

Description

The invention relates to a circuit arrangement for deriving a direct voltage from an alternating voltage, particularly the mains alternating voltage, said circuit arrangement comprising:

- two input terminals,
- two output terminals one of which is connected to one of the input terminals,
- a switching transistor whose main current path is coupled between the other input terminal and the other output terminal,
- a base control circuit for controlling the switching transistor, which base control circuit includes a thyristor which is coupled via a resistor between the two input terminals, the node between the resistor and thyristor being coupled to the control electrode of the switching transistor, and
- a time-determining circuit comprising a series arrangement of a resistor and a capacitor and a trigger element connected between the gate terminal of the thyristor and the node between the said resistor and capacitor.

A circuit arrangement of this type is known from British Patent Specification GB 1,252,637. In this known circuit arrangement the series arrangement of resistor and capacitor, which forms part of the time-determining circuit, is directly connected between the input terminals and the trigger element is constituted by a neon lamp. A full-wave rectified alternating voltage must be presented to the input terminals. At the start of each half cycle the capacitor in the RC series circuit will be charged until the ignition voltage of the neon lamp is reached. Ignition of the neon lamp will render the thyristor conducting so that in its turn the switching transistor is turned on.

The operation of this known time-determining circuit is very inaccurate. On the one hand the neon lamp is an element having ample tolerances. On the other hand the residual voltage across the capacitor at the start of a subsequent cycle is not always equal, which together with the tolerances of the resistor and the capacitor leads to ample margins in the instant when the neon lamp and hence the thyristor are ignited. Consequently, considerable variations in the amplitude of the direct voltage may occur at the output terminals, which particularly applies when relatively low direct voltages must be obtained from relatively high alternating voltages. This is undesirable or inadmissible for many applications, for example, for the power supply of low-voltage elements such as small lamps, light-emitting diodes and the like.

A circuit arrangement of the type described in the opening paragraph can be used, for example for supplying a control circuit and/or indicator lamps. The circuit arrangement according to the invention is particularly suitable for use in a domestic appliance, like a vacuum cleaner.

It is an object of the invention to indicate in which way such a circuit arrangement must be formed to obtain a direct voltage at the output terminals with an amplitude which will vary only within very narrow margins. Such a circuit arrangement will be particularly suitable for mass production without an extensive being required in the arrangement to meet the requirements of tolerance of the output voltage.

In a circuit arrangement of the type described in the opening paragraph for deriving a direct voltage from an alternating voltage, particularly the mains alternating voltage, these objects are realized in that the trigger element is constituted by a diac, in that the other input terminal is coupled to an alternating voltage terminal via a rectifier diode arranged in the forward direction with the main current path of the switching transistor, in that the said series arrangement of resistor and capacitor is coupled between the alternating voltage terminal and the one input terminal and in that a diode is arranged across the capacitor in such a way that this diode conducts during the periods when the rectifier diode is blocked.

By controlling the RC circuit in the time-determining circuit with the non-rectified alternating voltage and by shunting the capacitor in the RC circuit with a diode, which conducts when the rectifier diode from which the switching transistor receives its supply is blocked, it is achieved that the capacitor in the time-determining circuit is completely discharged when the rectifier diode starts conducting. This implies that only the tolerances of the resistor and the capacitor in the time-determining circuit and the tolerances of the diac may influence the accuracy of the instant when the thyristor is ignited. Components having a relatively small tolerance may be chosen for the capacitor and the resistor and diacs having a small tolerance are also commercially available. These components which are normally commercially available provide the possibility of building up a circuit arrangement functioning very accurately.

The invention will now be described in greater detail, by way of example, with reference to the accompanying drawings in which

Fig. 1 shows a first embodiment of a circuit arrangement according to the invention,

Fig. 2 shows a second embodiment of a circuit arrangement according to the invention,

Fig. 3 shows an application of the circuit arrangement of Fig. 1 for controlling a number of small incandescent lamps and for supplying a smoothed direct voltage,

Fig. 4 shows an application of the circuit arrangement of Fig. 2 for controlling a number of light-emitting diodes and for supplying a smoothed direct voltage as well,

Fig. 5 shows a vacuum cleaner with indicator lamps.

