

PROCESS FOR TREATING A STRUCTURE

FIELD OF THE INVENTION

5 The present invention relates to a method for processing a structure.

TECHNICAL BACKGROUND OF THE INVENTION

10 A structure 1 comprises from its rear side to its front side a carrier substrate 4, an insulating layer 3, and a useful layer 2, with the useful layer 2 having a free surface S. In a method for processing such a structure 1 known from the state of the art, and illustrated in Figures 1 and 2, the structure 1 is
15 placed in an atmosphere comprising chemical species in a gaseous form 6, with the chemical species 6 being likely to chemically react with the useful layer 2, with kinetics strictly increasing with the temperature of the useful layer 2.

20 During the treatment process, the structure 1 is held on a support structure 5 (or "chuck"). The structure support 5 is positioned in a reaction chamber 9.

25 The useful layer 2 is generally uniformly heated using a heating system 7, for example heating resistors or still halogen lamps.

 The chemical species 6 injected into the reaction chamber 9 thus chemically react with the free surface S of the useful layer 2. The type of chemical reaction

depends on the nature of the chemical species 6 and on the useful layer 2, and may then take the form of a thinning by etching of the useful layer 2, or thickening by epitaxy of the useful layer 2.

5 However, the useful layer 2 generally has variations in thickness and the methods for etching or thickening by epitaxy are known to be non-uniform and even increasing a bit more the variations in thickness of the useful layer 2. Variations in the thickness of
10 the useful layer 2 thus remain after the treatment process.

 Therefore, the main disadvantage of such treatment method is that, during the thinning or thickening reaction, the variations in thickness of the
15 useful layer 2 remain and may even be increased.

 The structures 1, such as the structures of the semiconductor-on-insulator (SeOI) type thus have variations in thickness, the spectral analysis of which reveals components having spatial wavelengths varying
20 from a few nanometers (roughness-like) to the size of the structure 1 (non-uniformity-like). Some techniques (smoothing annealing in a reducing atmosphere, for example) make it possible to reduce the variations in spatial wavelength thickness below a certain threshold,
25 for example 2 μ m. However, over the range of spatial wavelengths beyond such threshold, for example from 2 μ m to a few centimeters, reducing the non-uniformities in the thickness of the useful layer 2 remains very difficult.

In particular, a method for thickening the semiconductor layer by epitaxy, or for thinning the semiconductor layer by etching, in a structure 1 of the SeOI type, does not significantly reduce the variations
5 in thickness of the semiconductor layer on an extensive range of wavelengths.

The invention therefore provides a method for treating a structure 1 aiming at reducing the variations in thickness of the useful layer 2.

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BRIEF DESCRIPTION OF THE INVENTION

The present invention aims at wholly or partly remedying the aforementioned drawback, and relates to a method for treating a structure, with the structure
15 comprising from its rear side to its front side a carrier substrate, an insulating layer, and a useful layer, with the useful layer having a free surface, with the structure being placed in an atmosphere containing chemical species in a gaseous form, with the
20 chemical species being likely to chemically react with the useful layer, with kinetics strictly increasing with the temperature of the useful layer; with said treatment process being characterized in that the useful layer is heated by a pulsed laser beam, with the
25 beam sweeping at least partially the free surface of the useful layer, with the wavelength of the beam being different by less than 15nm, preferably by less than 7nm, from a central wavelength for which the

sensitivity of the estimated reflectivity of the structure relative to the insulator layer is zero.

The sensitivity of the estimated reflectivity of the structure relative to a layer corresponding to the partial derivative of the reflectivity relative to the thickness of said layer.

The estimated reflectivity is obtained, in turn, by a preliminary modeling of the structure.

The laser pulses make it possible to generate a heating at the point of impact of said pulses on the free surface of the useful layer.

The temperature thus reached by the useful layer at said point of impact makes it possible to activate the chemical reaction of the chemical species with the useful layer. This temperature is lower than the melting temperature of the material of the useful layer.

For a wavelength of the beam different by less than 15nm, preferably by less than 7nm, from the central wavelength, the Applicant has found that the heating of the useful layer only depends on the thickness of such layer.

In other words, the heating of the useful layer, during the sweeping by the laser beam, is substantially independent of the small variations in the thickness of the insulating layer. "Small variations" in the thickness of the insulating layer means variations in the thickness by plus or minus 1nm.

The wavelength of the laser pulses may be so selected as to heat the thicker areas of the useful layer to a higher temperature than the thinner areas.

