

CROSS-FLOW WIND TURBINE

Cross Reference to Related Applications

This application is a continuation-in-part of United States Patent Application
5 serial number 10/831,515 entitled "Wind Turbine Having Airfoils for Blocking and
Directing Wind and Rotors With or Without a Central Gap" by Ronald Taylor and
Scott Taylor, filed April 23, 2004, which claims the benefit of and priority to United
States Provisional Patent Application serial number 60/467,773 entitled "Wind
Turbine" by Ronald Taylor and Scott Taylor, filed April 30, 2003. The present patent
10 application further claims the benefit of U.S. Provisional Patent Application Serial
No. 60/639,448, filed on December 23, 2004, entitled "Cross-Flow Wind Turbine."
The entire contents of the above mentioned applications are hereby specifically
incorporated herein by reference for all they disclose and teach.

15 Background of the Invention

a. Field of the Invention

The present invention pertains generally to wind turbines and more
particularly to cross-flow wind turbines.

20 b. Description of the Background

Wind turbines have provided a valuable source of alternative energy.
Constant improvements in wind turbine systems have been made over the past few
years. Most of the wind turbine systems in use today are axial-flow systems that are
otherwise known as propeller systems. In axial-flow wind turbine systems, air travels
25 in a direction that is substantially parallel to the rotating axis of the wind turbine. The
large propeller blades are driven by the wind at a rotational speed that creates tip
speeds of the blade that can range from approximately six to nine times the speed of
the wind. Tip speeds of over several hundred miles an hour can be achieved in
moderately strong to strong winds which will cause axial-flow wind turbines to break
30 apart. Hence, expensive braking systems and systems for feathering the angle of the
blades must be used to control the speed of axial-flow wind turbines in moderately
strong to strong winds. As a result, axial-flow wind turbines are inefficient in
moderately strong to strong winds and, as such, are unable to extract power from wind

energy when it is at its greatest energy producing level. In effect, axial-flow wind turbines are designed for use in light to moderate winds.

Further, axial-flow wind turbines are very dangerous to birds. Birds are frequently killed by the inability of these avians to sense the presence of the rapidly
5 moving blades of the axial-flow wind turbines.

Cross-flow wind turbines constitute a different class of wind turbines. See United States Patent Application 10/831,515, entitled "Wind Turbine Having Airfoils for Blocking and Directing Wind and Rotors With or Without a Central Gap," filed April 23, 2004, and United States Patent 6,015,258, entitled "Wind Turbine," issued January 18, 2000, the entire contents of which is hereby incorporated herein by reference for all it discloses and teaches. In cross-flow wind turbines, the wind flows across the rotors in a direction that is substantially normal to the axis of the rotating shaft. Cross-flow wind turbines have certain advantages over axial-flow wind turbines, but have not previously been seriously considered as a source of alternative energy because of the comparatively lower efficiencies with respect to the axial-flow wind turbines. An advantage of the cross-flow wind turbine is that the tip speed of the rotors of the cross-flow wind turbines move at a maximum speed that is only slightly greater than the speed of the wind. As such, cross-flow turbines can operate equally as well in both low and high wind conditions. In addition, the cross-flow wind turbine is easily seen by birds resulting in no avian deaths. Cross-flow wind turbines are also much quieter than the axial-flow wind turbines, primarily because the cross-flow wind turbines do not move at a high rate of speed and do not create a substantial amount of turbulence.

25 **Summary of the Invention**

The present invention overcomes the disadvantages and limitations of the prior art by providing a cross-flow wind turbine that has greatly increased efficiencies.

The present invention may therefore comprise a method of capturing wind energy using a cross-flow wind turbine in an efficient manner comprising the steps of:

30 generating a low pressure area on a leading face of a rotor blade by accelerating the flow of air across the surface of an airfoil stator that is positioned to form a predetermined gap between the rotor blade and the air foil stator during a power stroke of the rotor blade; using a blocking stator to substantially block wind from

impeding movement of the rotor blade during a return cycle of the rotor blade and directing the substantially blocked wind to a trailing face of the rotor during the power stroke of the rotor blade so as to create a pressure differential between the leading face and the rotor blade and the trailing face of the rotor blade during the power stroke that creates a force that rotates the rotor blade in an efficient manner.

The present invention may further comprise a cross-flow wind turbine system that is capable of capturing wind energy with high efficiency over a wide range of wind speeds comprising: a rotor having two semicircular shaped rotor blades; an airfoil stator positioned to capture and accelerate wind across an airfoil surface of the airfoil stator and provide a gap having a predetermined size between the rotor blades and the airfoil surface so that a negative pressure area is formed on a leading face of the rotor blades as the rotor blades pass by the airfoil surface during a power stroke; and a blocking stator positioned to substantially block wind from impeding upon a leading face of the rotor blades during a return cycle, that is opposite to the power stroke, and direct wind that is blocked by the blocking stator onto a trailing face of the rotor blades during the power stroke such that a pressure differential is created between the leading face of the rotor blades and the trailing face of the rotor blades during the power stroke that creates a force that rotates the rotor blade in an efficient manner.

Brief Description of the Drawings

In the drawings,

Figure 1A is a top schematic view of one embodiment of the invention.

Figure 1B provides typical dimensions of the embodiment of Figure 1A.

Figure 2 is a schematic illustration of another embodiment of the invention.

