

Mercury Removal

This invention relates to mercury absorbents and to a process for the removal of mercury from a gaseous or liquid stream using said absorbents.

- 5 GB-B-1533059 discloses the use of a pre-sulphided absorbent comprising copper sulphide for the absorption of mercury from a natural gas stream containing mercury. The pre-sulphided absorbent is prepared by forming a precursor comprising basic copper carbonate and a refractory cement binder, and then contacting the precursor with a gaseous stream containing a sulphur compound, e.g. hydrogen sulphide, so as to fully sulphide the copper compound.
- 10 The pre-sulphided absorbent is then used to remove mercury from a natural gas stream. It is also shown that an absorbent comprising copper in the reduced, i.e. metallic, state is less effective at absorbing mercury than the pre-sulphided absorbent.

- EP 0480603 describes a process for the removal of mercury from a stream wherein an
- 15 absorbent comprising a metal sulphide is prepared in situ, preferably by the stream also containing a sulphur compound thereby concomitantly preparing the mercury absorbent and absorbing the mercury, such that the formation of ineffective and undesired metal compounds e.g. sulphates is avoided.

- 20 Such materials, especially those described in GB-1533059, undergo considerable physiochemical changes upon treatment with sulphur compounds to form the metal sulphide phases known to be effective for mercury removal. The physiochemical changes result in reduced crush strength and an increased susceptibility to attrition, particularly with high metal sulphide containing materials. It is therefore desirable to increase the crush strength whilst
- 25 maintaining attrition resistance. We have found that a combination of binders and support material in the absorbent overcomes the problems associated with prior art materials.

- Accordingly the invention provides a particulate mercury absorbent comprising a metal sulphide, a support material, a first binder and a second binder wherein said first binder is a
- 30 cement binder and the second binder is a high aspect ratio binder having an aspect ratio >2 .

- The invention further provides a mercury removal process comprising contacting a mercury-containing feed stream with a particulate mercury absorbent comprising a metal sulphide, a support material, a first binder and a second binder wherein said first binder is a
- 35 cement binder and the second binder is a high aspect ratio binder having an aspect ratio >2 .

The absorbent may be sulphided ex-situ or sulphided in-situ according to known methods. Hence the invention includes a particulate mercury absorbent precursor comprising a metal compound capable of forming the metal sulphide, a support material, a first cement binder and

a second high aspect ratio binder, that may be treated with sulphur compounds to form the metal sulphide and a mercury removal process comprising contacting a mercury-containing feed stream with a particulate mercury absorbent comprising a metal sulphide capable of absorbing mercury, wherein the absorbent is formed by contacting in-situ a particulate precursor comprising a metal compound capable of forming the metal sulphide, a support material, the first binder and the second binder with a stream containing a sulphur compound.

Whereas the precursor may be sulphided using a stream which contains a suitable sulphur compound to form the absorbent and then held in-situ in a non-oxidising environment, it is preferred, where the absorbent is not pre-sulphided, that the sulphiding of the precursor and the absorption of mercury occur together, i.e. they are concomitant, thereby avoiding the need for a separate sulphiding process and the subsequent storage difficulties. Hence in a preferred embodiment the feed stream and the first stream are the same and the present invention may be advantageously used on streams that contain both mercury and sulphur compounds.

The present invention may be used to treat both liquid and gaseous feed streams containing mercury. In a preferred process of the invention the fluid is a hydrocarbon stream. The hydrocarbon stream may be a refinery hydrocarbon stream such as naphtha (e.g. containing hydrocarbons having 5 or more carbon atoms and a final atmospheric pressure boiling point of up to 204°C), middle distillate or atmospheric gas oil (e.g. having an atmospheric pressure boiling point range of 177°C to 343°C), vacuum gas oil (e.g. atmospheric pressure boiling point range 343°C to 566°C), or residuum (atmospheric pressure boiling point above 566°C), or a hydrocarbon stream produced from such a feedstock by e.g. catalytic reforming. Refinery hydrocarbon streams also include carrier streams such as "cycle oil" as used in FCC processes and hydrocarbons used in solvent extraction. The hydrocarbon stream may also be a crude oil stream, particularly when the crude oil is relatively light, or a synthetic crude stream as produced from tar oil or coal extraction for example. The fluid may be a condensate such as natural gas liquid (NGL) or liquefied petroleum gas (LPG). Gaseous hydrocarbons may be treated using the process of the invention, e.g. natural gas or refined paraffins or olefins, for example.

