

Description

The present invention relates to a musical tone synthesizing apparatus which is suitable for the electronic wind instrument.

Conventionally known technique can synthesize the musical tone of non-electronic musical instrument (hereinafter, simply referred to as acoustic instrument) by operating the artificial tone-generation model which is obtained by simulating the tone-generation mechanism of acoustic instrument. Such musical tone synthesizing technique is disclosed in Japanese Patent Laid-Open Publication No. 63-40199 and the corresponding EP-A-0 248 527, for example. Hereinafter, description will be given with respect to the modeling of the above-mentioned tone-generation mechanism of the wind instrument, and thereafter description will be further given to the conventional musical tone synthesizing apparatus using such modeling.

Fig. 1 is a sectional view showing the diagrammatical construction of the wind instrument such as the clarinet, saxophone etc. In Fig. 1, 1 designates a resonance tube and 2 designates a reed. In addition, TH designates a tone hole (or sound hole) which is formed at the predetermined position of the resonance tube 1.

When the performer blows breath 2A into the reed 2, the reed 2 vibrates due to blowing pressure PA and elastic characteristic thereof in direction 2S. As a result, pressure wave (i.e., compression wave) of air is produced in the vicinity of the reed 2 within the tube 1. Then, such compression wave progresses toward a terminal portion 1E of the tube 1 as progressive compression wave F. This progressive compression wave F is reflected by the terminal portion 1E and then returned to the reed 2 as reflected compression wave R, so that the reed 2 is affected by pressure PR due to reflected compression wave R. Therefore, when blowing the wind instrument, the reed 2 is affected by the following pressure P.

$$P = PA - PR \quad (1)$$

For this reason, the reed 2 will vibrate by the pressure P and elastic characteristic thereof. When the resonance state is established between the vibration of the reed 2 and the reciprocating motion of the compression waves F, R, the musical tone is generated from the wind instrument.

In this case, the resonance frequency is changed over by open/close operation of the tone hole TH formed at the tube 1. More specifically, when the open/close operation is carried out on the tone hole TH by the performer's finger, the flow of the compression wave is varied in the vicinity of the tone hole TH so that the substantial length of the tube is varied, whereby the resonance frequency is to be changed over.

Fig. 2 shows electric configuration of the conven-

tional musical tone synthesizing apparatus which is obtained by simulating the tone-generation mechanism of the wind instrument. In Fig. 2, 11 designates a non-linear element which simulates the operation of the reed 2, 12 designates a resonance circuit which simulates the resonance tube 1, and 13 designates a subtractor which simulates the foregoing formula (1) to be operated by the reed 2. Herein, the output of the non-linear element 11 is applied to the resonance circuit 12 as progressive wave signal. Then, the resonance circuit 12 converts the progressive wave signal into reflected wave signal, which is supplied to the subtractor 13.

In the resonance circuit 12, BD₁, BD₂, ... designate bi-directional transmission circuits each simulating the transmission delay characteristic of the compression wave which propagates in the resonance tube 1. In each of the bi-directional transmission circuits BD₁, BD₂ etc., DF designates a delay circuit for transmitting the progressive wave signal and DR designates another delay circuit for transmitting the reflected wave signal. Further, TRM designates a terminal circuit which simulates the reflection of the compression wave which is reflected at the terminal portion 1E of the resonance tube 1 (see Fig. 1). This terminal circuit TRM consists of a low-pass filter ML and an inverter IV. Herein, the low-pass filter ML simulates the acoustic loss which is occurred due to the reflection of the compression wave, while the inverter IV simulates the phase inversion of the compression wave to be reflected. Incidentally, this inverter IV is not required when the terminal portion 1E is closed but required when the terminal portion 1E is opened.

Furthermore, JU₁ designates a junction circuit which simulates the scattering of the compression wave in the vicinity of the tone hole TH. In JU₁, M₁, M₂ designate multipliers; A₁, A₂ designate subtractors; and Aj designates an adder. The delay circuit DF in the bi-directional transmission circuit BD₁ outputs progressive wave signal F₁ to the multiplier M₁ wherein F₁ is multiplied by a coefficient a₁ so that multiplication result a₁F₁ is obtained. On the other hand, the delay circuit DR in the bi-directional transmission circuit BD₂ outputs reflected wave signal R₁ to the multiplier M₂ wherein R₁ is multiplied by another coefficient a₂ so that multiplication result a₂R₁ is obtained. Herein, the coefficients a₁, a₂ will be described later in detail. The adder Aj adds these two multiplication results together, and then its addition result is supplied to both of the subtractors A₁, A₂. The subtractor A₁ subtracts F₁ from the addition result of adder Aj to thereby output its subtraction result to the delay circuit DR in the bi-directional transmission circuit BD₁ as reflected wave signal R₂. On the other hand, the subtractor A₂ subtracts R₁ from the addition result of Aj to thereby output its subtraction result to the delay circuit DF in the bi-directional transmission circuit BD₂ as progressive wave signal F₂.

Next, description will be given with respect to the coefficients a_1 , a_2 to be used in the multipliers M_1 , M_2 with respect to two cases.

(i) First Case where the tone hole TH is opened:

The following formula (2) represents air pressure P_j at point j which is set in the vicinity of the tone hole TH in the tube 1 shown in Fig. 1.

$$P_j = a_{1off} P_{1+} + a_{2off} P_{2+} \quad (2)$$

Herein, P_{1+} designates the pressure of the compression wave which enters into the point j from the reed 2, while P_{2+} designates another pressure of the compression wave which enters into the point j from the terminal portion 1E. In addition, a_{1off} , a_{2off} designate ratios of two pressures of compression waves, which can be represented by the following formulae (3), (4) respectively.

$$a_{1off} = 2\phi_1^2/(\phi_1^2 + \phi_2^2 + \phi_3^2) \quad (3)$$

$$a_{2off} = 2\phi_2^2/(\phi_1^2 + \phi_2^2 + \phi_3^2) \quad (4)$$

In the above formulae, ϕ_1 designates the diameter of the tube 1 in reed side; ϕ_2 designates the diameter of the tube 1 in terminal side; and ϕ_3 designates the diameter of the tone hole TH. In Fig. 2, the progressive wave signal F_1 corresponds to the pressure P_{1+} , while the reflected wave signal R_1 corresponds to the pressure P_{2+} . In this first case where the tone hole TH is opened, the above-mentioned coefficients a_{1off} , a_{2off} are used as the foregoing coefficients a_1 , a_2 of the multipliers M_1 , M_2 respectively. For this reason, the adder A_j can output the operation result of foregoing formula (2), i.e., signal corresponding to the air pressure P_j at the point j in the tube 1.

