

BANDPASS SIGMA-DELTA MODULATOR WITH ANTI-RESONANCE CANCELLATION

Technical Field

The present invention relates generally to a bandpass sigma-delta modulator, and more particularly to a bandpass sigma-delta modulator using an acoustic resonator or micro-mechanical resonator. The present invention also generally relates to the cancellation of the anti-resonance signal from a resonator and more particularly to a method and apparatus for cancelling the anti-resonance in micro-mechanical, surface acoustic wave (SAW) and bulk acoustic wave (BAW) resonators.

Background Art

Cellular telephone systems have become very popular in many countries throughout the world. Unfortunately, the specific standards adopted by different countries are often different and cellular devices from one country will not be operable within another system. Accordingly, completely different handsets are necessary if a person is operating in two different countries having different standards.

As a result of this difficulty, there have been some efforts to provide a single device that is operable in different countries having different standards. A technology known as software-defined radio (SDR) provides one solution to this problem. In the SDR system, the entire band of RF or IF signal is digitized and the channel is selected using a programmable digital filter. Thus, the SDR can be reconfigured through the software to suit different standards. However, this effort has not been completely successful because it requires a high-speed A/D converter that must have not only high-speed, but also provide adequate resolution. In the ideal SDR arrangement, the RF is directly digitized in the receiver. It requires that the A/D converter have a speed in the gigahertz range,

and also have a dynamic range over a 100 dB, which is equivalent to a 16-bit resolution. Among the various A/D converters, the sigma-delta A/D converter has promise in achieving the desired dynamic range. However, it is only achievable at a much lower frequency band. As the frequency increases, circuit imperfections become dominant and degrade the dynamic range of the A/D converter. At the gigahertz sampling frequency range, the highest dynamic range for the reported bandpass sigma-delta modulator is 75 dB, which only corresponds to a 12.5 bit resolution.

A sigma-delta A/D converter consists of a sigma-delta modulator and a digital filter. Figure 1 shows a typical arrangement of a bandpass sigma-delta modulator. The key element in the modulator is the resonator 2 which provides the quantization noise shaping. That is, the resonator acts as a bandpass filter in a band around its resonance frequency. The resonator needs to operate at a high frequency and have a high Q (quality factor) value. The output of the resonator is passed to a quantizer 3 which produces a digital "1" signal if its input exceeds a threshold and a digital "0" signal if the input is less than the threshold. This digital signal of a series of 0's and 1's becomes the output of the sigma-delta modulator. These signals are also fed back to a D/A converter 4, and the resultant analog signal is applied as a second input to summation device 1 which also receives the input to the modulator. The difference between the input and the feedback of the summation device produces an input to the resonator.

Figure 2 shows a typical output spectrum from a fourth order bandpass sigma-delta modulator where the quantization noise is shaped away from the resonance frequency, resulting in a very high dynamic range. The depth of the notch is related to the Q value of the resonator. The higher the Q value is, the deeper the notch. The noise shaping is also dependent on the order of the modulator. Higher order modulators provide better noise shaping and hence a higher dynamic range.

Typically, the resonator is made of one of three different electronic circuits, namely, a passive L-C tank, a transconductor-capacitor or a switch-capacitor. However, none of these circuits have been successful in the situation described. The first two circuits cannot achieve a high Q value due to parasitic losses and non-linearity. Typical Q values are around 10 and 40 for the integrated L-C tank

with and without Q enhancement, respectively. The enhanced Q value for the transconductor-capacitor resonator can be up to 300 at a frequency of several hundred MHz. The switch-capacitor resonator is restricted by its low resonant frequency (< 100 MHz) due to the slow settling behavior of the circuit. The use of these types of resonators prevents the sigma-delta modulator from achieving a high speed and high dynamic range at the same time as is required in an SDR situation. In order to achieve a workable SDR system, it is necessary to find a resonator which is usable in a sigma-delta modulator to achieve high speed and high dynamic range.

In these resonators, there are two modes of resonance, namely the series mode and the parallel mode. In the series mode, the impedance of the resonator is at a minimum. In the parallel mode, the impedance of the resonator is at a maximum. The frequency at which the series resonance occurs is referred to as the resonant frequency while the frequency at which the parallel resonance mode occurs is called the anti-resonant frequency.

