

Sealing Arrangement

The invention concerns a rubber elastic sealing ring between two concentric machine parts which move with respect to each other and which keep the sealing ring held in a groove in the first machine component opening towards the second machine component and consisting of a groove bottom and groove sides, the sealing ring seating, with a dynamic sealing edge, on one peripheral surface fashioned on a second machine component which forms, with a first surface extending from the dynamic sealing edge towards the low pressure side N, a first wedge-shaped gap, the sealing ring forming, with an outer peripheral surface supported on the bottom of the groove, a second wedge-shaped gap opening toward the low pressure side N, the sealing ring defining a first plane orthogonal to the rotational axis of the second machine component and intersecting the dynamic sealing edge beyond which a first and a second sealing ring section, separated by a cut, extend towards the high pressure side H, whereby the first sealing section is defined by at least one surface with one end at the dynamic sealing edge and the second sealing ring surface protrudes beyond the first sealing ring surface towards the high pressure side H and is formed by the outer peripheral surface and by a fourth and fifth plane intersecting each other and forming a shoulder and a line of intersection which is separated from the bottom of the groove and which defines a second plane running parallel to the rotational axis.

A seal of this type is known in the art through DE 37 38 512

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With the conventional seal, the sealing ring is surrounded at the low pressure side by a conically shaped support ring. The support ring largely accepts the forces acting on the sealing ring when pressure is applied so that the dynamic sealing edge is pressure relieved. Furthermore, a first wedge-shaped gap is arranged between the support ring and the sealing ring into which the sealing ring is drawn when pressure is applied. The first wedge-shaped gap is thereby closed by the application of pressure. A second wedge-shaped gap is provided for on the groove bottom in the conventional sealing ring which is zeroed by further application of pressure to thereby pressure relieve the dynamic sealing edge. By means of the tilt in the angle of the gaps and the roughness of the diagonal surfaces of the support ring, it is possible to adjust the pressuring force of the dynamic sealing edge to the particular pressure and material conditions.

Although the dynamic sealing edge is pressure relieved by the reaction of the conventional sealing ring to the application of pressure, a wedge-shaped gap, necessary for the return transport performance of a sealing ring, is not formed. Completely absent is a pressing gradient formed towards the low pressure side and having a flat dependence. For these reasons the dynamic sealing edge can be destroyed by extrusion and the life-time of the sealing ring can be reduced.

It is therefore the underlying purpose of the invention to further improve the conventional sealing configuration in such a fashion that, even in an unpressurized state, the gap

between the machine components is securely sealed and, in the pressurized state, improved endurance is exhibited.

This purpose is achieved in accordance with the invention in that a line of intersection between a third and a fourth plane, in which the outer peripheral surface and the first surface lie in the undeformed state of the sealing ring, is located in a space between the second plane and the peripheral surface and that the sealing ring is configured between the first plane and the low pressure side N as a solid body, and the sealing ring, seating in the groove in the unpressurized state, exhibits a third wedge-shaped gap which opens towards the bottom of the groove and is formed from the low pressure side of the groove and a bordering sealing ring surface.

The deformation-free state of the sealing ring in accordance with the invention refers to the shape of the sealing ring in which it is produced having an over-dimension with respect to the groove space when not under tension or pressure.

The expression solid body refers to a material section which is produced without substantial cuts and which exhibits deformation characteristics corresponding to a massive block of material.

The shape of the sealing ring in accordance with the invention is configured in such a fashion that the sealing ring, in the deformation-free state, exhibits a second wedge-shaped gap in the vicinity of the line of intersection of the bottom of the groove and the low pressure side of the groove. This second wedge-shaped gap is maintained, although

to a reduced extent, in the installed state as well as in the pressurized state of the sealing ring in accordance with the invention. The second wedge-shaped gap allows for the outward pivoting during operation of the sealing ring into the free space formed by the second wedge-shaped gap.

Furthermore the sealing ring in accordance with the invention, in the installed and non-pressurized state, exhibits a third wedge-shaped gap facing the bottom of the groove. This third wedge-shaped gap is closed under the application of pressure. The third wedge-shaped gap facilitates the pivoting out, for pressurized applications of the sealing ring, into the free space formed by the third wedge-shaped gap.

An increasing pressurization of the sealing rings leads, due to its rubber elastic material properties, to a contraction of the sealing ring in the axial direction and a stretching of the sealing ring in the radial direction. The sealing ring in accordance with the invention can deform in such a fashion that pivotings into the second and third wedge-shaped gaps are possible. The dynamic sealing edge can, in this fashion, be pressure relieved.