Meanwhile, the following formulae (5), (6) respectively represent pressure P_{1-} of the reflected compression wave which flows from the point j toward the reed 2 and pressure P_{2-} of the progressive compression wave which flows from the point j toward the terminal portion 1E.

$$P_{1-} = P_j - P_{1+} \quad (5)$$

$$P_{2-} = P_j - P_{2+} \quad (6)$$

Thus, these pressures P_{1-} , P_{2-} correspond to the outputs of the subtractors A_1 , A_2 respectively.

(ii) Second Case where the tone hole TH is closed:

This case is equivalent to the state where the diameter ϕ_3 of the tone hole TH is at "0". Therefore, coefficients a_{1on} , a_{2on} can be obtained by putting " $\phi_3=0$ " in the foregoing formulae (3), (4) respectively.

$$a_{1on} = 2\phi_1^2/(\phi_1^2 + \phi_2^2) \quad (7)$$

$$a_{2on} = 2\phi_2^2/(\phi_1^2 + \phi_2^2) \quad (8)$$

These coefficients a_{1on} , a_{2on} are used as the foregoing coefficients a_1 , a_2 of the multipliers M_1 , M_2 .

Thus, the adder A_j can output the signal corresponding to the air pressure P_j at the point j of the tube 1 in accordance with the following formula (9).

$$P_j = a_{1on} P_{1+} + a_{2on} P_{2+} \quad (9)$$

Then, the subtractors A_1 , A_2 output signals corresponding to the pressures P_{1-} , P_{2-} .

As described heretofore, the circuit shown in Fig. 2 can simulate the scattering state of the compression wave in the tube 1 in response to the open/close operation of the tone hole TH.

In the present example of the conventional musical tone synthesizing apparatus, a bias value V_A corresponding to the blowing pressure P_A is applied to the non-linear element 11 via the subtractor 13. The output signal of the non-linear element 11 is transmitted to the terminal circuit TRM via the bi-directional transmission circuits BD_1 , BD_2 and junction circuit JU_1 etc. In the junction circuit JU_1 , values of the coefficients a_1 , a_2 are changed over in response to the open/close operation of the tone hole TH as described before, and consequently the scattering state in the junction circuit JU_1 is changed over. The progressive wave signal reached at the terminal circuit TRM is processed by the low-pass filter ML and inverter IV so that the reflected wave signal is obtained. This reflected wave signal is transmitted through the circuits BD_2 , JU_1 , BD_1 etc. and then supplied to the non-linear element 11 via the subtractor 13. Thus, the resonance state is established between the non-linear element 11 and resonance circuit 12. In this case, the resonance frequency can be changed over by changing over the coefficients a_1 , a_2 used in the junction circuit JU_1 in response to the open/close state of the tone hole TH.

In the actual performance of the wind instrument, the tone hole is gradually opened or closed by the performer's finger. However, the junction circuit of the above-mentioned conventional musical tone synthesizing apparatus can merely change over its operation in response to full-open and full-close states of the tone hole TH. For this reason, there is a problem in that the conventional apparatus cannot reproduce the real variation of the musical tone in response to the finger operation of the wind instrument.

Meanwhile, some wind instrument provides the tone hole portion which is projected from the tube as shown in Fig. 5. In such case, the compression wave is partially and discretely flown into the opening portion of the tone hole, and the compression wave is partially reflected by the opening portion of the tone hole. However, the conventional apparatus cannot simulate such projection of the tone hole portion. For this reason, there is a problem in that the conventional apparatus cannot simulate the wind instrument with accuracy.

In addition, the conventional apparatus as shown in Fig. 2 requires one junction circuit (including two multipliers, two subtractors and one adder) in order to carry out the operational process which simulates the operation of one tone hole. Therefore, there is a problem in that the hardware of the conventional apparatus must be enlarged. In contrast, when the above-mentioned operational process is carried out by the software to be executed by the digital signal proces-

sor (DSP) and the like, there is a problem in that the amount of software operations must be increased.

It is accordingly a primary object of the present invention to provide a musical tone synthesizing apparatus which can simulate the real variation of the musical tone in response to the actual finger operation of the wind instrument. This object is achieved by designing the musical tone synthesizing apparatus as stated in claim 1.

Further objects and advantages of the present invention will be apparent from the following description, reference being had to the accompanying drawings wherein preferred embodiments of the present invention are clearly shown.

In the drawings:

Fig. 1 is a sectional view showing the diagrammatical construction of the wind instrument;

Fig. 2 is a block diagram showing the electric configuration of the conventional musical tone synthesizing apparatus;

Fig. 3 is a block diagram showing an electric configuration of the musical tone synthesizing apparatus according to a first embodiment of the present invention;

Fig. 4 is a circuit diagram showing a detailed configuration of a junction circuit shown in Fig. 3;

Fig. 5 is a simulation model of another type of wind instrument to be used in the first embodiment;

Figs. 6 and 7 are circuit diagrams showing detailed configurations of coefficient operation circuits provided in the first embodiment;

Fig. 8 is a block diagram showing the musical tone synthesizing apparatus according to a second embodiment of the present invention;

Fig. 9 is a block diagram showing the musical tone synthesizing apparatus according to a first modified example of the second embodiment;

Fig. 10 is a circuit diagram showing a terminal circuit shown in Fig. 9; and

Figs. 11, 12, 13 are block diagrams showing second, third and fourth modified examples of the second embodiment respectively.

Next, description will be given with respect to the preferred embodiments of the present invention.

[A] FIRST EMBODIMENT

Fig. 3 is a block diagram showing the electric configuration of the musical tone synthesizing apparatus according to the first embodiment of the present invention, wherein parts identical to those shown in Fig. 2 will be designated by the same numerals, hence, description thereof will be omitted. In Fig. 3, 21 designates a musical tone control information generating circuit which generates musical tone control information (indicative of open/close signal of tone hole, blowing intensity, note-on event, note-off event etc.) in ac-

cordance with the detected operation of each manual operable member provided on the wind instrument body (not shown). In addition, 22 designates an excitation circuit consisting of the foregoing non-linear element 11 and subtractor 13 shown in Fig. 2. Herein, the musical tone control information generating circuit 21 outputs the information VA representative of the blowing intensity to the subtractor 13 in the excitation circuit 22.

