

PROCESSES OF CONTROLLING MOLECULAR WEIGHT DISTRIBUTION IN ETHYLENE/ALPHA-OLEFIN COMPOSITIONS

FIELD OF THE INVENTION

- 5 [0001] The present invention relates to compositions and processes of making ethylene/ α -olefin polymer compositions. More particularly, the invention relates to processes of producing ethylene/ α -olefin compositions having a controlled molecular weight distribution.

BACKGROUND AND SUMMARY OF THE INVENTION

- 10 [0002] It is desirable to produce ethylene/ α -olefin compositions of controlled molecular weight distribution in a cost-effective manner. In particular ethylene/ α -olefin compositions having a multi-modal (two or more modes wherein the case of two may interchangeably be referred to as bimodal or multi-modal) molecular weight composition distribution are often desirable for some applications, for example, pipes for natural gas, sewers, mining, etc.
- 15 Also, some applications may require compositions wherein a low molecular weight portion of said ethylene/ α -olefin interpolymer composition has a higher density than a high molecular weight portion of said ethylene/ α -olefin interpolymer composition. Unfortunately, to date the available processes do not effectively and efficiently control the distribution or result in compositions with the desired density and molecular weight
- 20 combinations.

- [0003] New processes have been discovered which result in effective control of molecular weight distribution. Advantageously, the inventive processes may be designed to result in compositions wherein a low molecular weight portion of said ethylene/ α -olefin interpolymer composition has a higher density than a high molecular weight portion of said
- 25 ethylene/ α -olefin interpolymer composition. Also, the ethylene/ α -olefin interpolymer composition may be produced in a single polymerization reactor and/or using a single catalyst. Novel compositions often may result from the aforementioned processes. Said novel compositions comprise an ethylene/ α -olefin interpolymer composition with a multi-modal molecular weight distribution and one or more molecules having a gram
- 30 molecular weight equal to about $((\text{the molecular weight of an aryl or hydrocarbyl-ligand of a pre-catalyst}) + 28 + 14 * X)$, wherein X represents an integer from zero to 10, preferably zero to 8.

BRIEF DESCRIPTION OF THE DRAWINGS

[0004] Figures 1-14 are a series of slides explaining multi-site behavior in copolymerizations.

[0005] Figures 15-19 are differential calorimetry scans (DSC) for polymer made from Examples 4, 6, 12, 14 and 15, respectively.

[0006] Figure 20 depicts molecular weight distributions of ethylene-octene copolymers.

[0007] Figure 21 depicts the effect of octene mole fraction on the fraction of high molecular weight polymer.

DETAILED DESCRIPTION OF THE INVENTION**General Definitions**

[0008] If and when employed herein the following terms shall have the given meaning for the purposes of this invention:

[0009] "Polymer" means a polymeric compound prepared by polymerizing monomers, whether of the same or a different type. The generic term "polymer" embraces the terms "homopolymer," "copolymer," "terpolymer" as well as "interpolymer."

[0010] "Interpolymer" means a polymer prepared by the polymerization of at least two different types of monomers. The generic term "interpolymer" includes the term "copolymer" (which is usually employed to refer to a polymer prepared from two different monomers) as well as the term "terpolymer" (which is usually employed to refer to a polymer prepared from three different types of monomers). It also encompasses polymers made by polymerizing four or more types of monomers.

[0011] The term "multi-block copolymer" or "segmented copolymer" refers to a polymer comprising two or more chemically distinct regions or segments (referred to as "blocks") preferably joined in a linear manner, that is, a polymer comprising chemically differentiated units which are joined end-to-end with respect to polymerized ethylenic functionality, rather than in pendent or grafted fashion. In a preferred embodiment, the blocks differ in the amount or type of comonomer incorporated therein, the density, the amount of crystallinity, the crystallite size attributable to a polymer of such composition, the type or degree of tacticity (isotactic or syndiotactic), regio-regularity or regio-irregularity, the amount of branching, including long chain branching or hyper-branching, the homogeneity, or any other chemical or physical property. The multi-block copolymers are

characterized by unique distributions of both polydispersity index (PDI or Mw/Mn), block length distribution, and/or block number distribution due to the unique process making of the copolymers. More specifically, when produced in a continuous process, the multi-block polymers often possess PDI from 1.7 to 2.9, preferably from 1.8 to 2.5, more preferably from 1.8 to 2.2, and most preferably from 1.8 to 2.1.

[0012] In the following description, all numbers disclosed herein are approximate values, regardless whether the word “about” or “approximate” is used in connection therewith. They may vary by 1 percent, 2 percent, 5 percent, or, sometimes, 10 to 20 percent. Whenever a numerical range with a lower limit, R^L and an upper limit, R^U , is disclosed, any number falling within the range is specifically disclosed. In particular, the following numbers within the range are specifically disclosed: $R=R^L+k*(R^U-R^L)$, wherein k is a variable ranging from 1 percent to 100 percent with a 1 percent increment, i.e., k is 1 percent, 2 percent, 3 percent, 4 percent, 5 percent,..., 50 percent, 51 percent, 52 percent,..., 95 percent, 96 percent, 97 percent, 98 percent, 99 percent, or 100 percent. Moreover, any numerical range defined by two R numbers as defined in the above is also specifically disclosed.

[0013] “Density” is tested in accordance with ASTM D792.

[0014] “Melt Index (I_2)” is determined according to ASTM D1238 using a weight of 2.16 kg at 190°C for polymers comprising ethylene as the major component in the polymer.

[0015] “Melt Flow Rate (MFR)” is determined for according to ASTM D1238 using a weight of 2.16 kg at 230°C for polymers comprising propylene as the major component in the polymer.

[0016] “Molecular weight distribution” or MWD is measured by conventional GPC per the procedure described by Williams, T.; Ward, I. M. *Journal of Polymer Science, Polymer Letters Edition* (1968), 6(9), 621-624. Coefficient B is 1. Coefficient A is 0.4316.

Controlling Molecular Weight and Density

[0017] It has been discovered that the molecular weight distribution of a resulting polymer may be controlled. For example, using the proper reaction conditions (e.g., a well mixed homogeneous reaction environment, a steady-state concentration of two or more monomers such as ethylene and an α -olefin like octene, and a proper pre-catalyst or catalyst) the bimodal molecular weight “split” of the polymer may be controlled by the

mole fractions (f) of the two or more monomers, n , such that the mole fraction of monomer m is defined as:

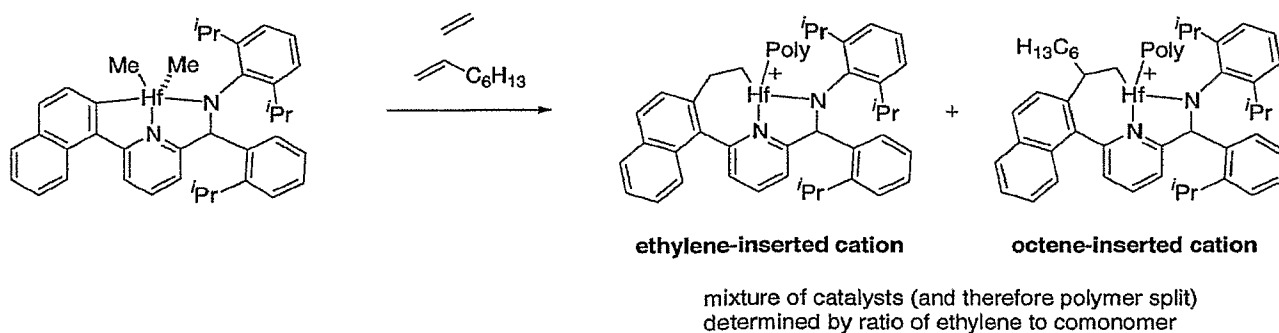
$$f_m = \frac{[Monomer_m]}{\sum_{i=1}^n [Monomer_i]}$$

[0018] That is, the molecular weight split can be controlled so that it is basically a function of the relative monomer concentrations in solution. These same relative monomer concentrations also, depending upon the reaction conditions, may determine the overall composition (i.e. density) of the total polymer.

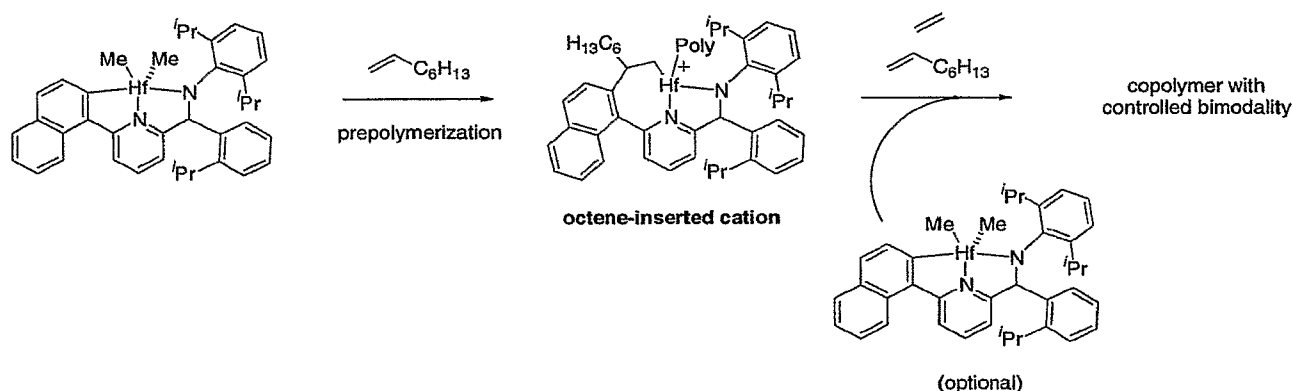
[0019] One aspect of controlling monomer purity useful herein is by utilizing a side stream of monomer in contact with a selected catalyst in a plug flow reactor. If the monomer is impure, then a lower than expected exotherm will be observed in the plug flow reactor. In this manner, monomer purity is monitored and adjusted if necessary.