Thus, a reaction of thinning by etching, activated by the laser pulses, will have greater kinetics in the thicker areas of the useful layer.

Similarly, the wavelength of the laser pulses may be so selected as to heat the thinner areas of the useful layer to a higher temperature than the thicker areas.

Thus, a reaction of thickening by epitaxy will have greater kinetics in the thinner areas of the useful layer.

Controlling the heating of the useful layer and thus the kinetics of the thickening or thinning reaction relative to thickness thus makes it possible to reduce the variations in thickness of the useful layer.

According to one embodiment, the structure is positioned in a reactive enclosure comprising the chemical species.

According to one embodiment, the duration of the laser beam pulses are less than a t_v value, with t_v being equal to: $t_v = l^2/D$, with D being the coefficient of thermal diffusion in the useful layer, and l corresponding to a threshold wavelength beyond which it is desired to reduce the variations in thickness of the layer.

"Duration" of a laser pulse means a unit time during which a beam is emitted.

For pulse durations smaller than t_v , a thermal equilibrium may not be reached over the entire surface of the impact point of the laser pulses on the useful layer. This is particularly advantageous when variations in thickness of the useful layer having a spatial wavelength smaller than the dimension of the impact point of the laser pulses must be corrected. As a matter of fact, for such pulse durations, the point of impact does not undergo a uniform heating over its entire surface, specifically the thinner areas of the point of impact are not heated to the same temperature as the thicker areas of the point of impact.

According to one embodiment, the pulsed laser beam has a pulse duration of less than 100ns.

According to one embodiment, the useful layer is a layer of a semiconductor material comprising at least one of the following materials: silicon, germanium, silicon germanium alloy.

According to one embodiment, the chemical species make it possible to etch the useful layer and the wavelength of the pulsed laser beam is so selected as to correspond to a negative value of the sensitivity of the reflectivity of the structure relative to the useful layer.

Thus, the thicker the area of the useful layer impacted by the laser pulses the higher the temperature reached during the heating. Therefore, the thicker the

area of the useful layer, the more important the etching kinetics. It is therefore possible to perform a partial etching of the useful layer over its entire surface while reducing the variation in thickness of
5 the useful layer.

According to one embodiment, the chemical species comprise HCl.

Thus, it is possible to etch a useful layer comprising semiconductor elements such as silicon,
10 germanium, or silicon germanium alloys.

According to one embodiment, the chemical species make it possible to thicken the useful layer by epitaxy, and the wavelength of the pulsed laser beam is so selected as to correspond to a positive value of the
15 sensitivity of the reflectivity of the structure relative to the useful layer.

Thus, the thinner the area of the useful layer impacted by the laser pulses, the higher the temperature reached during the heating.

Therefore, the thinner the area of the useful
20 layer, the more important the kinetics of the thickening by epitaxy. It is therefore possible to perform a thickening by epitaxy of the useful layer over its entire surface while reducing the variation in
25 thickness of the useful layer.

According to one embodiment, the chemical species comprise at least one of the following species: silane, disilane, trisilane, monochlorosilane, dichlorosilane, trichlorosilane, tetrachlorosilane germane,

monochlorogermane, dichlorogermane, trichlorogermane, tétrachlorogermane.

According to one embodiment, the insulating layer comprises silicon dioxide.

5 According to one embodiment, the insulating layer has a thickness of less than 150nm, preferably less than 50nm, and more preferably less than 25nm.

 According to one embodiment, the useful layer has a thickness of less than 50nm, preferably of less than
10 25nm.

 According to one embodiment, the surface of the impact point of the laser beam on the free surface of the useful layer is greater than 0.1mm^2 , preferably greater than 10mm^2 .

15 According to one embodiment, the pulsed laser beam has a pulse energy ranging from 100 to $1,500\text{mJ}/\text{cm}^2$, with such energy range making it possible to obtain a heating of the useful layer compatible with a chemical reaction of the species with the useful layer.

20 According to one embodiment, the pulsed laser beam has a pulse repetition frequency ranging from 1Hz to 10kHz.

 According to one embodiment, the useful layer has a variation in thickness of less than 3nm, preferably
25 of less than 2nm, even more preferably of less than 1nm.