Next, JA₁ designates a junction circuit corresponding to one tone hole. 23 designates a tone hole control circuit which controls coefficients used to carry out the operations in the junction circuit JA₁ in accordance with the open/close signal of tone hole. The tone hole control circuit 23 contains the coefficient operation circuit as shown in Fig. 6. In Fig. 6, M₁₁, M₁₂, M₁₃ designate multipliers, A₁₁ designates an adder and D₁₁ designates a divider.

Incidentally, Fig. 3 illustrates the circuit portion (i.e., 22, BD₁, JA₁, BD₂) corresponding to the instrument portion defined from the reed to first tone hole and another circuit portion (i.e., TRM) corresponding to the terminal portion of the resonance tube, however, the circuit portions corresponding to other instrument portions are omitted from Fig. 3. In other words, bi-directional transmission circuits BD₃, ..., BD_n (wherein BD_n is the closest to the terminal circuit TRM) corresponding to the tube length, junction circuits JA and other tone hole control circuits corresponding to other tone holes are provided between BD₂ and TRM in Fig. 3, however, they are omitted from Fig. 3.

Fig. 4 is a block diagram showing the circuit configuration of the junction circuit JA₁, wherein parts identical to those shown in Fig. 2 are designated by the same numerals, hence, description thereof will be omitted. This junction circuit JA₁ is designed to simulate the tone hole which is projected from the tube as shown in Fig. 5. When such tone hole is opened, the compression wave of air which is blown from the tube toward the outside via the tone hole at pressure P₃₊ is partially reflected by the opening of tone hole, and then the reflected compression wave of air is flown into the tube from the tone hole at pressure P₃₋. Thus, the following air pressure P_j will be caused at point j in the vicinity of the tone hole in the tube.

$$P_j = a_1 P_{1+} + a_2 P_{2+} + a_3 P_{3+} \quad (10)$$

As described before, P₁₊ represents the pressure of the progressive compression wave of air which is flown into point j from the reed, while P₂₊ represents the pressure of the reflected compression wave of air which is flown into point j from the terminal portion of the tube. In this case, the coefficients can be obtained from the following formulae.

$$a_1 = 2\phi_1^2 / (\phi_1^2 + \phi_2^2 + \phi_3^2) \quad (11)$$

$$a_2 = 2\phi_2^2 / (\phi_1^2 + \phi_2^2 + \phi_3^2) \quad (12)$$

$$a_3 = 2\phi_3^2 / (\phi_1^2 + \phi_2^2 + \phi_3^2) \quad (13)$$

On the other hand, when the tone hole is closed, the coefficients can be obtained from the following formulae.

$$a_1 = 2\phi_1^2/(\phi_1^2 + \phi_2^2) \quad (14)$$

$$a_2 = 2\phi_2^2/(\phi_1^2 + \phi_2^2) \quad (15)$$

$$a_3 = 0$$

In addition, P_{1-} represents the pressure of the reflected compression wave of air which is flown toward the reed from point j; P_{2-} represents the pressure of the progressive compression wave of air which is flown toward the terminal portion from point j; and P_{3-} represents the pressure of the compression wave of air which is flown through the tone hole from point j. These pressures can be obtained from the following formulae.

$$P_{1-} = P_j - P_{1+} \quad (17)$$

$$P_{2-} = P_j - P_{2+} \quad (18)$$

$$P_{3-} = P_j - P_{3+} \quad (19)$$

In Fig. 4, delay circuits DTF, DTR simulate the propagation delay of the compression wave of air which flows through the tube-like portion of the tone hole, wherein the delay times thereof are determined in response to height H of such tube-like portion of the tone hole. In addition, TL designates a low-pass filter (LPF) which simulates the acoustic loss due to the reflection of the compression wave of air at the terminal portion of the tone hole; and M_4 designates a multiplier which simulates the reflection of the compression wave of air at the tip edge portion of the tone hole. In addition, A_3 , M_3 designate a subtractor and a multiplier respectively which simulate the flow control of the compression wave of air to be flown from the tube to the tone hole and to be flown from the tone hole to the tube.

Hereinafter, description will be given with respect to the operation of the musical tone synthesizing apparatus. When the musical tone control information generating circuit 21 generates the blowing pressure information and note-on signal, the value VA corresponding to the blowing pressure is supplied to the non-linear element 11 via the subtractor 13. At this time, the non-linear element 11 is at the enable state so that the output thereof is transmitted to the terminal circuit TRM via the bi-directional transmission circuit BD_1 , junction circuit JA_1 , bi-directional transmission circuit BD_2 etc. Then, the reflected wave signal from the terminal circuit TRM is transmitted back to the non-linear element 11 via BD_2 , JA_1 , BD_1 etc. and 13. Thus, the excitation circuit 22 and resonance circuit (consisting of BD_1 , JA_1 , BD_2 etc. & TRM) are set in the resonance state so that the synthesized musical tone can be picked up.

In the above-mentioned state, a control variable "x" used in the tone hole control circuit 23 is varied in accordance with the tone hole open/close signal outputted from the musical tone control information generating circuit 21. When the tone hole open/close sig-

nal represents "tone hole open state", the control variable x is gradually varied from "0" to " ϕ_3^2 " (where ϕ_3 designates the diameter of tone hole) in lapse of time. Such variation of the control variable x corresponds to the variation of the substantial opening area of tone hole when the performer releases his finger off from the tone hole. On the other hand, when the tone hole open/close signal represents "tone hole close state", the control variable x is gradually varied from " ϕ_3^2 " to "0" in lapse of time. Such control variable x is applied to the coefficient operation circuit shown in Fig. 6, so that this coefficient operation circuit will carry out the following coefficient operations.

$$a_1(x) = 2\phi_1^2/(\phi_1^2 + \phi_2^2 + x) \quad (20)$$

$$a_2(x) = 2\phi_2^2/(\phi_1^2 + \phi_2^2 + x) \quad (21)$$

$$a_3(x) = 2x/(\phi_1^2 + \phi_2^2 + x) \quad (22)$$

Then, the operational results, i.e., $a_1(x)$, $a_2(x)$, $a_3(x)$ are respectively supplied to the multipliers M_1 , M_2 , M_3 shown in Fig. 4 so that the level of each signal to be supplied to the adder Aj is controlled. As described above, the circuits shown in Figs. 4 and 6 can carry out the signal processings which simulate the variation of the scattering state of the compression wave of air in the vicinity of the tone hole when the performer gradually opens the tone hole or gradually closes the tone hole by his finger.