Fig. 1 shows a first embodiment of a circuit ar-

rangement according to the invention. The circuit arrangement has two input terminals k1 and k2 and two output terminals k3 and k4. The terminals k2 and k4 are interconnected. A series arrangement of the rectifier diode D1 and the switching transistor T1 is provided between the terminals k1 and k3. In this embodiment the switching transistor T1 is in the form of a MOS power transistor, but it may alternatively be a bipolar transistor. The series arrangement of a resistor R1 and capacitor C1 is provided between the terminals k1 and k2. The capacitor C1 is shunted by the diode D2. A series arrangement of a resistor R4 and a thyristor Th is provided between the node of D1 and T1 and the lead between the terminals k2 and k4. The gate terminal of the thyristor Th is controlled via a diac D3 arranged in a series with a current-limiting resistor R2, which diac D3 is connected to the node between R1 and C1. The gate terminal of the thyristor Th is also connected via a resistor R3 to the lead between the terminals k2 and k4. The output signal of the thyristor Th, present at the node between R4 and Th, is applied via a diode D4 to the gate terminal of the transistor T1. This gate terminal is also connected via a resistor R5 and a zener diode D5 to the lead between k2 and k4. Finally, a zener diode D6 is arranged between the gate and the drain of transistor T1.

The circuit arrangement of Fig. 1 operates as follows. During operation an alternating voltage is presented to the input terminals k1 and k2. At the start of the positive cycle of this alternating voltage the capacitor C1 will be charged via the resistor R1. The diode D2 is blocked and therefore does not have any influence on the charging process. At the instant when the voltage across the capacitor C1 reaches the ignition voltage of the diac D3, this diac D3 will be ignited so that a trigger signal is presented via R2 to the gate terminal of the thyristor Th. This thyristor Th will consequently become conducting and apply a signal via D4 to the gate of T1.

During the period when the diac D3 and also the thyristor Th are not yet conducting, the voltage at the gate of T1 will follow the mains voltage via R4 and D4, so that also the source of T1 and hence the voltage at the output terminal k3 will follow the mains voltage. However, at the instant when the thyristor Th is rendered conducting, the gate of transistor T1 will be pulled down so that the transistor T1 is turned off. At that instant the voltage at the output terminal k3 will decrease to substantially 0. The gate of T1 will be discharged via R5.

During the negative half cycle of the sinusoidal alternating voltage at the input terminals the diode D1 will be blocked so that no output voltage appears at the output terminals. In this cycle the diode D2 will conduct and the capacitor C1 will be discharged across this diode D2. The result is that the capacitor C1 has a fixed known initial voltage at each start of a positive half cycle of the alternating voltage. If small

tolerance components are chosen for R1 and C1 and if a component having an accurately known breakdown voltage with a small tolerance is also chosen for D3, the ignition instant of the thyristor Th is fixed within given narrow limits. It will be evident that the value of the output pulses at the output terminals k3 and k4 is unambiguously related to the ignition instant of the thyristor Th. The amplitude of the output pulses is also fixed by accurately defining this instant.

The two zener diodes D5 and D6 have not been described hereinbefore. Both diodes have a protective function. The zener diode D5 ensures that the voltage at the gate of the transistor T1 can never become higher than the predetermined maximum value. This prevents a relatively high voltage peak from appearing once at the output k3/k4 when switching on the alternating voltage at the terminals k1 and k2, with C1 being generally discharged completely. The diode D6 which is arranged across the source and the gate of T1 limits the maximum gate-source voltage to the zener voltage of this diode D6.

Fig. 2 shows another embodiment of the circuit arrangement according to the invention. A comparison of Figs. 1 and 2 shows that actually only the circuit around T1 is modified. The other components are therefore denoted by the same reference numerals. In Fig. 2 the gate of transistor T1 is directly connected via a resistor R6 to the node between the resistor R4 and the thyristor Th. Furthermore, the gate-source trajectory of transistor T1 is not only shunted by a zener diode D6 but also by a further diode D7 arranged in series with D6.

By coupling the gate of transistor T1 via a resistor R6 to the node between R4 and Th, it is achieved that the gate can be discharged after igniting the thyristor Th via R6 and the thyristor Th. As compared with Fig. 1, the number of components connected to the gate T1 is reduced from 3 to 1.

The diode D7 is only incorporated to counteract a possible negative influence on the operation of the transistor T1 caused by the presence of the zener diode D6. If necessary, such a diode may also be used at the same location in the circuit arrangement of Fig. 1. On the other hand this diode D7 is not always necessary.

