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10 **IMPROVEMENT IN AN APPARATUS FOR PRODUCING
CONTAINERS OF THERMOPLASTIC MATERIAL**

DESCRIPTION

15 The present invention refers to an improved apparatus for the production of containers made of thermoplastic material, in particular polyethylene terephthalate (PET) and polypropylene (PP), intended for use in applications implying them being filled with liquids at elevated temperatures and/or containing CO₂ (carbon dioxide) gas, provided with devices that enable the productivity of the moulds during the blow moulding phase to be increased.

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In particular, the present invention is particularly advantageous when the described devices are associated to a preform manufacturing apparatus included in a so-called single-stage plant, but can be advantageously used also in conjunction with apparatuses that are supplied with previously manufactured preforms and are solely intended to carry out the final blow moulding phase (ie. two-stage plants).

30 In a two-phase process, a previously produced preform or parison, which is in a substantially amorphous state, is heated up again to its preferred molecular orientation temperature, at which it is then blow-moulded into the desired shape. As used in this context, the term "two-stage process", or "double-stage process", shall be understood to cover any process that produces a preform or parison which must

then be heated up from ambient temperature to the related blow-moulding temperature.

In contrast therewith, single-stage processes are so defined in that they are
5 capable of forming the so-called preform, or parison, and transferring said preform from the injection mould or extrusion die (upon it having been allowed to cool down to some appropriate temperature) to a conditioning station, where it is allowed to evenly level at a temperature of preferred molecular orientation. Said preform or parison is then transferred to a blow-moulding mould, in which it is finally moulded
10 into its desired form. According to a prior-art technique, the cavities in which the preforms are injection moulded and the preform transferring and conditioning devices are arranged in an on-line configuration along with the blow-moulding moulds, so as to ensure an easier, more convenient handling of the preforms, the containers and the various therewith associated members.

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According to such a construction principle, both preforms and finished containers are processed in successive groups, with the same processing and/or transferring operations occurring at the same time.

20 In particular, the blow moulding tools, ie. the moulds, are particularly critical in this connection, since with the increasing blow moulding pressure and the increase in the number of cavities contained in each pair of blow moulding platens, more rapid and powerful pumping stations are required. Furthermore, the increased total pressure produced by the bottles during blow moulding must be opposed by a
25 corresponding greater mould clamping pressure.

Such a greater pressure, which can be estimated to amount to a clamping force exerted on the moulds in excess of 100,000 kgf, would require all mechanical and pneumatic organs intended to produce and withstand such a pressure to be sized
30 accordingly, which generally means to a very burdensome extent.

Such a huge and, what's more, pulsating pressure, however, has a negative effect also on the resistance of the moulds themselves, which are not only so

exposed to a greater pressure, but have at the same time be capable of withstanding such a pressure over a much greater extension thereof, owing to the greater number of blow moulding gates, and this of course causes the rigidity thereof to become a critical factor. It makes also easier for the moulds to warp
5 outwardly, thereby affecting the bottle blow-moulding results in an easily understandable manner.

Furthermore, when use is made of blow moulding moulds provided with a large number of cavities, the time needed for all preforms to be transferred into the
10 respective cavities increases in a proportional manner with a corresponding increase in the cycle time and a resulting reduction in the overall productivity of the plant.

In order to do away with such drawbacks, a largely known solution lies in the
15 replacement of blow moulding moulds provided with a plurality of on-line cavities with a smaller number of individual moulds, ie. comprising a single respective blow moulding cavity, which are arranged along the periphery of a rotating carousel-like structure, such as this is for instance illustrated in WO 95/05933, WO 89/01400, US 4,850,850 and US 4,313,720.

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In particular, WO 89/01400 teaches that said blow moulding half-moulds are adapted to open and close in a book-like manner about respective axes of rotation that are orthogonal to the plane on which the preforms and the finished containers move.

