

Method for disintegrating an elastomer and
disintegrator

5 The present invention relates to a method for
disintegrating an elastomer and to a disintegrator for
disintegrating an elastomer, with the aid of which an
elastomeric item, in particular an elastomer strand
produced from chloroprene rubber, can be disintegrated
10 into slices that are as thin as possible, in order that
the disintegrated elastomer has a surface area that is
as large as possible, if for example it is to be
dissolved in a solvent, in order for example to produce
an adhesive.

15 It is known to disintegrate an elastomer with the aid
of a disintegrator, in which the elastomer is moved
with the aid of an advancing device over a base to a
cutting tool in the form of a peripheral miller, so
that the cutting tool can cut off individual slices
20 from the elastomer with the aid of a cutting wedge. A
disadvantage of such a disintegrator and such a method
for disintegrating an elastomer is that the elastomer
can deform when the cutting wedge is in contact with
the elastomer, whereby the elastomer may evade the
25 cutting edge of the cutting wedge. This has the effect
that a certain minimum thickness has to be provided for
the slices that are cut off, in order that a properly
planned disintegration of the elastomer can be achieved
at all. In the case of a twisted elastomer strand, a
30 minimum thickness of about 1.8 to 2.2 mm is therefore
required.

There is a constant need for disintegrating elastomers
into pieces that are as small, and in particular thin,
35 as possible without great effort, in order that for
example a specific surface area, that is to say outer
area per unit of weight, that is as large as possible
can be achieved for subsequent processes. The large

specific surface area allows the elastomer to be dissolved quickly in a solvent, in order in particular to produce an elastomer-based adhesive.

5 It is the object of the invention to provide a method for disintegrating an elastomer and a disintegrator for disintegrating an elastomer with the aid of which the specific surface area can be increased for the disintegrated elastomer, and in particular the layer
10 thickness of chips and/or slices that are cut off can be reduced.

The object is achieved according to the invention by a method for disintegrating an elastomer with the
15 features of claim 1 and a disintegrator for disintegrating an elastomer with the features of claim 12.

In the case of the method according to the invention
20 for disintegrating an elastomer, in particular at least one elastomer strand, the elastomer is moved in relation to a cutting tool over a base toward the cutting tool, the cutting tool having a cutting wedge with a cutting edge and a rake face adjoining the
25 cutting edge. According to the invention, once the cutting wedge comes into contact with the elastomer, the elastomer is initially at least partially compressed only by the rake face between the rake face and the base, before the cutting edge cuts through the
30 elastomer.

The movement of the cutting wedge of the cutting tool takes place in relation to the elastomer in a way that initially avoids linear contact of the cutting edge
35 with the elastomer, and instead there is surface-area contact of the rake face with the elastomer. The surface-area contact of the rake face with the elastomer has the effect that the force of the cutting

wedge acting on the elastomer is initially distributed over the relatively large rake face, so that initially a low force per unit area acts on the elastomer in comparison with a linear contact via the cutting edge.

5 This avoids spontaneous evasion of the elastomer. At the same time, the force per unit area gradually increases during the further movement of the cutting wedge, but the larger area causes a higher frictional force between the cutting wedge and the elastomer to be

10 achieved in comparison with a force applied linearly via the cutting edge. The higher friction avoids the possibility that the elastomer can move flexibly away from the cutting wedge due to stretching effects under the increasing loading. Only at a later point in time

15 when the elastomer has been sufficiently compressed by the rake face between the rake face and the base can the cutting wedge roll on the elastomer in such a way that substantially only the cutting edge of the cutting wedge is in contact with the elastomer, whereby part of

20 the elastomer can be cut off by the cutting wedge on account of the high shearing forces at the cutting edge. The cutting off of the elastomer may in this case take place after an initial holding by way of compressing and/or clamping of the elastomer between

25 the rake face and the base by means of wedge cutting or knife cutting, in particular by single-edged wedge cutting on an anvil, it being possible for the single-side wedge cutting edge to be formed by the cutting edge of the cutting wedge and the anvil to be formed by

30 the base. As a result, in a state in which it has elastically flipped up high from the base, the elastomer strand can be captured by the rake face on the flat rear side of the cutting wedge, then be pressed against the base and, in a position in which