BRIEF DESCRIPTION OF THE DRAWINGS

Other characteristics and advantages will emerge from the description which follows of two embodiments of a method for processing a structure according to the invention, given as non restrictive examples, with
5 reference to the appended drawings wherein:

- Figure 1 is a sectional view of a structure treated by a treatment process according to the known techniques of the prior art,

- Figure 2 schematically illustrates a reaction
10 chamber for processing a structure according to the known techniques of the prior art,

- Figure 3 is a sectional view of a structure treated by a treatment process according to the invention,

- Figure 4 schematically illustrates a reaction
15 chamber for processing a structure according to the invention,

- Figure 5 schematically illustrates the reflections occurring in two layers of a structure,

- Figure 6 shows the curves of the sensitivity of
20 the estimated reflectivity for a plurality of silicon-on-insulator structures, versus the wavelength, relative to the thin silicon layer (Si1 and Si2 curves) and relative to the buried oxide layer (BOX1 and BOX2
25 curves).

- Figure 7 shows the temperature rise generated respectively by a pulsed laser on a silicon on insulator structure comprising a 25nm buried silicon

oxide layer, a 12nm, and respectively 13nm silicon layer in another area of the structure,

- Figure 8 is a block diagram of the heating of an area of the useful layer having a variation in thickness in a range scale smaller than the size of the pulsed laser beam.

- Figure 9 illustrates the B heating mode wherein the intensity of the reflected radiation decreases as the thickness of the useful layer increases.

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DETAILED DESCRIPTION OF THE EMBODIMENTS OF THE INVENTION

In the various embodiments, the same references are used for elements which are identical or perform the same function for the sake of simplifying the description.

According to the treatment process illustrated in Figures 3 and 4, the structure 1, comprising from its rear side to its front side a carrier substrate 4, an insulating layer 3, and a useful layer 2 having a free surface S, is positioned in an atmosphere comprising chemical species 6 in a gaseous form which are likely to chemically react with the useful layer 2 with kinetics strictly increasing with the temperature of the useful layer 2. The active layer 2 is heated by a pulsed laser beam 8, with the beam 8 sweeping at least in part the free surface S of the useful layer 2.

The heating obtained in a complex multilayer structure such as the structure 1, is dependent on the

way the radiation of the laser beam is reflected on the various interfaces of the structure. As is well known, such reflectivity depends on the the nature and the thickness of the layers, on the polarization of the laser, on the angle of incidence and on the wavelength thereof. For a given structure and given conditions of application of the laser, i.e. when the nature of the layers, the polarization, the angle of incidence and the wavelength of the laser are set, the heating of the useful layer 2 obtained at two distinct points of application of the laser will differ according to the variations in thickness of each layer 2 and 3 between these two points. Accordingly, and all other things being equal, the heating profile of the free surface of the useful layer 2 reflects the non-uniformity in the thickness of the useful layer 2 and of the insulating layer 3.

The invention tries to position the structure under processing conditions such that the heating profile of the free surface of the useful layer 2 obtained during the sweeping by the laser only depends on the variations in thickness of the useful layer 2 and remains insensitive to the variations in thickness of the insulating layer 3.

For this purpose, the wavelength of the laser beam 8 is so selected as to be different by less than 15nm, preferably by less than 7nm, from a central wavelength, for which the sensitivity of the estimated reflectivity of the structure 1 relative to the insulating layer 3 is zero.

The value of the central wavelength is determined by computing, on the basis of a reflectivity model of the structure 1; i.e. a mathematical model of a structure having the nominal characteristics of the structure 1. The laser wavelength is selected, within the above range, according to the availability of laser having a beam wavelength close to the central wavelength.

The invention takes advantage of the thus determined processing conditions to reduce the variations in thickness of the useful layer 2.

Using a pulse laser beam 8, rather than a continuous laser, makes it possible to limit the heating at the beam 8 impact point P (shown in Figure 4) on the useful layer 2 and the underlying volume thereof. A pulsed laser beam sweeping the free surface S of the useful layer 2 individually heats the various impact points of the useful layer 2. And according to the invention, the heating of each point of impact of the useful layer 2 depends on the thickness of the useful layer 2 at said point of impact P and on the duration of the laser pulse.

The invention can more particularly be applied to structures of the silicon on insulator type. The insulating layer 3 may then comprise silicon dioxide. The insulating layer 3 may have a thickness of less than 150nm, preferably of less than 50nm, more preferably of less than 25nm. The silicon useful layer 2 may have a thickness of less than 50nm, preferably of less than 25nm. Advantageously, the useful layer 2 may

have, prior to the treatment, a variation in thickness of less than 3nm, preferably of less than 2nm, even more preferably of less than 1nm.