Non-hydrocarbon fluids which may be treated using the process of the invention include solvents, such as liquid CO₂, used in extractive processes for enhanced oil recovery or decaffeination of coffee, flavour and fragrance extraction, solvent extraction of coal etc. Fluids, such as alcohols (including glycols) and ethers used in wash processes or drying processes (e.g. triethylene glycol, monoethylene glycol, Rectisol™, Purisol™ and methanol) may be treated by the inventive process. Natural oils and fats such as vegetable and fish oils may be treated by the process of the invention, optionally after further processing such as hydrogenation or transesterification e.g. to form biodiesel.

Gaseous feed streams which are susceptible to being treated by absorbents comprising metal sulphide precursors may also include those which inherently contain both mercury and a sulphur compound e.g. certain natural gas streams, or a mercury containing gaseous stream to which a sulphur compound has been added to effect mercury absorption. Suitable liquid streams include mercury containing LPG and naphtha streams. Other fluid streams that may be treated include mercury-containing nitrogen, argon, helium and carbon dioxide.

Preferably the absorption of mercury is conducted at a temperature below 100°C in that at such temperatures the overall capacity for mercury absorption is increased. Temperatures as low as 4°C may be used to good effect in the present invention.

The mercury may be in the form of mercury vapour, organomercuric, or organomercurous compounds. Typically the concentration of mercury in a gaseous feed stream is from 0.01 to 1000 µg/Nm³, and more usually between 10 to 200µg/Nm³.

The absorbent may usefully be prepared by combining a metal compound capable of forming a metal sulphide with the support material and the first and second binders in the presence of a little water to form a particulate precursor which is then dried and sulphided. As stated above, the sulphiding step may be performed on the dried material ex-situ to provide the final absorbent, or may be performed in situ, in which case the particulate precursor is installed and undergoes sulphidation in the vessel in which it is used to absorb mercury compounds.

The sulphur compound used to sulphide the precursor may be one or more sulphur compounds such as hydrogen sulphide, carbonyl sulphide, mercaptans and polysulphides. Hydrogen sulphide is preferred.

Where concomitant sulphiding and mercury absorption occurs, the amount of sulphur compound that is present depends on the type of sulphur compound and metal compound used. Usually, a concentration ratio, as defined by the ratio of sulphur compound (expressed as hydrogen sulphide) concentration (v/v) to mercury concentration (v/v), of at least one, and preferably of at least 10 is used so that the precursor is sufficiently sulphided. Should the initial concentration of the sulphur compound in the feed stream be below the level necessary to establish the desired ratio of sulphur compound to mercury compound concentration then it is preferred that the concentration of the sulphur compound is increased by any suitable method.

The metal sulphide is desirably one with a high capacity for mercury. One or more metal sulphides may be present. The metal may be any which provides a metal compound which shows a suitable capacity for being sulphided and hence for mercury absorption. Examples of

suitable metals are iron, nickel and copper, preferably copper and nickel and in particular copper. Certain other metals, however, are generally unable to provide either compounds which can be suitably sulphided, e.g. aluminium, or sulphided compounds which can adequately absorb mercury. Nevertheless, a compound of such an other metal may be present
5 as a binding or support agent, which improves the structural integrity of the absorbent, and/or as a promoter which enhances the sulphiding of the precursor and/or the absorption of mercury by the absorbent.

A preferred absorbent composition comprises copper and zinc. Copper and zinc compounds
10 may be added separately to the support and binders to prepare the absorbent precursor. Alternatively, a single copper-zinc composition may be used. A support material such as alumina may also be present in such a composition.

