

Description

The invention relates to an amplifier arrangement having an input and an output and comprising, between a first and a second power-supply terminal, a first transistor having a control terminal coupled to the input of the amplifier arrangement, a first main terminal connected to a first end of a first resistor whose second end is coupled to the first power-supply terminal, and a second main terminal coupled to an input terminal of a first current multiplier circuit, which multiplier circuit has an output terminal for supplying the multiplied input current and a sum terminal for supplying the sum of the currents in the input terminal and the output terminal, which sum terminal is coupled to the input terminal of a second current multiplier circuit which has an output terminal for supplying the multiplied input current and a sum terminal for supplying the sum of the currents in the input terminal and the output terminals which sum terminal is coupled to the second power-supply terminal.

Such an amplifier arrangement may be used for various purposes in audio and video amplifiers and, in particular, as an input amplifier in a radio receiver.

Such a circuit arrangement is known from the article "A low-noise large dynamic range pulse amplifier" in Nuclear Instruments & Methods, Vol. 176, No. 1, 2 October 1980, pages 283—286. The output terminals of the first and the second current multiplier circuit in this arrangement are connected to the first end of the first resistor. The amplifier arrangement may be of the non-inverting type, in which case the output voltage is available across the first resistor, or of the inverting type, in which case the output voltage appears across a resistor which connects the sum terminal of the second current multiplier circuit to the second power-supply terminal. The first and the second current multiplier circuit provide stray negative feed-back for the amplifier arrangement, so that the output signal has only a low distortion. It is the object of the present invention to improve the known circuit arrangement in such a way that distortion is reduced even further.

If the arrangement is a non-inverting amplifier, in which the output terminal of the second current multiplier circuit is connected to the first end of the first resistor *via* a second resistor and in which the output of the amplifier arrangement is connected to that end of the second resistor which is remote from the first end, the output terminal of the first current multiplier circuit, in accordance with a first solution, may be connected to the first power-supply terminal and, in accordance with a second solution, it may be connected to that end of the second resistor which is remote from the first end. As a result of the negative feedback in the amplifier arrangement the current through the first resistor is always substantially undistorted. In the first embodiment the current through the second resistor is therefore substantially distortion-free, because the components causing the

distortion are drained to the first power-supply terminal *via* the first current multiplier circuit, so that substantially the same current will flow through the first resistor and through the second resistor. In the second embodiment the current through the second resistor is substantially distortion-free, because again the current through the second resistor is substantially the same as that through the first resistor.

If the resistance value of the second resistor is chosen to be zero, the non-inverting amplifier becomes a voltage-follower circuit.

If the amplifier arrangement operates as an inverting amplifier in which the sum terminal of the second current multiplier circuit is connected to the second power supply terminal *via* a third resistor and the output of the amplifier arrangement is connected to that end of the third resistor which leads to the sum terminal of the second current multiplier circuit, the output terminal of the first current multiplier circuit, in accordance with a third solution may be connected, by means of a capacitor to that end of the third resistor which leads to the sum terminal of the second current multiplier circuit.

The distortion of the output signal in the amplifier arrangements in accordance with the invention may be reduced even further if, in accordance with a further embodiment, at least a third current multiplier circuit is arranged between the second main terminal of the first transistor and the input terminal of the first current multiplier circuit, which third multiplier circuit has an output terminal to which the multiplied current from the input terminal is supplied and a sum terminal on which the sum of the currents in the input terminal and the output terminal appears and which is coupled to the input terminal of the first current multiplier circuit.

Embodiments of the invention will now be described in more detail, by way of example, with reference to the accompanying drawings, in which:

Figure 1 shows a known amplifier arrangement, Figure 2a shows the basic diagram of a known non-inverting amplifier arrangement,

Figure 2b shows a practical version of the arrangement shown in Figure 2a,

Figure 3 shows a first non-inverting amplifier arrangement in accordance with the invention,

Figure 4 shows a second non-inverting amplifier arrangement in accordance with the invention,

Figure 5 shows a known inverting amplifier arrangement,

Figure 6 shows a first inverting amplifier arrangement in accordance with the invention,

Figure 7 shows a third non-inverting amplifier arrangement in accordance with the invention, and

Figure 8 shows a second inverting amplifier arrangement in accordance with the invention.