5 **Determining the estimated reflectivity of a structure**

- Figure 5 schematically illustrates the reflections occurring in the useful layer 2 and the insulating layer 3 of a structure 1 (the carrier
10 substrate 4 is not shown).

A radius E_0^+ incident on the free surface S is partially reflected on said surface and partially transmitted through the useful layer 2.

The part of the transmitted beam is in turn
15 partly reflected at the interface between the useful layer 2 and the insulating layer 3, and partly transmitted through the insulating layer 3. And such reflections/transmissions are repeated at each one of the interfaces of the structure, the reflected energy E^-
20 $_0$ thus results from these complex interactions.

The reflectivity of a structure corresponds to the ratio between the reflected energy E^-_0 and the incident energy E^+_0 .

As is well known per se, the reflectivity of a
25 stack, such as the one formed by the structure 1, is determined by applying Fresnel equations, and depends on several parameters including the thickness of each layer, the polarization of the incident light flux, the angle of incidence and the wavelength of the luminous

flux. In this regard, reference can be made to Appendix C of the book "Spectroscopic Ellipsometry and reflectometry, a user guide" by H.G. Tompkins and W.A. McGahan, published by Wiley Interscience Publication,
5 1999.

Operationally, for nominal parameters of a structure and of a luminous flux, the reflectivity is determined by widely available digital simulation software. The so-called IMD software, available for
10 download at <http://www.rxollc.com/idl/> and described in the publication "IMD-Software for modeling the optical properties of multilayer films", by D.L. Windt, COMPUTER IN PHYSICS, VOL12, No. 4, JUL/AUG 1998.

The model established by such software makes it
15 possible to obtain an estimated reflectivity of a real structure.

Using simulation, the estimated reflectivity of a structure, for a series of values of the wavelength of the incident ray, can thus be represented as a digital
20 table or graphically, with the other parameters of the model being set at their nominal values.

Determining the sensitivity of the estimated reflectivity

25 The sensitivity of the estimated reflectivity of the structure 1 relative to the insulating layer 3 (respectively the useful layer 2) corresponds to the partial derivative of the reflectivity relative to the

thickness of the insulating layer 3 (respectively the useful layer 2).

In practice, such step of derivation is performed using digital derivation algorithms, well known per se, such as, for instance, the differential quotient method. Such algorithms may belong to the tools offered in digital simulation software making it possible to determine the reflectivity of the structure, or may be available in separate software.

For example, the sensitivity of the estimated reflectivity of the structure 1 relative to the useful layer 2 can be calculated, on the basis of the established model, by taking the difference between the estimated reflectivity of the structure 1 for two different thicknesses of the useful layer 2, with the difference between such two thicknesses being 0.1nm, for example, and the other parameters of the model remaining set at their nominal values.

Similarly, for the same structure 1, the sensitivity of the reflectivity of the structure 1 relative to the insulating layer 3 is calculated on the basis of the established model by taking the difference between the estimated reflectivity of the structure 1 for two different thicknesses of the insulating layer 3, with the difference between these two thicknesses being for instance 0.1nm.

Thus, Figure 6 graphically shows the sensitivity of the estimated reflectivity (noted SR, expressed as $\text{\AA}^{-1}$) of a plurality of silicon on silicon dioxide

structures 1 as a function of the λ wavelength with a calculated non polarized light having a normal incidence.

5 In this Figure 6, the Si1 curve represents the sensitivity of the estimated reflectivity relative to the useful layer versus the laser wavelength, in the case of a structure having a nominal thickness of the silicon useful layer 2 of 12nm and a nominal thickness of the silicon oxide insulating layer 3 of 25nm.

10 The Si2 curve represents the sensitivity of the estimated reflectivity relative to the useful layer versus the laser wavelength, in the case of a structure having a nominal thickness of the silicon useful layer 2 of 13nm and a nominal thickness of the silicon oxide
15 insulating layer 3 of 25nm.

The BOX1 curve represents the sensitivity of the estimated reflectivity relative to the insulating layer versus the laser wavelength, in the case of a structure having a nominal thickness of the silicon useful layer
20 2 of 12nm and a nominal thickness of the silicon oxide insulating layer 3 of 25nm.