Upon treatment with sulphur compounds the metal compounds in the absorbent precursor
15 react to form metal sulphides. CuS is a particularly preferred metal sulphide. Absorbents used in the present invention preferably comprise copper in an amount 1-40% wt, preferably 1-20% wt, more preferably 5-15% wt Cu (based upon the sulphided composition).

The metal compound suitable for use in an absorbent precursor is one that may be readily
20 sulphided and may include the oxide, carbonate, bicarbonate and/or basic carbonate. A particularly suitable absorbent precursor comprises basic copper carbonate (i.e. a copper hydroxycarbonate).

Support materials are desirably oxide materials such as aluminas, titanias, zirconias, silicas
25 and aluminosilicates. Hydrated oxides may also be used, for example alumina trihydrate. Preferred supports are transition aluminas such as gamma, theta and delta alumina. The support may be present in an amount 50-90% wt, preferably 70-80% wt (based upon on the sulphided composition). By using the first and second binders we have found that the amount of support material may be increased compared to prior art materials without sacrificing rate of
30 mercury absorption, strength or attrition resistance.

In the present invention, the metal sulphide or precursor is combined with a support, a first binder and a second binder. The first binder is preferably a cement binder, in particular a calcium aluminate cement. By the term calcium aluminate cement we include such calcium
35 aluminate compounds as calcium monoaluminate ($\text{CaO} \cdot \text{Al}_2\text{O}_3$), tricalcium aluminate ($3\text{CaO} \cdot \text{Al}_2\text{O}_3$), pentacalcium trialuminate ($5\text{CaO} \cdot 3\text{Al}_2\text{O}_3$), tricalcium penta aluminate ($3\text{CaO} \cdot 5\text{Al}_2\text{O}_3$), dodeca calcium hepta aluminate ($12\text{CaO} \cdot 7\text{Al}_2\text{O}_3$) and high alumina cements which may contain alumina in admixture with, dissolved in, or combined with such calcium aluminate compounds. For example, a well-known commercial cement has a composition

corresponding to about 18% wt calcium oxide, 79% wt alumina and 3% wt water and other oxides. Another suitable commercially available calcium aluminate cement has a composition corresponding to about 40% wt calcium oxide, about 37% wt alumina, about 6% wt silica and about 20% other oxides. The second binder is preferably a high aspect ratio binder having an aspect ratio >2 . By the term high aspect ratio we mean that the ratio between the maximum dimension and the minimum dimension of the particles is >2 . The particles may thus be plate-like where the length and breadth are at least twice the thickness. Alternatively, and preferably, the particles are acicular, wherein the average length is at least twice, preferably at least 2.5 times, the breadth, e.g. having a "rod" configuration wherein the cross sectional dimensions, i.e. breadth and thickness are approximately equal, or a "lath" configuration, wherein the thickness is significantly less than the breadth. A suitable high aspect ratio binder is an aluminosilicate clay, preferably an aluminium-magnesium silicate clay, commonly referred to as an Attapulgite clay. Without wishing to be bound by theory, we believe that the acicular nature of this binder comprising elongate particles with an aspect ratio >2 contributes to the improved physical properties of the absorbent materials according to the present invention. We have found surprisingly that the combination of these two types of binder in combination with the metal sulphide and support are capable of providing absorbent materials of high crush strength and low attrition, as well as suitably high rate of mercury absorption. The amount of the first binder may be in the range 5 to 15% by weight based on the un-sulphided absorbent precursor. The amount of the second binder may be in the range 1 to 10%, preferably 2 to 6% by weight on the un-sulphided absorbent precursor. Preferably, the relative amounts of the binders are 2:1 to 3:1 first to second binder.