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Such a solution, although effective in solving the afore cited problems, does not however go without some drawbacks that are summarized below:

a) the need arises for two half-moulds to be handled and driven and this of
30 course adds to the complexity of the structures and causes costs to rise;

b) the lateral rotary movement of both said half-moulds requires of course the availability of adequate lateral space and this of course puts a penalty on the compactness of the plant;

5 c) the handling means provided must be able to introduce the preforms from the front zone of the half-moulds, as well as to again remove the respective finished containers from the same front zone, and this of course understandably adds significantly to the complexity of both construction and operation of the plant.

10 However, during operating tests carried out on some types of plants having the characteristics as recited in the appended claims 1 to 5, and made with the use of known techniques of more obvious and immediate choice, such as the use of a direct pneumatic control or electromagnetic actuators or means like a lever joint generally known as toggle joint in the art, it has been observed that a number of
15 problems tend to come afloat in connection with the opening and closing, or clamping, of the moving half-mould, i.e.:

- the final closing and opening movement of said moving half-mould is an abrupt, not adequately slowed-down one, so that it may give rise to blows and clattering;

20 - owing to the rapid wear-down of the mechanical organs and parts concerned (it should be noticed that these must be able to operate on a continuous-duty basis over very long periods of time), the duration of the machine life is significantly affected, i.e. reduced, thereby giving rise to immediate problems of planned maintenance and/or repair work;

25 - the noise generated by the entire system controlling and actuating the movement of the moving half-mould is in general quite high and tends to further increase owing to the above cited wear-down effect;

- since the moving half-mould must perform an alternating opening and closing movement at a relatively high rate, vibrations are generated which tend to be
30 transferred to the entire structure of the plant, and this has obviously a negative impact on the duration and the operation of the machine organs involved; furthermore, the final opening and closing phase of the moulds is an extremely short

and therefore strongly accelerated phase, and this of course contributes to an increased level of the so induced vibrations;

- for such accelerations to be obtained, over-sized movement control and driving organs must be used, but this fact not only has a negative effect on the level of the vibrations, but also, due to the greater extent of wear-down caused, to the ability of ensuring the desired precision standards over adequately long periods of time.

Based on these considerations, it therefore is a main purpose of the present invention to provide a blow-moulding apparatus of a plant for producing hollow bodies, as well as the operating principles and manners thereof, allowing for the productivity thereof to be increased through an accelerated handling of both preforms and finished containers, without incurring any of the afore cited drawbacks, which is capable of being easily implemented with the aid of readily available techniques and means and therefore is reasonably low-cost, reliable and preferably capable of being integrated with a preform production stage arranged upstream..

This aim, along with further features of the present invention, is reached in a blow-moulding apparatus having the characteristics as recited in the appended claims, and may concretize itself in definite parts and arrangements of parts, as this can be more readily understood from the detailed description of a preferred embodiment that is given below by way of non-limiting example with reference to the accompanying drawings, in which:

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- Figure 1 is a side vertical-section view of a pair of half-moulds according to the present invention, as shown at a closing angle enabling the preforms to be introduced therein;

30 - Figure 2 is a side view similar to the above one, however with the same half-moulds shown in a minimum opening position thereof enabling the blow-moulded container to be removed therefrom;



- Figure 3 is a schematical view of the path, as seen from above, followed by a preform to enter and to come out of a pair of half-moulds in a book-like open arrangement according to the prior art;

5 - Figure 4 is again a schematical view of the path, as seen from above, followed by a preform to enter and to come out of a pair of half-moulds according to the present invention;

10 - Figure 5 is a vertical front view of the half-moulds in their opened state, in the exact moment when the blow-moulded container starts to be removed therefrom;

- Figure 6 is a schematical top view of the geometry and the mutual arrangement of a plurality of moulds according to the present invention;

15 - Figure 7 synthetically illustrates a comparison between two diagrams representing on a horizontal scale the time requirements for carrying out a preform moulding phase according to the prior art and the present invention, respectively;

20 - Figures 8 through to 12 are views of as many positions of the moving half-mould, and the related actuation organs, from a fully open to a fully closed position thereof;

25 - Figures 8A through to 12A are schematical views of the locations on which forces concentrate, as well as the axes along which said forces acting on the actuation organs of Figures 8 through to 12 concentrate;

30 - Figure 13 is a schematical view of the positions of the fundamental point vectors and the force vectors acting on the actuation organs of Figure 8, with the mould in an open state;

- Figure 14 is a diagrammatical view of the position characteristics of the moving half-mould with respect to the position of the actuation pin from a reference position thereof.