Figure 11 is a graph showing the relationship between the frequency of the resonator and the admittance (inverse of impedance). A maximum point is seen at 21 which is the series resonance mode. This occurs at frequency f_r . A minimum point 22 is the parallel resonance mode which occurs at the anti-resonance frequency f_a .

Figure 12 shows a typical equivalent circuit for a resonator. It includes a static capacitance C_p , 23 which is connected in parallel to a series circuit of resistor R_m , 26, capacitor C_m , 25 and inductor L_m , 24. The static capacitance 23 alters the transfer function of the ideal resonator by introducing two transmission zeros. In different applications, the presence of the anti-resonance may be desirable, such as in filtering and making oscillators. However, in other situations, it is not desirable such as in the sigma-delta modulator of Figure 1 discussed above. The presence of anti-resonance makes it difficult to realize the transfer function of the modulator and therefore it is desirable that it be cancelled. Likewise, in other modulators and in other situations, it may be desirable to cancel the anti-resonance in order that the resonance peak is emphasized.

DISCLOSURE OF INVENTION

Embodiments of the present invention provide a bandpass sigma-delta modulator having high-speed and high-dynamic range.

Embodiments of the present invention provide a bandpass sigma-delta modulator using a micro-mechanical resonator.

Embodiments of the present invention provide a bandpass sigma-delta modulator utilizing an acoustic resonator.

Embodiments of the present invention provide a second order bandpass sigma-delta modulator having two D/A converters.

Embodiments of the present invention provide a fourth order sigma-delta modulator having two D/A converters and two summation devices.

Embodiments of the present invention provide a sigma-delta A/D converter including a sigma-delta modulator having a resonator of the micro-mechanical or acoustical type.

Embodiments of the present invention provide a method for canceling the anti-resonance in resonators.

Embodiments of the present invention provide a circuit for the cancellation of anti-resonance in resonators.

Embodiments of the present invention provide a method for the cancellation of anti-resonance in micro-mechanical and acoustic wave resonators.

Embodiments of the present invention provide a circuit for the cancellation of anti-resonance and micro-mechanical and acoustic wave resonators.

Embodiments of the present invention provide a circuit having a resonator and a cancellation network providing inputs to a subtractor.

Embodiments of the present invention provide a capacitor which acts as the cancellation network for a resonator.

Embodiments of the present invention provide a method and circuit for the cancellation of anti-resonance in micro-mechanical, SAW and BAW resonators.

In a first aspect of the invention, there is provided a resonator system, comprising: a resonator to receive an input signal and provide a first output signal at a first output; a cancellation network to receive said input signal and provide a second output signal at a second output; a subtractor having a positive input coupled to said first output and a negative input coupled to said second output to combine said first and second output signals and cancel at least a portion of an anti-resonance from said first output signal; and a first load and a second load coupled to said first output and said second output, respectively.

In a second aspect of the invention, there is provided a method comprising: receiving an input signal at an input of a resonator, the resonator having a resonator output coupled to a first load; receiving the input signal at an input of a cancellation circuit, the cancellation circuit having a cancellation circuit output coupled to a second load; and applying, via a subtractor, a first output signal from the cancellation circuit output to a second output signal from the resonator output to remove an anti-resonance portion from the second output signal.

In a third aspect of the invention, there is provided a wireless apparatus comprising: a radio adapted to receive a resonance signal; and a resonator system coupled to the radio, wherein the resonator system comprises: a resonator configured to output a signal, wherein the signal is filtered around a resonance frequency; and a cancellation network coupled to the resonator, and configured to remove an anti-resonance portion of the output signal to generate the resonance signal.

Briefly, these and other embodiments of the invention are achieved by using either a micro-mechanical resonator or an accoustical resonator as a bandpass filter which provides an output to a quantizer. The output of the quantizer acts as

the output of the modulator and is also fed back to two different D/A converters. The output of the two converters is adjusted by a gain and applied to a summation device, along with the input. The output of the summation device is applied as an input to the resonator. In the fourth order device, two resonators are used along with a second summation device. A cancellation network having a common input with a resonator and having an output which is subtracted from the output of the resonator is provided to cancel the anti-resonance.