The absorbent comprising the sulphided metal compound may be in any suitable physical form, e.g. as a granule, extrudate, or tablet so that the mercury-containing stream may be contacted with a bed of solid absorbent particles. Particularly effective absorbents are those prepared from precursors containing unsulphided metal compounds having a capacity to be highly sulphided. It is preferred that the amount of unsulphided metal compound present is such that the precursor may be sulphided to achieve a sulphur loading of at least 0.5% w/w, e.g. from 1 – 10% wt sulphur, although higher loadings of sulphur may be provided.

The absorbent precursor may be in the form of tablets formed by moulding a suitable powder composition, generally containing a material such as graphite or magnesium stearate as a moulding aid, in suitably sized moulds, e.g. as in conventional tableting operation. Alternatively, the shaped units may be in the form of extruded pellets formed by forcing a suitable composition, containing the absorbent precursor material and often a little water and/or a moulding aid as indicated above, through a die followed by cutting the material emerging from the die into short lengths. For example extruded pellets may be made using a pellet mill of the type used for pelleting animal feedstuffs, wherein the mixture to be pelleted is charged to

a rotating perforate cylinder through the perforations of which the mixture is forced by a bar or roller within the cylinder: the resulting extruded mixture is cut from the surface of the rotating cylinder by a doctor knife positioned to give extruded pellets of the desired length.

Alternatively, and preferably, the absorbent or absorbent precursor may be in the form of agglomerates formed by mixing the absorbent precursor material with a little water, insufficient to form a slurry, and then causing the composition to agglomerate into roughly spherical, but generally irregular, granules.

If desired the absorbent or absorbent precursors may be heated or treated in another way to accelerate the setting of the cement binder.

The different shaping methods have an effect on the surface area, porosity and pore structure within the shaped articles and in turn this often has a significant effect on the absorption characteristics and on the bulk density.

The absorbent preferably has an average particle size within the range 1-10 mm.

The invention is further described by reference to the following Examples.

In all cases, absorbent precursor particles were prepared using a granulation technique wherein the solid components were combined with a little water and mixed to form granules in a Hobart mixer. A copper-zinc composition comprising basic copper carbonate and containing 60% wt copper, and 25% wt zinc (expressed as oxides) and about 15% wt alumina was used. Alumina trihydrate (ATH) was used as the support material unless otherwise stated. Binders were added to these two components, sometimes as a mix of two binders to produce the desired affect. Binder 1 in each case was a calcium aluminate cement having a CaO content of about 40% wt. Binder 2 in each case was an Attapulgite clay. The granules were dried prior to sulphiding. Unless otherwise stated, drying was performed at 105°C in air for 16 hours after a period of 2 hours at ambient temperature (ca 20°C). The size range of granules obtained was 2.80 – 4.75mm.

To assess the performance of each of the materials screened, the physical properties of the 2.80 – 4.75mm material were measured before the sulphiding step. Mean Crush Strength (MCS), Tapped Bulk Density (TBD) and attrition resistance of the precursor were measured. The MCS and attrition of the materials were also tested after each of the materials was sulphided using H₂S.

Mean Crush Strength (MCS): This analysis was carried out using a CT5 crush strength tester fitted with a 50Kg load cell. The granules selected for testing were sized from 3.35 – 4.00mm taken from the 2.80 – 4.75mm bulk sample, this would reduce any effect of the granule size on

strength. 30 granules were chosen at random from the 3.35 – 4.00mm size range and tested. The average of these results was taken to be the resultant value. The standard deviation was also recorded as a measure of the variability within the sample.

- 5 Tapped Bulk Density (TBD): This was carried using a 100ml measuring cylinder into which was poured approximately 60ml of the test material then the cylinder was manually tapped to achieve a constant volume. At this point the mass of the materials and the volume it held were recorded.
- 10 Attrition Testing: Attrition testing was carried out using the 'tube method'. In the tube method, a 50ml of sample of the sulphided absorbent was weighed accurately into a 37 mm id tube of length 25 cm. Following a 45-minute tumbling period, the sample was reweighed after the removal of the <1.00mm fraction by sieving. The % weight loss owing to attrition was calculated based on the weight <1.0mm and the total weight of material at the start of the test.
- 15 The tumbling period of 45 minutes subjected the sample to 3600 falls.