Fig. 3 shows the application of the circuit arrangement of Fig. 1 for the control of a plurality of small incandescent lamps, and the part of the circuit arrangement between the terminals k1/k2 and k3/k4 is fully identical to the circuit arrangement of Fig. 1 and will therefore not be described in greater detail. The part receiving the supply from the circuit arrangement of Fig. 1 is arranged between the terminals k3/k4 and the further terminals k5/k6. A plurality of lamps and thyristors are arranged in series across the terminals k3 and k4. The lamps are denoted by L1, L2, L3 and the thyristors are denoted by Th1, Th2 and Th3. If, for example, the thyristor Th1 is rendered conducting by

a suitable signal at its gate terminal, the pulsatory direct voltage output signal across the terminals k3 and k4 will result in a pulsatory current through the incandescent lamp L1 so that the lamp will light up. Since the amplitude of the pulsatory current is accurately fixed because of the circuit arrangement according to the invention, even if relatively low values of this amplitude are concerned, known and normally available low-voltage lamps (for example, 6 V or 12 V lamps) can be used in this circuit arrangement, even if the full mains voltage of 220 V (or 110 V) is presented to the terminals k1 and k2. The lamps L2 and L3 can also be switched on by means of suitable signals at the gate terminals of the thyristors Th2 and Th3. The circuits for controlling the thyristors Th1, Th2 and Th3 do not play a role within the scope of the invention and are consequently not shown in detail.

On the right-hand side of the Figure a known smoothing circuit is shown, which comprises the resistor R7, the zener diode D8, the rectifier diode D9 and the capacitor C2, and this in such a manner that a smoothed direct voltage is available at the output terminals k5 and k6. This circuit is well known to those skilled in the art and does not require any further explanation.

This circuit arrangement can be used in, for example a vacuum cleaner. The lamps L1, L2 and L3 may then be indicator lamps indicating useful information to the user, such as the presence of a dust bag and/or whether it is full, and the power supplied to a vacuum cleaner with automatic or non-automatic power control.

In Fig. 4 the circuit arrangement of Fig. 2 is used for the control of a plurality of light-emitting diodes. These diodes could be arranged in the same way as the lamps L1, L2, L3 in Fig. 3. However, a special application is shown in Fig. 4. Firstly, a light-emitting diode D10 and a zener diode D11 are arranged in series across the terminals k3 and k4, which series arrangement is fed through a resistor R8. The same resistor R8 also feeds a second series arrangement of a thyristor Th4 and the light-emitting diodes D12 and D13. A switching transistor T2 whose base can be controlled in a manner not further shown is arranged parallel to D13. Furthermore, the gate terminal of Th4 is connected via a switching transistor T3 to the lead between the terminals k4 and k6. The base of T3 can also be controlled in a manner not further shown. The resistor R9 is required for the gate control of the thyristor Th4.

If the transistor T3 is turned off, the thyristor Th4 will not conduct. In that case the pulsatory output voltage at the terminals k3/k4 will only lead to a current through the circuit R8-D10-D11. It is assumed that the amplitude of the pulsatory voltage at the terminals k3/k4 is higher than the zener voltage of the diode D11. In that case only the diode D10 will convey a current and will emit light. However, if the thyristor Th4 is

rendered conducting by switching the transistor T3, a current may also start flowing through the circuit R8-Th4-D12-D13. The zener voltage across D11 must be chosen to be so high that a current will only start flowing through the circuit R8-Th4-D12-D13 when Th4 becomes conducting. In that case D10 will therefore not emit light but only D12 and possibly D13 will be able to emit light. D13 will emit light if T2 is turned off. However, if this transistor T2 is turned on, only D12 will light up.

Similarly as in Fig. 3, a smoothing circuit is also provided in Fig. 4 and its components have been denoted by the same reference numerals as those in Fig. 3.

Both in Fig. 3 and in Fig. 4 the smoothed direct voltage at the terminals k5/k6 may be used, for example, for supplying a control circuit (not shown) with which the thyristors Th1, Th2, Th3 are controlled in the case of Fig. 3 and with which the transistors T2, T3 are controlled in the case of Fig. 4.