[0020] While not wishing to be bound by any theory the Applicants have discovered that the reason that the monomer concentration:molecular weight split relationship can be made to occur is that a different catalyst species can be made from each monomer reactant. This means that a lower molecular weight polymer is formed by an "ethylene-inserted" form of the catalyst, while an " α -olefin-inserted" form of the catalyst gives a higher molecular weight polymer. Advantageously, this results in a molecular weight split which is controlled by controlling the relative amounts of the various catalyst species that are formed.

[0021] As an example it is believed that the Hafnium catalyst below can be made to form an ethylene-inserted cation and an octene-inserted cation in the presence of ethylene and octene and the proper reaction conditions including, for example, a well mixed homogeneous reaction environment.



[0022] Therefore, the present invention allows one to control the molecular weight split in numerous ways. One method of the present invention involves changing the ligand structure of a given catalyst to affect the resulting split for a given overall density copolymer. Thus, one may select suitable pre-catalyst(s) for the polymerization to control the concentrations of an ethylene-inserted cation and/or an octene-inserted cation and thereby control the resulting molecular weight split. Alternatively, the present invention allows one to control the polymer split from a given catalyst precursor. For example, one such method would be to do a pre-reaction or pre-polymerization of sorts, e.g., contacting a pre-catalyst with a single monomer to generate the desired catalyst species concentrations, then feeding part or all of this pre-reaction product to the reactor. This could optionally be done with the addition of pure pre-catalyst, providing a high degree of control over the resulting polymer bimodality.



[0023] In yet another alternative of the present invention, the polymer split can be modified by changing process variables. For example, one can control the amount of inserted catalyst by controlling composition gradients -- especially in instances when the insertion occurs in the early stages of catalyst activation. In a solution loop reactor, for example, a gradient of monomer composition can be achieved by modifying the speed at which the reactor effluent circulates through the reactor. This can result in differences in the comonomer mole fraction at different places within the reactor. The reactor can be configured to take advantage of this by strategic placement of catalyst and monomer injection points and/or the timing of said catalyst and monomer contact.

[0024] In yet another alternative, one or more compounds can be synthesized directly so that the desired ratio of ethylene-inserted cation: α -olefin-inserted cation can be directly controlled.

General Processes of Using a Pre-Catalyst to Control Molecular Weight

[0025] As stated above, the Applicants have discovered a number of ways to control the molecular weight distribution in the production of an ethylene/ α -olefin interpolymers composition. One process comprises:

- (a) selecting at least one suitable pre-catalyst comprising at least one metal-aryl or metal-hydrocarbyl bond, wherein each pre-catalyst molecule is essentially the same as every other pre-catalyst molecule;
- (b) contacting ethylene, at least one α -olefin, and said suitable pre-catalyst;
- (c) selecting ethylene: α -olefin concentration ratios sufficient to activate the pre-catalyst, and
- (d) forming an ethylene/ α -olefin interpolymers composition under continuous reaction polymerization conditions; and, optionally,
- (e) selecting a molecular weight split of the interpolymers as determined by the mole fractions (f) of the two or more monomers, n , such that the mole fraction of monomer m is defined as:

$$f_m = \frac{[Monomer_m]}{\sum_{i=1}^n [Monomer_i]}$$

to produce an ethylene/ α -olefin interpolymers composition with a controlled bimodal or multi-modal molecular weight distribution.

[0026] Another process comprises:

- (a) selecting at least one suitable pre-catalyst comprising at least one metal-aryl or metal-hydrocarbyl bond, wherein each pre-catalyst molecule is essentially the same as every other pre-catalyst molecule;
- (b) contacting at least one organic compound, and said suitable pre-catalyst;
- (c) selecting at least one organic compound concentration sufficient to activate the pre-catalyst, and
- (d) forming an ethylene/ α -olefin interpolymers composition under continuous reaction polymerization conditions; and, optionally,
- (e) selecting a molecular weight split of the interpolymers as determined by the concentration of the one or more organic compound(s) to produce an ethylene/ α -

olefin interpolymers with a controlled bimodal or multi-modal molecular weight distribution.

Suitable Pre-catalyst Contact With (1) Ethylene and an α -olefin or (2) Organic Compound

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[0027] The suitable pre-catalysts may be selected from any of those comprising at least one metal-aryl or metal-hydrocarbyl bond. The aryl may be any molecule or ligand which has the ring structure characteristic of, for example, phenyl, naphalenyl, phenanthrenyl, anthracenyl, etc. The hydrocarbyl may be any molecule or ligand comprising hydrogen and carbon such as benzyl. Additionally, a heteroatom such as nitrogen, oxygen, etc. may be substituted for one or more carbon atoms of the aryl or hydrocarbyl such that aryl includes heteroaryl and hydrocarbyl includes heterohydrocarbyl. Similarly, one or more hydrogens on the aryl or hydrocarbyl may be replaced with any substituent which does not substantially interfere with the desired activity of the pre-catalyst. Such substituents include, but are not limited to, substituted or unsubstituted alkyl, halo, nitro, amino, alkoxy, aryl, aliphatic, cycloaliphatic, hydroxy, and the like. Preferably each pre-catalyst molecule is essentially the same as every other pre-catalyst molecule. By this is meant that the chemical structures of the molecules are substantially the same. Also preferable are those structures in which ring strain is capable of being relieved from the metal-hydrocarbyl ligand when contacted with ethylene or an α -olefin.

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[0028] Particularly suitable pre-catalysts are selected from the group consisting of hydrocarbylamine substituted heteroaryl compounds corresponding to the formula:



wherein:

25

R^{11} is selected from alkyl, cycloalkyl, heteroalkyl, cycloheteroalkyl, aryl, and inertly substituted derivatives thereof containing from 1 to 30 atoms not counting hydrogen or a divalent derivative thereof;

T^1 is a divalent bridging group of from 1 to 41 atoms other than hydrogen, preferably 1 to 20 atoms other than hydrogen, and most preferably a mono- or di- C_{1-20} hydrocarbyl substituted methylene or silane group; and

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R^{12} is a C_{5-20} heteroaryl group containing Lewis base functionality, especially a pyridin-2-yl- or substituted pyridin-2-yl group or a divalent derivative thereof;

M^1 comprises hafnium or other Group 4 metal;

X^1 is an anionic, neutral or dianionic ligand group;

5 x' is a number from 0 to 5 indicating the number of such X^1 groups; and

bonds, optional bonds and electron donative interactions are represented by lines, dotted lines and arrows respectively, or a mixture thereof, in contact with a suitable co-catalyst.

[0029] The pre-catalyst and optional catalysts if desired are contacted with either (1) ethylene and an α -olefin or (2) an organic compound such as, for example, acetone or a
 10 mixture of ketones or (3) mixtures thereof, in a manner and in amounts sufficient to activate the pre-catalyst. One skilled in the art will recognize that a cocatalyst such as the ones described below may be useful at this stage or a later stage. The conditions will generally vary depending upon the polymer desired and the equipment employed. However, one skilled in the art can readily determine the suitable conditions using the instant
 15 specification, background knowledge, the prior art, and routine experimentation. Guidance is given in, for example, U.S. Patent Nos. 6,960,635; 6,946,535; 6,943,215; 6,927,256; 6,919,407; and 6,906,160 which are incorporated herein by reference. One advantage of the instant processes is that a single catalyst may be employed in a single reactor.

[0030] The ethylene, α -olefin, and/or organic compound concentrations are typically
 20 selected so as to be sufficient to activate the pre-catalyst, and form the desired ethylene/ α -olefin interpolymer composition having the desired molecular weight distribution. These activation conditions vary depending on the reactants and equipment employed and may be the same but are preferably different than the continuous polymerization reaction conditions used to form the interpolymer. More specifically, the initial monomer ratio used during
 25 activation may be the same but is preferably different than the monomer ratio used during the interpolymer polymerization. While these ratios often vary according the reaction conditions and the product desired, the molecular weight split of the interpolymer may usually be controlled by selecting the mole fractions (f) of the two or more monomers, n , such that the mole fraction of monomer m is defined as:

$$f_m = \frac{[Monomer_m]}{\sum_{i=1}^n [Monomer_i]}$$

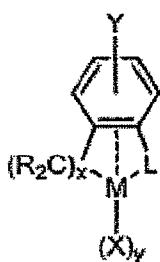
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[0031] Advantageously, the resulting polymer often has a low molecular weight portion that has a higher density than the high molecular weight portion. While batch or continuous polymerization reaction conditions may be employed, it is preferable to employ continuous polymerization reaction conditions during the formation of the interpolymer. However,

5 continuous polymerization reaction conditions can still be employed even if the pre-catalyst is activated separately from the main polymerization.