Figure 3 is an efficiency graph illustrating efficiencies of the embodiment of Figure 1A based on wind direction.

Figure 4A is an illustration of pressure gradients that are produced by the embodiment of Figure 1A as calculated from computer simulations using computational fluid dynamics.

Figure 4B is an efficiency graph of the embodiment of Figure 4A.

Figure 5 is a wind velocity and directional flow diagram of the embodiment of Figure 4A.

Figure 6A is an illustration of pressure gradients that are produced by the embodiment of Figure 6A as calculated from computer simulations using computational fluid dynamics.

Figure 6B is an efficiency graph of the embodiment of Figure 6A.

5 Figure 7 is a wind velocity and directional flow diagram of the embodiment of Figure 6A.

Figure 8A is an illustration of pressure gradients that are produced by the embodiment of Figure 8A as calculated from computer simulations using computational fluid dynamics.

10 Figure 8B is an efficiency graph of the embodiment of Figure 8A.

Figure 9 is a wind velocity and directional flow diagram of the embodiment of Figure 8A.

Figure 10A is an illustration of pressure gradients that are produced by the embodiment of Figure 10A as calculated from computer simulations using computational fluid dynamics.

Figure 10B is an efficiency graph of the embodiment of Figure 10A.

Figure 11 is a wind velocity and directional flow diagram of the embodiment in Figure 10A.

Figure 12A is an illustration of pressure gradients that are produced by the embodiment of Figure 12A as calculated from computer simulations using computational fluid dynamics.

Figure 12B is an efficiency graph of the embodiment of Figure 12A.

Figure 13 is a wind velocity and directional flow diagram of the embodiment of Figure 12A.

25 Figure 14A is an illustration of pressure gradients that are produced by the embodiment of Figure 14A as calculated from computer simulations using computational fluid dynamics.

Figure 14B is an efficiency graph of the device of Figure 14A.

Figure 15 is a wind velocity and directional flow diagram of the embodiment of Figure 14A.

Figure 16A is an illustration of pressure gradients that are produced by the embodiment of Figure 16A as calculated from computer simulations using computational fluid dynamics.

Figure 16B is an efficiency graph of the embodiment of Figure 16A.

Figure 17 is a wind velocity and directional flow diagram of the device of Figure 16A.

Figure 18A is an illustration of pressure gradients that are produced by the embodiment of Figure 18A as calculated from computer simulations using
5 computational fluid dynamics.

Figure 18B is an efficiency graph of the embodiment illustrated in Figure 18A.

Figure 19 is a wind velocity and directional flow diagram of the embodiment illustrated in Figure 18A.

Figure 20A is an illustration of pressure gradients that are produced by the
10 embodiment of Figure 20A as calculated from computer simulations using computational fluid dynamics.

Figure 20B is an efficiency graph of the embodiment illustrated in Figure 20A.

Figure 21 is a wind velocity and directional flow diagram of the embodiment illustrated in Figure 20A.

Figure 22A is an illustration of pressure gradients that are produced by the
15 embodiment of Figure 22A as calculated from computer simulations using computational fluid dynamics.

Figure 22B is an efficiency graph of the embodiment of Figure 22A.

Figure 23 is a wind velocity and directional flow diagram of the embodiment
20 of Figure 22A.

Figure 24 is a schematic illustration of the manner in which the embodiment of Figure 1A can be constructed.

Figure 25 is an isometric view of the embodiment of Figure 1A.

Figure 26 is an isometric view of the embodiment of Figure 1A viewed from a
25 different orientation.

Figure 27 is an isometric view of the rotor of the embodiment of Figure 1A.

Figure 28 is a schematic illustration that shows one manner of coupling the shaft of the rotor to a generator.

Figure 29 is a schematic illustration that shows another manner of coupling the
30 shaft to the generator.

Detailed Description of the Invention

Figure 1A is an illustration of one embodiment of a cross-flow wind turbine 100. The cross-flow wind turbine includes an air foil stator 102 that is fixed, stator 104 that is fixed and stator 106 that is also fixed. The rotor 108 rotates in response to forces created by wind. Rotor 108 includes rotor blade 110, rotor blade 112 and a rotating shaft 114. The cross-flow wind turbine 100, illustrated in Figure 1A, is designed for maximum efficiency for wind flowing in a primary direction 116 which may be aligned with the prevailing wind at a specific geographical location. However, the cross wind flow turbine 100 also produces high efficiencies for winds flowing from other directions, as described in more detail below with respect to Figure 3.

As also shown in Figure 1A, the angular positions of the stators are shown with respect to the primary wind flow direction 116. The cross-flow wind turbine 100 that is illustrated in Figure 1A shows each of the elements generally in their relative proportional sizes with respect to each other. It is believed that scaling of the cross-flow wind turbine 100 will not change the relative proportional sizes of the various elements or their location with respect to each other. It is anticipated that as the cross-flow wind turbine 100 is scaled to larger sizes that Reynolds numbers and differences in flow characteristics on larger scales will result in higher efficiencies as compared to wind tunnel testing of the cross-flow wind turbine 100. Rotor blade 110 and rotor blade 112 are attached to the shaft 114 so that as the rotor blades 110, 112 are moved by the wind, shaft 114 rotates. Rotor blades 110, 112, as illustrated in Figure 1A, have shapes that are circular arcs of 120°. Empirical data gathered from both wind tunnel testing and computational fluid dynamics indicate that the 120° circular arc shape of rotor blades provides the highest efficiency.