Figure 1 shows a known amplifier arrangement which operates as a non-inverting amplifier. The arrangement comprises an NPN-transistor T_1

whose emitter 5 is connected to the negative power-supply terminal 2 by means of a resistor R_1 and whose base is connected to the input 4 of the amplifier arrangement, to which the input signal V_i is applied. The collector 6 of transistor T_1 is connected to the input 7 of a current multiplier circuit 8 comprising a resistor R_3 arranged in parallel with the base-emitter junction of a PNP-transistor T_2 . The sum terminal 9 of the current multiplier, which is the junction point of the emitter of transistor T_2 and the resistor R_3 , is connected to the positive power-supply terminal 3. The collector 10 of transistor T_2 is connected to the emitter 5 of transistor T_1 by means of a resistor R_2 . The output voltage V_o appears across the resistors R_1 and R_2 . Owing to the voltage division between R_1 and R_2 a fraction of this output voltage is applied to the emitter 5 of transistor T_1 , resulting in negative feedback. As a result of this negative feedback the voltage on the emitter 5 of transistor T_1 is substantially undistorted in comparison with the input voltage V_i applied to the base, so that the current through resistor R_1 is substantially undistorted. In order to obtain an undistorted output voltage the current through resistor R_2 should also be undistorted and, since the current through resistor R_1 is equal to the sum of the currents through resistor R_2 and transistor T_1 , the current through transistor T_1 should also be undistorted. However, the currents through transistor T_1 and resistor R_2 cannot both be undistorted, because the current through transistor T_1 is equal to the sum of the current through resistor R_3 and the base current of transistor T_2 , which currents both have a non-linear relationship with the collector current of transistor T_2 . Therefore, the current through resistor R_2 is distorted, so that the output voltage V_o is also distorted. The distortion of the output voltage also follows from the equation for the gain of the arrangement. If the transconductances of the transistors T_1 and T_2 are S_1 and S_2 , respectively it is easy to see that this gain is equal to:

$$A = V_o/V_i = \frac{\frac{1}{1+1/a} \cdot R_2/R_1 + 1}{1 + \frac{1}{S_1 R_1 (1+a)}} \quad (1)$$

where $a = S_2 R_3$ is the multiplication factor of the current multiplier. For simplicity the base currents of the transistors are ignored. If $D_1 = (1+1/a)^{-1}$ and $D_2 = S_1 R_1 (1+a)^{-1}$ this equation becomes

$$A = \frac{D_1 \cdot R_2/R_1 + 1}{1 + D_2} \quad (2)$$

The factors D_1 and D_2 depend on signal currents and are the factors which give rise to distortion. For a minimal distortion it is desirable that $D_1 = 1$ and $D_2 = 0$, which means maximal factor a and

maximal transconductance S_1 . However, increasing the bias current through transistor T_1 imposes limitations on the value of resistor R_3 and hence on the transconductance S_2 , and conversely, increasing the value of the resistor R_3 limits the bias current through transistor T_1 and consequently the transconductance S_2 . Therefore, the factors D_1 and D_2 cannot be made arbitrarily small.

Figure 2a shows the basic circuit diagram of a non-inverting amplifier arrangement known from the afore-mentioned article, in which similar parts bear the same reference numerals as in Figure 1. The first current multiplier circuit is shown schematically and bears the reference numeral 8. The sum terminal 9 of the current multiplier 8 is again connected to the positive power-supply terminal 3 and the output terminal 10 is again connected to the emitter 5 of the transistor T_1 via a resistor R_2 . The input terminal 7 is connected to the sum terminal 13 of the second current multiplier 14, whose input terminal 15 is connected to the collector 6 of transistor T_1 . In the present example the output terminal 16 is connected to the emitter 5 of transistor T_1 . If the transconductance of transistor T_1 is again S_1 and the multiplication factors of the current multipliers 8 and 14 are a and b , respectively, it follows readily that the gain satisfies the following relationship

$$A = \frac{\frac{1}{1+1/a} \cdot R_2/R_1 + 1}{1 + \frac{1}{S_1 R_1 (1+a+b)}} \quad (3)$$