At the same time, the tone hole control circuit 23 computes the coefficient $f(x)$ used for the multiplier M_4 . Incidentally, the circuit used to compute such coefficient $f(x)$ is omitted from the drawings of the present invention. Herein, when $x=0$ representing the full close state of tone hole, $f(0)=1$; when $x=\phi_3^2$ representing the full open state of tone hole, $f(\phi_3^2)=-1$. If x gradually increases from "0" to " ϕ_3^2 ", the coefficient $f(x)$ gradually decreases from "1" to "-1". Then the computed coefficient $f(x)$ is supplied to the multiplier M_4 . As described above, the computation of $f(x)$ corresponding to the signal processings which simulate the variation of the reflection characteristic of the compression wave of air to be reflected at the tip edge portion of tone hole when the performer gradually opens and closes the tone hole by his finger. Due to the variation of the coefficients $a_1(x)$, $a_2(x)$, $a_3(x)$, $f(x)$, the resonance waveform to be generated from the present musical tone synthesizing apparatus is varied. Thus, it is possible to reproduce the variation of musical tone signal when the performer gradually opens and closes the tone hole.

The above description relates to the wind instrument of which tone hole is projected from the tube as shown in Fig. 5. Next, description will be given with respect to the wind instrument of which tone hole is cut through the tube as shown in Fig. 1 (i.e., the height H of tone hole is zero). In this instrument, the junction circuit JU_1 shown in Fig. 2 is applied as the junction circuit JA_1 , and circuit as shown in Fig. 7 is used as the coefficient operation circuit of the tone hole control circuit 23. In Fig. 7, M_{21} , M_{22} designate multipliers,

A₂₁ designates an adder and D₂₁ designates a divider. When the control variable x representative of the opening degree of tone hole is applied to this circuit shown in Fig. 7, the foregoing operations of formulae (20), (21) are executed so that the coefficients $a_1(x)$, $a_2(x)$ are obtained. Then, these coefficients $a_1(x)$, $a_2(x)$ are supplied to the multipliers M₁, M₂ as a_1 , a_2 in the junction circuit JU₁ as shown in Fig. 2. Thus, as similar to the tone hole shown in Fig. 5, it is possible to reproduce the variation of musical tone when the performer gradually opens and closes the tone hole as shown in Fig. 1.

The first embodiment discloses the musical tone synthesizing apparatus according to the present embodiment. However, the present embodiment is not limited to such apparatus, hence, it is possible to modify the present embodiment to the reverberation effect applying apparatus, for example. In this case, it is possible to simulate the variation of reverberation effect which is caused when the performer opens or closes the hole provided in the sound field of the reverberation effect applying apparatus. In addition, it is possible to apply the present embodiment to the apparatus which simulates the vibration of string of the string instrument when the performer slightly touches the string by his finger and the like.

[B] SECOND EMBODIMENT

Fig. 8 is a block diagram showing the musical tone synthesizing apparatus according to the second embodiment of the present invention. In Fig. 8, 111 designates a non-linear function circuit; 113 designates an adder; INV designates an inverter; BD₁, BD₂ designate bi-directional transmission circuits; JA₁ designates a junction circuit including a multiplier Mk and an adder Ak; and TRMa designates a terminal circuit consisting of a multiplier Mj and a low-pass filter (LPF) ML.

The junction circuit JA₁ directly transmits progressive wave data F from the bi-directional transmission circuit BD₁ to next bi-directional transmission circuit BD₂. In the junction circuit JA₁, the multiplier Mk multiplies the progressive wave data F by a coefficient r_1 , and then the multiplication result is added to reflected wave data R₁. The addition result of the adder Ak is transmitted to the bi-directional transmission circuit BD₁ as reflected wave data R₂. Herein, the coefficient r_1 used in the multiplier Mk is changed over by control means (not shown) in response to the operation of the tone hole. For example, this coefficient r_1 is set at the relatively small value when the tone hole is closed, while r_1 is set at the relatively large value when the tone hole is opened. As the method of changing over the coefficient r_1 , the following two methods can be employed. In first method, one of the predetermined two values is selected in response to the open/close state of the tone hole. In second meth-

od, the value of r_1 is continuously varied in response to the substantial opening area of the tone hole when the performer actually performs the wind instrument by opening or closing each tone hole.

In the terminal circuit TRMa, the multiplier Mj multiplies the progressive wave data F by a coefficient r_2 , and then the multiplication result is subject to the filtering operation in the LPF ML. Thereafter, the output of the LPF ML is transmitted from the terminal circuit TRMa as reflected wave data. Herein, the coefficient r_2 used in the multiplier Mj is changed over by control means (not shown) in synchronism with the foregoing change-over operation of r_1 . More specifically, when the tone hole is closed, r_1 is set smaller but r_2 is set larger. On the other hand, when the tone hole is opened, r_1 is set larger but r_2 is set smaller. In the present embodiment, the following relation can be established between the coefficients r_1 , r_2 .

$$r_1 + r_2 \leq 1 \quad (30)$$

The reflected wave data is transmitted through BD₂, JA₁, BD₁ etc. and then supplied to the inverter INV. The inverter INV inverts the reflected wave data R₂, and then the inverted data is fed back to the adder 113.

In the present embodiment, the output data of the non-linear function circuit 111 will reach at the terminal circuit TRMa as the progressive wave data without being attenuated. When the tone hole is closed, the coefficient r_2 is set larger so that the progressive wave data is supplied to the LPF ML without being substantially attenuated. Then, the LPF ML carries out the filtering operation which simulates the acoustic loss to be caused at the terminal portion of the resonance tube of the wind instrument. Thereafter, the terminal circuit TRMa will transmit the reflected wave data toward the adder 113. In such transmission, the reflected wave data must pass through the junction circuit JA₁ wherein the multiplication coefficient r_1 is set smaller. Therefore, in the junction circuit JA₁, the progressive wave data is not substantially mixed in the reflected wave data. In this case, the resonance frequency is substantially determined by the time which is required when the output data of the non-linear function circuit 111 is transmitted through BD₁, BD₂, JA₁, TRMa etc. in forward and backward directions.

On the other hand, when the tone hole is opened, the coefficient r_2 is set smaller so that the progressive wave data is attenuated and then supplied to the LPF ML in the terminal circuit TRMa. In this case, the reflected wave data can be negligible. In addition, the coefficient r_1 is set larger in the junction circuit JA₁, corresponding to the tone hole which is opened. Thus, the progressive wave data is not substantially attenuated by the multiplier Mk and then transmitted toward the adder 113 as the reflected wave data. In this case, the resonance frequency can be substantially determined by the time which is required when the output

data of the non-linear function circuit 111 is transmitted through BD_1 , BD_2 , JA_1 , $TRMa$ in forward and backward directions.