Sulphiding of Materials: The precursor materials were taken to a fully sulphided state using 1% H₂S in an inert carrier gas, (typically N₂ or CH₄). In all cases the flow rate of the gas was 42 litres hr⁻¹ at ambient temperature and pressure.

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Example 1.

Samples were prepared with the following compositions (all amounts are parts weight).

Example	Cu/Zn composition	ATH	Binder 1	Binder 2
Comparative 1	100	0	7	0
Comparative 2	25	75	14	0
Comparative 3	25	75	0	14
1(a)	25	75	7	7

25 Results: Before sulphiding

Example	MCS (Kg)	TBD (Kg/m ³)	Attrition loss (% wt)
Comparative 1	1.28	0.77	1.4
Comparative 2	2.81	1.06	4.6
Comparative 3	1.42	0.92	0.6
1(a)	1.94	0.945	0.42

Results: After sulphiding

Example	Sulphur (wt %)	MCS (Kg)	TBD (Kg/m ³)	Attrition loss (% wt)
Comparative 1	21.1	1.13	0.76	0.8
Comparative 2	2.9	2.66	1.06	4.8
Comparative 3	4.8	1.03	0.88	0.2
1(a)	3.64	1.68	0.92	0.6

From the combination of properties Example 1(a) shows high MCS and TBD and low attrition pre and post sulphiding. The Comparative Example 2 has a high crush strength but a very poor attrition resistance (i.e. a high attrition loss).

Example 2.

In this example, further variations of the binder ratio were studied together with the use of hot (55°C) and cold (ca 15°C) water during the granulation process.

Example	Treatment	Cu/Zn composition	ATH	Binder 1	Binder 2
2(a)	Cold water	25	75	10	4
2(b)	Hot water	25	75	10	4
Comparative	Hot water	25	75	14	0

Results

Example	MCS (Kg) (Unsulphided)	MCS (Kg) (Sulphided)	Attrition (%wt) (Sulphided)
2(a)	2.40	2.36	0.76
2(b)	2.37	2.52	2.13
Comparative	3.06	2.98	5.17

The results show that by using the combination of first and second binders that the attrition losses are reduced markedly over the single binder sample. The use of hot or cold water does not appear to have had a significant effect.

Example 3.

A further variation studied was to increase the copper level from the 25% level in the above formulations to 50%.

Example	Cu/Zn composition	ATH	Binder 1	Binder 2
3(a)	50	50	10	4

Result

Example	MCS (Kg) (Unsulphided)	MCS (Kg) (Sulphided)	Attrition (% wt) (Sulphided)
3(a)	1.87	1.42	1.37

5 Example 4: Mercury Pickup Tests

Those formulations selected for study were;

- 1) Example 2(a).
- 2) Example 3(a).
- 10 3) A comparative Example (Example 1 Comparative 3), containing only Binder 2.

The materials were prepared for testing by crushing a portion of the 2.8 – 4.75mm precursor granules to grain size 1.0 – 2.0mm, then fully sulphiding in 1.0% of H₂S in nitrogen at 42 litres/hr. Following the sulphiding stage, the H₂S was purged from the reactor. The testing
 15 was carried out using a 25ml charge of the above prepared absorbents, at LHSV = 7.0hr-1, using n-hexane saturated with elemental mercury to ca. 1.0ppm w/v for a total run period of 750 hours unless otherwise stated. This would allow comparison with standard runs carried out previously. During the test period, the reactor effluent was occasionally sampled and analysed for mercury slippage.