General Processes of Using a Synthesized Catalyst to Control Molecular Weight Distribution

10 [0032] Another process of controlling molecular weight comprises contacting ethylene, an α -olefin, and a suitable catalyst under reaction conditions sufficient to form an ethylene/ α -olefin interpolymer composition wherein the catalyst comprises a catalytic amount of a molecule having the structure:



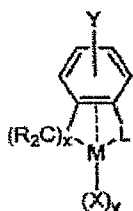
15 wherein M = group 2 - 8 metal, preferably group 4 as a neutral or charged moiety;
 Y = any substituent including fused rings;
 L = any ligating group, especially a pyridyl or pyridylamide;
 X = alkyl, aryl, substituted alkyl, H or hydride, halide, or other anionic moiety;
 y = an integer from 0 to the complete valence of M;
 20 R = alkyl, aryl, haloalkyl, haloaryl, hydrogen, etc;
 x = 1 - 6, especially 2;
 Dashed line = optional bond, especially a weak bond; and
 X and (CR₂)_x may be tethered or part of a ring.

25 [0033] Use of various forms of the aforementioned catalyst structure allows one skilled in the art to directly control the concentrations of an "ethylene-inserted" form of the catalyst and an " α -olefin-inserted" form of the catalyst. By directly controlling these concentrations the molecular weight split of the interpolymer may be controlled. This allows one skilled in the art to employ a much wider range of reaction conditions yet still control the molecular

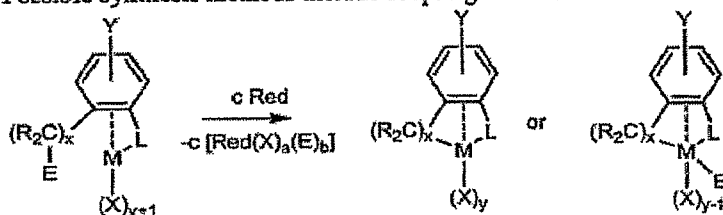
30 weight distribution. For example, it is then possible to control the molecular weight distribution over a wider range of monomer concentrations.

[0034] The above catalyst may be synthesized by any convenient method.

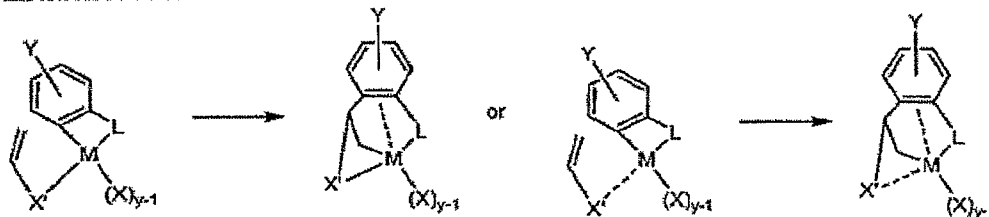
Catalyst Structures



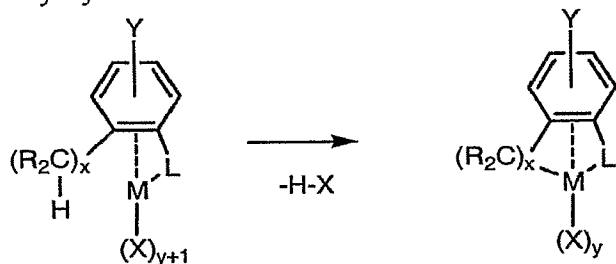
Possible synthesis methods include coupling such as



Insertion such as



or by cyclometalation such as



- 5 wherein M = group 2 - 8 metal, preferably group 4 as a neutral or charged moiety.
Y = any substituent including fused rings.
L = any ligating group, especially a pyridyl or pyridylamide.
X = alkyl, aryl, substituted alkyl, H or hydride, halide, or other anionic moiety.
y = number to complete valence of M.
- 10 R = alkyl, aryl, haloalkyl, haloaryl, hydrogen, etc.
x = 1 - 6, especially 2.
Dashed line = optional bond, especially a weak bond.
X and (CR₂)_x may be tethered or part of a ring.
E = any anionic moiety, (including alkyl or aryl) or H of a C-H unit
- 15 Red = reducing agent
a + b = number to complete the valence of Red when oxidized
c = number of equivalents of Red required to join (CR₂)_x to M

[0035] As one skilled in the art can appreciate it may also be desirable in some situations to use an *in-situ* synthesis method such that the catalyst is formed during the polymerization reaction.

Cocatalysts

5 [0036] As one skilled in the art will appreciate it may be useful to combine the pre-catalyst or synthesized catalyst with a suitable cocatalyst, preferably a cation forming cocatalyst, a strong Lewis acid, or a combination thereof. In a preferred embodiment, the shuttling agent, if employed, is employed both for purposes of chain shuttling and as the cocatalyst component of the catalyst composition.

10 [0037] The metal complexes desirably are rendered catalytically active by combination with a cation forming cocatalyst, such as those previously known in the art for use with Group 4 metal olefin polymerization complexes. Suitable cation forming cocatalysts for use herein include neutral Lewis acids, such as C₁₋₃₀ hydrocarbyl substituted Group 13 compounds, especially tri(hydrocarbyl)aluminum- or tri(hydrocarbyl)boron compounds and
15 halogenated (including perhalogenated) derivatives thereof, having from 1 to 10 carbons in each hydrocarbyl or halogenated hydrocarbyl group, more especially perfluorinated tri(aryl)boron compounds, and most especially tris(pentafluoro-phenyl)borane; nonpolymeric, compatible, noncoordinating, ion forming compounds (including the use of such compounds under oxidizing conditions), especially the use of ammonium-,
20 phosphonium-, oxonium-, carbonium-, silylium- or sulfonium- salts of compatible, noncoordinating anions, or ferrocenium-, lead- or silver salts of compatible, noncoordinating anions; and combinations of the foregoing cation forming cocatalysts and techniques. The foregoing activating cocatalysts and activating techniques have been previously taught with respect to different metal complexes for olefin polymerizations in the
25 following references: EP-A-277,003, US-A-5,153,157, US-A-5,064,802, US-A-5,321,106, US-A-5,721,185, US-A-5,350,723, US-A-5,425,872, US-A-5,625,087, US-A-5,883,204, US-A-5,919,983, US-A-5,783,512, WO 99/15534, and WO99/42467.

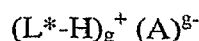
[0038] Combinations of neutral Lewis acids, especially the combination of a trialkyl aluminum compound having from 1 to 4 carbons in each alkyl group and a halogenated
30 tri(hydrocarbyl)boron compound having from 1 to 20 carbons in each hydrocarbyl group, especially tris(pentafluorophenyl)borane, further combinations of such neutral Lewis acid mixtures with a polymeric or oligomeric alumoxane, and combinations of a single neutral Lewis acid, especially tris(pentafluorophenyl)borane with a polymeric or oligomeric

alumoxane may be used as activating cocatalysts. Preferred molar ratios of metal complex:tris(pentafluorophenyl-borane:alumoxane are from 1:1:1 to 1:5:20, more preferably from 1:1:1.5 to 1:5:10.

[0039] Suitable ion forming compounds useful as cocatalysts in one embodiment of the present invention comprise a cation which is a Bronsted acid capable of donating a proton, and a compatible, noncoordinating anion, A⁻. As used herein, the term “noncoordinating” means an anion or substance which either does not coordinate to the Group 4 metal containing precursor complex and the catalytic derivative derived there from, or which is only weakly coordinated to such complexes thereby remaining sufficiently labile to be displaced by a neutral Lewis base. A noncoordinating anion specifically refers to an anion which when functioning as a charge balancing anion in a cationic metal complex does not transfer an anionic substituent or fragment thereof to said cation thereby forming neutral complexes. “Compatible anions” are anions which are not degraded to neutrality when the initially formed complex decomposes and are noninterfering with desired subsequent polymerization or other uses of the complex.

[0040] Preferred anions are those containing a single coordination complex comprising a charge-bearing metal or metalloid core which anion is capable of balancing the charge of the active catalyst species (the metal cation) which may be formed when the two components are combined. Also, said anion should be sufficiently labile to be displaced by olefinic, diolefinic and acetylenically unsaturated compounds or other neutral Lewis bases such as ethers or nitriles. Suitable metals include, but are not limited to, aluminum, gold and platinum. Suitable metalloids include, but are not limited to, boron, phosphorus, and silicon. Compounds containing anions which comprise coordination complexes containing a single metal or metalloid atom are, of course, well known and many, particularly such compounds containing a single boron atom in the anion portion, are available commercially.

[0041] Preferably such cocatalysts may be represented by the following general formula:



wherein:

L* is a neutral Lewis base;

(L*-H)⁺ is a conjugate Bronsted acid of L*;

A^{g-} is a noncoordinating, compatible anion having a charge of $g-$, and g is an integer from 1 to 3.

[0042] More preferably A^{g-} corresponds to the formula: $[M'Q_4]^-$;

5 wherein:

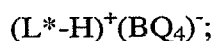
M' is boron or aluminum in the +3 formal oxidation state; and

10 Q independently each occurrence is selected from hydride, dialkylamido, halide, hydrocarbyl, hydrocarbyloxy, halosubstituted-hydrocarbyl, halosubstituted hydrocarbyloxy, and halo- substituted silylhydrocarbyl radicals (including perhalogenated hydrocarbyl- perhalogenated hydrocarbyloxy- and perhalogenated silylhydrocarbyl radicals), said Q having up to 20 carbons with the proviso that in not more than one occurrence is Q halide. Examples of suitable hydrocarbyloxy Q groups are disclosed in US-A-5,296,433.