35 the elastomer strand can substantially no longer elastically evade it, be cut by rolling of the cutting edge on the partially compressed elastomer strand and moving of the cutting wedge through the elastomer

strand in a wedge-like manner. The cutting edge of the cutting wedge may be moved past the base acting as an anvil, a minimum distance s of the cutting wedge from the base being in particular $10\text{ }\mu\text{m} \leq s \leq 2\text{ mm}$,
5 preferably $50\text{ }\mu\text{m} \leq s \leq 1\text{ mm}$, more preferably $150\text{ }\mu\text{m} \leq s \leq 700\text{ }\mu\text{m}$ and particularly preferably $300\text{ }\mu\text{m} \leq s \leq 500\text{ }\mu\text{m}$. During the movement of the cutting wedge past the base, the cutting edge is in particular not substantially parallel to the surface of the base but
10 angled in relation to the surface of the base, so that an angle bisector taken through the cutting edge is angled with respect to the surface of the base preferably by an angle α of $15^\circ \leq \alpha \leq 90^\circ$, in particular $30^\circ \leq \alpha \leq 60^\circ$, more preferably $40^\circ \leq \alpha \leq 55^\circ$
15 and particularly preferably $45^\circ \leq \alpha \leq 50^\circ$. The cutting off of the elastomer, for example by single-edged wedge cutting, takes place in this case by means of one cutting edge, and consequently without an opposing edge, whereby the maintenance costs for a second
20 cutting edge can be avoided. The fact that evasion of the elastomer can be avoided as a result of the surface-area contact by way of the rake face during the compressing of the elastomer means that it is possible to achieve particularly small layer thicknesses of the
25 pieces that are cut off from the elastomer, whereby a particularly large specific surface area, that is to say outer area per unit weight, is obtained for the disintegrated elastomer. The method is suitable in particular for disintegrating a latex strand of butyl
30 rubber or chloroprene rubber, in order for example to be able to produce a latex-based adhesive. Furthermore, it is possible to disintegrate more than one elastomer strand at the same time, in that for example two or more elastomer strands are fed next to one another to
35 the same cutting wedge of the cutting tool. If two or more elastomer strands are fed in, the disintegration capacity can be increased correspondingly.

The movements of the elastomer and the movement of the cutting wedge are preferably adapted to one another in such a way that slices that are cut off from the elastomer have a thickness t of $t \leq 1.5$ mm, in particular $t \leq 1.2$ mm, preferably $t \leq 1.0$ mm and particularly preferably $t \leq 0.8$ mm. On account of the particularly slender thicknesses of the pieces that are cut off from the elastomer, a correspondingly large specific surface area is obtained for the pieces cut off from the elastomer. The slices that are cut off have in particular a minimum thickness t of $t \geq 0.2$ mm, preferably $t \geq 0.4$ mm and particularly preferably $t \geq 0.6$ mm, in order to facilitate the handling of the slices that are cut off from the elastomer as bulk material.

In a preferred embodiment, the elastomer has a cut end facing the cutting tool, an oscillation between a bottom dead center, assigned to the base, and a top dead center, remote from the base, being imparted to the cut end of the elastomer by the cutting of the cutting tool, and the cutting wedge contacting the elastomer substantially whenever the cut end is substantially at the top dead center. The oscillation of the cut end of the elastomer, in particular the amplitude of the oscillation, may be dependent on the distance of the cut end of the elastomer from the nearest clamping or fixing of the elastomer, for example of a conveying roller. As a result, it may be that the oscillation of the cut end, in particular the amplitude, can be influenced by the arrangement and/or configuration of the roller for the conveyance of the elastomer, for example a roller arranged directly at the cutting tool and/or the cut end being able to bring about a smaller amplitude of the cut end than a roller further away from the cutting tool and/or the cut end. The distance of the roller from the cut end and/or cutting tool is in this case substantially dependent on