The tendency of the sealing elements to extrude is also significantly improved. The sealing ring in accordance with the invention thereby has the essential advantage that a substantial interference between the sealing ring and the groove space is, in the installed state of the sealing ring, reduced in such a fashion that increased pressure does not occur on the dynamic sealing edge. The sealing edge thereby exhibits reduced frictional values relative to conventional sealing rings. Thereby reduced wear and increased endurance

result.

A stable pressure distribution establishes itself in the vicinity of the sealing edge so that one guarantees that the first wedge-shaped gap opening towards the low pressure side N is always maintained. The first wedge-shaped gap remains undiminished even following very long operating times. In this fashion the return transport drag performance of a fluid from the low pressure region into the high pressure region is guaranteed when the second machine component is, for example, a rod exercising a back and forth motion relative to the first machine component.

The first wedge-shaped gap facing towards the low pressure side N in the vicinity of the dynamic sealing edge is in direct functional relationship with the second wedge-shaped gap in the vicinity of the groove bottom. In the installed pressurized state, corresponding forces are present on the sealing ring in accordance with the invention in the vicinity of the first and the second wedge-shaped gaps. The working connection between the first and the second wedge-shaped gaps is facilitated by the mutual alignment of the outer peripheral surface and the first surface of the sealing ring. The alignment is determined by the position of the line of intersection of the defined third and fourth planes and of the third wedge-shaped gap.

The biasing of the rubber elastic sealing ring in accordance with the invention in the installed state transpires through material deformation of the sealing ring shape largely in front of the sealing edge so that one guarantees that nearly no biasing forces act in the radial direction in the low pressure region of the sealing ring in the area behind the

sealing edge.

The degree of deformation of the sealing ring in accordance with the invention in the installed and in the pressurized state can also be influenced through the selection of the elastic material.

A cut in the sealing ring in accordance with the invention separates two sealing ring sections facing the high pressure side H. The cut acts, under application of pressure, like a hinge which can be opened or closed under the action of loads of greater or lesser strength. A sealing ring configured in this fashion can, as a so-called check valve, reliably transport fluid from the low pressure side to the high pressure side when the fluid on the low pressure side N is subjected to a larger force than the fluid on the high pressure side H.

In an improvement of the invention the sealing ring, in the installed state, forms a second wedge-shaped gap with the low pressure side of the groove which opens towards the bottom of the groove and which, for low pressure sealing ring applications, exhibits a larger radial extent than for high pressure sealing ring applications. This has the advantage that the pressure response of the sealing ring in accordance with the invention can be individually adjusted to particular applications. Low as well as strong fluid pressure increases can produce a comparable pressure relief on the dynamic sealing edge of the the sealing ring to the extent that the sealing ring shape is configured in accordance with the concept of the invention.

In further configurations of the invention the sealing ring,

in the pressurized state, is separated from the bottom of the groove in the corner region of the groove bottom and at the low pressure side of the groove. This has the advantage that the dynamic sealing edge of the sealing ring is capable of pressure relief to the extent that the sealing ring can be pressed by means of an increased fluid pressure into the free space at the low pressure side of the groove bottom.

In a further embodiment of the present invention the solid body of the sealing ring exhibits, in the deformation-free state, an axial length which is limited to 2.2 times the length of the second sealing ring section and the sealing ring surface, in the deformation-free state of the sealing ring, runs parallel to the low pressure side of the groove.

This has the advantage that the solid body of the sealing ring in accordance with the invention, due to its rubber elasticity, is deformable in such a fashion that, when pressure is applied, the third wedge-shaped gap is closed and the second wedge-shaped gap is reduced. The sealing ring is thereby capable of reacting to increased applied pressures by pressure relieving the dynamic sealing edge.

In a particularly preferred embodiment of the sealing ring in accordance with the invention, the sealing ring exhibits the third wedge-shaped gap in the installed unpressurized state due to a deformation.

The sealing ring in accordance with the invention is pivoted during installation in that it is strongly pressed against the low pressure side of the groove. Towards this end the sealing ring can be configured in a partial section of the third wedge-shaped gap which opens towards the bottom of the

groove. In this fashion the free space located on the low pressure side, as defined by the second wedge-shaped gap, is automatically enlarged when installing the sealing ring and, under the application of pressure, the sealing ring in accordance with the invention can fill-up this free space in that it is pressed into this free space to a greater or lesser degree by the applied pressure. In this fashion a sealing ring is created which, with increased fluid pressure, can, depending on the dimensions, be ever increasingly pressure relieved.