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[0043] In a more preferred embodiment, d is one, that is, the counter ion has a single negative charge and is A^- . Activating cocatalysts comprising boron which are particularly useful in the preparation of catalysts of this invention may be represented by the following general formula:

20



wherein:

L^* is as previously defined;

B is boron in a formal oxidation state of 3; and

25

Q is a hydrocarbyl-, hydrocarbyloxy-, fluorinated hydrocarbyl-, fluorinated hydrocarbyloxy-, or fluorinated silylhydrocarbyl- group of up to 20 nonhydrogen atoms, with the proviso that in not more than one occasion is Q hydrocarbyl.

30

[0044] Preferred Lewis base salts are ammonium salts, more preferably trialkylammonium salts containing one or more C_{12-40} alkyl groups. Most preferably, Q is each occurrence a fluorinated aryl group, especially, a pentafluorophenyl group.

[0045] Illustrative, but not limiting, examples of boron compounds which may be used as an activating cocatalyst in the preparation of the improved catalysts of this invention are tri-substituted ammonium salts such as:

trimethylammonium tetrakis(pentafluorophenyl) borate,
 triethylammonium tetrakis(pentafluorophenyl) borate,
 tripropylammonium tetrakis(pentafluorophenyl) borate,
 tri(n-butyl)ammonium tetrakis(pentafluorophenyl) borate,
 5 tri(sec-butyl)ammonium tetrakis(pentafluorophenyl) borate,
 N,N-dimethylanilinium tetrakis(pentafluorophenyl) borate,
 N,N-dimethylanilinium n-butyltris(pentafluorophenyl) borate,
 N,N-dimethylanilinium benzyltris(pentafluorophenyl) borate,
 N,N-dimethylanilinium tetrakis(4-(t-butyl dimethylsilyl)-2, 3, 5, 6-tetrafluorophenyl)

10 borate,
 N,N-dimethylanilinium tetrakis(4-(triisopropylsilyl)-2, 3, 5, 6-tetrafluorophenyl)
 borate,

N,N-dimethylanilinium pentafluorophenoxytris(pentafluorophenyl) borate,

N,N-diethylanilinium tetrakis(pentafluorophenyl) borate,

15 N,N-dimethyl-2,4,6-trimethylanilinium tetrakis(pentafluorophenyl) borate,

dimethyloctadecylammonium tetrakis(pentafluorophenyl) borate,

methyldioctadecylammonium tetrakis(pentafluorophenyl) borate,

dialkyl ammonium salts such as:

di-(i-propyl)ammonium tetrakis(pentafluorophenyl) borate,

20 methyloctadecylammonium tetrakis(pentafluorophenyl) borate,

methyloctadodecylammonium tetrakis(pentafluorophenyl) borate, and

dioctadecylammonium tetrakis(pentafluorophenyl) borate;

tri-substituted phosphonium salts such as:

triphenylphosphonium tetrakis(pentafluorophenyl) borate,

25 methyldioctadecylphosphonium tetrakis(pentafluorophenyl) borate, and

tri(2,6-dimethylphenyl)phosphonium tetrakis(pentafluorophenyl) borate;

di-substituted oxonium salts such as:

diphenyloxonium tetrakis(pentafluorophenyl) borate,

di(o-tolyl)oxonium tetrakis(pentafluorophenyl) borate, and

30 di(octadecyl)oxonium tetrakis(pentafluorophenyl) borate;

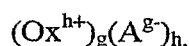
di-substituted sulfonium salts such as:

di(o-tolyl)sulfonium tetrakis(pentafluorophenyl) borate, and

methyloctadecylsulfonium tetrakis(pentafluorophenyl) borate.

[0046] Preferred $(L^*-H)^+$ cations are methyldioctadecylammonium cations, dimethyloctadecylammonium cations, and ammonium cations derived from mixtures of trialkyl amines containing one or 2 C_{14-18} alkyl groups.

[0047] Another suitable ion forming, activating cocatalyst comprises a salt of a cationic oxidizing agent and a noncoordinating, compatible anion represented by the formula:



wherein:

10 Ox^{h+} is a cationic oxidizing agent having a charge of $h+$;
 h is an integer from 1 to 3; and
 A^{g-} and g are as previously defined.

[0048] Examples of cationic oxidizing agents include: ferrocenium, hydrocarbyl-substituted ferrocenium, Ag^+ or Pb^{+2} . Preferred embodiments of A^{g-} are those anions
 15 previously defined with respect to the Bronsted acid containing activating cocatalysts, especially tetrakis(pentafluorophenyl)borate.

[0049] Another suitable ion forming, activating cocatalyst comprises a compound which is a salt of a carbenium ion and a noncoordinating, compatible anion represented by the formula:



wherein:

$[C]^+$ is a C_{1-20} carbenium ion; and
 25 A^- is a noncoordinating, compatible anion having a charge of -1. A preferred carbenium ion is the trityl cation, that is triphenylmethylium.

[0050] A further suitable ion forming, activating cocatalyst comprises a compound which is a salt of a silylium ion and a noncoordinating, compatible anion represented by the formula:



wherein:

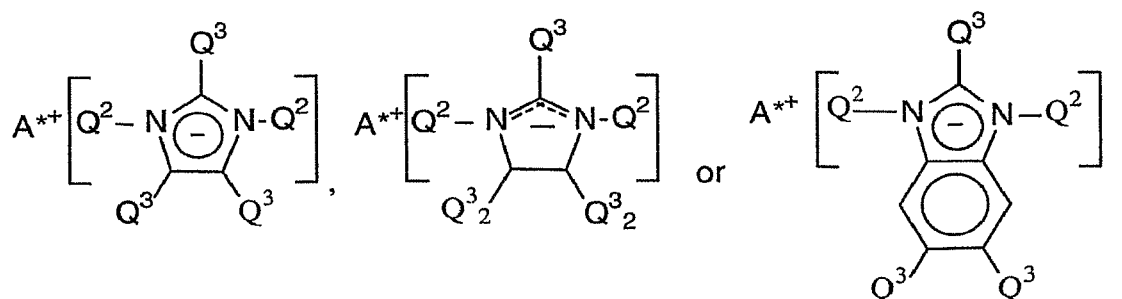
Q^1 is C_{1-10} hydrocarbyl, and A^- is as previously defined.

[0051] Preferred silylium salt activating cocatalysts are trimethylsilylium tetrakis(pentafluorophenyl)borate, triethylsilylium tetrakis(pentafluorophenyl)borate and ether substituted adducts thereof. Silylium salts have been previously generically disclosed in J. Chem Soc. Chem. Comm., 1993, 383-384, as well as Lambert, J. B., et al., Organometallics, 1994, 13, 2430-2443. The use of the above silylium salts as activating cocatalysts for addition polymerization catalysts is disclosed in US-A-5,625,087.

[0052] Certain complexes of alcohols, mercaptans, silanols, and oximes with tris(pentafluorophenyl)borane are also effective catalyst activators and may be used according to the present invention. Such cocatalysts are disclosed in US-A-5,296,433.

[0053] Suitable activating cocatalysts for use herein also include polymeric or oligomeric alumoxanes, especially methylalumoxane (MAO), triisobutyl aluminum modified methylalumoxane (MMAO), or isobutylalumoxane; Lewis acid modified alumoxanes, especially perhalogenated tri(hydrocarbyl)aluminum- or perhalogenated tri(hydrocarbyl)boron modified alumoxanes, having from 1 to 10 carbons in each hydrocarbyl or halogenated hydrocarbyl group, and most especially tris(pentafluorophenyl)borane modified alumoxanes. Such cocatalysts are previously disclosed in US Patents 6,214,760, 6,160,146, 6,140,521, and 6,696,379.

[0054] A class of cocatalysts comprising non-coordinating anions generically referred to as expanded anions, further disclosed in US Patent 6,395,671, may be suitably employed to activate the metal complexes of the present invention for olefin polymerization. Generally, these cocatalysts (illustrated by those having imidazolidine, substituted imidazolidine, imidazolinide, substituted imidazolinide, benzimidazolidine, or substituted benzimidazolidine anions) may be depicted as follows:



wherein:

A^{*+} is a cation, especially a proton containing cation, and preferably is a trihydrocarbyl ammonium cation containing one or two C_{10-40} alkyl groups,

especially a methyl
(C₁₄₋₂₀ alkyl)ammonium cation,

Q³, independently each occurrence, is hydrogen or a halo, hydrocarbyl, halocarbyl,
halohydrocarbyl, silylhydrocarbyl, or silyl, (including mono-, di- and
5 tri(hydrocarbyl)silyl) group of up to 30 atoms not counting hydrogen, preferably C₁₋₂₀ alkyl, and

Q² is tris(pentafluorophenyl)borane or tris(pentafluorophenyl)alumane).