The BOX2 curve represents the sensitivity of the estimated reflectivity relative to the insulating layer versus the laser wavelength, in the case of a structure
25 having a nominal thickness of the silicon useful layer 2 of 12nm and a nominal thickness of the silicon oxide insulating layer 3 of 26nm.

Selection of the pulsed laser beam wavelength

The wavelength of the central pulse laser is the wavelength, noted λ_0 , which cancels the sensitivity of the estimated reflectivity of a structure 1 relative to the insulating layer 3.

5 For wavelengths of the pulsed laser close to the central wavelength λ_0 , the applicant has confirmed that the useful layer 2 is heated substantially independently of the variations in thickness of the insulating layer 3.

10 "Wavelengths" close to the central wavelength means wavelengths ranging from $\lambda_0-15\text{nm}$ to $\lambda_0+15\text{nm}$, even more preferably ranging from $\lambda_0-7\text{nm}$ to $\lambda_0+7\text{nm}$.

In some cases, the wavelength of the pulsed laser may be so selected that the thinner the useful layer 2,
15 the higher the temperature reached by the useful layer 2. This result is obtained when the sensitivity of the estimated reflectivity of the structure 1 given relative to the useful layer 2 is positive.

These two conditions relating to the wavelength
20 of the luminous flux are noted heating mode A, as shown in Figure 6.

According to the heating mode A, the intensity of the reflected radiation increases as the thickness of the active layer increases. Therefore, the heating is
25 less important when the thickness of the useful layer 2 increases. Besides, as the sensitivity of the estimated reflectivity relative to the insulating layer 3 is close to 0, the heating is substantially

independent of the variations in thickness of the insulating layer.

In other cases, the wavelength of the pulsed laser may be so selected that the thicker the useful layer 2, the higher the temperature reached by the useful layer 2. This result is obtained when the sensitivity of the estimated reflectivity of the structure 1 given relative to the useful layer 2 is negative.

These two conditions relating to the wavelength of the luminous flux are noted heating mode B, and are illustrated in Figure 9, wherein the BOX3 curve shows the sensitivity of the estimated reflectivity of a structure relative to the insulating layer versus the wavelength of the laser; and the Si3 curve shows the sensitivity of the estimated reflectivity of the structure relative to the useful layer versus the wavelength of the laser.

According to the heating mode B, the intensity of the reflected radiation decreases as the thickness of the useful layer increases. Therefore, the heating is greater when the thickness of the useful layer 2 increases. Besides, as the sensitivity of the estimated reflectivity relative to the insulating layer 3 is close to 0, the heating is substantially independent of the variations in thickness of the insulating layer.

It should be noted that λ_0 is determined on the basis of a model with the nominal thickness parameters

of the structure 1. During the treatment according to the invention of a real structure, such structure can have parameters, and specifically thickness, which vary from the model. This is particularly true when the treatment comprises a thickening or a thinning of the active layer 2 of the structure. If they remain reasonable (of the order of 1nm), such discrepancies do not question the validity of the model, i.e. the ability to selectively heat a useful layer 2 according to its variation in thickness only. This is remarkable for example in Figure 6 by noting that the BOX1 and BOX2, respectively Si1 and Si2, curves of the sensitivity of the estimated reflectivity of the structures remain similar in spite of a variation in the thickness of the insulating layer 3, respectively of the useful layer 2, of 1nm.

By way of illustration, a structure 1 made of silicon-on-insulator shall be considered, which comprises a layer of silicon dioxide having a nominal thickness of 25nm, and a silicon layer having a nominal thickness of 12nm.

According to Figure 6 (BOX1 curve), the energy of a laser beam 8 having a wavelength equal to 510nm corresponds to a heating mode A.

The structure 1 is then irradiated with a pulsed laser having the following characteristics:

- a wavelength of 510nm;
- pulses of 10ns;
- a repetition frequency of the pulses of 10kHz;

- pulse energy of 500mJ/cm².

As shown in Figure 7, the temperature reached by the silicon layer is 1,000°C for a 12nm layer (i.e. corresponding to the nominal thickness of the structure 1), while it is only 950°C for a 13nm layer (i.e. varying by 1nm from the nominal thickness of the structure 1).

The thinner areas of the silicon layer are heated to higher temperatures than the thicker areas.

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Determination of the duration of the laser pulse.

The heating of the useful layer 2 generated by the pulsed laser diffuses over a distance d according to the law:

$$d = \sqrt{Dt}$$

15

where t is the duration of a laser pulse, D is the thermal diffusion coefficient of the material composing the useful layer, and d the distance travelled by the heat diffusion front.