BRIEF DESCRIPTION OF THE DRAWINGS

A more complete appreciation of the invention and many of the attendant advantages thereof will be readily obtained as the same becomes better understood by reference to the following detailed description when considered in connection with the accompanying drawings, wherein:

Figure 1 is a block diagram of a prior art bandpass sigma-delta modulator.

Figure 2 is a graph of the output spectrum from a typical fourth order modulator.

Figure 3 is a block diagram of a second order bandpass sigma-delta modulator using a micro-mechanical resonator according to the present invention.

Figure 4 is a graph of the output spectrum from the second order bandpass sigma-delta modulator of Figure 3.

Figure 5 block diagram of a fourth order bandpass sigma-delta modulator using micro-mechanical resonators.

Figure 6 is a graph of the output spectrum from a fourth order bandpass sigma-delta modulator according to Figure 5.

Figure 7 is a block diagram of the second order bandpass sigma-delta modulator using an acoustical resonator.

Figure 8 is a graph of the output spectrum from a second order bandpass sigma-delta modulator shown in Figure 7.

Figure 9 is a block diagram of a fourth order bandpass sigma-delta modulator using acoustical resonators.

Figure 10 is a graph showing the output spectrum from a fourth order bandpass sigma-delta modulator as shown in Figure 9.

Figure 11 is a graph illustrating the relationship between frequency and admittance of a resonator;

Figure 12 is an equivalent circuit for a prior art resonator;

Figure 13 is a circuit diagram of a first embodiment of the present invention;

Figure 14 is a detailed circuit diagram of the embodiment shown in Figure 13;

Figure 15 is a detailed circuit diagram of the second embodiment of the present invention;

Figure 16 is a graph of a frequency response for a resonator according to the prior art; and

Figure 17 is a graph of a frequency response for a resonator according to the present invention.

BEST MODES FOR CARRYING OUT THE INVENTION

Referring now to the drawings, wherein like reference numerals designate identical corresponding parts throughout the several views, and more particularly to Figure 3 which shows a second order sigma-delta modulator using a micro-mechanical resonator. The summing circuit 1 adds the analog input to two outputs from two gain stages. The sum forming the output of the summing circuit becomes the input to the micro-mechanical resonator 2. The resonator selectively passes the signal at its resonance frequency and attenuates signals at other frequencies. The output from the resonator is adjusted by gain stage G1, 6 and fed to quantizer 3. The signal is quantized to form a series of binary bits as in Figure 1 which form the output of the modulator. The output is also fed back as an input to a pair of D/A converters, DAC1, 4, and DAC2, 5. The converters are both one bit converters but have different output pulses. One is a return to zero converter, whereas the other is a half return to zero converter. As a result, they have different transfer functions in the frequency domain. The output of the converters are analog signals which are fed back to the summing circuit through gain stages G2, 7 and G3, 8. The value of the gains in G1-G3 may be either positive or negative and often the gains in the feedback path are negative so that the feedback is subtracted from the input signal in a similar fashion to Figure 1.

Since the micro-mechanical resonator 2 is a second order system, the bandpass modulator shown in Figure 3 is of the second order, and provides second order noise-shaping as shown in Figure 4. This modulator based on the micro-mechanical resonator is capable of digitizing the analog input signal, but with a limited resolution. Better resolution can be obtained using a fourth order modulator as will be described below. However, since the Q values of the micro-mechanical resonator can easily be greater than 1000 and even as high as 10,000, it is possible to have a high resonance frequency, up to a gigahertz using this type of resonator. Accordingly, the use of this different resonator allows the modulator to operate at the gigahertz sampling frequency range with good resolution.

Figure 5 illustrates a corresponding fourth order bandpass sigma-delta modulator using a micro-mechanical resonator. Input summing circuit 1 adds the input to the modulator and the feedback from 2 gain stages in a similar fashion to Figure 3. The output of the summing circuit is fed to micro-mechanical resonator 2 which produces an output to gain stage G1, 6. This output is then applied to the second summing circuit 9 along with two additional feedback signals. The sum of these signals is used as the input to the second micro-mechanical resonator 10 which also selectively passes the signal at the resonance frequency and attenuates the signal at other frequencies. This output is adjusted by gain stage G4, 11 and its output is applied to quantizer 3. The output of the quantizer is a series of digital bits as described above and forms the output of the modulator. This output is fed back to two converters D/A converters 4 and 5 in a similar fashion to Figure 3. However, in addition to the analog feedback signal being applied to gain stages G2 and G3 as in Figure 3, they are also applied to gain stages G5, 12, and G6, 13 as inputs to the second summing circuit 9.