[0055] Examples of these catalyst activators include trihydrocarbylammonium- salts, especially, methyl(C₁₄₋₂₀ alkyl)ammonium- salts of:

- 10 bis(tris(pentafluorophenyl)borane)imidazolidide,
bis(tris(pentafluorophenyl)borane)-2-undecylimidazolidide,
bis(tris(pentafluorophenyl)borane)-2-heptadecylimidazolidide,
bis(tris(pentafluorophenyl)borane)-4,5-bis(undecyl)imidazolidide,
bis(tris(pentafluorophenyl)borane)-4,5-bis(heptadecyl)imidazolidide,
15 bis(tris(pentafluorophenyl)borane)imidazolinide,
bis(tris(pentafluorophenyl)borane)-2-undecylimidazolinide,
bis(tris(pentafluorophenyl)borane)-2-heptadecylimidazolinide,
bis(tris(pentafluorophenyl)borane)-4,5-bis(undecyl)imidazolinide,
bis(tris(pentafluorophenyl)borane)-4,5-bis(heptadecyl)imidazolinide,
20 bis(tris(pentafluorophenyl)borane)-5,6-dimethylbenzimidazolidide,
bis(tris(pentafluorophenyl)borane)-5,6-bis(undecyl)benzimidazolidide,
bis(tris(pentafluorophenyl)alumane)imidazolidide,
bis(tris(pentafluorophenyl)alumane)-2-undecylimidazolidide,
bis(tris(pentafluorophenyl)alumane)-2-heptadecylimidazolidide,
25 bis(tris(pentafluorophenyl)alumane)-4,5-bis(undecyl)imidazolidide,
bis(tris(pentafluorophenyl)alumane)-4,5-bis(heptadecyl)imidazolidide,
bis(tris(pentafluorophenyl)alumane)imidazolinide,
bis(tris(pentafluorophenyl)alumane)-2-undecylimidazolinide,
bis(tris(pentafluorophenyl)alumane)-2-heptadecylimidazolinide,
30 bis(tris(pentafluorophenyl)alumane)-4,5-bis(undecyl)imidazolinide,
bis(tris(pentafluorophenyl)alumane)-4,5-bis(heptadecyl)imidazolinide,
bis(tris(pentafluorophenyl)alumane)-5,6-dimethylbenzimidazolidide, and

bis(tris(pentafluorophenyl)alumane)-5,6-bis(undecyl)benzimidazolidine.

[0056] Other activators include those described in PCT publication WO 98/07515 such as tris (2, 2', 2''-nonafluorobiphenyl)fluoroaluminate. Combinations of activators are also contemplated by the invention, for example, alumoxanes and ionizing activators in combinations, see for example, EP-A-0 573120, PCT publications WO 94/07928 and WO 95/14044 and US Patents 5,153,157 and 5,453,410. WO 98/09996 describes activating catalyst compounds with perchlorates, periodates and iodates, including their hydrates. WO 99/18135 describes the use of organoboroaluminum activators. WO 03/10171 discloses catalyst activators that are adducts of Bronsted acids with Lewis acids. Other activators or methods for activating a catalyst compound are described in for example, US Patents 5,849,852, 5,859, 653, 5,869,723, EP-A-615981, and PCT publication WO 98/32775. All of the foregoing catalyst activators as well as any other known activator for transition metal complex catalysts may be employed alone or in combination according to the present invention, however, for best results alumoxane containing cocatalysts are avoided.

[0057] The molar ratio of catalyst/cocatalyst employed preferably ranges from 1:10,000 to 100:1, more preferably from 1:5000 to 10:1, most preferably from 1:1000 to 1:1. Alumoxane, when used by itself as an activating cocatalyst, is employed in large quantity, generally at least 100 times the quantity of metal complex on a molar basis. Tris(pentafluorophenyl)borane, when used as an activating cocatalyst is employed in a molar ratio to the metal complex of from 0.5:1 to 10:1, more preferably from 1:1 to 6:1 most preferably from 1:1 to 5:1. The remaining activating cocatalysts are generally employed in approximately equimolar quantity with the metal complex.

Novel Compositions of the Present Invention

[0058] Advantageously, novel compositions of the present invention comprise an ethylene/alpha-olefin interpolymer composition with a multi-modal molecular weight distribution and one or more molecules having a gram molecular weight equal to about ((the molecular weight of an aryl or hydrocarbyl-ligand of a pre-catalyst) + 28 + 14 * X), wherein X represents an integer from zero to 10, preferably zero to 8. The aryl or hydrocarbyl ligand may be any of those described herein. The molecule may be observed in the composition by extracting the interpolymer with a solvent such as methylene chloride, adding another solvent such as an alcohol, e.g. ethanol, and decanting. The decantate can then be analyzed by any convenient analytical method such as gas chromatography coupled

with mass spectroscopy. Said composition may also contain ethylene, an α -olefin, a reaction product or a mixture thereof.

[0059] Other novel compositions of the present invention include the catalyst which may be synthesized as described above optionally mixed with ethylene, an α -olefin, a reaction product or a mixture thereof.

Ethylene/ α -olefin Multi-Block Interpolymer Component(s)

[0060] The general processes described above may also be used to produce an ethylene/ α -olefin multi-block interpolymer such as those describe in, for example, copending U.S. Application No. 11/376,835 filed on March 15, 2006 and PCT Publication No. WO 2005/090427, filed on March 17, 2005, which in turn claims priority to U.S. Provisional Application No. 60/553,906, filed March 17, 2004. For purposes of United States patent practice, the contents of the aforementioned applications are herein incorporated by reference in their entirety. If such a multi-block polymer is desired then the processes described above will also generally include a catalyst such as zinc which is different than any pre-catalyst that may be employed. In addition, a shuttling agent such as diethyl zinc or others described in PCT Publication No. WO 2005/090427 will usually be employed. Such processes will typically then result in a polymer wherein the polymer has one or more of the following characteristics:

- (1) an average block index greater than zero and up to about 1.0 and a molecular weight distribution, M_w/M_n , greater than about 1.3; or
- (2) at least one molecular fraction which elutes between 40°C and 130°C when fractionated using TREF, characterized in that the fraction has a block index of at least 0.5 and up to about 1; or
- (3) an M_w/M_n from about 1.7 to about 3.5, at least one melting point, T_m , in degrees Celsius, and a density, d , in grams/cubic centimeter, wherein the numerical values of T_m and d correspond to the relationship:

$$T_m > -2002.9 + 4538.5(d) - 2422.2(d)^2, \text{ preferably } T_m \geq 858.91 - 1825.3(d) + 1112.8(d)^2; \text{ or}$$

(4) an Mw/Mn from about 1.7 to about 3.5, and is characterized by a heat of fusion, ΔH in J/g, and a delta quantity, ΔT , in degrees Celsius defined as the temperature difference between the tallest DSC peak and the tallest CRYSTAF peak, wherein the numerical values of ΔT and ΔH have the following relationships:

5 $\Delta T > -0.1299(\Delta H) + 62.81$ for ΔH greater than zero and up to 130 J/g,

$\Delta T \geq 48^\circ\text{C}$ for ΔH greater than 130 J/g ,

wherein the CRYSTAF peak is determined using at least 5 percent of the cumulative polymer, and if less than 5 percent of the polymer has an identifiable CRYSTAF peak, then the CRYSTAF temperature is 30°C ; or

10 (5) an elastic recovery, Re , in percent at 300 percent strain and 1 cycle measured with a compression-molded film of the ethylene/ α -olefin interpolymer, and has a density, d , in grams/cubic centimeter, wherein the numerical values of Re and d satisfy the following relationship when ethylene/ α -olefin interpolymer is substantially free of a cross-linked phase:

15 $Re > 1481 - 1629(d)$; or

(6) a molecular fraction which elutes between 40°C and 130°C when fractionated using TREF, characterized in that the fraction has a molar comonomer content of at least 5 percent higher than that of a comparable random ethylene interpolymer fraction eluting between the same temperatures, wherein said comparable random ethylene interpolymer has
20 the same comonomer(s) and has a melt index, density, and molar comonomer content (based on the whole polymer) within 10 percent of that of the ethylene/ α -olefin interpolymer; or

(7) a storage modulus at 25°C , $G'(25^\circ\text{C})$, and a storage modulus at 100°C , $G'(100^\circ\text{C})$, wherein the ratio of $G'(25^\circ\text{C})$ to $G'(100^\circ\text{C})$ is in the range of about 1:1 to
25 about 9:1.

Applications and End Uses

[0061] The polymers of the present invention can be used in a variety of conventional thermoplastic fabrication processes to produce useful articles. Such articles include objects comprising at least one film layer, such as a monolayer film, or at least one layer in a multilayer film prepared by cast, blown, calendered, or extrusion coating processes; molded articles, such as blow molded, injection molded, or rotomolded articles; extrusions; fibers; and woven or non-woven fabrics. The polymers described herein are also useful for wire and cable coating operations, as well as in sheet extrusion for vacuum forming operations, and forming molded articles, including the use of injection molding, blow molding process, or rotomolding processes. Compositions comprising the olefin polymers can also be formed into fabricated articles such as those previously mentioned using conventional polyolefin processing techniques which are well known to those skilled in the art of polyolefin processing. Dispersions, both aqueous and non-aqueous, can also be formed using the polymers or formulations comprising the same. Frothed foams comprising the invented polymers can also be formed, as disclosed in PCT application No. PCT/US2004/027593, filed August 25, 2004, and published as WO2005/021622. The polymers may also be crosslinked by any known means, such as the use of peroxide, electron beam, silane, azide, or other cross-linking technique. The polymers can also be chemically modified, such as by grafting (for example by use of maleic anhydride (MAH), silanes, or other grafting agent), halogenation, amination, sulfonation, or other chemical modification.