In the above-mentioned case, the coefficients r_1 , r_2 are determined in accordance with the foregoing formula (30), so that the closed-loop gain in the circuit shown in Fig. 8 can be normally held at the value lower than "1". Thus, it is possible to avoid the multifunctional phenomenon where the present apparatus as a whole is set in the oscillating state.

(1) First Modified Example

Next, description will be given with respect to the first modified example of the second embodiment by referring to Figs. 9 and 10.

Meanwhile, when the tone hole is opened, the progressive wave data reached at the junction circuit JA_1 is directly transmitted toward the adder 113 as the reflected wave data in the foregoing second embodiment as shown in Fig. 8. In other words, the second embodiment neglects the acoustic loss when the tone hole is opened.

However, in the case where the acoustic loss cannot be neglected, the second embodiment shown in Fig. 8 is modified to the first modified example as shown in Fig. 9. Instead of the junction circuit JA_1 shown in Fig. 8, the present example uses a junction circuit JB_1 as shown in Fig. 9. In this junction circuit JB_1 , the multiplier M_k multiplies the progressive wave data by the foregoing coefficient r_1 , and then the multiplication result is subject to the filtering operation in a LPF ML_1 . Thereafter, the output data of the LPF ML_1 is transmitted as the reflected wave data via the adder A_k . Herein, the cut-off frequency of LPF ML_1 can be changed over in response to function $f(r_1)$ using the coefficient r_1 as its parameter.

When the tone hole is closed so that the coefficient r_1 is set smaller, the cut-off frequency of LPF ML_1 is controlled to be higher. On the other hand, when the tone hole is opened so that r_1 is set larger, the cut-off frequency of LPF ML_1 is controlled to be lower. In addition, when the tone hole is opened, the progressive wave data is subject to the filtering operation corresponding to the acoustic loss in the tone hole in the LPF ML_1 , and then the output data of LPF ML_1 is outputted as the reflected wave data.

Instead of the terminal circuit $TRMa$, it is possible to employ another terminal circuit $TRMb$ to be connected to the circuit shown in Fig. 9. As similar to $TRMa$, this terminal circuit $TRMb$ consists of the multiplier M_j and LPF ML_2 . Herein, the cut-off frequency of LPF ML_2 is set higher when the output of multiplier M_j is relatively small, while the cut-off frequency of LPF ML_2 is set lower when the output of M_j is relatively large. By connecting several terminal circuits such as $TRMb$, it is possible to perform the experiment wherein the musical tone can be examined in response to

the open/close state of the tone hole of the wind instrument which is blown.

(2) Second Modified Example

Fig. 11 shows the second modified example of the second embodiment. In contrast to the foregoing second embodiment which uses the delay circuits for both of the progressive wave data and reflected wave data, the present example uses delay circuits DFF_1 , DFF_2 etc. only for the progressive wave data to be transmitted toward the terminal circuit $TRMa$. Herein, each of the delay circuits DFF_1 , DFF_2 , ... has the delay time corresponding to the sum of the delay times of delay circuits DF_i , DR_i (where $i = 1$ to n) in the second embodiment shown in Fig. 8. Thus, the present example can perform the pitch control as similar to that of the second embodiment. Instead of the junction circuit JA_1 shown in Fig. 8, the present example uses a junction circuit JC_1 consisting of the multiplier M_k and a LPF ML_0 . The output of multiplier M_k is subject to the filtering operation corresponding to the acoustic loss in the tone hole in the LPF ML_0 .

The present example is characterized by that it is possible to reduce the number of delay circuits as comparing to that of the foregoing second embodiment and its first modified example, so that the size of the present example can be reduced. Further, by employing the digital signal processor in the musical tone synthesizing apparatus according to the second modified example, it is possible to reduce the amount of operational processes as comparing to that of the foregoing second embodiment and its first modified example.

(3) Third Modified Example

Fig. 12 shows the third modified example of the second embodiment. As comparing to the foregoing second modified example as shown in Fig. 11, the third modified example as shown in Fig. 12 omits the LPFs ML_1 , ML_0 but newly provides another LPF ML_3 prior to the inverter INV . The filtering operation of this LPF ML_3 simulates the acoustic loss to be caused at the tone hole and opening end as a whole. This third modified example is characterized by further reducing the number of elements to be required to configure the musical tone synthesizing apparatus.

(4) Fourth Modified Example

Fig. 13 shows the fourth modified example of the second embodiment. In contrast to the foregoing third modified example wherein the output of DFF is directly supplied to the multiplier M_k , the fourth modified example uses a multi-stage delay circuit MFF which is used instead of the delay circuits DFF_1 , DFF_2 etc. Then, n -stage output and $(n+1)$ -stage output of this

multi-stage delay circuit MFF are respectively multiplied by coefficients (1-m), m in multipliers Ma, Mb. Thereafter, an adder Am adds two multiplication results from the multipliers Ma, Mb together, and its addition result is supplied to the multiplier Mk.

Herein, the whole delay time of the multi-stage delay circuit MFF is set equal to the sum of delay times of the delay circuits DFF₁, DFF₂. Meanwhile, data pick-up positions of MFF to be connected to Ma, Mb are determined in accordance with the positions of the tone holes in the wind instrument. In addition, the coefficients (1-m), m to be used for n-stage, (n+1)-stage of MFF are used to carry out the linear interpolation on the progressive wave data. For example, the value ranging from "0" to "1" is used as such coefficients (1-m), m. More specifically, the following linear interpolation operation is carried out on n-stage output F(n), (n+1)-stage output F(n+1) of MFF.

$$FT = (1 - m)F(n) + mF(n + 1) \quad (31)$$

Thus, the addition result of the adder Am can be represented by FT in the above formula. Therefore, the progressive wave data which simulates the compression wave of air at the actual position of the tone hole is to be outputted via the multiplier Mk and adder Ak as the reflected wave data.

Thus, the present example can perform the musical tone synthesizing control corresponding to the pitch-bend or vibrato performance. More specifically, when the pitch-bend control is carried out, the coefficients (1-m), m are varied in accordance with the predetermined curve after the tone-generation is started, so that these coefficients will be converged on the values corresponding to the regular positions of the tone holes after the predetermined time is passed. Thus, the pitch can be bent when starting to generate the musical tone, so that the pitch-bend performance can be embodied. In case of the vibrato performance, these coefficients are varied in the sine-wave manner, for example. Thus, the pitch can be intermittently varied, so that the vibrato performance can be embodied.