The output is the output of a fourth order bandpass sigma-delta modulator having a digitized form of the input analog signal. By having two micro-mechanical resonators in the loop, this device provides fourth order noise-shaping as shown in Figure 6. This fourth order modulator using two micro-mechanical resonators is able to provide digitization of the analog signal with high resolution.

As in the embodiment of Figure 3, the gain stages can be either positive or negative, and either gain or attenuation, as necessary.

Another type of resonator which has superior performance to electronic resonators are acoustic resonators. A surface acoustic wave (SAW) resonator has a resonance frequency of 50 - 2,000 MHz. It also has a Q factor of 4,000 - 15,000. A film bulk acoustic resonator (FBAR) has a resonance frequency of 300 - 10,000 MHz and a Q factor of 100 to 1000. The use of these types of resonators in the bandpass sigma-delta modulator also produces a digital output with high resolution at high frequencies.

Figure 7 shows a bandpass sigma-delta modulator using an acoustic resonator 2. The remaining parts of the circuit operate in a similar fashion to that of Figure 3. Since the acoustic resonator 2 is a second order system, the bandpass sigma-delta modulator shown in Figure 7 is of second order and provides second order noise-shaping as shown in Figure 8. This modulator using an acoustic resonator is capable of digitizing the analog input signal, but with less resolution than a fourth order modulator.

Figure 9 shows such a fourth order bandpass sigma-delta modulator using acoustic resonators. This arrangement is similar to that shown in Figure 5, but uses acoustic resonators rather than micro-mechanical resonators. Since there are two acoustic resonators in the loop, the modulator provides a fourth order noise shaping as shown in Figure 10 and is therefore of fourth order. This fourth order bandpass sigma-delta modulator using acoustic resonators is able to provide the digitization of the analog signal with a high resolution at high frequency.

Figure 13 shows the system with anti-resonance cancellation. An input signal from the signal generator X_{in} 34, is applied to both resonator 27 and cancellation network 28. The output of the cancellation network is subtracted from the output of the resonator circuit in the subtractor 31. Lumped loads Z_{11} , 29 and Z_{12} , 30 are provided at the outputs of the resonator and cancellation network, respectively. These consist of the input impedances of the subtractor as well as parasitic impedances at the respective nodes. Capacitor C_{in} 33, is a lumped parasitic capacitance at the input node. The output of the subtractor X_o , 32, provides a signal with the anti-resonance being removed from the usual resonator output. This is accomplished as long as certain parameters of the cancellation network assume the proper values.

Figure 14 shows a more detailed cancellation circuit of the first embodiment. As shown, the lumped loads 29 and 30 are each replaced by a parallel circuit of a resistor and capacitor. Thus, load 29 is shown as including resistor R_{L1} , 35, and capacitor C_{L1} , 36. Likewise, load 30 includes resistor R_{L2} , 38, and capacitor C_{L2} , 37. In this arrangement, the cancellation network is merely a capacitor C_c , 39. The resonator 27 includes the equivalent circuit such as shown in Figure 12. In order for the anti-resonance to be cancelled, it is necessary for the following conditions to be met:

$$C_p = C_c, R_{L1} = R_{L2} \text{ and } C_{L1} = C_{L2}.$$

The presence of the parasitic capacitance 33 at the input node has no effect on the cancellation of the anti-resonance.

When these specific relationships are true, the output of the cancellation circuit is applied to the subtracting input of subtractor 31 to remove the anti-resonance part of the output curve from the resonator. Thus, by matching the parameters of the cancellation circuit to the parameters of various parts of the resonator part of the circuit, a signal is produced in the cancellation network which follows the anti-resonance signal. When this is subtracted from the output of the resonator, the anti-resonance part of the output is removed leaving the resonance part of the signal without having any anti-resonance. Thus, the output signal shown in Figure 16 which corresponds to the output of the resonator is then changed in the subtractor to produce an output such is shown in Figure 17 which does not include an anti-resonance.