the diameter of the roller. In particular, the contact of the cutting wedge with the elastomer takes place with respect to the top dead center of the cut end with a phase shift φ of $\varphi \leq \pm 15^\circ$, in particular $\varphi \leq \pm 8^\circ$ and particularly preferably $\varphi \leq \pm 2^\circ$. The fact that the rake face of the cutting wedge contacts the elastomer substantially at the top dead center of the imparted up and down oscillation means that initially only small forces are exerted by the rake face on the elastomer, avoiding evasion of the elastomer. Compressing of the elastomer only takes place to a comparatively slight extent, if at all. As soon as the elastomer comes into contact with the base at the bottom dead center, an abutment, acting for example as an anvil against which the elastomer can be pressed by the cutting wedge in order to compress the elastomer, is formed by the base. The compressing of the elastomer and the cutting of the elastomer can then take place in a particularly short time period, so that substantially no blockages and/or longitudinal oscillations occur even with a continuously fed elastomer. Since the actual cutting only takes place in a particularly short time interval, a straight uniform cut is obtained. This makes it possible to produce the slices that are cut off from the elastomer with a uniform consistent quality over a relatively long time period. This makes it easier to maintain required product qualities with respect to the specific surface area of the pieces that are cut off from the elastomer at low cost.

Preferably, an angle α between the rake face and the base at the point in time of the beginning of the contact of the cutting wedge and the elastomer is $15^\circ \leq \alpha \leq 40^\circ$, in particular $20^\circ \leq \alpha \leq 35^\circ$ and preferably $25^\circ \leq \alpha \leq 30^\circ$. With such an angle α , a substantially parallel alignment of the rake face with the contacted surface of the elastomer is obtained when the rake face first comes into contact with the elastomer. This takes

into account in particular the fact that, on account of its own elasticity, the elastomer has sprung up from the base after a prior cutting operation. If the cutting tool is operated in a rotary manner, the center point of the rotary movement can be chosen particularly easily such that a rolling movement of the cutting wedge on the elastomer causes the cutting edge to be in substantially exclusive contact with the elastomer exactly at the intended beginning of the actual cutting process.

The cutting of the elastomer with the aid of the cutting edge preferably commences at a pressure p below a pressure p_k for the beginning of strain crystallizations of the elastomer, where in particular $0.20 \leq p/p_k \leq 0.95$, preferably $0.50 \leq p/p_k \leq 0.90$, more preferably $0.6 \leq p/p_k \leq 0.85$ and particularly preferably $0.7 \leq p/p_k \leq 0.80$. As a result, a strain crystallization of the elastomer that could change the product properties of the pieces that are cut off is reliably avoided. At the same time, it is possible to compress the elastomer with the aid of the rigid rake face to a pressure just below the strain crystallization, which makes a particularly high frictional force possible and also prevents an elastic evasive movement of the elastomer in the case of particularly small layer thicknesses. This makes it possible in the actual cutting process for particularly slender slices to be cut off cleanly from the elastomer with the aid of the cutting edge of the cutting wedge.

The rake face of the cutting wedge comes into contact with the elastomer particularly preferably on a peripheral surface of the elastomer. Contact of the cutting wedge with an end face of the elastomer facing the cutting tool is thereby avoided. This ensures that the chips that are cut off from the elastomer are substantially pieces in the form of slices with a

constant layer thickness and no irregularly cut-off corners.

In particular, the cutting edges of two successive cutting wedges are at a distance D , where, with respect to an effective diameter d of the elastomer, the distance D is $1.0 \leq D/d \leq 8.0$, in particular $1.5 \leq D/d \leq 6.0$, preferably $2.0 \leq D/d \leq 4.0$ and particularly preferably $D/d = 3.0 \pm 0.5$. This ensures that, with a moderate advancing rate for the elastomer in relation to the cutting tool, sufficient material of the elastomer gets between the cutting edges of two successive cutting wedges in order to make a clean cut possible. At the same time, it is possible to provide a sufficiently large space between two successive cutting wedges to be able to transport away from the elastomer the piece that is cut off from the elastomer. It may in this case be possible for the advancing rate of the elastomer to be synchronized with the rotational speed of for example a rotating cutting tool in dependence on the material properties of the elastomer, in particular the elasticity.