5 A main peculiar feature of the present invention lies in the use of pairs of half-moulds adapted to blow mould preforms 1 in view of converting them into finished containers 7, wherein said half-moulds are essentially arranged as illustrated in Figures 1, 2 and 6 showing respectively a schematical side vertical-section view of a pair of half-moulds in a partially open state, a schematical
10 side vertical-section view of the same half-moulds in an almost fully open state, and a schematical top view of the arrangement of the moulds 24, 25, 26 according to the present invention in a fully open state, as in the case of the moulds 24 and 25, and a fully closed state, as in the case of the mould 26.

15 On the outer periphery of a per se known rotating carousel 10 there are applied a plurality of pairs of half-moulds, wherein

- one of such half-moulds 2 is fixed and firmly joined to said carousel, and is further arranged on a vertical plane, with its respective half-cavity facing outwardly and radially oriented with respect to the carousel 10,

20 - the other half-mould 4 is movable with a rotary motion about an axis X arranged on the horizontal plane and hinged on a rotation device (not shown) so that, when raised into its closed position, it is moved into coupling exactly with the matching fixed half-mould that is firmly joined to said carousel. In this way, therefore, the need actually arises for only the moving half-mould 4 to be actuated
25 into closing and opening, since the other half-mould 2 is fixed and substantially firmly joined to the carousel.

In this connection, a look should be taken at the illustrations appearing in Figures 3 and 4. In particular, the illustration in Figure 3 can be seen to show, in an
30 extremely schematical manner, a top view of the path a followed by the preform, which is then moulded into a finished container, with respect to the two half-moulds 21 and 22 according to the prior art, and therefore both movable, as shown in an open state thereof. From this Figure it can be readily noticed that said path a must

include a deep sloping pattern in order to enable the preform to first slide into the half-moulds and then move out therefrom as a finished container.

As compared with such a situation, the illustration appearing in Figure 4 shows, again in a schematical manner, a corresponding top view of the path b followed by the preform, which is then moulded into a finished container, with respect to the fixed half-mould 2 and the moving half-mould 4. Although sketched in a rather simplified form, this illustration does not fail to immediately stress the point that the path b of the preform runs along an arc of circumference without any apparent diversion, or anyway a curvilinear trajectory without any point of inflection that is likely to slow down the movement of the preform/container along the path thereof and to add to the complexity of the construction of the motion control organs.

The line portions indicated at H, L, M, P and R in the diagram of Figure 7 respectively show the preform insertion time, the half-mould closing time, the blow moulding time (dashed line), the half-mould re-opening time, and the finished container removal time, according to the prior-art.

On the contrary, with the process according to the present invention, owing essentially to the closing phase of the moving half-mould occurring partially at the same time as the preform insertion phase, as well as the opening phase of the same moving half-mould occurring partially at the same time as the finished container removal phase, a reduction in the overall cycle-time of the blow moulding tools can be obtained.

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Since the above cited improvement allows for the preform insertion phase H' to partially overlap the closing phase L' of the sole moving half-mould, such a time during which said two phases are carried out simultaneously is identified as time T^0 which must necessarily be deducted from the overall cycle time. Furthermore, after the related blow moulding phase M', which has necessarily an unaltered duration, the opening phase P' of said moving half-mould is carried out. Even in this case, the possibility exists for the subsequent removal phase R' of the finished container to be caused to start earlier, by a time T^1 , before the mould is fully open, so that this

partial overlapping of the opening phase P' of the moving half-mould and the removal phase R' of the finished blow-moulded container again brings about a further reduction in the overall cycle time by such a period during which said phases are so overlapping, ie. by the above cited time T^1 .