Figure 15 shows a second embodiment where the lumped loads 29 and 30 are purely capacitive and thus, are indicated by capacitors C_{L1} , 36, and C_{L2} , 37. In this case, the anti-resonance cancellation can be achieved by the following simple condition:

$$\frac{C_p}{C_{L1}} = \frac{C_c}{C_{L2}}$$

In this case, it is only necessary that the ratio of capacitors C_p to C_{L1} be equal to that of C_c to C_{L2} . In this situation, the result is similar to that of the first

embodiment shown in Figure 14 and described in Figures 16 and 17.

Numerous additional modifications and variations of the present invention are possible in light of the above teachings. It is therefore to be understood that within the scope of the appended claims, the invention may be practiced otherwise than as specifically described herein.

CLAIMS

1. A resonator system, comprising:
 - a resonator to receive an input signal and provide a first output signal at a first output;
 - a cancellation network to receive said input signal and provide a second output signal at a second output ;
 - a subtractor having a positive input coupled to said first output and a negative input coupled to said second output to combine said first and second output signals and cancel at least a portion of an anti-resonance from said first output signal; and
 - a first load and a second load coupled to said first output and said second output, respectively.
2. A system according to claim 1, further comprising an input capacitance coupled to an input of said resonator and an input of said cancellation network.
3. A system according to claim 1, wherein said cancellation network includes a capacitor coupled between an input of said cancellation network and said second output.
4. A system according to claim 3, wherein said capacitor of said cancellation network comprises a capacitance substantially equal to a static capacitance of said resonator and wherein parameters of said first load and of said second load are substantially equal.
5. A system according to claim 4, wherein said first load includes a first load capacitor and said second load includes a second load capacitor, and wherein capacitances of said first load capacitor and said second load capacitor are substantially equal.

6. A system according to claim 4, wherein said first load includes a first load resistor and said second load includes a second load resistor and wherein resistances of said first load resistor and said second load resistor are substantially equal.

7. A system according to claim 4, wherein said first load includes only a first load capacitor and said second load includes only a second load capacitor, wherein a ratio of a static capacitance of the resonator to the first load capacitor is substantially equal to a ratio of the capacitance of the cancellation network to the second load capacitor.

8. The system according to claim 1, wherein said resonator includes a series circuit of a resistor, an inductor and a capacitor, wherein said series circuit has a first terminal connected to an input of said resonator and a second terminal connected to said first output of said resonator, and wherein said resonator also includes a static capacitor connected in parallel with said series circuit between said first terminal and said second terminal.

9. A method comprising:

receiving an input signal at an input of a resonator, the resonator having a resonator output coupled to a first load;

receiving the input signal at an input of a cancellation circuit, the cancellation circuit having a cancellation circuit output coupled to a second load; and

applying, via a subtractor, a first output signal from the cancellation circuit output to a second output signal from the resonator output to remove an anti-resonance portion from the second output signal.

10. The method of claim 9, wherein receiving the input signal at the input of the cancellation circuit comprises receiving the input signal at an input of a capacitor having a capacitance substantially equally to a static capacitance associated with the resonator.

11. A wireless apparatus comprising:
a radio adapted to receive a resonance signal; and
a resonator system coupled to the radio, wherein the resonator system comprises:
a resonator configured to output a signal, wherein the signal is filtered around a resonance frequency; and
a cancellation network coupled to the resonator, and configured to remove an anti-resonance portion of the output signal to generate the resonance signal.
12. The wireless apparatus of claim 11, wherein the resonator system further comprises a second resonator coupled to the output of the resonator, wherein the second resonator is configured to pass the signal at the resonance frequency.
13. The wireless apparatus of claim 11, wherein the resonator is one of a micro-mechanical resonator; an acoustic resonator, or a surface acoustic wave resonator.
14. The wireless apparatus of claim 11, wherein the resonator system further comprises a capacitor coupled to both the resonator and the cancellation network to provide an input capacitance to the resonator and the cancellation network.
15. The wireless apparatus of claim 11, wherein the cancellation network has one or more parameters matched to one or more corresponding parameters of the resonator to facilitate cancellation of the anti-resonance portion.
16. The wireless apparatus of claim 11, wherein the resonator system further comprises a first load coupled to the output of the resonator and a second load coupled to the output of the cancellation network