[0062] Suitable end uses for the foregoing products include elastic films and fibers; soft touch goods, such as tooth brush handles and appliance handles; antiblocking compositions; cap liners, gaskets and profiles; adhesives (including hot melt adhesives and pressure sensitive adhesives); footwear (including shoe soles and shoe liners); auto interior parts and profiles; foam goods (both open and closed cell); impact modifiers for other thermoplastic polymers; coated fabrics; hoses; tubing; weather stripping; cap liners; flooring; and viscosity index modifiers, also known as pour point modifiers, for lubricants.

Examples

[0063] As stated above, the bimodal molecular weight "split" of the polymer may be selected by controlling the mole fractions (f) of the two or more monomers, n , such that the mole fraction of monomer m is defined as:

$$f_m = \frac{[Monomer_m]}{\sum_{i=1}^n [Monomer_i]}.$$

[0064] This may be quantified for an ethylene-octene copolymer as depicted in Figures 20 and 21. At low f_2 , the low molecular weight fraction predominates, but at higher f_2 , the higher molecular weight species is more prevalent.

5 General Experimental Considerations

[0065] Unless specified otherwise, all reagents are handled under anaerobic conditions using standard procedures for the handling of extremely air- and water-sensitive materials. Solvents are used without further purification. All other chemicals are commercial materials and are used as received.

10 General Reactor Polymerization Procedure

[0066] A 1 ga. AE autoclave is purged at high temperature with N_2 . Isopar[®]E was added, and the reactor is heated to 120 °C. 1-Octene and hydrogen are added batchwise to the reactor and are not regulated during the run. The reactor is pressurized with ethylene (450 psi). Solutions of the pre-catalyst, cocatalyst (1.2 equivalents to pre-catalyst), and a scavenger (5 equivalents to pre-catalyst) are mixed and then added to the reactor using a flush of high pressure Isopar[®]E. Polymer yield is kept low to minimize monomer composition drift during the experiment. After the prescribed reaction time, reactor contents are dumped into a resin kettle and mixed with Irganox[®]1010/Irgafos[®]168 stabilizer mixture (1 g). The polymer is recovered by evaporating the majority of the solvent at room temperature and then dried further in a vacuum oven overnight at 90 °C. Following the run, the reactor is hot-flushed with Isopar[®]E to prevent polymer contamination from run to run.

Table 1. Batch reactor ethylene/octene copolymerization with Pre-catalyst.

Sample #	Pre-catalyst* (μmol)	Isopar [®] E feed (g)	Ethylene feed (g)	Octene feed (g)	f_2	Yield (g)
1	2.0	1591	153	11	0.02	44
2	2.0	1550	151	56	0.10	41
3	2.0	1506	153	100	0.16	46
4	2.5	1402	167	203	0.31	26
5	2.5	1201	168	400	0.47	36
6	2.5	1009	170	605	0.57	44
7	3.0	812	169	801	0.64	66
8	3.0	611	165	1003	0.69	60
9	3.0	401	166	1202	0.73	64
10	3.0	204	166	1402	0.75	52
11	3.5	10	168	1603	0.78	84

^a Polymerization conditions: 1.2 equiv. co-catalyst, T = 120 °C, 460 psig reactor pressure, 40 mmol hydrogen, t = 10 min.

* Pre-catalyst = [N-(2,6-di(1-methylethyl)phenyl)amido)(2-isopropylphenyl)(α -naphthalen-2-diyl(6-pyridin-2-diyl)methane)]hafnium dimethyl (as disclosed in U.S. Application No. 20040220050) and a co-catalyst of methyldi(C₁₄₋₁₈alkyl) ammonium salts of tetrakis(pentafluorophenyl)borate (as disclosed in U.S. Patent No. 5,919,983)

Example	M_w (kg/mol)	M_n (kg/mol)	M_w/M_n
1	671	174	3.86
2	588	164	3.59
3	517	139	3.71
4	851	116	7.35
5	972	137	7.10
6	906	164	5.51
7	1015	169	6.02
8	1108	232	4.78
9	1135	202	5.62
10	1148	239	4.81
11	1013	177	5.74

Examples 12-15, Continuous Solution Polymerization, Catalyst A1

[0067] Continuous solution polymerizations are carried out in a computer controlled autoclave reactor equipped with an internal stirrer. Purified mixed alkanes solvent (Isopar™ E available from ExxonMobil, Inc.), ethylene, 1-octene, and hydrogen (where used) are supplied to a reactor equipped with a jacket for temperature control and an internal thermocouple. The solvent feed to the reactor is measured by a mass-flow controller. A variable speed diaphragm pump controls the solvent flow rate and pressure to the reactor. At the discharge of the pump, a side stream is taken to provide flush flows for the catalyst and cocatalyst 1 injection lines and the reactor agitator. These flows are measured by Micro-Motion mass flow meters and controlled by control valves or by the manual adjustment of needle valves. The remaining solvent is combined with 1-octene, ethylene, and hydrogen (where used) and fed to the reactor. A mass flow controller is used to deliver hydrogen to the reactor as needed. The temperature of the solvent/monomer solution is controlled by use of a heat exchanger before entering the reactor. This stream enters the bottom of the reactor. The catalyst component solutions are metered using pumps and mass flow meters and are combined with the catalyst flush solvent and introduced into the bottom of the reactor. The reactor is run liquid-full at 500 psig (3.45 MPa) with vigorous stirring.

Product is removed through exit lines at the top of the reactor. All exit lines from the reactor are steam traced and insulated. Polymerization is stopped by the addition of a small amount of water into the exit line along with any stabilizers or other additives and passing the mixture through a static mixer. The product stream is then heated by passing through a

5 heat exchanger before devolatilization. The polymer product is recovered by extrusion using a devolatilizing extruder and water cooled pelletizer. Process details and results are contained in Table 2. Selected polymer properties are provided in Table 3.

Table 2

Ex.	C ₂ H ₄ kg/hr	C ₈ H ₁₆ kg/hr	Solv. kg/hr	H ₂ sccm ¹	T °C	Pre- cat Al ² ppm	Pre- cat Al Flow Kg/hr	Cocat Conc. ppm	Cocat Flow kg/hr	MMAO Conc. ppm	MMAO Flow kg/hr	Poly Rate ³ kg/hr	f ₂	Conv % ⁴	Solids %	Eff. ⁵
12	53.6	31.4	354	4,470	120	600	0.49	5000	0.49	600	0.45	82.5	0.63	89.6	19.3	281
13	38.6	32.4	288	2,303	"	"	0.38	"	0.38	"	0.40	66.7	0.68	89.1	20.6	303
14	62.1	18.8	425	4,768	"	"	0.63	"	0.62	"	0.65	79.0	0.51	90.1	16.9	202
15	65.5	13.4	345	3,951	130	"	0.86	"	0.85	"	0.44	73.4	0.34	92.2	19.0	145

¹ standard cm³/min² [N-(2,6-di(1-methylethyl)phenyl)amido](2-isopropylphenyl)(α -naphthalen-2-diyl(6-pyridin-2-diyl)methane)]hafnium dimethyl³ polymer production rate⁴ percent ethylene conversion in reactor⁵ efficiency, kg polymer/g M where g M = g Hf + g Zr

Table 3

Ex.	Density (g/cm ³)	I ₂	I ₁₀ /I ₂	Mw (g/mol)	Mn (g/mol)	Mw/Mn
12	0.8650	1.06	8.36	130	26.6	4.90
13	0.8560	0.92	8.00	142	49.6	2.87
14	0.8800	0.76	7.26	127	30.3	4.18
15	0.9030	0.97	7.00	107	24.3	4.40

5 [0068] The ethylene-octene copolymers in Figures 20-21 may be made in a similar manner.

Theoretical Methods and Explanation

10 [0069] To support the instant invention calculations were carried out using the commercially-available software package, Gaussian98 Revision A.10 distributed by Gaussian, Inc., Pittsburgh PA, 2001. The computations utilized the density functional theory (DFT) method, B3LYP as described in, for example, Becke, A. D. *J. Chem. Phys.* **1993**, 98, 5648; Lee, C.; Yang, W.; Parr, R. G. *Phys. Rev B* **1988**, 37, 785; and Miehlich, B.; Savin, A.; Stoll, H.; Preuss, H. *Chem. Phys. Lett.* **1989**, 157, 200 each of which is incorporated herein by reference. In a few cases,

15 the results were reconfirmed using conventional theory with correlation, Møller-Plesset perturbation theory to second order (MP2) as described in, for example, Møller, C.; Plesset, M. S. *Phys. Rev.* **1934**, 46, 618; Head-Gordon, M.; Pople, J. A.; Frisch, M. J. *Chem. Phys. Lett.* **1988**, 153, 503; Frisch, M. J.; Head-Gordon, M.; Pople, J. A. *Chem. Phys. Lett.* **1990**, 166, 275; Frisch, M. J.; Head-Gordon, M.; Pople, J. A. *Chem. Phys. Lett.* **1990**, 166, 281; Head-Gordon, M.; Head-Gordon, T. *Chem. Phys. Lett.* **1994**, 220, 122; and Saebo, S.; Almlof, J. *Chem. Phys. Lett.* **1989**, 154, 83 each of which is incorporated herein by reference. Qualitatively, the