In the second embodiment and its modified examples, the non-linear function circuit 111 is constructed by ROM. However, it is possible to construct the non-linear function circuit 111 by the random-access memory (RAM), operation circuit and other non-linear elements. Of course, the present embodiment is not limited to synthesize the wind instrument tone, hence, it is possible to synthesize the string instrument tone in which the size of string is not constant in one string, and also synthesize the reverberation effect applied tone and the like in the complicated three-dimensional space.

Claims

1. A musical tone synthesizing apparatus which

simulates a resonance tube of a musical instrument having at least one sound hole opened or closed by a performer comprising:

first and second signal processing means (BD₁, BD₂) each delaying an input signal thereof with a predetermined delay time;

junction means (JA₁) for carrying out a predetermined operational process on output signals of said first and second signal processing means to thereby effect scattering operation on the output signals of said first and second signal processing means, so that respective output signals of said junction means are fed back to said first and second signal processing means so that a synthesized musical tone signal which simulates said musical instrument providing said resonance tube with plural sound holes is obtained based on a signal picked up from a loop consisting of said first and second signal processing means and said junction means; characterized by

sound hole information generating means (23) for generating gradually varying sound hole information representative of a gradually varying open/close state of said sound hole to be gradually opened or closed,

wherein coefficients (f(x), a₃, r₁, r₂) used in said operational process to be carried out by said junction means are varied in response to said sound hole information.

2. A musical tone synthesizing apparatus according to claim 1 comprising

third signal processing means delaying an input signal thereof with a predetermined delay time, said junction means (JA₁) connecting said first, second and third signal processing means together,

wherein a synthesized musical tone signal is obtained by setting all of said first, second and third signal processing means and connecting means at resonance states respectively.

3. A musical tone synthesizing apparatus according to claim 1 or 2 wherein at least one of said signal processing means carries out a level control on the input signal thereof in addition to delaying the input signal thereof with the predetermined delay time.

4. A musical tone synthesizing apparatus according to claim 2 wherein said third signal processing means (23) are designed for carrying out a frequency band control on an input signal thereof.

5. A musical tone synthesizing apparatus according to claim 4 wherein said third signal processing means carries out a level control on the input sig-



multi-stage delay circuit MFF are respectively multiplied by coefficients (1-m), m in multipliers Ma, Mb. Thereafter, an adder Am adds two multiplication results from the multipliers Ma, Mb together, and its addition result is supplied to the multiplier Mk.

Herein, the whole delay time of the multi-stage delay circuit MFF is set equal to the sum of delay times of the delay circuits DFF₁, DFF₂. Meanwhile, data pick-up positions of MFF to be connected to Ma, Mb are determined in accordance with the positions of the tone holes in the wind instrument. In addition, the coefficients (1-m), m to be used for n-stage, (n+1)-stage of MFF are used to carry out the linear interpolation on the progressive wave data. For example, the value ranging from "0" to "1" is used as such coefficients (1-m), m. More specifically, the following linear interpolation operation is carried out on n-stage output F(n), (n+1)-stage output F(n+1) of MFF.

$$FT = (1 - m)F(n) + mF(n + 1) \quad (31)$$

Thus, the addition result of the adder Am can be represented by FT in the above formula. Therefore, the progressive wave data which simulates the compression wave of air at the actual position of the tone hole is to be outputted via the multiplier Mk and adder Ak as the reflected wave data.

Thus, the present example can perform the musical tone synthesizing control corresponding to the pitch-bend or vibrato performance. More specifically, when the pitch-bend control is carried out, the coefficients (1-m), m are varied in accordance with the predetermined curve after the tone-generation is started, so that these coefficients will be converged on the values corresponding to the regular positions of the tone holes after the predetermined time is passed. Thus, the pitch can be bent when starting to generate the musical tone, so that the pitch-bend performance can be embodied. In case of the vibrato performance, these coefficients are varied in the sine-wave manner, for example. Thus, the pitch can be intermittently varied, so that the vibrato performance can be embodied.

In the second embodiment and its modified examples, the non-linear function circuit 111 is constructed by ROM. However, it is possible to construct the non-linear function circuit 111 by the random-access memory (RAM), operation circuit and other non-linear elements. Of course, the present embodiment is not limited to synthesize the wind instrument tone, hence, it is possible to synthesize the string instrument tone in which the size of string is not constant in one string, and also synthesize the reverberation effect applied tone and the like in the complicated three-dimensional space.

Claims

1. A musical tone synthesizing apparatus which

simulates a resonance tube of a musical instrument having at least one sound hole opened or closed by a performer comprising:

first and second signal processing means (BD₁, BD₂) each delaying an input signal thereof with a predetermined delay time;

junction means (JA₁) for carrying out a predetermined operational process on output signals of said first and second signal processing means to thereby effect scattering operation on the output signals of said first and second signal processing means, so that respective output signals of said junction means are fed back to said first and second signal processing means so that a synthesized musical tone signal which simulates said musical instrument providing said resonance tube with plural sound holes is obtained based on a signal picked up from a loop consisting of said first and second signal processing means and said junction means; characterized by

sound hole information generating means (23) for generating gradually varying sound hole information representative of a gradually varying open/close state of said sound hole to be gradually opened or closed,

wherein coefficients (f(x), a₃, r₁, r₂) used in said operational process to be carried out by said junction means are varied in response to said sound hole information.

2. A musical tone synthesizing apparatus according to claim 1 comprising

third signal processing means delaying an input signal thereof with a predetermined delay time, said junction means (JA₁) connecting said first, second and third signal processing means together,

wherein a synthesized musical tone signal is obtained by setting all of said first, second and third signal processing means and connecting means at resonance states respectively.

3. A musical tone synthesizing apparatus according to claim 1 or 2 wherein at least one of said signal processing means carries out a level control on the input signal thereof in addition to delaying the input signal thereof with the predetermined delay time.

4. A musical tone synthesizing apparatus according to claim 2 wherein said third signal processing means (23) are designed for carrying out a frequency band control on an input signal thereof.

5. A musical tone synthesizing apparatus according to claim 4 wherein said third signal processing means carries out a level control on the input sig-



nal thereof in addition to carrying out a frequency band control on the input signal thereof.

