronize insulation fault signaling between the insulation monitoring device (4) and the device for insulation fault location (10).
25
12. The method for insulation fault location according to claim 11,
characterized in that

the differential measuring current curve (I_{dm}) is assessed by detecting a change in amplitude of the differential measuring current (I_{dm}).

13. The method for insulation fault location according to claim 11 or 12, characterized in that

5 the differential measuring current curve (I_{dm}) is assessed by detecting a change in pattern (M_1 , M_2) of the differential measuring current (I_{dm}).