In a further embodiment of the present invention, the solid body of the sealing ring exhibits, in the deformation-free state, an axial length which is larger than 2.2 times the length of the second sealing ring section, and the sealing ring exhibits, in its finished state, a sealing ring surface which slants with respect to the rotational axis and which defines, in the installed and pressureless states of the sealing ring and together with the low pressure side of the groove, the third wedge-shaped gap.

Sealing rings in accordance with the invention of this length are, due to their torsion stiffness, no longer capable of pivoting in order to form a third wedge-shaped gap towards the low pressure side. Also with these embodiments, which can be installed in a rectangularly shaped groove, a third wedge-shaped gap establishes itself due to the slanted sealing ring surface.

In another improvement of the sealing ring in accordance with the invention the solid body portion of the sealing ring, which exceeds 2.2 times the axial length of the second section of the sealing ring, exhibits a second outer

peripheral surface forming an angle relative to the bottom of the groove which is smaller than the angle between the first outer peripheral surface and the bottom of the groove.

Due to a reduced tilting of the second outer peripheral surface relative to the first outer peripheral surface, the pressurized sealing ring can seat over an increased area on the low pressure side of the groove and on the groove bottom. The static sealing seating behaviour of the sealing ring is thereby stabilized. The reliability of the static sealing thereby positively influences the stabilization of the pressure distribution of the sealing ring, in particular at the dynamic sealing edge.

Further advantages can be derived from the description of the accompanying drawing. Likewise the above mentioned features and those which are to be described further below in accordance with the invention can be utilized individually or collectively in arbitrary combination. The embodiments mentioned are not to be taken as exhaustive enumeration rather have exemplary character only.

The invention is represented in the drawing and will be described more closely with regard to the embodiments.

Fig. 1 shows a cross-section of a sealing ring in accordance with the invention whose solid body, in the deformation-free state, exhibits an axial length which is limited to 2.2 times the length of the second sealing ring section in the deformation-free state;

Fig. 2 shows a cross-section of a sealing ring in

accordance with the invention according to Fig. 1 in the installed state;

Fig. 3 shows a cross-section of the sealing ring in accordance with the invention according to Fig. 1 in the pressurized state;

Fig. 4 shows a cross-section of the sealing ring in accordance with the invention whose solid body, in the deformation-free state, exhibits an axial length which is larger than 2.2 times the length of the second sealing ring section in the deformation-free state.

The individual figures of the drawing show the object in accordance with the invention in a strongly schematic fashion and are not to be taken to scale. The individual proportions of the sealing ring can differ as long as one guarantees that the finished sealing ring exhibits an over dimension at the high pressure side H relative to the groove provided for which changes into an under dimension towards the low pressure side.

The same reference symbols are utilized for the same features in Figures 1 through 4.

Fig. 1 shows a sealing configuration 10 comprising a first machine component 11, a second machine component 12 and a sealing ring 13. The concentric machine components 11, 12 can move with respect to each other. That is to say, the machine components can exercise a rotation or a back and forth motion relative to each other.

A groove 14 is formed in the first machine component 11 which opens towards a peripheral surface 15 of the second machine component 11. The groove 14, for its part, is formed from a high pressure groove side 16, a low pressure groove side 17, and a groove bottom 18. The machine components 11, 12 are separated from each other by means of a gap 19.

The sealing ring 13 exhibits a rotational axis 20 which corresponds to the symmetry axis of the second machine component 12. A dynamic sealing edge 21 of the sealing ring 13 is formed from the line of intersection of a first surface 22 and a second surface 23. Clearly, the second surface 23 can also extend up to the step in the sealing ring 13. The first surface 22 forms, together with the peripheral surface 15, a first wedge-shaped gap 24 which opens towards the low pressure side N even when the seal is pressurized (see Fig. 3). An outer peripheral surface 25 is formed on the sealing ring 13 opposite the groove bottom 18 which, in the vicinity of a static seal, is adjacent to the bottom of the groove 18.

In Fig. 1, the sealing ring 13 is shown in the completely unloaded produced state. The sealing ring 13 is, in Fig. 1, assigned to a groove 14, whereby the groove bottom 18 is shown with dot-dashed lines so that the outer contours of the sealing ring 13 in the produced, non-biased state, can be shown. An interference can be seen in Fig. 1, that is to say, the sealing ring 13 is over-dimensioned relative to the groove 14.