Comparing formula (3) with formulas (1) and (2) shows that by the addition of the second current multiplier 14 the factor D_2 is reduced as a result of the increased loop gain, thereby also reducing the distortion of the output voltage.

Figure 2b shows a practical version of the arrangement shown in Figure 2a. The first current multiplier 8 is of the same type as the current multiplier in Figure 1, i.e. it comprises a resistor R_3 and a transistor T_2 . The current multiplier 14 is of the same type and comprises a resistor R_4 and a PNP-transistor T_3 whose base emitter junction is arranged in parallel with this resistor. If the transconductances of the transistors T_2 and T_3 are S_2 and S_3 , respectively, the multiplication factors in equation 3 are given by $a = S_2 R_3$ and $b = S_3 R_4$.

A first non-inverting amplifier arrangement in accordance with the invention is shown in Figure 3 in which identical parts bear the same reference numerals as in Figure 2b. The arrangement differs from that shown in Figure 2b in that the output terminal 16 of the second current multiplier is not connected to the emitter 5 of transistor T_1 but to the negative power supply terminal 2. If the transconductance of transistor T_1 is again S_1 and

the multiplication factors of the first and the second current multiplier are again $a=S_2R_3$ and $b=S_3R_4$, where S_2 and S_3 are the transconductances of transistors T_2 and T_3 , respectively, the gain will comply with:

$$A = \frac{\frac{1}{1 + \frac{1}{a+ab}} \cdot \frac{1}{R_2/R_1 + 1}}{1 + \frac{1}{S_1R_1(1+a+ab)}} \quad (4)$$

A comparison of formula (4) with formulas (1) and (2) shows that not only the factor D_2 has decreased but that the factor D_1 more closely approximates to the value 1. A comparison with formula (3) shows that compared with the arrangement of Figure 2 the arrangement of Figure 3 leads to an even further reduction of the distortion. This may be explained as follows. In order to obtain a distortion-free output voltage V_o , the currents through the resistors R_1 and R_2 must be undistorted. The negative feedback ensures that the current through the resistor R_1 is substantially undistorted. If it is assumed that the current through the resistor R_2 is undistorted, the current in the sum terminal 13 will be distorted owing to the non-linear relationship between the collector current of transistor T_2 and the current through resistor R_3 and between the collector current of T_2 and the base current of this transistor. Most of this distorted current, for example 90% in the case of a multiplication factor $b=9$, is drained to the negative power-supply terminal 2 via transistor T_3 . The current through the resistor R_2 is then substantially equal to the current through resistor R_1 , so that the current through resistor R_2 is substantially undistorted. In the arrangement of Figure 2b, if the same reasoning is adopted, the distorted current through transistor T_3 is fed to the first resistor, so that the current through resistor R_2 is not equal to the current through resistor R_1 and therefore neither is it undistorted.

Figure 4 shows a second non-inverting amplifier arrangement in accordance with the invention, in which identical parts bear the same reference numerals as in Figure 3. The arrangement differs from that in Figure 3 in that the output terminal 16 of the second current multiplier is not connected to the negative power-supply terminal 2 but to the output terminal 10 of transistor T_2 . It is easy to demonstrate that the gain of the circuit complies with:

$$A = \frac{\frac{1}{1 + \frac{1}{a+ab}} \cdot \frac{1}{R_2/R_1 + 1}}{1 + \frac{1}{S_1R_1(1+a+ab)}} \quad (5)$$

A comparison of this formula with formulas (1) and (2) again shows that the distortion is reduced because the factor D_2 has decreased and because the factor D_1 more closely approximates to the value 1. The reduced distortion may also be explained as follows. In order to obtain a substantially undistorted output voltage, the currents through resistors R_1 and R_2 should be substantially undistorted. The negative feedback ensures that the current through the resistor R_1 is substantially undistorted. As most of the current in sum terminal 13 is fed to the resistor R_2 via transistor T_3 , the current through the resistor R_2 is substantially equal to the current through resistor R_1 , so that the current through resistor R_2 is also substantially undistorted.