The air foil stator 102 that is shown in Figure 1A has a cambered profile that acts like an airplane wing so that air flowing across surface 118 of air foil stator 102 is accelerated. The accelerated flow of air across surface 118 creates a low pressure region on the leading face 120 of rotor blade 110 which helps to pull the rotor blade 110 through its power stroke. Because the wind flowing in the primary wind flow direction 116 is pushing on the trailing face 122 of rotor blade 110, a large pressure differential exists between the trailing face 122 and the leading face 120 of rotor blade 110. This large pressure differential assists the rotor blade 110 in moving in a

counterclockwise direction around the shaft 114. The pressure gradients created are disclosed in more detail in Figure 4A. Stator 104 is positioned to block wind, flowing from the primary wind flow direction 116, from impinging upon the leading face of the rotor blades during the return cycle, which is illustrated by the position of the rotor blade 112 in Figure 1A. Stator 104 not only blocks wind from hitting the rotor blades during the return cycle, but also redirects the wind flowing from direction 116 to impinge upon the trailing face 122 of the rotor blade 110.

Stator 106 of Figure 1A functions to guide the air flow on the downwind side of the rotor 108 away from the cross-flow wind turbine 100. Stator 106 also provides a third leg of a tripod structure to add structural rigidity to the system. Stator 106 also can perform other valuable functions. Wind flow studies for many geographical locations have provided data that the prevailing wind flows from a predominant direction during the windy season, which may, for example, be Winter season at many geographical sites. During the opposite season (off-season), such as Summer, the wind typically comes from a substantially opposite direction. Although the wind flow in the off-season may be only a fraction of the wind flow from the primary season, it still may be advantageous to capture the off-season wind with some degree of efficiency and convert it to mechanical energy. As can be seen from Figure 1A, stator 106 can assist in redirecting wind into rotor blade 112 when the wind is from a direction 130 that is opposite to the primary wind flow direction 116. In that regard, it may also be desirable in some embodiments to provide camber to the stator 106 so that it creates an air foil, in a manner similar to the air flow stator 102. However, the primary purpose of the stator 106 is to provide structural rigidity and to assist the flow of wind in exiting the turbine without creating back pressure that would impede the performance of the cross-flow wind turbine 100.

Of course, to provide structural rigidity, stator 106 could be replaced with simply a structural member. Depending on the wind studies of a particular area, replacement of stator 106 with a structural member may make sense if the wind flow direction is almost exclusively from direction 116. Wind flow from direction 132 would allow stator 106 to function in a manner similar to stator 104, i.e., stator 106 would block wind from direction 132 during the return cycle of the rotor blades and redirect the wind to the trailing face of the rotor blades during the power stroke. Hence, if off-season wind comes from direction 132, as shown in Figure 1A, stator 106 may provide advantageous properties for the cross-flow wind turbine 100.

Collected wind data from wind studies at a large majority of geographical sites have shown that a very large percentage (up to 90% or more) of the wind comes from the same quadrant as the prevailing wind direction. These studies have also shown that winds during the off-season are usually from the opposite quadrant, as indicated
5 above. For example, if the primary wind flow direction 116 is the primary wind direction during the windy season, wind typically flows from direction 130 during the off season, at most geographical sites. However, the off-season winds carry only a fraction of the energy that is available from the winds in the primary wind flow direction in most geographical sites. Hence, the system of Figure 1A is optimized for
10 wind coming from the quadrant of the prevailing wind such that the primary flow direction 116 is aligned with the prevailing wind flow direction when the cross-flow wind turbine is installed at a site. As discussed in more detail with respect to Figure 3, the system shown in Figure 1A is an omni-directional system which has optimized efficiencies for a primary wind flow direction 116 and reduced efficiencies when the
15 wind flows from a direction other than the primary wind flow direction 116. Again, however, the largest overall efficiency and the best return on investment comes from optimization of a system that captures wind from the prevailing wind direction for most geographical sites.

The embodiment of Figure 1A has produced the highest efficiencies of the
20 various embodiments disclosed herein for wind tunnel testing. Computer simulations using computational fluid dynamics have shown that the embodiment of Figure 2 provides the highest efficiencies. Empirical data collected from live testing of full scale systems will provide the best data as to which embodiment provides the highest efficiencies.

25 Figure 1B provides a list of dimensions for both a 10 kilowatt cross-flow wind turbine having a total height of 33 feet and 1000 kilowatt turbine having a total height of 230 feet for the embodiment of Figure 1A. Again, it is believed that the dimensions of these devices scale linearly with size.

Figure 2 illustrates another embodiment 200 of a cross-flow wind turbine.
30 The embodiment of Figure 2 utilizes a stationary shaft 202. The shaft 202 remains stationary as the rotor blades 204, 206 rotate around the shaft 202. As can be seen from Figure 2, stationary shaft 202 has a recessed portion which causes a gap 208 to form between the end of the rotor blade 206 adjacent to the shaft and the recessed portion of the shaft. Hence, a gap opens up between the inside end of the rotor and

the shaft during certain portions of the cycle which causes deventing of the wind captured by the rotor blades during the power stroke. The wind that is vented through the gap 208 is directed towards rotor blade 206 to assist rotor blade 206 in moving through the return cycle. This is disclosed in more detail below. In other words, wind
5 captured by the trailing face 212 of the rotor blade 204 is directed through the gap 208 and flows onto the trailing face 210 of the rotor blade 206 to create positive pressure on the trailing face 210.