6. A musical tone synthesizing apparatus according to anyone of the preceding claims comprising:

excitation means (111, 113, INV) for generating an excitation signal in response to performance information of a musical instrument,

said signal processing means being designed as bi-directional transmission means (BD₁, BD₂) for propagating said excitation signal outputted from said excitation means to a terminal portion as a progressive wave signal and also feeding back said excitation signal reflected by said terminal portion toward said excitation means as a reflected wave signal, so that a synthesized musical tone signal is obtained by setting both of said excitation means and said bi-directional transmission means at resonance states respectively;

further comprising pitch information generating means (23) for generating first and second coefficients concerning pitch information in response to said performance information, both of said first and second coefficients being used to designate a pitch of a musical tone to be generated;

said junction means (JA₁) being inserted in said bi-directional transmission means at its middle position which is determined such that a predetermined pitch can be obtained, said progressive wave signal reached at said middle position being multiplied by said first coefficient and then its multiplication result being added to said reflected wave signal reached at said middle position, thereafter addition result being outputted from said middle position of said bi-directional transmission means toward said excitation means; and

terminal means (TRMa) connected at said terminal portion of said bidirectional transmission means, said progressive wave signal supplied to said terminal means being multiplied by said second coefficient to thereby output its multiplication result as said reflected wave signal,

wherein the sum of said first and second coefficients is set lower than a predetermined value.

7. A musical tone synthesizing apparatus according to anyone of the preceding claims comprising:

computing means (21, 23) for computing open/close-degree of said sound hole to thereby produce sound hole information, said sound hole information representing an opening or closed state of said sound hole ranging between a full-open state and a full-closed state.

Patentansprüche

1. Vorrichtung zur Synthese von Musiktönen, die ein Resonanzrohr eines Musikinstrumentes mit wenigstens einem Tonloch, das vom Spieler geöffnet oder geschlossen wird, simuliert, und folgendes aufweist:

erste und zweite Signalverarbeitungsmittel (BD₁, BD₂), die jeweils ihr Eingangssignal mit einer vorgegebenen Verzögerungszeit verzögern;

Verbindungsmittel (JA₁), um einen vorgegebenen Operationsvorgang auf Ausgangssignale der ersten und zweiten Signalverarbeitungsmittel auszuüben, um dabei auf die Ausgangssignale der ersten und zweiten Signalverarbeitungsmittel eine Streuwirkung auszuüben, so daß die jeweiligen Ausgangssignale der Verbindungsmittel zu den ersten und zweiten Signalverarbeitungsmitteln zurückgeführt werden und ein synthetisches Musiktonsignal, welches das aus einem Resonanzrohr mit mehreren Tonlöchern bestehende Musikinstrument simuliert, auf der Grundlage eines Signals erhalten wird, welches von einer aus den ersten und zweiten Signalverarbeitungsmitteln und den Verbindungsmitteln bestehenden Schleife abgenommen wird; gekennzeichnet durch

Tonlochinformationerzeugungsmittel (23) zur Erzeugung einer fortschreitend variierenden Tonlochinformation, die für einen fortschreitend variierenden Offen- oder Geschlossenzustand des Tonloches, das fortschreitend geöffnet oder geschlossen werden soll, repräsentativ ist,

wobei Koeffizienten ($f(x)$, a_3 , r_1 , r_2), die bei dem durch die Verbindungsmittel durchgeführten Operationsvorgang verwendet werden, im Ansprechen auf die Tonlochinformation variiert werden.

2. Vorrichtung zur Synthese von Musiktönen nach Anspruch 1, die folgendes aufweist:

dritte Signalverarbeitungsmittel, die ihr Eingangssignal mit einer vorgegebenen Verzögerungszeit verzögern, wobei die Verbindungsmittel (JA₁) die ersten, zweiten und dritten Signalverarbeitungsmittel miteinander verbinden,

wobei ein synthetisches Musiktonsignal durch Einstellen aller ersten, zweiten und dritten Signalverarbeitungsmittel und der verbindenden Mittel auf die jeweiligen Resonanzzustände erhalten wird.

3. Vorrichtung zur Synthese von Musiktönen nach Anspruch 1 oder 2, bei der wenigstens eines der Signalverarbeitungsmittel eine Pegelsteuerung an seinem Eingangssignal zusätzlich zur Verzögerung des Eingangssignals um eine vorgegebene



ne Verzögerungszeit durchführt.

4. Vorrichtung zur Synthese von Musiktönen nach Anspruch 2, bei der die dritten Signalverarbeitungsmittel (23) auf ihr Eingangssignal eine Frequenzbandsteuerung ausüben. 5
5. Vorrichtung zur Synthese von Musiktönen nach Anspruch 4, bei der die dritten Signalverarbeitungsmittel eine Pegelsteuerung ihres Eingangssignales zusätzlich zur Frequenzbandsteuerung ausführen. 10
6. Vorrichtung zur Synthese von Musiktönen nach einem der vorhergehenden Ansprüche, die folgendes aufweist: 15

Erregungsmittel (111, 113, INV), um ein Erregungssignal im Ansprechen auf eine Spielinformation eines Musikinstrumentes zu erzeugen, 20

wobei die Signalverarbeitungsmittel als bidirektionale Übertragungsmittel (BD_1 , BD_2) gebaut sind, um das von den Erregungsmitteln ausgegebene Erregungssignal an einen Abschlußabschnitt als ein fortschreitendes Wellensignal auszusenden, und um außerdem das durch den Abschlußabschnitt reflektierte Erregungssignal an die Erregungsmittel als ein reflektiertes Wellensignal zurückzukoppeln, so daß ein synthetisches Musiktonsignal durch Einstellen sowohl der Erregungsmittel als auch der bidirektionalen Übertragungsmittel auf die jeweiligen Resonanzzustände erhalten wird, 25

weiterhin mit Tonhöheinformationserzeugungsmitteln (23), um die Tonhöheninformation betreffende erste und zweite Koeffizienten im Ansprechen auf die Spielinformation zu erzeugen, wobei sowohl die ersten als auch die zweiten Koeffizienten verwendet werden, um eine Tonhöhe eines zu erzeugenden Musiktones zu kennzeichnen; 30

wobei die Verbindungsmittel (JA_1) bei den bidirektionalen Übertragungsmitteln in deren Mittelposition zwischengeschaltet werden, die so bestimmt wird, daß eine vorgegebene Tonhöhe erhalten werden kann, und das diese Mittelposition erreichende progressive Wellensignal mit den ersten Koeffizienten multipliziert wird und sein Multiplikationsergebnis dann zu dem reflektierten Wellensignal, das die Mittelposition erreicht hat, addiert wird, und wobei danach das Additionsergebnis von der Mittelposition der bidirektionalen Übertragungsmittel an die Erregungsmittel ausgegeben wird; und 35