The value of the resistor R_2 in the arrangements of Figures 3 and 4 may be selected to be zero, so that the non-inverting amplifier becomes a voltage-follower circuit.

Figure 5 shows an amplifier arrangement known from said article and constructed as an inverting amplifier. Identical parts bear the same reference numerals as in Figure 4. The arrangement is operated as an inverting amplifier in that the sum terminal 9 of the first current multiplier is connected to the positive power-supply terminal 3 by means of a resistor R_5 and the output voltage V_o appears across this resistor R_5 . The output terminals 10 and 16 of the first and the second current multiplier circuit respectively are connected to the emitter 5 of transistor T_1 . The following equation can be derived in a simple manner for the gain of the arrangement:

$$A = \frac{\frac{R_4/R_1}{1 + \frac{1}{S_1R_1(1+a)(1+b)}}}{1 + D_2} = \frac{R_4/R_1}{1 + D_2} \quad (6)$$

It is simple to demonstrate that the second current multiplier the factor D_2 is reduced by a factor $(1+b)$ which also reduces the distortion.

A first inverting amplifier arrangement in accordance with the invention is shown in Figure 6, in which identical parts bear the same reference numerals as in Figure 5. By means of a capacitor C_1 the output terminal 16 of the second current multiplier circuit is connected to the sum terminal 9 of the first current multiplier and by means of a resistor R_6 it is connected to the negative power-supply terminal 2. The signal current through the resistor R_1 is substantially distortion-free owing to the negative feedback. For a distortion-free output

voltage the current through the resistor R_5 should be distortion-free. The current through resistor R_1 flows mainly through transistor T_2 , so that the current through this transistor is substantially distortion-free. Then the current through resistor R_3 and the base current of transistor T_2 are not distortion-free. For the greater part these distortion components are fed back to the first current multiplier circuit via transistor T_3 and capacitor C_1 , so that the distortion components appear in a closed loop and cannot reach the resistors R_1 and R_5 . The voltage across the resistor R_5 is therefore substantially distortion-free. The gain of the arrangement then complies with:

$$A = \frac{R_4/R_1}{1 + \frac{R_4/R_1}{SR_1(1+a+ab)}} = \frac{R_4/R_1}{1+D_2} \quad (7)$$

from which it readily follows that the factor D_2 is reduced by thus adding the second current multiplier circuit.

In the amplifier arrangements shown the distortion of the output voltage may be reduced even further by arranging at least a third current multiplier between the collector of transistor T_1 and the input terminal of the second current multiplier. This will be explained by means of two examples. A non-inverting amplifier arrangement as shown in Figure 4 provided with a third current multiplier is shown in Figure 7, in which identical parts bear the same reference numerals. The third current multiplier comprises a resistor R_7 arranged in parallel with the base-emitter junction of a transistor T_4 . The input terminal 19 is connected to the collector 6 of transistor T_1 and the sum terminal 18 is connected to the input terminal 15 of the second current multiplier. The output terminal 20 should now be connected to the negative power-supply terminal 2. Indeed, without the third current multiplier the difference between the currents through resistors R_1 and R_2 is equal to the current through transistor T_1 . As the current through resistor R_1 is substantially distortion-free owing to the negative feedback, the current through transistor T_1 determines the distortion of the current through the resistor R_2 . The third current multiplier substantially reduces the current through transistor T_1 , because the greater part of the incoming current is drained to the negative power-supply terminal via transistor T_4 . As a result of this, the current through resistor R_2 becomes more equal to the current through resistor R_1 , thereby reducing the distortion of the output signal.