Figure 5 shows a vacuum cleaner 10. It has, inter alia, a connection 11 for a hose, a lid 12 and a handle 13 of a space for accommodating a dust bag, and wheels for easily moving the vacuum cleaner. Furthermore, it has a number of small indicator lamps 21, 22 and 23 which light up, for example, when conditions occur which are important to the user. Such conditions are for example, "dust bag present", "dust bag full", and the power supplied by the motor in a power-controlled vacuum cleaner. According to the invention, the lamps 21, 22 and 23 are supplied by the circuit arrangement as described hereinbefore.

Claims

1. A circuit arrangement for deriving a direct voltage from an alternating voltage, particularly the mains alternating voltage, said circuit arrangement comprising:

- two input terminals (k1,k2),
- two output terminals (k3,k4) one of which is connected to one (k2) of the input terminals,
- a switching transistor (T1) whose main current path is connected between the other input terminal (k1) and the other output terminal (k3),
- a base control circuit for controlling the switching transistor, which base control circuit includes a thyristor (Th) which is connected via a resistor (R4) between the two input terminals (k1,k2), the node between the resistor and thyristor being connected to the control electrode of the switching transistor, and
- a time-determining circuit comprising a series arrangement of a resistor (R1) and a capacitor (C1) and a trigger element (D3) connected between the gate terminal of the thyristor



a suitable signal at its gate terminal, the pulsatory direct voltage output signal across the terminals k3 and k4 will result in a pulsatory current through the incandescent lamp L1 so that the lamp will light up. Since the amplitude of the pulsatory current is accurately fixed because of the circuit arrangement according to the invention, even if relatively low values of this amplitude are concerned, known and normally available low-voltage lamps (for example, 6 V or 12 V lamps) can be used in this circuit arrangement, even if the full mains voltage of 220 V (or 110 V) is presented to the terminals k1 and k2. The lamps L2 and L3 can also be switched on by means of suitable signals at the gate terminals of the thyristors Th2 and Th3. The circuits for controlling the thyristors Th1, Th2 and Th3 do not play a role within the scope of the invention and are consequently not shown in detail.

On the right-hand side of the Figure a known smoothing circuit is shown, which comprises the resistor R7, the zener diode D8, the rectifier diode D9 and the capacitor C2, and this in such a manner that a smoothed direct voltage is available at the output terminals k5 and k6. This circuit is well known to those skilled in the art and does not require any further explanation.

This circuit arrangement can be used in, for example a vacuum cleaner. The lamps L1, L2 and L3 may then be indicator lamps indicating useful information to the user, such as the presence of a dust bag and/or whether it is full, and the power supplied to a vacuum cleaner with automatic or non-automatic power control.

In Fig. 4 the circuit arrangement of Fig. 2 is used for the control of a plurality of light-emitting diodes. These diodes could be arranged in the same way as the lamps L1, L2, L3 in Fig. 3. However, a special application is shown in Fig. 4. Firstly, a light-emitting diode D10 and a zener diode D11 are arranged in series across the terminals k3 and k4, which series arrangement is fed through a resistor R8. The same resistor R8 also feeds a second series arrangement of a thyristor Th4 and the light-emitting diodes D12 and D13. A switching transistor T2 whose base can be controlled in a manner not further shown is arranged parallel to D13. Furthermore, the gate terminal of Th4 is connected via a switching transistor T3 to the lead between the terminals k4 and k6. The base of T3 can also be controlled in a manner not further shown. The resistor R9 is required for the gate control of the thyristor Th4.

If the transistor T3 is turned off, the thyristor Th4 will not conduct. In that case the pulsatory output voltage at the terminals k3/k4 will only lead to a current through the circuit R8-D10-D11. It is assumed that the amplitude of the pulsatory voltage at the terminals k3/k4 is higher than the zener voltage of the diode D11. In that case only the diode D10 will convey a current and will emit light. However, if the thyristor Th4 is

rendered conducting by switching the transistor T3, a current may also start flowing through the circuit R8-Th4-D12-D13. The zener voltage across D11 must be chosen to be so high that a current will only start flowing through the circuit R8-Th4-D12-D13 when Th4 becomes conducting. In that case D10 will therefore not emit light but only D12 and possibly D13 will be able to emit light. D13 will emit light if T2 is turned off. However, if this transistor T2 is turned on, only D12 will light up.