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In practice, the total cycle time is reduced from a value T_x indicated in Figure 7 to a lower value T_c , since $T_c = T_x - T^0 - T^1$.

Only a slight mention is made here of the fact that the actual blow moulding time
10 T_s , which is also identified by a dashed portion in both diagrams of Figure 7, is common to and unaltered for both blow moulding processes, so that it is not affected, ie. modified by the present invention.

However, the advantages brought about by the present invention do not end
15 here. In fact, a further improvement of the invention itself can be easily obtained in the manner that is described below with particular reference to Figures 1 and 2.

Referring to Figure 1, it can be noticed that the introduction of the preforms in the blow moulding half-moulds, ie. the exclusive movement of the preforms towards
20 said half-moulds, can be accomplished through just a partial opening of the moving half-mould 4, ie. when the opening angle is an angle ℓ that is smaller than the maximum opening angle, which thing is on the contrary not possible in those cases in which both half-moulds are movable owing to the particular kinematic mechanisms that would be needed to such a purpose, as anyone skilled in the art is
25 well aware of.

This furthermore leads to the advantage of the overall plant to be capable of being adjusted to the length of the preforms, since it can be easily appreciated that shorter preforms require a smaller opening angle and, therefore, shorter mould
30 insertion times. Similarly, as better illustrated in Figure 2, the movement for the removal of the finished blow-moulded container can be started before the moving

half-mould is fully opened, provided that the trajectory S of the lower edge of the same container does not interfere with the moving half-mould.

A further advantageous improvement of the present invention lies in providing
5 an appropriately curved guide element 15, illustrated in Figures 4 and 5, arranged in a stable manner in such a position as to be able to intercept the path of the preform neck from the trajectory b, and to assist it in its movement of insertion in the respective cavity of the corresponding fixed half-mould 2.

10 As far as the technical improvements in the organs controlling the movement of the moving half-mould are concerned, reference should be made to Figures 8 through to 12, as well as the corresponding schematics appearing in Figures 8A through to 12A. The latter can be seen to symbolically represent the fundamental points of application of the action and reaction forces on the organs of the plant, the
15 vectors representing such forces, and the direction of action thereof.

From the illustrations in the above cited Figures it can be noticed that said actuation organs of the moving half-mould 4 comprise:

- a first class lever provided with arms 52 and 53 separated by a fulcrum F1,
20 whose power and resistance points are located at the extreme ends of said two arms, ie. at P1 and R1, respectively;
- a third class lever provided with respective arms 55 and 56, a respective fulcrum F2, and respective power and resistance points at P2 and R2;
- a rigid connecting member 54 that links the resistance point R1 of said first
25 class lever with the power point P2 of said third class lever, said resistance and power points being connected to the extreme ends of said connecting member pivotally;
- an actuating member 51 provided with two end portions, the first one of which is connected to the power point P1 of said first class lever.

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The fulcra F1 and F2 of said first class lever and said third class lever, respectively, are applied pivotally on respective distinct points of a structure 60 that is integral with or firmly joined to said fixed half-moulds; furthermore, said moving

half-mould 4 is applied on the arm 56 of said third class lever opposite to the related fulcrum F2 with respect to the corresponding power point P2.

The second extreme end 57 of said actuating member 51 is adapted to be
5 movably actuated by a moving member 58 on a plane that is orthogonal to the axis of rotation of the fulcrum F1 of said first class lever.

The whole assembly of said levers, connecting members and actuating members is adapted to move, clearly in a synchronous and coherent manner since
10 each moving member is linked to another member, between two respective extreme positions, in which one of such extreme positions corresponds to the full-open position (Figures 8, 8A and 12) of said moving half-mould, whereas the other one of said extreme positions corresponds to the full-closed position (Figure 12, 12A and 16) of the same half-mould.