Finally, Figure 8 shows an inverting amplifier arrangement as shown in Figure 6, employing a third current multiplier. In the present case the output terminal 20 of the third current multiplier should be connected to the emitter 5 of the transistor T_1 , because the current through resistor R_5 should be equal to the current through the resistor R_1 , as far as this is possible. The distortion is reduced by the increased loop gain.

The invention is not limited to the embodiments shown, many variants being possible within the scope of the claims. For example, instead of the current multipliers shown, any other type of current multiplier may be employed. Further, in order to increase the quiescent current in the arrangement, a current source may be arranged in series with the resistor R_1 , which source is decoupled for signal currents by means of a capacitor. The transistors in the present embodiments are all bipolar transistors. However, it is alternatively possible to replace all or some of the transistors by field-effect transistors. In the embodiments shown it may be advantageous, in particular, to replace only transistor T_1 by a field-effect transistor. Finally, it is to be noted that the arrangement may be constructed both in integrated and in discrete form.

Claims

1. An amplifier arrangement having an input and an output and comprising, between a first and a second power-supply terminal, a first transistor having a control terminal coupled to the input of the amplifier arrangement, a first main terminal connected to a first end of a first resistor whose second end is coupled to the first power-supply terminal, and a second main terminal coupled to an input terminal of a first current multiplier circuit which multiplier circuit has an output terminal for supplying the multiplied input current and a sum terminal for supplying the sum of the currents in the input terminal and the output terminal, which sum terminal is coupled to the input terminal of a second current multiplier circuit which has an output terminal for supplying the multiplied input current and a sum terminal for supplying the sum of the currents in the input terminal and the output terminal, which sum terminal is coupled to the second power-supply terminal, characterized in that the output terminal of the second current multiplier circuit is connected to the first end of the first resistor via a second resistor and the output of the amplifier arrangement is connected to that end of the second resistor which is remote from the first end, and in that the output terminal of the first current multiplier circuit is connected to the first power-supply terminal.

2. An amplifier arrangement having an input and an output end comprising, between a first and a second power-supply terminal, a first transistor having a control terminal coupled to the input of the amplifier arrangement, a first main terminal connected to a first end of a first resistor whose second end is coupled to the first power-supply terminal, and a second main terminal coupled to an input terminal of a first current multiplier circuit which multiplier circuit has an output terminal for supplying the multiplied input current and a sum terminal for supplying the sum of the currents in the input terminal and the output terminal, which sum terminal is coupled to the input terminal of a second current-multiplier circuit which has an output terminal for supplying the multiplied input

voltage the current through the resistor R_5 should be distortion-free. The current through resistor R_1 flows mainly through transistor T_2 , so that the current through this transistor is substantially distortion-free. Then the current through resistor R_3 and the base current of transistor T_2 are not distortion-free. For the greater part these distortion components are fed back to the first current multiplier circuit via transistor T_3 and capacitor C_1 , so that the distortion components appear in a closed loop and cannot reach the resistors R_1 and R_5 . The voltage across the resistor R_5 is therefore substantially distortion-free. The gain of the arrangement then complies with:

$$A = \frac{R_4/R_1}{1 + \frac{1}{SR_1(1+a+ab)}} = \frac{R_4/R_1}{1+D_2} \quad (7)$$

from which it readily follows that the factor D_2 is reduced by thus adding the second current multiplier circuit.