If not controlled, such diffusion effect thus does not make it possible to selectively heat nearby areas, for example areas included in the impact point of the laser beam.

When non-uniformities in thickness of relatively small wavelengths, in particular smaller than the size of the impact point of the beam are desired to be corrected anyway, the diffusion of heat has to be

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controlled. This is achieved by choosing the duration t of a pulse of the laser.

More specifically, if variations in thickness of the useful layer in its spectral components having a wavelength greater than a threshold I (I being possibly smaller than the dimension of the beam) are desired to be corrected, a duration of laser pulse smaller than t_v is selected, where t_v is defined by the following law:

$$t_v = \frac{l^2}{D}$$

Thus, for pulse durations t smaller than t_v , a thermal equilibrium may not be reached over the entire surface of the impact point of the laser pulses on the useful layer 2, and the impact point does not undergo a uniform heating over its entire surface.

More specifically, the thinner areas of the impact point are not heated to the same temperature as the thickest areas of the impact point.

As an exemplary application, the case of the SOI (silicon on insulator) structure 1 which has non-through holes will be considered. Such holes contribute to the variations in the thickness of the useful layer 2, and such variations can be modeled, for example as a spatial wave having a 1 micrometer wavelength.

"Non-through holes" means holes that do not extend through the entire thickness of the useful layer 2.

The thermal diffusion coefficient of silicon is equal to $87 \text{ micrometer}^2/\text{sec}$. t_v is then equal to 11.5ns, when applying the previous formula and taking $I=1 \text{ micrometer}$ as the threshold value.

5 As illustrated in Figure 8, a structure 1 has a region S1 which is thicker than a region S2 which thus forms a non-through hole. The regions S1 and S2 are irradiated with a pulsed laser beam 8, the point of impact of which has a size of several mm^2 , i.e. much
10 greater than the dimension S2. The wavelength of the laser corresponds to the conditions of the heating mode A, and the duration of the pulse is chosen to be equal to 10ns, i.e. smaller than t_v .

As the thermal equilibrium over the entire
15 surface of the impact point is not reached for pulses having a duration smaller than t_v , a more important heating can be noted in the area S2 than in the area S1. Such selective heating enables the reduction of the thickness variation when thickening the useful
20 layer 2. For conditions according to a heating mode B, the opposite effect will be noted and a thickness correction by etching the useful layer 2 will thus be applied.

Particularly advantageously, the heating modes A
25 and B are carried out with a pulse laser having at least one of the following characteristics:

- The impact point P of the pulse laser beam 8 can have a surface greater than 0.1mm^2 , preferably greater than 10mm^2 .

- Pulse duration smaller than 100ns, preferably smaller than 50ns, for instance 10ns.
- Pulse energy ranging from 100 to 1,500mJ/cm²
- A pulse repetition frequency ranging from 1Hz
5 to 10kHz.

First embodiment.

In a first embodiment, illustrated in Figures 3 and 4, thickening by epitaxy the useful layer 2 of a
10 structure 1 consisting of a silicon on insulator substrate has been considered.

The insulating layer 3 is a 25nm layer of silicon dioxide.

The useful layer 2 is a 12nm layer of silicon on
15 an average and has a thickness variation ranging from 11.5nm to 12.5nm.

A preliminary step of modeling the structure leads to determining the sensitivities of the reflectivity of the structure 1 relative to the silicon
20 layer (SOI1 curve in Figure 6) and the silicon dioxide layer (BOX1 curve in Figure 6) respectively.

The dotted rectangle appearing in the graph of Figure 6 shows a range of wavelengths suitable for a heating mode A. In the case of this example, a laser
25 having a 51nm wavelength has been selected.

The structure 1 is thus preferably installed on a structure support 5 in a reaction chamber 9.

Chemical species 6 in a gaseous form are introduced into the reaction chamber 9, with the chemical species 6 being capable of chemically reacting with the useful layer 2, with kinetics strictly increasing with the temperature of the useful layer 2.

Particularly advantageously, the chemical species 6 introduced into the reaction chamber may include at least one of the following species: silane, disilane, trisilane, monochlorosilane, dichlorosilane, trichlorosilane, tetrachlorosilane, germane, monochlorogermane, dichlorogermane, trichlorogermane, tetrachlorogermane.