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Both in Fig. 3 and in Fig. 4 the smoothed direct voltage at the terminals k5/k6 may be used, for example, for supplying a control circuit (not shown) with which the thyristors Th1, Th2, Th3 are controlled in the case of Fig. 3 and with which the transistors T2, T3 are controlled in the case of Fig. 4.

Figure 5 shows a vacuum cleaner 10. It has, inter alia, a connection 11 for a hose, a lid 12 and a handle 13 of a space for accommodating a dust bag, and wheels for easily moving the vacuum cleaner. Furthermore, it has a number of small indicator lamps 21, 22 and 23 which light up, for example, when conditions occur which are important to the user. Such conditions are for example, "dust bag present", "dust bag full", and the power supplied by the motor in a power-controlled vacuum cleaner. According to the invention, the lamps 21, 22 and 23 are supplied by the circuit arrangement as described hereinbefore.

Claims

1. A circuit arrangement for deriving a direct voltage from an alternating voltage, particularly the mains alternating voltage, said circuit arrangement comprising:
 - two input terminals (k1,k2),
 - two output terminals (k3,k4) one of which is connected to one (k2) of the input terminals,
 - a switching transistor (T1) whose main current path is connected between the other input terminal (k1) and the other output terminal (k3),
 - a base control circuit for controlling the switching transistor, which base control circuit includes a thyristor (Th) which is connected via a resistor (R4) between the two input terminals (k1,k2), the node between the resistor and thyristor being connected to the control electrode of the switching transistor, and
 - a time-determining circuit comprising a series arrangement of a resistor (R1) and a capacitor (C1) and a trigger element (D3) connected between the gate terminal of the thy-



istor (Th) and the node between the said resistor (R1) and capacitor (C1), characterized in that the trigger element (D3) is constituted by a diac, in that the other input terminal (k1) is connected to an alternating voltage terminal via a rectifier diode (D1) arranged in the forward direction with the main current path of the switching transistor (T1), in that the said series arrangement of resistor and capacitor (C1) is connected between the alternating voltage terminal and the one input terminal (k1) and in that a diode (D2) is arranged across the capacitor (C1) in such a way that said diode conducts during the periods when the rectifier diode (D1) is blocked.

2. A circuit arrangement as claimed in Claim 1, characterized in that the control electrode of the switching transistor (T1) is connected to the one input terminal (k2) via a resistor (R5).
3. A circuit arrangement as claimed in Claim 1, characterized in that the control electrode of the switching transistor is connected via a resistor (R6) to the said node between resistor and thyristor (Th).
4. A circuit arrangement as claimed in Claim 1, 2 or 3, characterized in that a zener diode (D6) is arranged between the gate and the source or between the base and the emitter of the switching transistor (T1), the zener voltage of said diode being not higher than the maximum admissible gate-source voltage or base-emitter voltage, respectively, of the switching transistor.
5. A circuit arrangement as claimed in any one of the preceding Claims, characterized in that the control electrode of the switching transistor is connected to the one input terminal (k2) via a further zener diode (D5) whose zener voltage is equal to the maximum peak voltage allowed to occur across the output terminals during operation.
6. A circuit arrangement as claimed in any one of the preceding Claims, characterized in that one or more series arrangements each comprising a lamp (L1;L2;L3) and a thyristor (Th1;Th2;Th3) are connected between the output terminals.
7. A circuit arrangement as claimed in any one of Claims 1 to 5, characterized in that a first series arrangement of a light-emitting diode (D10) and a zener diode (D11) and at least a second series arrangement of a light-emitting diode (D12;D13) and a thyristor (Th4) are arranged between the output terminals, the zener voltage of the zener diode being higher than the voltage across the

second series arrangement if the thyristor in this arrangement conducts.

8. A circuit arrangement as claimed in Claim 7, characterized in that the second series arrangement includes a plurality of light-emitting diodes (D12,D13) which, with the exception of one diode, are each shunted by the main current path of a further switching transistor (T2).
9. A household appliance, particularly a vacuum cleaner, including a circuit arrangement as claimed in any one of the preceding claims.