The sealing 13 furthermore exhibits two sealing ring sections 28, 29 separated by a cut 26 which project beyond a first plane 27 towards the high pressure side H. The first

plane 27 runs perpendicular to the rotational axis 20 through the sealing edge 21. The first sealing ring section 28 is defined by the second surface 23 and a third surface 30. The second sealing ring section 29 is defined by a fourth surface 31 and a fifth surface 32. The fourth surface 31 and the fifth surface 32 intersect each other at a line of intersection 33 to form a shoulder. The line of intersection 33 defines a second plane 34 which runs parallel to the rotational axis 20 through the line of intersection 33. The outer peripheral surface 25 lies in a third plane 35 which has a common line of intersection 37 with a fourth plane 36. The fourth plane 36 is defined in that the first surface 22 lies therein. The line of intersection 33 is located in a space which is defined by the peripheral surface 15 and the second plane 34.

The outer peripheral surface 25 which borders on the high pressure sided fourth surface 31 of the sealing ring 13, is tilted relative to the rotational axis 20, whereby the rotational axis 20 defines an angle α_1 with the outer peripheral surface 25. It can be seen from the figure that the over-dimensioning which is formed in the region of the line of intersection of the outer peripheral surface 25 and the high pressure sided fourth surface 31, ends in the vicinity of the dynamic sealing edge 21. In the remaining region of the outer surface 25, the sealing ring 13 is produced with an under-dimensioning, that is to say, a second wedge-shaped gap 38 forms in the vicinity of the groove bottom 18 and of the low pressure side of the groove 17. The sealing ring 13 itself is produced in such a fashion that it is adjacent, at one of its radially extended sealing ring surfaces 39, to the low pressure side of the groove 17.

Fig. 2 shows a cross-section of the sealing ring 13 in the installed state between the machine components 11, 12. The sealing ring 13 seats, via the dynamic sealing edge 21, on the peripheral surface 15 of the second machine component 12. The sealing ring 13 is biased in the groove 14 so that the sealing ring 13 is deformed in such a fashion that an angle α_2 between the rotational axis 20 and the outer peripheral surface 25 is established which is smaller than the angle α_1 as shown in Fig. 1. The second wedge-shaped gap is maintained in the vicinity of the low pressure side of the groove 17 towards the groove bottom 18 even after installation of the sealing ring 13. By means of the deformation of the sealing ring 13 in the installed state, the third wedge-shaped gap 40 is formed between the low pressure side of the groove 17 and the adjacent sealing surface 39 of the sealing ring 13. The first wedge-shaped gap 24 is also formed in the installed state.

Fig. 3 shows the sealing ring 13 of Fig. 1 and Fig. 2 in the pressurized state. H designates the high pressure side and N the low pressure side. The sealing ring 13 exhibits, as seen from the high pressure side H, the cut 26 which serves the function of a hinge under the application of pressure. The sealing ring 13 is, under pressure, pressed into the free space defined by the second and third wedge-shaped gaps 38, 40. The sealing edge 21 is pressure relieved by the deflection of the sealing ring 13. The first wedge-shaped gap 24 as well as the second wedge-shaped gap 38 are also present under the application of pressure. The third wedge-shaped gap 40 can completely close under the application of pressure so that the sealing edge surface 39 seats on the low pressure side of the groove 17.

Fig. 4 shows a sealing configuration 50 which comprises a first machine component 51, a second machine component 52 and a sealing ring 53. The concentric machine components 51, 52 can move with respect to each other. That is to say, the machine components can exercise a rotation or a back and forth motion with respect to each other.

A groove 54 is formed in the first machine component 51 which opens towards the peripheral surface 55 of the second machine component 52. The groove 54 itself is formed from a high pressure side of the groove 56, a low pressure side of the groove 57 and a groove bottom 58. The machine components 51, 52 are separated from each other by means of a gap 59.

The sealing ring 53 exhibits a rotational axis 60 which corresponds to the symmetry axis of the second machine component 52. A dynamic sealing edge 61 of the sealing ring 53 is formed from the line of intersection of a first surface 62 and a second surface 63. Clearly, the second surface 63 can also extend up to the step in the sealing ring 53. The first surface 62 forms a first wedge-shaped gap 64 with the peripheral surface 55 which, even when the seal is subjected to pressure, is opened towards the low pressure side N (see Fig. 3). A first outer peripheral surface 65 is formed on the sealing ring 53 opposite the groove bottom 58 which is adjacent to the bottom of the groove 58 in the vicinity of a static seal.