Figure 3 is a graph illustrating efficiencies of the cross-flow wind turbine 100 that is illustrated in Figure 1A, versus the direction of wind flow. As can be seen
10 from Figure 3, the highest efficiencies are obtained from wind flowing from directions of approximately 10° to 335°. In these directions, efficiencies of 40% to 45% are achieved. When the wind flows from the directions of approximately 210° to 240°, efficiencies range from 35% to 37%. In addition, reasonable efficiencies can be obtained in the range of 27% to 29% when the wind flows from the direction of 90° to
15 120°. Hence, the cross-flow wind turbine 100 illustrated in Figure 3 is somewhat omni-directional, but clearly achieves the highest efficiencies of over 40% between 10° and 335°.

Figure 4A illustrates pressure gradients calculated by computer simulations using computational fluid dynamics for cross-flow wind turbine 100. The scale
20 shows positive pressures as lighter shades and negative pressures as darker shades. As can be seen from Figure 4A, large negative pressures are created on the leading face 120 of rotor blade 110 as rotor blade 110 passes by air foil stator 102 during the power stroke. The large negative pressures created on the leading face 120 of rotor blade 110 result from the accelerated air flow across the surface of air foil stator 102.
25 These negative pressures function to pull the rotor blade 110 in a counterclockwise direction around the shaft. Positive pressure indicated by lighter shades is created on the trailing face 122 of the rotor blade 110. The large differential in pressure created between the trailing face 122 and the leading face 120 of the rotor blade 110 creates a large amount of force on rotor blade 110 to cause the rotor blade 110 to rotate in a
30 counterclockwise direction around the shaft 114. This large amount of force created during the power stroke of the cross-flow wind turbine 100 results in higher efficiencies.

Figure 4B is an illustration of instantaneous efficiency and average efficiency of a single rotor blade versus time for the embodiment of Figure 1A. As can be seen

from Figure 4B, the average efficiency illustrated by plot 402 ranges between 28% and 32%. The plot 404 is the instantaneous calculated efficiency for the leading face 120 of rotor blade 110 of the embodiment illustrated in Figure 1A.

The efficiency graphs, such as graph 4B are calculated from computational
 5 fluid dynamics simulations on a computer. In the computational fluid dynamics simulations, the blades complete a full rotation every second. The dynamic loads on the blades are shown for one half revolution. A half second window shows all of the cyclical force patterns as the patterns repeat over the next half revolution with the forces on the blades reversed. Non-dimensional pressure coefficients are measured at
 10 each time step as the blades rotate through this half cycle. The pressure on the blades is a function of the pressure coefficient and the reference flow head,

15 $P = C_p \times q_{ref}$; where q_{ref} is the reference flow head.

$q_{ref} = 1/2 \rho (U_{ref})^2$ where $\rho = \text{air density}$
 $U_{ref} = \text{upstream velocity measured at mid-rotor height}$

20 The moments on each blade face, which act to produce energy when they are positive, are then summed and plotted as the overall efficiency. The graphs only illustrate a single blade. Hence, the average efficiency plot 402 is generated from the addition of efficiencies calculated for both blades. The practical result is that another set of plots that are 180° out of phase with the plots shown are added to the plots that are shown
 25 in Figure 4B, as well as the other efficiency graphs illustrated herein.

The efficiency of the turbine in the wind tunnel and full scale is calculated from the following formulas:

Power Available in the Wind:

30

$$P_w = \frac{1}{2} \rho A S^3 \quad [\text{Watts}]$$

$P_w = \text{power available in the wind}$

$\rho = \text{air density, kg/m}^3$

$= 1.225 \text{ kg/m}^3 \text{ @ sea level}$

$A = \text{rotor swept area, m}^2$

$= \text{rotor height x rotor diameter}$

$S = \text{wind speed, m/s}$

35

Turbine Power:

40

$$P_t = \text{Rotor Torque (Nm) x Rotational Velocity (rad/sec)} \quad [\text{Watts}]$$

Turbine Efficiency:

$$\% \text{ Efficiency} = (P_t/P_w) \times 100$$

- 5 Once the turbine's efficiency is determined, the turbine power can also be calculated by:

$$P_t = P_w \times \text{efficiency} = \frac{1}{2} \rho A S^3 \times \text{eff}$$

- 10 Figure 5 is a wind velocity and directional flow diagram that illustrates the direction of flow of the wind and its intensity. As is illustrated in Figure 5, the wind accelerates in the gap between the air foil stator 102 and rotor blade 110 as a result of the air flow characteristics of the air foil stator 102 that causes the wind to accelerate on the surface 118 of airfoil stator 102. The length of the arrows in Figure 5 illustrate
- 15 the magnitude of the speed of the wind. As shown in Figure 5, large wind velocities are created along the leading face of the rotor blade 120 which are directed to the trailing face of rotor 112. The large velocities along the surface of the leading face of the rotor blade 110 create a negative pressure while the wind impinging upon the trailing face of rotor 112 create a positive pressure. In addition, stator 104 directs the
- 20 wind so that it impinges upon the trailing face of rotor blade 110.