In the amplifier arrangements shown the distortion of the output voltage may be reduced even further by arranging at least a third current multiplier between the collector of transistor T_1 and the input terminal of the second current multiplier. This will be explained by means of two examples. A non-inverting amplifier arrangement as shown in Figure 4 provided with a third current multiplier is shown in Figure 7, in which identical parts bear the same reference numerals. The third current multiplier comprises a resistor R_7 arranged in parallel with the base-emitter junction of a transistor T_4 . The input terminal 19 is connected to the collector 6 of transistor T_1 and the sum terminal 18 is connected to the input terminal 15 of the second current multiplier. The output terminal 20 should now be connected to the negative power-supply terminal 2. Indeed, without the third current multiplier the difference between the currents through resistors R_1 and R_2 is equal to the current through transistor T_1 . As the current through resistor R_1 is substantially distortion-free owing to the negative feedback, the current through transistor T_1 determines the distortion of the current through the resistor R_2 . The third current multiplier substantially reduces the current through transistor T_1 , because the greater part of the incoming current is drained to the negative power-supply terminal via transistor T_4 . As a result of this, the current through resistor R_2 becomes more equal to the current through resistor R_1 , thereby reducing the distortion of the output signal.

Finally, Figure 8 shows an inverting amplifier arrangement as shown in Figure 6, employing a third current multiplier. In the present case the output terminal 20 of the third current multiplier should be connected to the emitter 5 of the transistor T_1 , because the current through resistor R_5 should be equal to the current through the resistor R_1 , as far as this is possible. The distortion is reduced by the increased loop gain.

The invention is not limited to the embodiments shown, many variants being possible within the scope of the claims. For example, instead of the current multipliers shown, any other type of current multiplier may be employed. Further, in order to increase the quiescent current in the arrangement, a current source may be arranged in series with the resistor R_1 , which source is decoupled for signal currents by means of a capacitor. The transistors in the present embodiments are all bipolar transistors. However, it is alternatively possible to replace all or some of the transistors by field-effect transistors. In the embodiments shown it may be advantageous, in particular, to replace only transistor T_1 by a field-effect transistor. Finally, it is to be noted that the arrangement may be constructed both in integrated and in discrete form.

Claims

1. An amplifier arrangement having an input and an output and comprising, between a first and a second power-supply terminal, a first transistor having a control terminal coupled to the input of the amplifier arrangement, a first main terminal connected to a first end of a first resistor whose second end is coupled to the first power-supply terminal, and a second main terminal coupled to an input terminal of a first current multiplier circuit which multiplier circuit has an output terminal for supplying the multiplied input current and a sum terminal for supplying the sum of the currents in the input terminal and the output terminal, which sum terminal is coupled to the input terminal of a second current multiplier circuit which has an output terminal for supplying the multiplied input current and a sum terminal for supplying the sum of the currents in the input terminal and the output terminal, which sum terminal is coupled to the second power-supply terminal, characterized in that the output terminal of the second current multiplier circuit is connected to the first end of the first resistor via a second resistor and the output of the amplifier arrangement is connected to that end of the second resistor which is remote from the first end, and in that the output terminal of the first current multiplier circuit is connected to the first power-supply terminal.

2. An amplifier arrangement having an input and an output end comprising, between a first and a second power-supply terminal, a first transistor having a control terminal coupled to the input of the amplifier arrangement, a first main terminal connected to a first end of a first resistor whose second end is coupled to the first power-supply terminal, and a second main terminal coupled to an input terminal of a first current multiplier circuit which multiplier circuit has an output terminal for supplying the multiplied input current and a sum terminal for supplying the sum of the currents in the input terminal and the output terminal, which sum terminal is coupled to the input terminal of a second current-multiplier circuit which has an output terminal for supplying the multiplied input



current and a sum terminal for supplying the sum of the currents in the input terminal and the output terminal, which sum terminal is coupled to the second power-supply terminal characterized in that the output terminal of the second current multiplier circuit is connected to the first end of the first resistor via a second resistor and the output of the amplifier arrangement is connected to the end of the second resistor which is remote from the first end, and in that the output terminal of the first current multiplier circuit is connected to the end of the second resistor which is remote from the first end.