In particular, the cutting edge of the cutting wedge has a circumferential speed v of $1.0 \text{ m/s} \leq v \leq 50.0 \text{ m/s}$, in particular $10.0 \text{ m/s} \leq v \leq 35.0 \text{ m/s}$, preferably $20.0 \text{ m/s} \leq v \leq 30.0 \text{ m/s}$ and particularly preferably $25.0 \text{ m/s} \leq v \leq 27.0 \text{ m/s}$. The circumferential speed corresponds substantially to the cutting speed when cutting a piece from the elastomer and is chosen such that, while taking into account the elasticity of the elastomer, cutting of the elastomer can take place without any major problems. On account of the elasticity of the elastomer, the elastomer has a recovery, measured in accordance with DIN 53518, of in particular $\leq 30\%$, preferably $\leq 25\%$, more preferably $\leq 20\%$ and particularly preferably $\leq 15\%$.

Particularly preferably, the cutting tool rotates about a center point, the center point being offset in relation to a center line of the elastomer substantially perpendicularly to the direction of movement of the elastomer by a distance s , where in particular the distance s with respect to the effective diameter d of the elastomer is $0.4 \leq s/d \leq 1.0$, preferably $0.45 \leq s/d \leq 0.6$ and particularly preferably $0.5 \leq s/d \leq 0.55$. The fact that the center point of the rotating cutting tool is arranged off-center in relation to the elastomer, in particular of a twisted elastomer strand of chloroprene rubber, means that it is easier to achieve the effect that the cutting wedge exerts a force on the elastomer initially only with its rake face and only later with a cutting edge. The cutting tool is in particular offset by the distance s counter to the direction of gravitational force. This creates additional space below the cutting tool in the direction of gravitational force to allow the pieces that are cut off from the elastomer to be transported away from the elastomer.

The rake face is preferably inclined in the circumferential direction by an angle β in relation to a radius of the cutting tool running through the cutting edge, where in particular $20^\circ \leq \beta \leq 40^\circ$, preferably $25^\circ \leq \beta \leq 35^\circ$ and particularly preferably $\beta = 30^\circ \pm 2.5^\circ$. The inclination of the rake face allows a suitable rolling movement of the cutting wedge on the elastomer to be set.

Particularly preferably, an elastomer film, in particular chloroprene rubber, is twisted into a strand before the cutting. The twisting of the elastomer film provides the resultant strand with sufficiently high strength in order that individual pieces can be cut off from the strand.

The invention also relates to a disintegrator for disintegrating an elastomer, in particular an elastomer strand, which is suitable in particular for carrying out the method described above. The disintegrator has a cutting tool for cutting off slices from the elastomer, the cutting unit having a cutting wedge with a cutting edge and a rake face adjoining the cutting edge. The disintegrator also has an advancing device for moving the elastomer over a base toward the cutting unit. According to the invention, the advancement of the advancing device and the geometry of the cutting tool are made to match one another in such a way that, once the cutting wedge comes into contact with the elastomer, the elastomer is initially at least partially compressed only by the rake face between the rake face and the base, before the cutting edge cuts through the elastomer. The base may take the form of a fixed mounting on one side, for example in the form of a sliding plate, for the feeding of the elastomer. For example in the case of single-edged wedge cutting of the elastomer by the cutting edge of the cutting wedge, the base may be formed as an anvil. The fact that the elastomer is initially compressed by way of the rake face, which has a larger surface area in comparison with the cutting edge, means that an elastic evasive movement of the elastomer is avoided, so that particularly thin slices can be cut off from the elastomer and a particularly large specific surface area is obtained for the pieces that are cut off from the elastomer. In particular, the advantages that can be achieved on the basis of the method described above can be achieved with the aid of the disintegrator. The disintegrator may in particular be formed and developed in the way described above on the basis of the method. The disintegrator is suitable in particular for disintegrating a latex strand of butyl rubber or chloroprene rubber, in order for example to be able to produce a latex-based adhesive.