- Figure 6A illustrates pressure gradients calculated by computer simulations using computational fluid dynamics for the cross-flow wind turbine 200 that is illustrated in Figure 2. Scale 602 shows positive pressures as lighter shades and negative pressures as darker shades. In a manner similar to Figure 4A, large negative
- 25 pressures are created on the leading face of rotor blade 204 as the rotor blade 204 passes by the air foil stator 214 during the power stroke. The large negative pressures created on the leading face of rotor blade 204 result from the accelerated air flow across the surface of air foil stator 214. These negative pressures function to pull the rotor blade 204 in a counter-clockwise direction around the shaft 202. Positive
- 30 pressure indicated by lighter shades is created on the trailing face of the rotor blade 204. The large differential pressure created between the leading face and the trailing face of the rotor blade 204 creates a large amount of force on the rotor blade 204 to cause the rotor blade 204 to rotate in a counter-clockwise direction around the shaft 202. This large amount of force created during the power stroke of the cross-flow
- 35 wind turbine 200 results in higher efficiencies. The gap 208 functions to prevent the trailing face of the rotor blade 204, as described above. Wind flows through the gap

208 an impinges upon the trailing face of rotor blade 206. This helps to increase the pressure on the trailing face of rotor blade 206 and minimize the effect of any negative pressures on the trailing face of rotor blade 206 during the return cycle of the rotor blades.

5 Figure 6B is an illustration of the instantaneous efficiency and average efficiency of a single rotor blade versus time for the embodiment of Figure 2. As can be seen from Figure 6B the average efficiency illustrated by plot 602 ranges between 33% and 35%. Plot 604 is the instantaneous efficiency of the leading face of the rotor blades of the embodiment of Figure 2, while plot 606 illustrates the instantaneous
10 efficiency of the trailing face of the rotor blades of the embodiment of Figure 2.

 Figure 7 is a wind velocity and directional flow diagram that illustrates the direction of flow of the wind and its intensity for the embodiment of Figure 2. As illustrated in Figure 7, the wind accelerates in the gap between the air foil stator 214 and the rotor blade 204 as a result of the flow characteristics of the air foil stator 214
15 that cause the wind to accelerate on the surface of the air foil stator 214. The length of the arrows in Figure 7 illustrate the magnitude of the speed of the wind. As also shown in Figure 7, large wind velocities are created along the leading face of the rotor blade 204 that are directed to the trailing face of rotor blade 206. In addition, wind flowing through the gap 208 also impinges on the trailing face of rotor blade 206.
20 Figure 7 provides a good visual impression of the wind flow characteristics of the embodiment of Figure 2.

 Figure 8A illustrates the pressure gradients calculated by computer simulations using computational fluid dynamics for the embodiment of the cross-flow wind turbine that is illustrated in Figure 8A. The embodiment of the cross-flow wind
25 turbine illustrated in Figure 8A is very similar to the embodiment illustrated in Figure 2, with the exception that the stationary shaft 802 is somewhat larger, thereby creating a larger gap during certain portions of the cycle of rotation. In addition, the rotors are slightly shorter. As can be seen from Figure 8A, the wind flow patterns create a vortex 804 on the trailing face of rotator blade 806 during the return cycle. This
30 vortex is not created in the embodiment of Figure 2, as shown in Figure 6A. As a result, the efficiencies of the embodiment of Figure 8A are not quite as high as the efficiencies of the embodiment of Figure 2, as illustrated with more specificity in Figure 8B.

Figure 8B is an illustration of instantaneous efficiency and average efficiency of a single rotor blade versus time for the embodiment illustrated in Figure 8A. As can be seen from Figure 8B, the average efficiency illustrated by plot 808 ranges between 27% and 33%. Plot 810 illustrates the instantaneous efficiency of the leading face of the rotor blades of the embodiment of Figure 8A, while plot 812 illustrates the instantaneous efficiency of the trailing face of the rotor blades of the embodiment of Figure 8A.

Figure 9 is a wind velocity and directional flow diagram that illustrates the direction of flow of the wind and its intensity for the embodiment of Figure 8A. Figure 9 illustrates the manner in which large negative pressures are created on the leading face of the rotor blade as a result of the accelerated air flow on the air foil. Figure 9 also illustrates the manner in which the vortex is formed from wind flowing between the gap caused by the recessed portion of the shaft 802 and the rotor blade, as well as the accelerated wind from the air foil.

Figure 10A illustrates pressure gradients calculated by computer simulations using computational fluid dynamics for the cross-flow wind turbine embodiment illustrated in Figure 10A. The embodiment illustrated in Figure 10A is similar to the embodiment of Figure 8A but includes a stationary shaft 1002 that is larger than the stationary shaft 802 of Figure 8A. As a result, a larger gap 1004 is formed between the rotor blades in the stationary shaft 1002 during certain portions of the cycle of rotation. A vortex 1006 is also created by the embodiment of Figure 10A.

Figure 10B is an illustration of instantaneous efficiency and average efficiency of a single rotor blade versus time for the embodiment of Figure 10A. As can be seen from Figure 10B, the average efficiency illustrated by plot 1008 ranges between 29% and 33%. Plot 1010 illustrates the instantaneous efficiency of the leading face of the rotor blades of the embodiment of Figure 10A. Plot 1012 illustrates the instantaneous efficiency of the trailing face of the rotor blades. Average efficiencies are calculated in the manner described above.

Figure 11 is a wind velocity and directional flow diagram that illustrates the direction of flow of the wind and its intensity for the embodiment of Figure 10A. Figure 11 provides a good visual manner of disclosing the operation of the embodiment of Figure 10A.