The chemical species 6 injected into the reaction chamber are generally diluted in a carrier gas comprising at least one of the following gases: Nitrogen, Argon, Dihydrogen.

The useful layer 2 is then heated by a pulsed laser beam 8, with the beam 8 sweeping at least partially the free surface S of the useful layer 2.

A window transparent to the pulse laser beam 8 is provided in the enclosure, so as to enable the pulsed laser beam 8 generated outside the reactive chamber to produce a heating of the useful layer 2 positioned inside the reactive enclosure.

The free surface S of the useful layer 2 is then swept by moving the pulsed laser beam 8 and/or by moving the support 5 whereon the structure 1 is laid.

The useful layer 2 is thus heated of at the point of impact P, upon the pulsed laser beam 8 impacting the free surface S of the useful layer 2.

Thus, when the pulsed laser beam 8 sweeps the
5 surface, the heating is more important in the thinner areas of the active layer 2 than in the thicker areas, regardless of the variations in thickness of the insulating layer 3.

Such heating causes the reaction of the chemical
10 species 6 with the useful layer 2.

In this embodiment, the chemical reaction is a reaction of thickening by epitaxy of the useful layer 2.

As the thinner areas of the useful layer 2 are
15 exposed to a more important heating than the thick areas, the reaction of thickening by epitaxy takes place at a higher speed in the thin areas than in the thick areas.

When the useful layer 2 is thickened, the
20 difference in thickness between the thin areas and the thick areas of the useful layer 2 thus decreases.

Thus, the structure 1 is irradiated with a pulsed laser having a wavelength of 510nm, with 10ns pulses, with the pulses being repeated at a frequency of 10kHz, and each pulse having an energy of 500mJ/cm² makes it
25 possible to heat the silicon layer. The treatment time is 10 seconds per irradiated area. The laser beam impact point is 10mm².

During the irradiation, the structure 1 is in an atmosphere of chemical species 6 comprising a mixture of dichlorosilane and dihydrogen, under a pressure of 80mT.

5 Such treatment executed on the whole structure 1 makes it possible to reduce the non-uniformity in thickness to 0.2nm relative to an initial non-uniformity of 1nm. Such non-uniformity corresponds to variations in thickness of the useful layer 2 with a
10 spatial wavelength above the 0.9 micrometer threshold I.

Besides, for 10ns pulses, it is possible to reduce the variations in thickness of the useful layer 2 with a wavelength above the threshold of the order of
15 1 micron, which is much smaller than the dimension of the beam impact point.

Second embodiment.

In a second embodiment, a thinning by etching a
20 useful layer 2 has been considered.

A structure 1, the sensitivity curves of which are shown in Figure 9, is thus preferably installed on a support structure 5 in a reaction chamber 9.

25 Chemical species 6 in a gaseous form are introduced into the reaction chamber 9, with the chemical species 6 being likely to chemically react to etch the useful layer 2, with kinetics strictly increasing with the temperature of the useful layer 2.

Particularly advantageously, the chemical species 6 introduced into the reaction chamber comprise at least one of the following species: HCL.

The chemical species 6 injected into the reaction
5 chamber are generally diluted in a carrier gas comprising at least one of the following gases: Argon, Dihydrogen.

The useful layer 2 is then heated using a pulsed laser beam 8, with the beam 8 sweeping at least
10 partially the free surface S of the useful layer 2. A window transparent to the pulsed laser beam 8 is provided in the enclosure, so as to enable the pulsed laser beam 8 generated outside the reactive chamber to heat the useful layer 2 positioned inside the reactive
15 chamber.

The free surface S of the useful layer 2 is then swept by moving the pulse laser beam 8 and/or by moving the structure 1.

The wavelength of the laser beam 8 is so selected
20 as to meet both conditions of a heating mode B shown in Figure 9, for example the wavelength thereof is so selected as to be different by less than 15nm, preferably less than 7nm, from the central wavelength of 350nm. The other laser parameters are the same as
25 those selected in the first embodiment.

Thus, when the pulsed laser beam 8 impacts the free surface S of the useful layer 2, the useful layer 2 is heated at the point of impact.

Moreover, when the pulsed laser beam 8 sweeps the free surface S of the useful layer 2, the heating is more important in the thicker areas of the active layer 2 than in the thinner areas.

5 Such heating causes the reaction of the chemical species 6 with the useful layer 2.

In this embodiment, the chemical reaction is a reaction of thinning by etching the useful layer 2.