In particular, the position of the cutting tool in relation to the base can be set with the aid of at least one adjusting device. With the aid of the
5 adjusting device, the position of the cutting tool in the vertical direction and/or horizontal direction can be set in particular, whereby it is possible to adapt the compressing and cutting movement of the cutting wedge in dependence on the elasticity and effective
10 diameter of the elastomer. The adjusting device may for example have a fastening plate which is connected to the base and/or to the cutting tool and has at least one slot, so that, with the aid of screws, the base and/or the cutting tool can be fixed in various
15 positions in a way corresponding to the configuration of the slot.

Particularly preferably, the cutting tool is rotatably mounted and in particular provided with exchangeable
20 cutting wedges. The cutting wedges may for example be configured as exchangeable inserts, which can be quickly exchanged and can be detachably connected to the cutting tool. The cutting wedges may in particular be exchangeably screwed to the cutting tool.

25 The invention also relates to an elastomer slice which can be produced from chloroprene rubber and has a thickness t of $t \leq 1.5$ mm, in particular $t \leq 1.2$ mm, preferably $t \leq 1.0$ mm and particularly preferably $t \leq$
30 0.8 mm. The particularly slender thickness t produces a correspondingly large specific surface area for the elastomer slice, which can for example facilitate and accelerate dissolution of the elastomer slice in a solvent, in particular for the production of an
35 adhesive. The elastomer slice has in particular a minimum thickness t of $t \geq 0.2$ mm, preferably $t \geq 0.4$ mm and particularly preferably $t \geq 0.6$ mm, in order to facilitate the handling of the elastomer slice as bulk

material. The elastomer slice can preferably be produced by the method described above. In particular, the elastomer slice can be produced with the aid of the disintegrator described above. The elastomer slice may
5 in particular be formed and developed in the way described above on the basis of the method and the disintegrator. In particular, the elastomer slice that can be produced from a twisted strand of chloroprene rubber has a density ρ of $\rho = 1.23 \text{ g/cm}^3 \pm 0.02 \text{ g/cm}^3$.

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The elastomer slice is in particular formed as a substantially circular-cylindrical slice, the elastomer slice having in particular a diameter d of $1.0 \text{ cm} \leq d \leq 10.0 \text{ cm}$, preferably $2.0 \text{ cm} \leq d \leq 7.0 \text{ cm}$, more
15 preferably $2.5 \text{ cm} \leq d \leq 4.0 \text{ cm}$ and particularly preferably $d = 3.0 \text{ cm} \pm 0.3 \text{ cm}$.

In the case of a thickness $t = 1.0 \text{ mm}$, the elastomer slice preferably has a mass-related specific surface
20 area S_m of $S_m = 1.73 \text{ m}^2/\text{kg} \pm 0.2 \text{ m}^2/\text{kg}$. In the case of a thickness $t = 2.0 \text{ mm}$, a corresponding elastomer slice may have a mass-related specific surface area S_m of $S_m = 0.92 \text{ m}^2/\text{kg}$. In the case of a thickness $t = 4.0 \text{ mm}$, a corresponding elastomer slice may have a mass-related
25 specific surface area S_m of $S_m = 0.51 \text{ m}^2/\text{kg}$, while a corresponding elastomer slice with a thickness of $t = 8.0 \text{ mm}$ would merely have a mass-related specific surface area S_m of $S_m = 0.31 \text{ m}^2/\text{kg}$. In comparison with an elastomer slice with a thickness of $t = 4.0 \text{ mm}$, the
30 mass-related specific surface area S_m of the elastomer slice according to the invention in the case of a thickness of $t = 1.0 \text{ mm}$ is in any case about 3.4 times greater and, in comparison with an elastomer slice with a thickness of $t = 8.0 \text{ mm}$, the mass-related specific
35 surface area S_m of the elastomer slice according to the invention in the case of a thickness of $t = 1.0 \text{ mm}$ is even about 5.5 times greater. The mass-related specific surface area S_m is determined in particular according to

DIN ISO 9277:2003-05 Determination of the specific surface area of solids by gas adsorption using the BET method (ISO 9277:1995).

5 The invention is explained in more detail below with reference to the appended drawings on the basis of a preferred exemplary embodiment.