Figure 12A illustrates pressure gradients calculated by computer simulations using computational fluid dynamics for the embodiment of the cross-flow wind

turbine that is illustrated in Figure 12A. Stationary shaft 1202 is a kidney bean shaped stationary shaft that forms a large gap during certain portions of the rotational cycle of the rotor blades around the stationary shaft 1202. As can be seen from Figure 12A, a fairly large low pressure vortex is formed on the trailing face of the rotors during the return cycle.

Figure 12B is an illustration of the instantaneous efficiency and average efficiency of a single rotor blade versus time for the embodiment illustrated in Figure 12A. As can be seen from Figure 12B, the average efficiency that is illustrated by plot 1206 ranges between 28% and 30%. The instantaneous efficiency of the leading face of the rotor blades is illustrated by plot 1208. The instantaneous efficiency of the trailing face of the rotor blades is illustrated by plot 1210. The average efficiency illustrated by plot 1206 is calculated in the manner described above.

Figure 13 is a wind velocity and directional flow diagram that illustrates the direction of flow of the wind and its intensity for the embodiment illustrated in Figure 12A. The diagram of Figure 13 illustrates the manner in which the vortex 1202 is formed.

Figure 14A illustrates pressure gradients calculated by computer simulations using computational fluid dynamics for the embodiment of a cross-flow wind turbine illustrated in Figure 14A. The embodiment of Figure 14A uses a kidney shaped stationary shaft 1402 that is similar to the kidney shaped stationary shaft 1202 of the embodiment of Figure 12A, but stationary shaft 1402 is positioned so that a gap is formed during a different portion of the rotational cycle. Again, a vortex 1404 is formed near the trailing face of the rotor blades during the return cycle.

Figure 14B is a illustration of the instantaneous efficiency and average efficiency of a single rotor blade versus time for the embodiment illustrated in Figure 14A. As can be seen from Figure 14B, the average efficiency illustrated by plot 1406 ranges between 27% and 32%. Plot 1408 illustrates the instantaneous efficiency of the leading face of the rotor blades of the embodiment of Figure 14A. Plot 1410 illustrates the instantaneous efficiency of the trailing face of the rotor blades.

Figure 15 is a wind velocity and directional flow diagram that illustrates the direction of flow of the wind and its intensity for the embodiment of Figure 14A. Figure 15 illustrates the flow patterns and intensities that allows a visual interpretation of the manner of operation of the cross-flow wind turbine illustrated in Figure 14A.

Figure 16A illustrates pressure gradients calculated by computer simulations using computational fluid dynamics for an embodiment of a cross-flow wind turbine that is illustrated in Figure 16A. Figure 16A is similar to the embodiment of Figure 12A, except that Figure 16A uses a kidney bean shaped stationary shaft 1602 that is
5 larger than stationary shaft 1202 of Figure 12A. The larger shaft reduces the size of the rotor blades and provides a larger gap between the shaft and the rotor blades. The result is a large vortex 1604 that creates a large negative pressure area on the trailing face of the rotor blades during the return portion of the rotational cycle.

Figure 16B is an illustration of instantaneous efficiency and average efficiency
10 of a single rotor blade versus time for the embodiment illustrated in Figure 16A. As can be seen from Figure 16B, the average efficiency, illustrated by plot 1606, ranges between 24% and 26%. Plot 1608 illustrates the instantaneous efficiency of the leading face of the rotor blades of the embodiment illustrated in Figure 16A. Plot 1610 illustrates the instantaneous efficiency of the trailing face of the rotor blades.

Figure 17 is a wind velocity and directional flow diagram that illustrates the
15 direction of flow of the wind and its intensity for the embodiment illustrated in Figure 16A. Figure 17 provides a good visual interpretation of the operation of the embodiment of Figure 16A.

Figure 18A illustrates pressure gradients calculated by computer simulations
20 using computational fluid dynamics for the embodiment of a cross-flow wind turbine that is illustrated in Figure 18A. The rotor blades illustrated in Figure 18A have a J-shaped pattern rather than the semi-circular 120° arc pattern used in other embodiments disclosed herein. Shaft 1802 is a rotating shaft that is connected to the rotor blades of the embodiment illustrated in Figure 18A.

Figure 18B is an illustration of the instantaneous efficiency and average
25 efficiency of a single rotor blade versus time for the embodiment illustrated in Figure 18A. As can be seen from Figure 18B, the average efficiency illustrated by plot 1804 ranges between 27% and 34%. Plot 1806 illustrates the instantaneous efficiency of the leading face of the rotor blades of the embodiment of Figure 18A. Plot 1808
30 illustrates the instantaneous efficiency that is calculated for the trailing face of the rotor blades using the methods described above.

Figure 19 is a wind velocity and directional flow diagram that illustrates the
direction of flow of the wind and its intensity for the embodiment illustrated in Figure

18A. Figure 19 provides a good visual interpretation of the operation of the embodiment of the cross-flow wind turbine illustrated in Figure 18A.

Figure 20A illustrates pressure gradients calculated by computer simulations using computational fluid dynamics for the embodiment of a cross-flow wind turbine that is illustrated in Figure 20A. As shown in Figure 20A, the rotor blades are arranged in a reverse offset configuration so that a gap is formed between the rotor blades. This simulation shows the creation of a vortex 2002 that is located more centrally on the trailing face of the rotor blades during the return cycle. The negative pressure area 2004 formed between the rotor blade and the air foil during the power stroke is much smaller than the negative pressure areas in other embodiments disclosed herein.