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At the end of the test period, the beds were dried using a gentle flow of nitrogen, and removed from the reactor as 9 discrete sub-beds using a vacuum method. Each of the sub-beds was analysed for total mercury, using an ICP-atomic emission spectroscopic technique, to allow the mercury profile to be determined. A further check was made, calculating the average mercury
 25 concentration inlet the reactor during the run. From the analysis of the mercury level on each weighed sub-bed, the weight of mercury was calculated on each, and the summation gave the total weight of mercury passed through the bed during the run. Knowing the total number of hours the run had lasted and the hexane flow rate in ml/hr, then the average [Hg] inlet the bed in ppb of Hg (w/v) would be;

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$$\frac{\text{weight of Hg on beds (g)}}{\text{hrs on line x flow rate (ml/hr)}} = \text{ppb Hg}$$

35 The results were as follows;

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	Total Mercury on Discharged Sub-beds (ppm w/w)		
	Example 1 Comparative 3	Example 2(a)	Example 3(a)
1 Exit	Nil	Nil	Nil
2	Nil	Nil	Nil
3	Nil	Nil	Nil
4	Nil	10	Nil
5	17	92	Nil
6	76	810	35
7	1635	6250	440
8	17040	1900	10000
9 Inlet	47800	36200	45300
Calculated Inlet [Hg] ppb (w/v)	1230	986	929

Claims.

1. A particulate mercury absorbent comprising a sulphide of iron, copper or nickel, a support material, a first binder and a second binder wherein said first binder is a cement binder and the second binder is a high aspect ratio aluminosilicate clay binder having an aspect ratio >2 .
2. An absorbent according to claim 1 wherein the support material is an alumina or hydrated alumina.
3. An absorbent according to claim 1 or claim 2 wherein the first binder is a calcium aluminate cement binder.
4. An absorbent according to any one of claims 1 to 3 wherein the second binder is an Attapulgite clay.
5. An absorbent according to any one of claims 1 to 4 wherein the relative amounts of the first and second binder are in the range 2:1 to 3:1 (first to second binder).
6. A method for making the mercury absorbent according to any one of claims 1 to 5 comprising the steps of
 - (i) combining a compound of iron, copper or nickel capable of forming a metal sulphide with a support material, a first binder and a second binder in the presence of water to form a particulate absorbent precursor material,
 - (ii) drying the absorbent precursor material, and
 - (iii) sulphiding the precursor material to form the metal sulphide from the iron, copper or nickel compound
 wherein said first binder is a cement binder and the second binder is a high aspect ratio aluminosilicate clay binder having an aspect ratio >2 .
7. A method according to claim 6 wherein the iron, copper or nickel compound capable of forming the metal sulphide is combined with the support material, the first binder and the second binder in the presence of water in a granulator.
8. A method according to claim 6 or claim 7 wherein the sulphiding step is performed by reacting a sulphur compound selected from hydrogen sulphide, carbonyl sulphide, mercaptans and polysulphides with the iron, copper or nickel compound capable of forming the metal sulphide in the dried absorbent precursor material.

9. A mercury removal process comprising contacting a mercury-containing feed stream with an absorbent according to any of claims 1 to 5 or prepared according to any of claims 6 to 8.
10. A particulate mercury absorbent precursor comprising an iron, copper or nickel compound capable of forming a metal sulphide upon treatment with a sulphur compound, a support material, a first binder and a second binder, wherein said first binder is a cement binder and the second binder is a high aspect ratio aluminosilicate clay binder having an aspect ratio >2 .
11. A mercury absorbent precursor according to claim 10 wherein the support material is an alumina or hydrated alumina.
12. A mercury absorbent precursor according to claim 10 or claim 11 wherein the first binder is a calcium aluminate cement binder.
13. A mercury absorbent precursor according to any one of claims 10 to 12 wherein the second binder is an Attapulgite clay.
14. A mercury removal process comprises contacting a mercury-containing feed stream with an absorbent comprising a metal sulphide capable of absorbing mercury and wherein the absorbent is formed by contacting in-situ a precursor comprising an iron, copper or nickel compound capable of forming the metal sulphide, a support material, a first binder and a second binder with a first stream containing a sulphur compound, wherein said first binder is a cement binder and the second binder is a high aspect ratio aluminosilicate clay binder having an aspect ratio >2 .