In the drawings:

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Figure 1 shows a schematic sectional view of a disintegrator;

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Figure 2 shows a schematic view of a detail of the disintegrator from Figure 1 in a first position;

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Figure 3 shows a schematic view of a detail of the disintegrator from Figure 1 in a second position;

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Figure 4 shows a schematic view of a detail of the disintegrator from Figure 1 in a third position;

Figure 5 shows a schematic view of a detail of the disintegrator from Figure 1 in a fourth position;

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Figure 6 shows a schematic view of a detail of the disintegrator from Figure 1 in a fifth position; and

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Figure 7 shows a schematic view of a detail of the disintegrator from Figure 1 in a sixth position.

The disintegrator 10 that is partially represented in Figure 1 has a rotating cutting tool 12, to the circumference of which multiple cutting wedges 14 in the form of exchangeable inserts are attached. With the aid of an advancing device 16, an elastomer 20 (not represented) can be moved by way of an advancing element in the form of a driven roller 18 over a base 22 toward the cutting tool 12. The roller 18 may have in particular radially outwardly protruding teeth, which can press themselves somewhat into the elastomer to be disintegrated, in order that the elastomer does not unintentionally slip backward during the disintegration. The base 22 can be adjusted in height with the aid of screwed connections 24. The pieces that are cut off from the elastomer 20 may be directed by way of a ramp 26, for example to a collecting container (not represented).

As represented in Figure 2, at the beginning of the cutting operation, a cut end 28 of the elastomer 20 facing the cutting tool 12 is located at a top dead center, which is located substantially at the maximum distance away from the base 22. A rake face 32 of the cutting wedge 20 adjoining a cutting edge 30 is substantially parallel to a peripheral surface 34 of the elastomer 20 in the upper region of the cut end 28. As represented in Figure 3, the rake face 32 makes substantially surface area contact with the peripheral surface 34 of the elastomer 20 located at the top dead center. As represented in Figure 4, the elastomer 20 is pressed by the rake face 32 of the cutting wedge 40 downward onto the base 20. As represented in Figure 5, in this case the elastomer 20 may be already compressed. As represented in Figure 6, at the moment when the compressed elastomer 20 arrives at the base 22, substantially only the cutting edge 30 can be in contact with the elastomer 20. As represented in Figure 7, after that the actual cutting takes place, by which

a piece in the form of a slice is cut off from the elastomer 20. Since the elastomer is continuously replenished by the advancing device 16, in the situation represented in Figure 7 the elastomer may
5 already be pressing with its peripheral surface against the cutting wedge 14 with some force and, after the cutting off of the piece in the form of a slice, spring upward until the cut end 28 has again reached the top dead center. The next cutting wedge 14 can subsequently
10 repeat the cutting process that is represented in Figures 2 to 7.

Claims

1. A method for disintegrating an elastomer (20), in particular at least one elastomer strand, in which
5 the elastomer (20) is moved in relation to a cutting tool (12) over a base (22) toward the cutting tool (12), the cutting tool (12) having a cutting wedge (14) with a cutting edge (30) and a rake face (32) adjoining the cutting edge (30), and
10 once the cutting wedge (14) comes into contact with the elastomer (20), the elastomer (20) is initially at least partially compressed only by the rake face (32) between the rake face (32) and the base (22),
15 before the cutting edge (30) cuts through the elastomer (20).
2. The method as claimed in claim 1, characterized in
20 that the movement of the elastomer (20) and the movement of the cutting wedge (14) are adapted to one another in such a way that slices that are cut off from the elastomer (20) have a thickness t of $t \leq 1.5$ mm, in particular $t \leq 1.2$ mm, preferably $t \leq 1.0$ mm and particularly preferably $t \leq 0.8$ mm.
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3. The method as claimed in claim 1 or 2, characterized in that the elastomer (20) has a cut end (28) facing the cutting tool (12), an
30 oscillation between a bottom dead center, assigned to the base (22), and a top dead center, remote from the base (22), being imparted to the cut end (28) of the elastomer (20) by the cutting of the cutting tool (12), and the cutting wedge (14)
35 contacting the elastomer (20) substantially whenever the cut end (28) is substantially at the top dead center, the contact of the cutting wedge (14) with the elastomer (20) in particular taking

place with respect to the top dead center of the cut end (28) with a phase shift ϕ of $\phi \leq \pm 15^\circ$, in particular $\phi \leq \pm 8^\circ$ and particularly preferably $\phi \leq \pm 2^\circ$.