Patentansprüche

1. Schaltungsanordnung zur Ableitung einer Gleichspannung aus einer Wechselspannung, insbesondere der Netzspannung, welche Anordnung folgende Elemente enthält:
 - zwei Eingangsklemmen (k1, k2)
 - zwei Ausgangsklemmen (k3, k4), von denen eine mit einer der Eingangsklemmen (k2) verbunden ist,
 - einen Schalttransistor (T1), dessen Leitungspfad zwischen die andere Eingangsklemme (k1) und die andere Ausgangsklemme (k3) geschaltet ist,
 - eine Basissteuerungsschaltung zur Steuerung des Schalttransistors, welche Basissteuerungsschaltung einen Thyristor (Th) enthält, der über einen Widerstand (R4) zwischen die beiden Eingangsklemmen (k1, k2) geschaltet ist, wobei der Verbindungspunkt zwischen dem Widerstand und dem Thyristor mit der Steuerelektrode des Schalttransistors verbunden ist, und
 - eine Zeitbestimmungsschaltung, die eine Reihenschaltung aus einem Widerstand (R1) und einem Kondensator (C1) enthält, sowie ein Triggerelement (D3), das zwischen den Gate-Anschluß des Thyristors (Th) und den Verbindungspunkt zwischen dem Widerstand (R1) und dem Kondensator (C1) geschaltet ist, dadurch gekennzeichnet, daß das Triggerelement von einem DIAC gebildet wird, daß die andere Eingangsklemme (k1) über eine Gleichrichterdiode (D1), die so angeordnet ist, daß ihre Durchlaßrichtung mit der des Leitungspfades des Schalttransistors (T1) übereinstimmt, mit einer Wechselspannungsanschlußklemme verbunden ist, daß die Reihenschaltung aus Widerstand und Kondensator (C1) zwischen die Wechselspannungsanschlußklemme und die eine Eingangsklemme (k2) geschaltet ist und daß eine Diode (D2) so entlang des Kondensators (C1) angeordnet



ist, daß diese Diode während der Zeiten, in denen die Gleichrichterdiode (D1) gesperrt ist, leitet.

2. Schaltungsanordnung nach Anspruch 1, dadurch gekennzeichnet, daß die Steuerelektrode des Schalttransistors (T1) mit der einen Eingangsklemme (k2) über einen Widerstand (R5) verbunden ist.
3. Schaltungsanordnung nach Anspruch 1, dadurch gekennzeichnet, daß die Steuerelektrode des Schalttransistors (T1) über einen Widerstand (R6) mit dem Verbindungspunkt zwischen Widerstand und Thyristor (Th) verbunden ist.
4. Schaltungsanordnung nach Anspruch 1, 2 oder 3, dadurch gekennzeichnet, daß eine Zenerdiode (D6) zwischen dem Gate und der Source oder zwischen der Basis und dem Emittor des Schalttransistors (T1) angeordnet ist, wobei die Zenerspannung der Diode nicht höher ist als die maximal zulässige Gate-Source- bzw. Basis-Emittor-Spannung des Schalttransistors.
5. Schaltungsanordnung nach einem der vorhergehenden Ansprüche, dadurch gekennzeichnet, daß die Steuerelektrode des Schalttransistors mit der einen Eingangsklemme (k2) über eine weitere Zenerdiode (D5), deren Zenerspannung gleich der maximal an den Ausgangsklemmen während des Betriebs zugelassenen Spitzenspannung ist, verbunden ist.
6. Schaltungsanordnung nach einem der vorhergehenden Ansprüche, dadurch gekennzeichnet, daß eine oder mehr Reihenschaltungen, die jeweils eine Lampe (L1; L2; L3) und einen Thyristor (Th1; Th2; Th3) enthalten, zwischen die Ausgangsklemmen geschaltet sind.
7. Schaltungsanordnung nach einem der Ansprüche 1 bis 5, dadurch gekennzeichnet, daß eine erste Reihenschaltung aus einer lichtemittierenden Diode (D10) und einer Zenerdiode (D11) und mindestens eine zweite Reihenschaltung aus einer lichtemittierenden Diode (D12; D13) und einem Thyristor (Th4) zwischen den Ausgangsklemmen angeordnet ist, wobei die Zenerspannung der Zenerdiode höher als die Spannung an der zweiten Reihenschaltung ist, wenn der Thyristor in dieser Schaltung leitet.
8. Schaltungsanordnung nach Anspruch 7, dadurch gekennzeichnet, daß die zweite Reihenschaltung eine Vielzahl lichtemittierender Dioden (D12, D13) enthält, die, mit Ausnahme einer der Dioden, jeweils durch den Leitungspfad eines wei-

teren Schalttransistors (T2) überbrückt sind.