3. An amplifier arrangement having an input and an output and comprising between a first and a second power-supply terminal, a first transistor having a control terminal coupled to the input of the amplifier arrangement, a first main terminal connected to a first end of a first resistor whose second end is coupled to the first power-supply terminal, and a second main terminal coupled to an input terminal of a first current multiplier circuit, which multiplier circuit has an output terminal for supplying the multiplied input current and a sum terminal for supplying the sum of currents in the input terminal and the output terminal which sum terminal is coupled to the input terminal of a second current multiplier circuit which has an output terminal for supplying the multiplied input current to the first end of the first resistor and a sum terminal for supplying the sum of the currents in the input terminal and the output terminal which sum terminal is connected to the second power-supply terminal via a third resistor and the output of the amplifier arrangement is connected to the end of the third resistor which leads to the sum terminal of the second current multiplier circuit, characterized in that the output terminal of the first current multiplier circuit is connected, by means of a capacitor, to that end of the third resistor which leads to the sum terminal of the second current multiplier circuit and by means of a second resistor to the second power supply terminal.

4. An amplifier arrangement as claimed in any one of the preceding claims, characterized in that at least a third current multiplier circuit is arranged between the second main terminal of the first transistor and the input terminal of the first current multiplier circuit, which third current multiplier circuit has an output terminal to which the multiplied current in the input terminal is supplied and a sum terminal on which the sum of the currents in the input terminal and the output terminal appears and which is coupled to the input terminal of the first current multiplier circuit.

Patentansprüche

1. Verstärkeranordnung mit einem Eingang und einem Ausgang, wobei die Anordnung zwischen einer ersten und einer zweiten Stromversorgungs-klemme einen ersten Transistor mit einer Steuerklemme, die mit dem Eingang der Verstärkeranordnung gekoppelt ist, ein erste Haupt-

klemme, die an ein erstes Ende eines ersten Widerstands angeschlossen ist, dessen zweites Ende mit der ersten Stromversorgungs-klemme gekoppelt ist, und eine zweite Hauptklemme enthält, die an eine Eingangsklemme einer ersten Stromverstärkerschaltung angeschlossen ist, die eine Ausgangsklemme zum Ausgeben des verstärkten Eingangsstroms und eine Summenklemme zum Ausgeben der Summe der an der Eingangsklemme und an der Ausgangsklemme vorhandenen Ströme enthält, wobei die Summenklemme mit der Eingangsklemme einer zweiten Stromverstärkerschaltung gekoppelt ist, die eine Ausgangsklemme zum Ausgeben des verstärkten Eingangsstroms und eine Summenklemme zum Ausgeben der Summe der an der Eingangsklemme und an der Ausgangsklemme vorhandenen Ströme enthält, und diese Summenklemme mit der zweiten Stromversorgungs-klemme gekoppelt ist, dadurch gekennzeichnet, daß die Ausgangsklemme der zweiten Stromverstärkerschaltung an das erste Ende des ersten Widerstands über einen zweiten Widerstand und der Ausgang der Verstärkeranordnung an das im Abstand vom ersten Ende liegende Ende des zweiten Widerstands angeschlossen sind, und daß die Ausgangsklemme der ersten Stromverstärkerschaltung an die erste Stromversorgungs-klemme angeschlossen ist.

2. Verstärkeranordnung mit einem Eingang und einem Ausgang, wobei die Anordnung zwischen einer ersten und einer zweiten Stromversorgungs-klemme einen ersten Transistor mit einer Steuerklemme, die mit dem Eingang der Verstärkeranordnung gekoppelt ist, eine erste Hauptklemme, die an ein erstes Ende eines ersten Widerstands angeschlossen ist, dessen zweites Ende mit der ersten Stromversorgungs-klemme gekoppelt ist, und eine zweite Hauptklemme enthält, die an eine Eingangsklemme einer ersten Stromverstärkerschaltung angeschlossen ist, die eine Ausgangsklemme zum Ausgeben des verstärkten Eingangsstroms und eine Summenklemme zum Ausgeben der Summe der an der Eingangsklemme und an der Ausgangsklemme vorhandenen Ströme enthält, wobei die Summenklemme mit der Eingangsklemme einer zweiten Stromverstärkerschaltung gekoppelt ist, die eine Ausgangsklemme zum Ausgeben des verstärkten Eingangsstroms und eine Summenklemme zum Ausgeben der Summe der an der Eingangsklemme und an der Ausgangsklemme vorhandenen Ströme enthält, und diese Summenklemme mit der zweiten Stromversorgungs-klemme gekoppelt ist, dadurch gekennzeichnet, daß die Ausgangsklemme der zweiten Stromverstärkerschaltung an das erste Ende des ersten Widerstands über einen zweiten Widerstand und der Ausgang der Verstärkeranordnung an das im Abstand vom ersten Ende liegende Ende des zweiten Widerstands angeschlossen sind, und daß die Ausgangsklemme der ersten Stromverstärkerschaltung an das im Abstand vom ersten Ende liegende Ende des zweiten Widerstands angeschlossen ist.