Fig. 4 shows the sealing ring 53 in a completely unloaded state, as it is produced. The sealing ring 53 is, in Fig. 4, assigned to a groove 54 whereby the bottom of the groove 58 is shown as a dot-dashed line so that the outer contours of the sealing ring 53 in the produced non-pressurized state

can be shown. An interference can be seen in Fig. 4, that is to say, the sealing ring 53 exhibits an over-dimension relative to the groove 54.

The sealing ring 53 furthermore exhibits two sealing ring sections 68, 69 which are separated by a cut 66 and which extend past a first plane 67 towards the high pressure side H. The first plane 67 runs perpendicular to the rotational axis 60 through the sealing edge 61. The first sealing ring section 68 is defined by the second surface 63 and a third surface 70. The second sealing ring section 69 is defined by a fourth surface 71 and a fifth surface 72. The fourth surface 71 and the fifth surface 72 intersect each other at an intersection line 73 and form a shoulder. The line of intersection 73 defines a second plane 74 which runs parallel to the rotational axis 60 through the line of intersection 73. The first outer peripheral surface 65 lies in a third plane 75 which shares a common line of intersection 77 with a fourth plane 76. The fourth plane 76 is defined in that the first surface 62 lies therein. The line of intersection 77 is located in a region which is defined by the peripheral surface 55 and the second plane 74.

The first outer peripheral surface 65, which borders on the high pressure sided fourth surface 71 of the sealing ring 53, is tilted relative to rotational axis 60, whereby the rotational axis 60 defines an angle α_1 relative to the first outer peripheral surface 65. As can be seen in the figure, the over-dimensioning which is formed in the region of the line of intersection of the first outer peripheral surface 65 and the high pressure sided fourth surface 71 ends in the vicinity of the dynamic sealing edge 61. In the remaining

region of the first outer peripheral surface 65, the sealing ring 53 is produced with an under-dimension, that is to say, a second wedge-shaped gap 78 forms in the vicinity of the groove bottom 58 and of the low pressure side of the groove 57. A second outer peripheral surface 79 of the sealing ring 53 forms an angle with the groove bottom 58 which is smaller than the angle between the first outer peripheral surface 65 and the groove bottom 58.

The sealing ring 53 itself is manufactured in such a fashion that it seats with a slanted sealing ring surface 80 on the low pressure side of the groove 57 in such a fashion that, in the deformation-free state of the sealing ring 53, a third wedge-shaped gap 81 is formed. The wedge-shaped gap 81 is defined by the groove side 57 and the sealing ring surface 80. The third wedge-shaped gap 81 closes with increasing applied pressure so that the sealing ring surface 80 seats with its entire radial length on the low pressure side of the groove 57.

A sealing ring 13 between two concentric mutually movable machine components 11, 12 is manufactured from a rubber elastic material and is inserted in a groove 14 which is opened from the first machine component 11 towards the second machine component 12. The sealing ring 13 exhibits an over dimension relative to the groove 14 in which the sealing ring 13 is to be inserted which is formed at the high pressure side region of the sealing ring 13. In the low pressure sided region of the sealing ring 13, the sealing ring 13 is manufactured with an under dimension. The outer peripheral surface 25 lying across from the bottom of the groove 18 exhibits, in the completely unloaded state of the sealing ring 13, an angle α_1 relative to a rotational axis

20 which, in the installed position of the sealing ring 13, is reduced to an angle α_2 . The second wedge-shaped gap 38, formed in the installed state of the sealing ring 13 in the vicinity of the low pressure side of the groove 17 and of the groove bottom 18, is also maintained in the pressurized state of the sealing ring 13. A first wedge-shaped gap 24 is formed between the peripheral surface 15 of the second machine component 12 and the sealing ring 13 which also is maintained under applied pressure.

A rubber elastic sealing ring 13 is arranged between two concentric machine components 11, 12 which move relative to each other. The sealing ring 13 exhibits a surface 22 which, on the one hand, ends in a dynamic sealing edge 21 and, on the other hand, extends towards the low pressure side N. Furthermore, an outer peripheral surface 25 is formed on the sealing ring 13 which is slanted to the groove bottom 18 when the sealing ring 13 is not pressurized. Imaginative planes 35, 36 which are also conically extending annular surfaces forming a line of intersection 37 extend through the conical annular surfaces 22, 25. The line of intersection 37 is always disposed between a plane 34 (annular surface) and the peripheral surface 15 of the second machine component 12.