20 results using MP2 were similar to those for B3LYP. A series of different basis sets

were used and tested. Initially the modest LANL2DZ basis set as described in, for example, Dunning, Jr., T. H.; Hay, P. J. in *Modern Theoretical Chemistry*, Ed. H. F. Schaefer, III, Plenum, New York, 1976, vol 3, 1; Hay, P. J. Wadt, W. R. *J. Chem. Phys.* **1985**, 82, 270; Wadt, W. R.; Hay, P. J. *J. Chem. Phys.* **1985**, 82, 284; and Hay, P. J. Wadt, W. R. *J. Chem. Phys.* **1985**, 82, 299, was used for all atoms, but progressively larger basis sets were employed such as i) LANL2DZ on the transition metal and 6-31G* on the all other atoms as described in Ditchfield, R.; Hehre, W. J.; Pople, J. A. *J. Chem. Phys.* **1971**, 54, 724; Hehre, W. J.; Ditchfield, R.; Pople, J. A. *J. Chem. Phys.* **1972**, 56, 2257; and Gordon, M. S. *Chem. Phys. Lett.* **1980**, 76, 163 and ii) LANL2DZ on the transition metal and 6-311G** on all other atoms as described in McLean, A. D.; Chandler, G. S. *J. Chem. Phys.* **1980**, 72, 5639; and Krishnan, R.; Binkley, J. S.; Seeger, R.; Pople, J. A. *J. Chem. Phys.* **1980**, 72, 650 and these did not qualitatively change the results. The inclusion of enthalpic and free energy corrections at a given temperature also did not change the results significantly.

[0070] The calculations involved locating four stationary points on the potential energy surface (see Diagram 1). Standard optimizations and defaults within the Gaussian98 program were utilized which included the Berny optimizer in redundant internal coordinates as described in Peng, C.; Ayala, P. Y.; Schlegel, H. B. Frisch, M. J. *J. Comp. Chem.* **1996**, 17, 49; and Peng, C.; Schlegel, H. B. *Israel. J. Chem.* **1994**, 33, 449. The four structures located were the transition state for ethylene inserting into the M-aryl or M-hydrocarbyl bond of the original species (1), the transition state for ethylene inserting in the polymeryl chain of the original species (2), the product of inserting into the aryl or hydrocarbyl group (3), and the product of inserting into the polymeryl chain (4). The stationary points defined as transition states were confirmed by one and only one imaginary frequency (corresponding to the reaction coordinate) as determined from mass-weighting of the eigenvalues from the diagonalization of the second derivative or Hessian matrix. The two products, 3 and 4, have no imaginary frequencies upon this analysis.

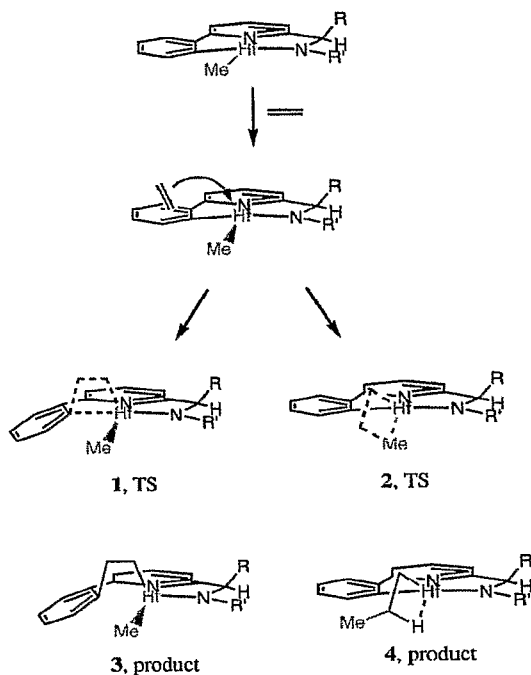
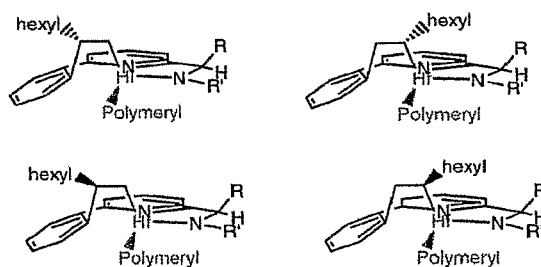


Diagram 1. Pathways to aryl or hydrocarbyl inserted and alkyl inserted products.

[0071] In examples involving ethylene/octene, more than one potential
 5 'inserted' catalyst could be formed. Diagram 2 depicts the four possible octene inserted catalysts from one face. These four unique catalysts each could create polymer with different properties such as molecular weight and comonomer incorporation.



10 **Diagram 2. Four possible octene inserted catalysts.**

[0072] Insertions can occur on the top and bottom faces of the catalyst and these can be unique depending on the overall symmetry of the initial catalyst (Diagram 3). For the specific catalyst below, insertions into the top and bottom

faces lead to unique isomers. Thus for ethylene/octene polymerizations, up to ten unique 'inserted' catalysts are possible. The aforementioned calculations indicate that not all are favorable, but certainly more than one is possible. As described above, the Applicants have determined that different conditions can be used to

5 favor one or some over others.

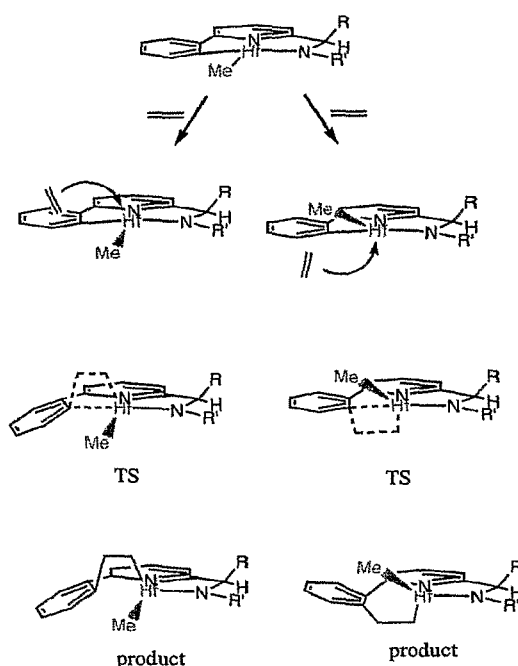


Diagram 3. Ethylene inserting into top and bottom faces of the initial catalyst. Whether these two products are different depends on the symmetry of the catalyst (groups at R and R').

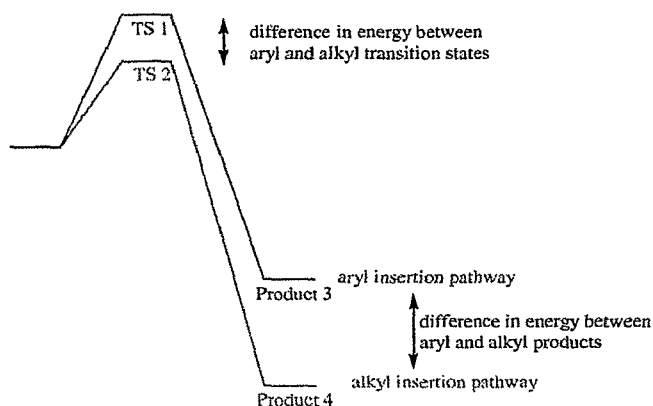
10

[0073] Based on catalyst activity such as the one above, barriers important for the polymerization may be estimated. If insertion into the aryl or hydrocarbyl is less than 10 kcal/mol higher than insertion into the alkyl, this reaction should occur during the polymerization cycle. From Diagrams 1 and 4, this implies that TS 1

15 lies no higher than 10 kcal/mol above TS 2. It is preferable that this difference is less than 5 kcal/mol and even more preferable that insertion into the aryl or hydrocarbyl is less than insertion into the alkyl. Insertion into the alkyl is not a reversible process, but to avoid reversibility of insertion into the aryl or hydrocarbyl, the product of insertion into the aryl or hydrocarbyl cannot lie more

20 than 5 kcal/mol above insertion into the alkyl. From Diagrams 1 and 4, this

implies that Product 3 lies no higher than 5 kcal/mol above Product 4. However, it is preferable that this difference is less and even more preferable that the product of aryl or hydrocarbyl insertion is lower than the product of alkyl insertion. Diagram 4 depicts a potential energy surface of the two processes.



5

Diagram 4. Potential energy surface for insertion into the Hf-aryl and Hf-alkyl bonds.

[0074] One skilled in the art may apply the above principles in selecting
10 reaction conditions and catalyst to achieve a desired controlled molecular weight.

What is claimed is:

1. A process of controlling molecular weight distribution in the production of an ethylene/ α -olefin interpolymer composition comprising:

- 5 (a) selecting at least one suitable pre-catalyst comprising at least one metal-aryl or metal-hydrocarbyl bond, wherein each pre-catalyst molecule is essentially the same as every other pre-catalyst molecule;
- (b) contacting ethylene, at least one α -olefin, and said suitable pre-catalyst;
- 10 (c) selecting ethylene: α -olefin concentration ratios sufficient to activate the pre-catalyst, and
- (d) forming an ethylene/ α -olefin interpolymer composition under continuous reaction polymerization conditions; and, optionally,
- (e) selecting a molecular weight split of the interpolymer as determined by the mole fractions (f) of the two or more monomers, n , such that the
- 15 mole fraction of monomer m is defined as:

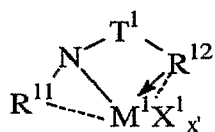
$$f_m = \frac{[Monomer_m]}{\sum_{i=1}^n [Monomer_i]}.$$

to produce an ethylene/ α -olefin interpolymer composition with a controlled bimodal or multi-modal molecular weight distribution.