Abschlußmittel (TRMa), die mit dem Abschlußabschnitt der bidirektionalen Übertragungsmittel verbunden sind, wobei das den Abschlußmitteln zugeführte progressive Wellensi- 40

gnal mit dem zweiten Koeffizienten multipliziert wird, um dabei sein Multiplikationsergebnis als das reflektierte Wellensignal auszugeben,

wobei die Summe der ersten und zweiten Koeffizienten niedriger eingestellt wird als ein vorgegebener Wert. 45

7. Vorrichtung zur Synthese von Musiktönen nach einem der vorherigen Ansprüche, die folgendes aufweist: 50

Berechnungsmittel (21, 23) zur Berechnung des Öffnungsgrades des Tonloches, um dabei Tonlochinformation zu erzeugen, wobei die Tonlochinformation einen geöffneten oder geschlossenen Zustand des Tonloches repräsentiert, der von einem vollkommen geöffneten bis einem vollkommen geschlossenen Zustand reicht. 55

Revendications

1. Dispositif pour la synthèse des sons musicaux qui simule un tube de résonance d'un instrument de musique ayant au moins un orifice sonore ouvert ou fermé par un exécutant comprenant: 60

des premier et second moyens de traitement de signal (BD_1 , BD_2) chacun retardant un signal d'entrée de celui-ci avec un retard prédéterminé; 65

des moyens de jonction (JA_1) pour réaliser un traitement opératoire prédéterminé sur les signaux de sortie desdits premier et second moyens de traitement de signal pour effectuer de ce fait l'opération de diffusion sur les signaux de sortie desdits premier et second moyens de traitement de signal, de sorte que les signaux de sortie respectifs de ladite jonction sont réinjectés auxdits premier et second moyens de traitement de signal de sorte qu'un signal de son musical synthétisé qui simule ledit instrument de musique fournissant ledit tube de résonance avec plusieurs orifices sonores est obtenu en se fondant sur un signal prélevé sur une boucle constituée des premier et second moyens de traitement de signal et ledit moyen de jonction; caractérisé par le moyen de génération d'information d'orifice sonore (23) pour générer l'information d'orifice sonore variant progressivement représentative d'un état ouvert/fermé dudit orifice sonore variant progressivement pour être progressivement ouvert ou fermé, 70

où les coefficients ($f(x)$, a_3 , r_1 , r_2) utilisés dans ledit traitement opératoire à réaliser par ledit moyen de jonction varient en réponse à l'information d'orifice sonore. 75

2. Dispositif pour la synthèse de sons musicaux se- 80



- lon la revendication 1 comprenant
un troisième moyen de traitement de signal retardant un signal d'entrée de celui-ci avec un retard prédéterminé, ledit moyen de jonction (JA₁) raccordant entre eux lesdits premier, second et troisième moyens de traitement de signal, où le signal de son musical de synthèse est obtenu par réglage de tous les premier, deuxième et troisième moyens de traitement de signal et moyens de connexion à des états de résonance respectifs.
3. Dispositif pour la synthèse de sons musicaux selon la revendication 1 ou 2 où au moins un desdits moyens de traitement de signal exécute une commande de niveau sur le signal d'entrée correspondant en plus du retardement du signal d'entrée de celui-ci avec un retard prédéterminé.
4. Dispositif pour synthétiser les sons musicaux selon la revendication 2 où ledit troisième moyen de traitement de signal (23) est conçu pour exécuter une commande de bande de fréquence sur un signal d'entrée correspondant.
5. Dispositif pour synthétiser les sons musicaux selon la revendication 4 où ledit troisième moyen de traitement de signal exécute une commande de niveau sur le signal d'entrée correspondant en plus de l'exécution d'une commande de bande de fréquence sur ledit signal.
6. Dispositif pour synthétiser les sons musicaux selon une quelconque des revendications précédentes comprenant:
les moyen d'excitation (111, 113, INV) pour générer un signal d'excitation en réponse à l'information d'exécution d'un instrument de musique,
ledit moyen de traitement de signal étant conçu comme moyen de transmission bidirectionnelle (BD₁, BD₂) pour propager ledit signal d'excitation présenté en sortie dudit moyen d'excitation vers la partie terminale sous la forme d'un signal d'onde progressive et également pour réinjecter ledit signal d'excitation réfléchi par ladite partie terminale vers ledit moyen d'excitation sous la forme d'un signal d'onde réfléchi, de sorte qu'un signal de son musical synthétisé est obtenu en établissant à la fois ledit moyen d'excitation et ledit moyen de transmission bidirectionnelle aux états de résonance respectivement.
comprenant en outre le moyen de génération de l'information de hauteur de note (23) pour générer des premier et second coefficients concernant l'information de hauteur de note en réponse à ladite information d'exécution, les deux dits premier et second coefficients étant

utilisés pour désigner une hauteur de note d'un son musical à générer;

ledit moyen de jonction (JA₁) étant inséré dans ledit moyen de transmission bidirectionnelle à sa position médiane qui est déterminée de telle sorte qu'une hauteur de note prédéterminée puisse être obtenue, ledit signal d'onde progressive atteignant ladite position médiane étant ajouté audit signal d'onde réfléchi qui a atteint ladite position médiane, après quoi le résultat de l'addition étant présenté en sortie de ladite position médiane dudit moyen de transmission bidirectionnelle vers ledit moyen d'excitation; et

le moyen terminal (TRMa) raccordé à ladite partie terminale dudit moyen de transmission bidirectionnelle, ledit signal d'onde progressive fourni audit moyen terminal étant multiplié par ledit second coefficient pour présenter de ce fait en sortie son résultat de multiplication en tant que dit signal d'onde réfléchi,

où la somme desdits premier et second coefficients est établie pour être inférieure à une valeur prédéterminée.

7. Dispositif pour synthétiser les sons musicaux selon une quelconque des revendications précédentes comprenant:

le moyen de calcul (21, 23) pour calculer le degré d'ouverture / fermeture dudit orifice sonore pour produire de ce fait l'information d'orifice sonore, ladite information d'orifice sonore représentant un état d'ouverture ou de fermeture dudit orifice sonore dans une plage se situant entre un état d'ouverture totale et un état de fermeture totale.