Claims

1. Rubber elastic sealing ring (13; 53) between two concentric machine components (11, 12; 51, 52) which can move relative to each other and which hold the sealing ring (13; 53) in place within a groove (14; 54) in the first machine component (11; 51) opening towards the second machine component (12; 52) and formed from a groove bottom (18; 58) and groove sides (16, 17; 56, 57), whereby the sealing ring (13; 53) seats, with a dynamic sealing edge (21; 61) on a peripheral surface (15; 55) formed on the second machine component (12; 52) constituting, together with a first surface (22; 62) which extends from the dynamic sealing edge (21; 61) towards the low pressure side N, a first wedge-shaped gap (24; 64), the sealing ring (13; 53) forming, with an outer peripheral surface (25; 65) supported on the bottom of the groove (18; 58), a second wedge-shaped gap (38; 78) opening towards the low pressure side N, the sealing ring (13; 53) defining a first plane (27; 67) which is orthogonal to the rotational axis (20; 60) of the second machine component (12; 52), which intersects the dynamic sealing edge (21; 61), and beyond which a first and a second sealing ring section (28, 29; 68, 69), separated from each other by means of a cut (26; 66), project towards the high pressure side H, whereby



the first sealing ring section (28; 68) is defined by at least one surface (22, 23; 62, 63) having an end at the dynamic sealing edge (21; 61) and the second sealing ring section (29; 69) projects beyond the first sealing ring section (28; 68) in the direction towards the high pressure side H and is formed by the outer peripheral surface (25; 65) and by fourth and fifth mutually intersecting surfaces (31, 32; 71, 72) which form a shoulder and a line of intersection (33; 73) separated from the bottom of the groove (18, 58) and defining a second plane (34; 74) running parallel to the rotational axis (20; 60), characterized in that a line of intersection (37; 77) of a third and a fourth plane (35, 36; 75, 76) in which the outer peripheral surface (25; 65) and the first surface (22; 62), in the deformation-free state of the sealing ring (13; 53), are located lies in a region between the second plane (34; 74) and the peripheral surface (15; 55), and the sealing ring (13; 53) is configured as a solid body between the first plane (27; 67) and the low pressure side N, and the sealing ring (13; 53), in the state in which it is installed in the groove (14; 54) and not subjected to pressure, exhibits a third wedge-shaped gap (40; 81) which opens towards the bottom of the groove (18; 58) and which is formed by the low pressure side of the groove (17; 57) and an adjacent sealing ring surface (39; 80).

2. Sealing ring according to claim 1, characterized in that the third wedge-shaped gap (40; 81) exhibits, for low pressure sealing ring applications, a larger radial extension than for high pressure sealing ring applications.



3. Sealing ring according to claim 1 or 2 characterized in that the sealing ring (13; 53) is, in the pressurized state, separated in the corner region between the bottom of the groove (18; 58) and the low pressure side of the groove (17; 57) from the groove bottom (18; 58).
4. Sealing ring according to one of the preceding claims, characterized in that the solid body of the sealing ring (13), in the deformation-free state, exhibits an axial length which is limited to 2.2 times the length of the second sealing ring section (29) and the sealing ring surface (39), in the deformation-free state of the sealing ring (13), runs parallel to the low pressure side of the groove (17).
5. Sealing ring according to claim 4, characterized in that the sealing ring (13), in the installed pressureless state, exhibits the third wedge-shaped gap (40) due to a deformation.
6. Sealing ring according to one of the claims 1 through 3, characterized in that the solid body of the sealing ring (53), in the deformation-free state, exhibits an axial length which is larger than 2.2 times the length of the second sealing ring section (69) and the sealing ring (53), in the completed state, exhibits a sealing ring surface (80) which is slanted relative to the rotational axis and, in the installed and pressureless state of the sealing ring (53), defines together with the low pressure side of the groove (57) the third wedge-shaped gap (81).



7. Sealing ring according to claim 6, characterized in that the solid body portion of the sealing ring (53) which exceeds 2.2 times the axial length of the second sealing ring section (69), exhibits a second outer peripheral surface (79) which forms an angle with the bottom of the groove (58) which is smaller than the angle between the first outer peripheral surface (65) and the bottom of the groove (58).