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Referring now to Figure 13, which illustrates the condition of the mould assembly in its fully open position, it can be noticed that when said second extreme end 57 of said actuating member 51 is urged to start moving in the direction in which said moving half-mould 4 is caused to close, the vector V1 of the force transmitted from
20 said point of resistance R1 of said first class lever to said rigid connecting member 54 has a component V2 in the direction of action of said connecting member, ie. along the straight line joining R1 with P2, wherein said component V2, if considered as being applied on said point of power P2 of said third class lever, indicated at V2,1 in the Figure, may be in turn broken down into two mutually orthogonal
25 components, one of which, ie. the one indicated at V2,2 in the Figure, is oriented towards F2 and acts so as to only compress the related arm 55, with practically no effect at all within the overall geometry, whereas the other component V2,3 is radial with respect to said arm 55 and therefore acts on the arm 56 supporting the half-mould 4, in such a manner as to cause said third class lever to rotate, thereby
30 causing said moving half-mould to close.

As far as the spatial configuration and the possible components of the force vectors, the lever arms and the other connecting/actuating members, it has

practically been found that the most effective and logical arrangement thereof is obtained when all of them are provided on a same plane, in particular on the plane shown in the Figures 8 through to 12. However, as anyone skilled in the art is capable of readily understanding, said vectors, members and components may
5 also be arranged three-dimensionally, provided that they meet the pre-condition of their projections or components on a given, suitable plane reflecting the subsequent conditions illustrated in the Figures.

Figures 9 through to 11 illustrate subsequent dispositions of the whole assembly
10 of said levers and said connecting and actuating members, along with the respective vectors, corresponding to some subsequent positions of said moving half-mould 4 as it is moved into closing. They are anyway readily understandable by all those skilled in the art, so that no further explanation needs to be given here in this connection.

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Figures 12 and 12A represent the situation when the moving half-mould is fully closed. This is a quite particular situation since, further to representing a kind of end-of-stroke point, it also represents the condition in which the "toggle effect" shows up in all of its effectiveness. In other words, this is the condition in which the
20 clamping force of said half-mould reaches its peak, ie. is maximized, while the angular displacement of said half-mould is at a minimum. Use is anyway made also of other means, further to this fact, in order to ensure a fully stable clamping of said half-mould.

25 Reference should be made now to Figure 12: the point of resistance R1 of the lever 52, 53 is in an articulated arrangement with respect to the connecting member 54, so that the arm 53 and said connecting member 54 are capable of rotating with respect to each other. However, a further rotation thereof beyond a pre-established position is prevented by the presence of a mechanical or positive retainer (not
30 shown) that really acts as a toggle, ie. enables two levers hinged on an extreme end thereof to rotate with respect to each other only up to a certain angle and not any further.

The geometric configurations and the dimensions of the various members and components involved are so defined as to make sure that, when such a limit stop position is reached, this position also coincides with both

- the full-closed condition of the moving half-mould against the respective fixed
5 half-mould and

- the particularly favourable condition created by the three geometrical sites identified by P2, R1 and F1 are aligned, as this is shown in Figure 12A.

The advantageous character of such a circumstance has already been hinted at
10 above and lies essentially in the fact that, in the final portion of the closing path covered by the moving half-mould, the force that is produced and can therefore be used to close and clamp said half-mould, is at its maximum, ie. reaches a peak. In this case in fact, as this is most clearly shown in Figure 14 illustrating the opening or closing angle of the moving half-mould in accordance with the progressive
15 displacement of the moving member 58, or rolling pin, the most favourable condition is obtained in view of making the best possible use of the so-called "toggle effect", said condition being reached through the illustrated combination and association of the described leverages. In a more detailed manner, Figure 14 can be noticed to emphasize how, in correspondence of the portion of curve
20 indicated at M, at a certain progressive displacement of the device or rolling pin 58, whose scale in the lower portion of the Figure is a linear one, a rotation is obtained with a progressively decreasing increment of the angle between the members 54 and 55 until an angle of 0° is eventually reached between said members 54 and 55 in correspondence of a value of approx. 1 in the abscissa.