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4. The method as claimed in one of claims 1 to 3, characterized in that an angle α between the rake face (32) and the base (22) at the point in time of the beginning of the contact of the cutting wedge (14) and the elastomer (20) is $15^\circ \leq \alpha \leq 40^\circ$, in particular $20^\circ \leq \alpha \leq 35^\circ$ and preferably $25^\circ \leq \alpha \leq 30^\circ$.
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5. The method as claimed in one of claims 1 to 4, characterized in that the cutting of the elastomer (20) with the aid of the cutting edge (32) commences at a pressure p below a pressure p_k for the beginning of strain crystallization of the elastomer (20), where in particular $0.20 \leq p/p_k \leq 0.95$, preferably $0.50 \leq p/p_k \leq 0.90$, more preferably $0.6 \leq p/p_k \leq 0.85$ and particularly preferably $0.7 \leq p/p_k \leq 0.80$.
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6. The method as claimed in one of claims 1 to 5, characterized in that the rake face (32) of the cutting wedge (14) comes into contact with the elastomer (20) on a peripheral surface (34) of the elastomer (20).
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7. The method as claimed in one of claims 1 to 6, characterized in that the cutting edges (30) of two successive cutting wedges (14) are at a distance D , where, with respect to the effective diameter d of the elastomer (20), the distance D is $1.0 \leq D/d \leq 8.0$, in particular $1.5 \leq D/d \leq 6.0$, preferably $2.0 \leq D/d \leq 4.0$ and particularly preferably $D/d = 3.0 \pm 0.5$.
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8. The method as claimed in one of claims 1 to 7,
characterized in that the cutting edge (30) of the
cutting wedge (14) has a circumferential speed v of
1.0 m/s $\leq v \leq$ 50.0 m/s, in particular 10.0 m/s $\leq v \leq$
5 35.0 m/s, preferably 20.0 m/s $\leq v \leq$ 30.0 m/s and
particularly preferably 25.0 m/s $\leq v \leq$ 27.0 m/s.
9. The method as claimed in one of claims 1 to 8,
characterized in that the cutting tool (12) rotates
10 about a center point, the center point being offset
in relation to a center line of the elastomer (20)
substantially perpendicularly to the direction of
movement of the elastomer (20) by a distance s ,
where in particular the distance s with respect to
15 the effective diameter d of the elastomer (20) is
 $0.4 \leq s/d \leq 1.0$, preferably $0.45 \leq s/d \leq 0.6$ and
particularly preferably $0.5 \leq s/d \leq 0.55$.
10. The method as claimed in one of claims 1 to 9,
20 characterized in that the rake face (32) is
inclined in the circumferential direction by an
angle β in relation to a radius of the cutting tool
(12) running through the cutting edge (30), where
in particular $20^\circ \leq \beta \leq 40^\circ$, preferably $25^\circ \leq \beta \leq$
25 35° and particularly preferably $\beta = 30^\circ \pm 2.5^\circ$.
11. The method as claimed in one of claims 1 to 10,
characterized in that an elastomer film, in
particular chloroprene rubber, is twisted into a
30 strand before the cutting.
12. A disintegrator for disintegrating an elastomer
(20), in particular an elastomer strand, in
particular for carrying out the method as claimed
35 in one of claims 1 to 11, having

a cutting tool (12) for cutting off slices from the
elastomer (20), the cutting tool (12) having a

cutting wedge (14) with a cutting edge (30) and a rake face (32) adjoining the cutting edge (30), and

5 an advancing device (16) for moving the elastomer (20) over a base (22) toward the cutting tool (12),

the advancement of the advancing device (16) and the geometry of the cutting tool (12) being made to match one another in such a way that, once the
10 cutting wedge (14) comes into contact with the elastomer (20), the elastomer (20) is initially at least partially compressed only by the rake face (32) between the rake face (32) and the base (22), before the cutting edge (30) cuts through the
15 elastomer (20).