Figure 20B is an illustration of instantaneous efficiency and average efficiency of a single rotor blade versus time for the embodiment illustrated in Figure 20A. As can be seen from Figure 20B, the average efficiency illustrated by plot 2006 ranges between 25% and 26%. Plot 2008 illustrates the instantaneous efficiency of the leading face of the rotor blades of the embodiment of Figure 20A. Plot 2010 illustrates the instantaneous efficiency of the trailing face of the rotor blades. As is apparent from Figure 20B, the smaller negative pressure area during the power stroke results in much lower efficiencies in the embodiment of Figure 20A.

Figure 21 is a wind velocity and directional flow diagram that illustrate the direction and flow of the wind and its intensity for the embodiment of Figure 20A. Figure 21 provides a good visual indication of the operation of the embodiment of Figure 20A.

Figure 22A illustrates pressure gradients calculated by computer simulations using computational fluid dynamics for an embodiment of the cross-flow wind turbine that is illustrated in Figure 22A. The embodiment of Figure 22A uses a split rotor blade and a small rotating shaft.

Figure 22B is an illustration of instantaneous efficiency and average efficiency of a single rotor blade versus time for the embodiment of Figure 22A. As can be seen from Figure 22B, the average efficiency illustrated by plot 2202 ranges between 23% and 24%. Plot 2204 illustrates the calculated instantaneous efficiency of the leading face of the rotor blades of the embodiment of Figure 22A. Plot 2206 illustrates the instantaneous efficiency calculated for the trailing face of the rotor blades. Efficiencies are calculated in the manner described above.

Figure 23 is a wind velocity and directional flow diagram that illustrates the direction of flow of the wind and its intensity for the embodiment of Figure 22A. Figure 23 provides a good visual interpretation of the manner of operation of the embodiment illustrated in Figure 22A.

5 Figure 24 is a schematic illustration of the manner in which the embodiment of Figure 1A can be constructed. Air foil stator 102 can be formed by using pipes 140, 142 and 144 to provide structural support. A braced framework 146 can be formed between pipe 142 and 144 to add further structural rigidity. The skin 148 of the air foil stator 102 can be formed from sheet metal, or any other desired material
10 and can be laser cut to the desired shape shown in Figure 24. Sheet metal having thicknesses of 14 gauge or 16 gauge, such as used in car fenders, can be employed to provide the desired shape. Other materials can also be used such as light weight laminates. Similarly, stator 104 can be formed by pipes 150 and 152 with standard braced framework that is covered with a sheet metal skin. Stator 106 can include
15 pipes 154, 156 to form a structural member in the same manner as described above. Stators 102, 104, 106 may also be constructed from pre-cast concrete forms, or cast in place concrete forms, or any other construction technique known in the art.

Figure 25 is an isometric view of the embodiment illustrated in Figure 24 without a top lid. A low base member 2502 may be provided to direct ground winds
20 into the device. This low base member is not a required element of the embodiment illustrated in Figure 25 and can be replaced with simply a flat base plate.

Figure 26 is an isometric view of the embodiment of Figure 25 that is viewed from a different direction. Again, the embodiment of Figure 26 is shown without a top plate.

25 Figure 27 is an isometric view of the manner in which the rotor blades can be constructed. As shown in Figure 27, ribs 2702, 2704, 2706 and 2708 provide structural rigidity and the desired shape of each of the rotor blades. A braced framework (not shown) can be provided between each of the ribs 2702-2708. Skin 2710 is then applied to the surface of the braced framework to form the leading and
30 trailing faces of the rotor blades. Rotating shaft 2712 is connected to each of the ribs 2702 – 2708 and to the skin 2710. The skin 2710 may be constructed from metal, aluminum, composites, or any other material known in the art.

Figure 28 is a schematic illustration of one embodiment of a power generation plant that can be used with any of the embodiments disclosed herein. As shown in

Figure 28, a rotating shaft 2712 is connected to a right-angle gear box 2702. Rotational energy is transferred in a horizontal direction to the variable speed gear box 2804. Generator 2806 then generates electrical energy from the mechanical energy of the variable speed gear box 2804.

5 Figure 29 illustrates the manner in which the generator 2806 can be connected directly to the rotating shaft 2712. This direct connection in a vertical manner eliminates mechanical losses resulting from the right angle gear box 2802 and the variable speed gear box 2804. The rotating shaft 2712 may also be directly connected to a direct drive generator. This configuration eliminates any mechanical losses from
10 the gearbox by eliminating the gearbox altogether. Various electrical techniques, known in the art, can be used to generate a 60-cycle signal that can be applied to the electrical grid.

 The present invention therefore provides a cross-flow wind turbine that is capable of achieving high efficiencies and is operable in low-level, mid-level and
15 high-level wind conditions. Because of the high efficiencies that can be achieved over a wide range of wind speeds, the overall efficiency of the embodiments disclosed herein are substantially greater than the overall efficiencies of axial-flow wind turbines.

 The foregoing description of the invention has been presented for purposes of
20 illustration and description. It is not intended to be exhaustive or to limit the invention to the precise form disclosed, and other modifications and variations may be possible in light of the above teachings. The embodiment was chosen and described in order to best explain the principles of the invention and its practical application to thereby enable others skilled in the art to best utilize the invention in various
25 embodiments and various modifications as are suited to the particular use contemplated. It is intended that the appended claims be construed to include other alternative embodiments of the invention except insofar as limited by the prior art.