As the thicker areas of the useful layer 2
10 undergo a more important heating than the thinner areas, the reaction of thinning by etching proceeds at a higher speed in the thick areas than in the thin areas.

The difference in thickness between the thin
15 areas and the thick areas of the useful layer 2 thus decreases when the reaction of thinning by etching the useful layer 2 takes place.

During the irradiation, the structure 1 is in an atmosphere of chemical species 6 comprising a mixture
20 of hydrochloric acid and of dihydrogen under a pressure ranging from 2.67Pa to $1 \cdot 10^5$ Pa (20mTorr and 760Torr).

Such treatment executed on the whole structure 1 makes it possible to reduce the non-uniformity in thickness relative to an initial non-uniformity of the
25 useful layer 2. Such non-uniformity corresponds to variations in thickness of the useful layer 2 having a spatial wavelength above the 0.9 micrometer threshold I.

CLAIMS

1. A method for treating a structure (1), the structure (1) comprising, from its rear side to its front side a carrier substrate (4), an insulating layer (3), and a useful layer (2), the useful layer (2) having a free surface (S), the structure (1) being placed in an atmosphere containing chemical species (6) in a gaseous form, with the chemical species (6) being likely to chemically react with the useful layer (2) with kinetics strictly increasing with the temperature of the useful layer (2); with said treatment process being characterized in that the useful layer (2) is heated by a pulsed laser beam (8), with the beam (8) sweeping at least partially the free surface (S) of the useful layer (2), with the wavelength of the beam (8) being different by less than 15nm, preferably by less than 7nm, from a central wavelength, for which the sensitivity of the estimated reflectivity of the structure (1) relative to the insulating layer (3) is zero.

2. A treatment process according to claim 1, wherein the duration of the pulses of the laser beam is less than a t_v value, with t_v being equal to l^2/D , with D being the coefficient of thermal diffusion in the useful layer (2), and l corresponding to a treatment threshold wavelength.

3. A treatment process according to claim 1, wherein the pulsed laser beam (8) has a pulse duration of less than 100ns.

4. A treatment process according to one of claims
5 1 to 3, wherein the useful layer (2) is a layer of a semiconductor material comprising at least one of the following materials: silicon, germanium, silicon germanium alloy.

5. A treatment process according to one of claims
10 1 to 4, wherein the chemical species (6) make it possible to etch the useful layer (2), the wavelength of the pulsed laser beam (8) is so selected as to correspond to a negative value of the sensitivity of the estimated reflectivity of the structure (1)
15 relative to the useful layer (2).

6. A treatment process according to claim 5, wherein the chemical species (6) comprise HCl.

7. A treatment process according to one of claims
1 to 4, wherein the chemical species (6) make it
20 possible to thicken the useful layer (2) by epitaxy, and the wavelength of the pulsed laser beam (8) is so selected as to correspond to a positive value of the sensitivity of the estimated reflectivity of the structure (1) relative to the useful layer (2).

25 8. A treatment process according to claim 7, wherein the chemical species (6) comprise at least one of the following species: silane, disilane, trisilane, monochlorosilane, dichlorosilane, trichlorosilane,

tetrachlorosilane germane, monochlorogermane,
dichlorogermane, trichlorogermane, tétrachlorogermane.

9. A treatment process according to one of
claims 1 to 8, wherein the insulating layer (3)
5 comprises silicon dioxide.

10. A treatment process according to one of claims
1 to 9, wherein the insulating layer (3) has a
thickness of less than 150nm, preferably less than
50nm, and more preferably less than 25nm.

10 11. A treatment process according to one of claims
1 to 10, wherein the useful layer (2) has a thickness
of less than 50nm, preferably less than 25nm.

12. A treatment process according to one of claims
1 to 11, wherein the surface of the impact point (P) of
15 the laser beam on the free surface (S) of the useful
layer (2) is greater than 0.1mm^2 , preferably greater
than 10mm^2 .

13. A treatment process according to one of claims
1 to 12, wherein the pulsed laser beam (8) has a pulse
20 energy ranging from 100 to $1,500\text{mJ/cm}^2$.

14. A treatment process according to one of claims
1 to 13, wherein the pulsed laser beam (8) has a pulse
repetition frequency ranging from 1Hz to 10kHz.

15. A treatment process according to one of claims
25 1 to 14, wherein the useful layer (2) has a variation
in thickness of less than 3nm, preferably of less than
2nm, and even more preferably of less than 1nm.