9. Haushaltsgerät, insbesondere ein Staubsauger, der eine Schaltungsanordnung nach einem der vorhergehenden Ansprüche enthält.

Revendications

1. Circuit pour deduire une tension continue d'une tension alternative, en particulier la tension alternative du secteur, ledit circuit comportant:
 - deux bornes d'entrée (ki, k2)
 - deux bornes de sortie (k3, k4) dont l'une est reliée à une première borne d'entrée (k2),
 - un transistor de commutation (T1) dont le trajet de courant principal est relié entre l'autre borne d'entrée (k1) et l'autre borne de sortie (k3),
 - un circuit de commande de base pour commander le transistor de commutation, circuit de commande de base comprenant un thyristor (Th) relié, par l'intermédiaire d'une résistance (R4), entre les deux bornes d'entrée (ki, k2), le noeud situé entre la résistance et le thyristor étant relié à l'électrode de commande du transistor de commutation, et
 - un circuit de détermination de temps comportant un montage en série d'une résistance (R1) et d'un condensateur (C1) et un élément de déclenchement (D3) relié entre la borne de gachette du thyristor (Th) et le noeud situé entre lesdits résistance (R1) et condensateur (C1), caractérisé en ce que l'élément de déclenchement (D3) est constitué d'un diac, en ce que l'autre borne d'entrée (k1) est reliée à une borne de tension alternative (k1) par l'intermédiaire d'une diode redresseuse (D1) montée en sens direct, en série avec le trajet de courant principal du transistor de commutation (T1), en ce que ledit montage en série de la résistance et du condensateur (C1) est relié entre la borne de tension alternative (k1) et la première borne d'entrée (k2) et en ce qu'une diode (D2) est montée aux bornes du condensateur (C1) de manière que ladite diode est conductrice pendant les périodes dans lesquelles la diode redresseuse (D1) est bloquée.
2. Circuit selon la revendication 1, caractérisé en ce que l'électrode de commande du transistor de commutation (T1) est reliée à la première borne d'entrée (k2) par l'intermédiaire d'une résistance (R5).
3. Circuit selon la revendication 1, caractérisé en ce que l'électrode de commande du transistor de



commutation est reliée par l'intermédiaire d'une résistance (R6) audit noeud situé entre la résistance et le thyristor (Th).

4. Circuit selon la revendication 1, 2 ou 3, caracté- 5
risé en ce qu'une diode Zener (D6) est montée
entre la grille et la source ou entre la base et
l'émetteur du transistor de commutation (T1), la
tension Zener de ladite diode n'étant pas supé- 10
rieure à la tension de grille-source ou de base-
émetteur maximale admissible du transistor de
commutation.

5. Circuit selon l'une quelconque des revendica- 15
tions précédentes, caractérisé en ce que l'élec-
trode de commande du transistor de commuta-
tion est reliée à la première borne d'entrée (k2)
par l'intermédiaire d'une autre diode Zener (D5)
dont la tension Zener est égale à la tension de 20
crête maximale pouvant se produire aux bornes
de sortie pendant le fonctionnement.

6. Circuit selon l'une quelconque des revendica- 25
tions précédentes, caractérisé en ce qu'un ou
plusieurs montages en série, comportant chacun
une lampe (L1; L2; L3) et un thyristor (Th1; Th2;
Th3), sont reliés entre les bornes de sortie.

7. Circuit selon l'une quelconque des revendica- 30
tions 1 à 5, caractérisé en ce qu'un premier mon-
tage en série d'une diode électroluminescente
(D10) et d'une diode Zener (D11) et au moins un
deuxième montage en série d'une diode émettri-
ce de lumière (D12; D13) et d'un thyristor (Th4) 35
sont disposés entre les bornes de sortie, la ten-
sion Zener de la diode Zener étant plus élevée
que la tension aux bornes du deuxième montage
en série si le thyristor, dans ce montage, est
conducteur. 40

8. Circuit selon la revendication 7, caractérisé en ce 45
que le deuxième montage en série comprend plu-
sieurs diodes électroluminescentes (D12, D13)
qui, à l'exception d'une diode, sont toutes shun-
tées par le trajet de courant principal d'un autre
transistor de commutation (T2).

9. Appareil ménager, en particulier un aspirateur, 50
comprenant un circuit selon l'une quelconque des
revendications précédentes.