Claims

What is claimed is:

1. A method of capturing wind energy using a cross-flow wind turbine in an efficient manner comprising the steps of:
 - generating a low pressure area on a leading face of a rotor blade by accelerating the flow of air across the surface of an airfoil stator that is positioned to form a predetermined gap between said rotor blade and said air foil stator during a power stroke of said rotor blade;
 - using a blocking stator to substantially block wind from impeding movement of said rotor blade during a return cycle of said rotor blade and directing said substantially blocked wind to a trailing face of said rotor during said power stroke of said rotor blade so as to create a pressure differential between said leading face and said rotor blade and said trailing face of said rotor blade during said power stroke that creates a force that rotates said rotor blade in an efficient manner.
2. A cross-flow wind turbine system that is capable of capturing wind energy with high efficiency over a wide range of wind speeds comprising:
 - a rotor having two semicircular shaped rotor blades;
 - an airfoil stator positioned to capture and accelerate wind across an airfoil surface of said airfoil stator and provide a gap having a predetermined size between said rotor blades and said airfoil surface so that a negative pressure area is formed on a leading face of said rotor blades as said rotor blades pass by said airfoil surface during a power stroke; and
 - a blocking stator positioned to substantially block wind from impeding upon a leading face of said rotor blades during a return cycle, that is opposite to said power stroke, and direct wind that is blocked by said blocking stator onto a trailing face of said rotor blades during said power stroke such that a pressure differential is created between said leading face of said rotor blades and said trailing face of said rotor blades during said power stroke that creates a force that rotates said rotor blade in an efficient manner.

3. A crossflow wind turbine that generates mechanical energy from wind comprising:
- 5 a rotor having a plurality of rotor blades that are symmetrically disposed around a rotor, said rotor blades disposed in said rotor so that a gap is formed between leading edges of said rotor blades and said rotor axis during at least a portion of the rotation of said rotor blades around said rotor axis;
- 10 a rotor space formed in a volume that is swept out by said rotor blades, said rotor space having a drive portion in which said rotor blades are driven by said wind and a return portion in which said rotor blades return to said drive portion;
- 15 a plurality of airfoils that direct wind into said drive portion and direct wind away from said return portion to cause said rotor to turn and generate said mechanical energy, said airfoils being placed non-symmetrically around said rotor to provide a substantially bidirectional crossflow turbine.
4. The crossflow turbine of claim 3 wherein said rotor axis has a non-circular cross-section.
5. The crossflow turbine of claim 3 wherein said rotor blades are disposed in said rotor so that said wind flows across said rotor blades in said drive portion, through said gap, and into said return portion of said rotor space.
- 20 6. The crossflow turbine of claim 4 wherein said rotor blades are disposed in said rotor so that said wind flows across said rotor blades in said drive portion, through said gap, and into said return portion of said rotor space.
- 25 7. The crossflow turbine of claim 3 wherein said rotor axis is vertical and said airfoils extend at least partially over a base so that said base and said airfoils capture wind along lower portions of said crossflow turbine and direct winds from said lower portion of said crossflow turbine.
- 30

8. A method of generating mechanical energy from wind comprising:
providing a crossflow wind turbine having airfoils and a rotor that sweeps out a rotor space, said rotor space having a drive portion and a return portion;
symmetrically placing a plurality of rotor blades in said rotor that form
5 a gap between leading edges of said rotor blades and a rotor axis during at least a portion of the rotation of said rotor blades around said rotor axis;
placing said airfoils non-symmetrically around said rotor to provide a substantially bidirectional crossflow turbine by substantially directing said
10 wind into said drive portion of said rotor space so that said wind drives said rotor blades in said drive portion, and by substantially blocking said wind from entering said return portion of said rotor space so that said rotor blades return to said drive portion to generate said mechanical energy.
9. The method of claim 8 wherein said step of symmetrically placing a plurality
15 of rotor blades in said rotor further comprises:
placing said plurality of rotor blades in said rotor so that said leading edges are spaced apart from said rotor axis during at least a portion of said rotation of said rotor blades around said rotor axis as a result of said rotor axis having a non-circular cross-section.
20
10. The method of claim 8 wherein said step of placing said airfoils around said rotor further comprises:
placing at least one airfoil in a position to block said wind from
entering said second portion whenever said wind flows substantially from at
25 least one predetermined direction, and placing at least one other airfoil in a position to direct said wind into said first portion whenever said wind is flowing substantially from said at least one predetermined direction.
11. The method of claim 8 wherein:
30 providing a crossflow turbine comprises providing a vertical crossflow turbine; and,
placing said airfoils comprises placing said airfoils so that said airfoils at least partially extend over a base to form an airfoil so that said utility

enclosure and said airfoils direct wind from lower portions of said crossflow turbine into said crossflow turbine.

12. The crossflow turbine of claim 8 wherein symmetrically placing said plurality
5 of rotor blades in said rotor that form a gap during at least a portion of said
rotation of said rotor blades around said rotor axis comprises symmetrically
placing said plurality of rotor blades in said rotor to form said gap so that said
wind flows across said rotor blades in said drive portion, through said gap, and
into said return portion of said rotor space.

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