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The particular pattern followed by said curve in correspondence of the above cited point M, which corresponds to said moving half-mould being closed, and also of the point H at the opposite end of the same curve, which corresponds to the full-open position of said half-mould, ensures a movement of the same half-mould
30 with progressively slowed-down accelerations and decelerations towards the respective end-of-stroke positions thereof, until practically a condition of zero acceleration is reached when the half-mould approaches said respective end-of-stroke positions thereof.

Such a moving pattern of said half-mould translates into a number of significant practical advantages, ie. a noticeable reduction in vibrations, the prevention of the moving half-mould from bumping when moving into its end-of-stroke positions, and the possibility for said moving device to be actuated with the help of simple,
5 reliable and accurate means that are furthermore durable, ie. well resistant to wear-down since they are not subject to the action of "forces".

This condition is further strengthened by the fact that, immediately upon said moving half-mould having so been moved into its fully closed position, the same
10 half-mould is automatically clamped in such a position with the help of such supplementary external means as readily conceivable by all those skilled in the art, said means being linked to the pins 41, 42 that are firmly joined with the fixed half-mould and the moving half-mould, respectively.

15 It will of course be appreciated that when it is stated that the geometrical sites identified by P2, R1 and F1 are aligned, as this is shown in Figure 12A, this is meant to be understood in the broadest sense of the word, since this is actually intended to mean that, in order to ensure the desired "toggle effect", it is sufficient for the axes of rotation of the pins centered on P2, R1 and F1 to be not only parallel, but also
20 arranged on a same plane.

The continuous operation of the described assembly for alternately opening and closing the moving half-mould can be obtained through a corresponding to-and-fro movement of the moving device or rolling pin 58, wherein such a
25 movement can be easily obtained by means of a continuously rotating cam device adapted to control the movement and the position of said rolling pin in full synchrony with all other devices, mechanisms and actuators that altogether ensure the various phases for opening the half-mould, introducing the preform, closing the half-mould, blow moulding said preform, opening the half-mould and simultaneous
30 removal of the finished container.

A further advantage of the present invention, as exemplified in the illustrated embodiment thereof, derives from the fact that if, as just stated above, the

alternating to-and-fro movement of the moving device or rolling pin 58 is actuated by two rotating cams, preferably on the same vertical axis of rotation of the carousel 10 in Figure 6, the limited wear-down effect that unavoidably takes place between the actuating surfaces of said rotating cams and said rolling pin has only a very limited impact on the opening and closing accuracy of the moulds. This fact brings about the remarkable benefit deriving from the possibility for the maintenance or re-adjustment of said cams and therewith associated organs to be carried out at quite extended intervals, without incurring any loss in processing precision.

10 A confirmation of the fact that the wear-down effect of the cams, and possibly also of the therewith associated rolling pin or moving device, has only a very limited impact on the precision of the end-of-stroke positions of the moving half-mould can be simply obtained by having again a look at Figure 14, in which it can in fact be observed that the condition actually occurs in which, in front of a certainly
15 non-negligible displacement, ie. oscillation of the rolling pin about said points M and H, the angle of rotation of the moving half-mould is almost nihil and practically negligible. As a result, if such an oscillation is due to wear-down, this practically has no significant effect on the precision of the end-of-stroke positions of said moving half-mould.

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CLAIMS

1. Apparatus for blow moulding hollow plastic bodies comprising:
- a plurality of pairs of mutually joinable half-moulds capable of being opened and closed, associated to an appropriate rotary apparatus (10) carrying said
 - 15 half-moulds,
 - support devices for carrying the preforms corresponding to said half-moulds,
 - a preform feeding mechanism adapted to supply an orderly sequence of preforms held at an appropriate blow-moulding temperature into the respective pairs of half-moulds associated to said rotary apparatus, which are to this purpose
 - 20 kept in their opened position,
 - a retrieval device adapted to remove the finished container from the respective pair of half-moulds after the opening thereof,
 - an opening and closing mechanism adapted to close the half-moulds after the passage thereof through the position of the preform feeding mechanism, and to
 - 25 open them before the passage thereof through the position of the finished-container removal mechanism, characterized in that
 - said pairs of half-moulds are constituted by a fixed half-mould (2) and a moving half-mould (4) that is capable of being opened from and closed against said fixed half-mould.
 - 30
2. Apparatus according to claim 1, characterized in that said fixed half-moulds are essentially linked to said rotary apparatus (10).