20 2. The process of Claim 1 wherein the pre-catalyst has been activated under one set of conditions and the interpolymer has been polymerized under a different set of conditions.

25 3. The process of Claim 2 wherein the pre-catalyst is activated with an initial monomer ratio that differs from the monomer ratio during the interpolymer polymerization.

4. The process of Claim 1 which further comprises employing a pre-catalyst comprising a ligand and terminating the reaction conditions via a catalyst quench.
5. The process of Claim 4 wherein a ligand fragment with an appended olefin can be detected from the catalyst quenchate.
6. The process of Claim 1 wherein the reaction conditions comprise at least one other catalyst differing from the pre-catalyst.
7. The process of Claim 6 wherein one of the catalysts differing from the pre-catalyst is zinc.
8. The process of Claim 1 wherein the reaction conditions further comprise at least one shuttling agent.
9. The process of Claim 8 wherein the shuttling agent is diethyl zinc.
10. The process of Claim 1 wherein the suitable pre-catalyst is selected from the group consisting of hydrocarbylamine substituted heteroaryl compounds corresponding to the formula:



wherein:

- R^{11} is selected from alkyl, cycloalkyl, heteroalkyl, cycloheteroalkyl, aryl, and inertly substituted derivatives thereof containing from 1 to 30 atoms not counting hydrogen or a divalent derivative thereof;
- T^1 is a divalent bridging group of from 1 to 41 atoms other than hydrogen, preferably 1 to 20 atoms other than hydrogen, and most preferably a mono- or di- C_{1-20} hydrocarbyl substituted methylene or silane group; and

R^{12} is a C_{5-20} heteroaryl group containing Lewis base functionality, especially a pyridin-2-yl- or substituted pyridin-2-yl group or a divalent derivative thereof;

M^1 comprises hafnium or other Group 4 metal;

5 X^1 is an anionic, neutral or dianionic ligand group;

x' is a number from 0 to 5 indicating the number of such X^1 groups; and bonds, optional bonds and electron donative interactions are represented by lines, dotted lines and arrows respectively, or a mixture thereof, in contact with a suitable co-catalyst.

10

11. The process of Claim 1 wherein the ethylene/ α -olefin interpolymer composition is produced in a single polymerization reactor.

12. The process of Claim 1 wherein the ethylene/ α -olefin interpolymer
15 composition is produced using N-(2,6-di(1-methylethyl)phenyl)amido)(2-isopropylphenyl)(α -naphthalen-2-diyl(6-pyridin-2-diyl)methane)]hafnium dimethyl.

13. The process of Claim 1 wherein a low molecular weight portion of said
20 ethylene/ α -olefin interpolymer composition has a higher density than a high molecular weight portion of said ethylene/ α -olefin interpolymer composition.

14. The product of the process of Claim 1.

25 15. A composition comprising an ethylene/ α -olefin interpolymer composition with a multi-modal molecular weight distribution and one or more molecules having a gram molecular weight equal to about ((the molecular weight of an aryl or hydrocarbyl-ligand of a pre-catalyst) + 28 + 14 * X), wherein X represents an integer from zero to 10.

16. The interpolymers of Claim 15, wherein the molecule is observed by extracting the interpolymers with methylene chloride, adding ethanol and decanting, analyzing the decantate by gas chromatography coupled with mass spectroscopy.

5

17. A process comprising:

- (1) selecting at least one suitable pre-catalyst comprising at least one metal-aryl or metal-hydrocarbyl bond, wherein each pre-catalyst molecule is essentially the same as every other pre-catalyst molecule;
- 10 (2) contacting ethylene, an α -olefin, and said suitable pre-catalyst; and
- (3) selecting ethylene:alpha-olefin concentration ratios sufficient to activate the pre-catalyst, and form an ethylene/ α -olefin interpolymers interpolymers wherein the ethylene/ α -olefin interpolymers

- (a) has a Mw/Mn from about 1.7 to about 3.5, at least one melting point, T_m , in degrees Celsius, and a density, d , in grams/cubic centimeter, wherein the numerical values of T_m and d correspond to the relationship:
- 15

$$T_m \geq 858.91 - 1825.3(d) + 1112.8(d)^2; \text{ or}$$

- (b) has a Mw/Mn from about 1.7 to about 3.5, and is characterized by a heat of fusion, ΔH in J/g, and a delta quantity, ΔT , in degrees Celsius defined as the temperature difference between the tallest DSC peak and the tallest CRYSTAF peak, wherein the numerical values of ΔT and ΔH have the following relationships:
- 20

$$\Delta T > -0.1299(\Delta H) + 62.81 \text{ for } \Delta H \text{ greater than zero and up to } 130 \text{ J/g,}$$

$$\Delta T \geq 48^\circ\text{C for } \Delta H \text{ greater than } 130 \text{ J/g,}$$

wherein the CRYSTAF peak is determined using at least 5 percent of the cumulative polymer, and if less than 5 percent of the polymer

has an identifiable CRYSTAF peak, then the CRYSTAF temperature is 30°C; or

5 (c) is characterized by an elastic recovery, Re, in percent at 300 percent strain and 1 cycle measured with a compression-molded film of the ethylene/ α -olefin interpolymer, and has a density, d, in grams/cubic centimeter, wherein the numerical values of Re and d satisfy the following relationship when ethylene/ α -olefin interpolymer is substantially free of a cross-linked phase:

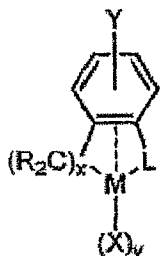
$$\text{Re} > 1481 - 1629(d); \text{ or}$$

10 (d) has a molecular fraction which elutes between 40°C and 130°C when fractionated using TREF, characterized in that the fraction has a molar comonomer content of at least 5 percent higher than that of a comparable random ethylene interpolymer fraction eluting between the same temperatures, wherein said comparable
15 random ethylene interpolymer has the same comonomer(s) and has a melt index, density, and molar comonomer content (based on the whole polymer) within 10 percent of that of the ethylene/ α -olefin interpolymer; or

20 (e) has a storage modulus at 25 °C, $G'(25\text{ °C})$, and a storage modulus at 100 °C, $G'(100\text{ °C})$, wherein the ratio of $G'(25\text{ °C})$ to $G'(100\text{ °C})$ is in the range of about 1:1 to about 9:1.

18. A process of controlling molecular weight distribution in the production of an ethylene/ α -olefin interpolymer composition comprising:

25 contacting ethylene, an α -olefin, a suitable catalyst, and a suitable co-catalyst, under reaction conditions sufficient to form an ethylene/ α -olefin interpolymer composition wherein the catalyst comprises a catalytic amount of a molecule having the structure:



wherein M = group 2 - 8 metal as a neutral or charged moiety;

Y = any substituent including fused rings;

L = a pyridyl; a pyridylamide or any other ligating group;

5 X = alkyl, aryl, substituted alkyl, H or hydride, halide, or other anionic moiety;

y = an integer from 0 to the complete valence of M;

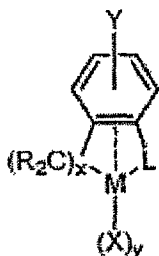
R = alkyl, aryl, haloalkyl, haloaryl, hydrogen;

x = 1 - 6;

Dashed line = optional bond; and

10 X and (CR₂)_x may be tethered or part of a ring.

19. A composition comprising a catalytic amount of a molecule having the structure:



15 wherein M = group 2 - 8 metal;

Y = any substituent including fused rings;

L = a pyridyl; a pyridylamide or any other ligating group;

X = alkyl, aryl, substituted alkyl, H or hydride, halide, or other anionic moiety;

y = an integer from 0 to the complete valence of M;

20 R = alkyl, aryl, haloalkyl, haloaryl, hydrogen;

x = 1 - 6;

Dashed line = optional bond; and

X and (CR₂)_x may be tethered or part of a ring.

25 20. The composition of Claim 19 further comprising ethylene or a reaction product of said molecule and ethylene.

21. The composition of Claim 19 further comprising an α -olefin or a reaction product of said molecule and an α -olefin.
- 5 22. The composition of Claim 19 further comprising ethylene and an α -olefin or a reaction product of said molecule, ethylene and an α -olefin.
23. A process of controlling molecular weight distribution in the production of an ethylene/ α -olefin interpolymer composition comprising:
- 10 (a) selecting at least one suitable pre-catalyst comprising at least one metal-aryl or metal-hydrocarbyl bond, wherein each pre-catalyst molecule is essentially the same as every other pre-catalyst molecule;
- (b) contacting at least one organic compound, and said suitable pre-catalyst;
- 15 (c) selecting at least one organic compound concentration sufficient to activate the pre-catalyst, and
- (d) forming an ethylene/ α -olefin interpolymer composition under continuous reaction polymerization conditions; and, optionally,
- 20 (e) selecting a molecular weight split of the interpolymer as determined by the concentration of the one or more organic compound(s) to produce an ethylene/ α -olefin interpolymer composition with a controlled bimodal or multi-modal molecular weight distribution.