3. Apparatus according to claim 2, characterized in that said fixed half-moulds (2) are arranged in a substantially vertical position, and that the respective moving half-mould (4) is adapted to be closed by accomplishing a substantially rotary movement about a horizontal axis of rotation.

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4. Apparatus according to claim 3, characterized in that said pairs of half-moulds are adapted to be opened and closed in an orderly sequence so as to be able to receive a respective orderly sequence of preforms.

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5. Apparatus according to claim 3 or 4, characterized in that an appropriate guide member (15) is provided in correspondence of the position in which the preform is inserted in the cavity of the respective fixed half-mould, in which said guide member is adapted to facilitate both the separation of the preform from the respective support and the insertion thereof in said respective cavity.

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6. Apparatus according to any of the preceding claims, characterized in that said opening and closing mechanism of any of said moving half-moulds (4) comprises:

- a first class lever (52, 53) and a third class lever (55, 56),
- 20 - a structure (60) firmly associated to said fixed half-moulds (2),
- a connecting member (54) that joins the point of resistance (R1) of said first class lever with the point of power (P2) of said third class lever, said resistance and power points being pivotally connected to the extreme ends of said connecting member,
- 25 - an actuating member (51) provided with two extreme ends, of which the first extreme end is connected to the power point (P1) of said first class lever (52, 53),
- the fulcra (F1, F2) of said first class lever and said third class lever being pivotally applied on respective distinct points of said structure (60) firmly associated to said fixed half-moulds, and
- 30 - said moving half-mould being applied on the arm (56) of said third class lever which is opposite to the related fulcrum (F2) with respect to the corresponding power point (P2).





7. Apparatus according to claim 6, characterized in that the second extreme portion (57) of said actuating member (51) is adapted to be forced by a moving device (58) into displacing on an orthogonal plane with respect to the axis of rotation of the fulcrum (F1) of said first class lever.

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8. Apparatus according to claim 6 or 7, characterized in that said levers and said connecting and actuating members are adapted to move between two respective extreme positions, in which one of said extreme positions corresponds to the full-open position of said moving half-mould, whereas the other one of said
10 extreme positions corresponds to the full-closed position of said moving half-mould.

9. Apparatus according to claim 8, characterized in that when said second extreme portion (57) of said actuating member is driven in the sense of starting the closing displacement of said moving half-mould (4) from the full-open position
15 thereof, the vector (V1) of the force transmitted from said resistance point (R1) of said first class lever to said connecting member (54) has a component (V2) in the direction of said connecting member which, when applied on to said power point of said third class lever, has in turn a respective second component (V2,3) that is oriented so as to induce a rotation of said third class lever in the closing direction of
20 said moving half-mould.

10. Apparatus according to any of the preceding claims 6 to 9, characterized in that in said fully closed position of said moving half-mould (4), said power point (P2) and said fulcrum (F2) of said third class lever, as well as said resistance point (R1) of
25 said first class lever are either aligned or the respective axes of rotation are parallel and lie on the same plane.

11. Apparatus according to any of the preceding claims 6 to 10, characterized in that said moving device (58) is adapted to be driven into alternatingly displacing
30 between two extreme positions corresponding to the conditions in which said moving half-mould is fully open and fully closed, respectively, by means of a cam device rotating about an axis that is orthogonal to the axes of rotation of said two levers.



12. Apparatus according to any of the preceding claims 6 to 11, characterized in that in said full-closed position thereof there is provided a retaining device adapted to prevent said moving half-mould (4) from further rotating beyond said full-closed position.

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13. Apparatus according to any of the preceding claims 6 to 12, characterized in that selectively actuatable means are provided, which are adapted to prevent said moving half-mould from rotating back towards the open position from said full-closed position.



This Sheet Has Been Replaced