3. Verstärkeranordnung mit einem Eingang und einem Ausgang, wobei die Anordnung zwischen einen ersten und einer zweiten Stromversorgungsklemme einen ersten Transistor mit einer Steuerklemme, die mit dem Eingang der Verstärkeranordnung gekoppelt ist, eine erste Hauptklemme, die an ein erstes Ende eines ersten Widerstands angeschlossen ist, dessen zweites Ende mit der ersten Stromversorgungsklemme gekoppelt ist, und eine zweite Hauptklemme enthält, die an eine Eingangsklemme einer ersten Stromverstärkerschaltung angeschlossen ist, die eine Ausgangsklemme zum Ausgeben des verstärkten Eingangstroms und eine Summenklemme zum Ausgeben der Summe der an der Eingangsklemme und an der Ausgangsklemme vorhandenen Ströme enthält, wobei die Summenklemme mit der Eingangsklemme einer zweiten Stromverstärkerschaltung gekoppelt ist, die eine Ausgangsklemme zum Ausgeben des verstärkten Eingangsstroms nach dem ersten Ende des ersten Widerstands und eine Summenklemme zum Ausgeben der Summe der an der Eingangsklemme und an der Ausgangsklemme vorhandenen Ströme enthält, wobei die Summenklemme mit der zweiten Stromversorgungsklemme über einen dritten Widerstand und der Ausgang der Verstärkeranordnung mit jenem Ende des dritten Widerstands verbunden sind, das zur Summenklemme der zweiten Stromverstärkungsschaltung führt, dadurch gekennzeichnet, daß die Ausgangsklemme der ersten Stromverstärkerschaltung mittels eines Kondensators an jenes Ende des dritten Widerstands, das zur Summenklemme der zweiten Stromverstärkerschaltung führt, und mittels eines zweiten Widerstands an die zweite Stromversorgungsklemme angeschlossen ist.

4. Verstärkeranordnung nach einem oder mehreren der vorangehenden Ansprüche, dadurch gekennzeichnet, daß wenigstens eine dritte Stromverstärkungsschaltung zwischen der zweiten Hauptklemme des ersten Transistors und der Eingangsklemme der ersten Stromverstärkungsschaltung angeordnet ist, wobei die dritte Stromverstärkungsschaltung eine Ausgangsklemme, die mit dem verstärkten Strom an der Eingangsklemme beliefert wird, und eine Summenklemme enthält, an der die Summe der an der Eingangsklemme und an der Ausgangsklemme vorhandenen Ströme erscheint und die mit der Eingangsklemme der ersten Stromverstärkungsschaltung gekoppelt ist.

Revendications

1. Montage amplificateur muni d'une entrée et d'une sortie et comportant, entre une première et une deuxième borne d'alimentation, un premier transistor présentant une borne de commande couplée à l'entrée du montage amplificateur, d'une première borne principale connectée à une première extrémité d'une première résistance dont la deuxième extrémité est couplée à la première borne d'alimentation, et d'une

deuxième borne principale couplée à une borne d'entrée d'un premier circuit multiplicateur de courant, circuit multiplicateur qui comporte une borne de sortie pour l'amenée du courant d'entrée multiplié et une borne de somme pour l'amenée de la somme des courants à la borne d'entrée et la borne de sortie, borne de somme qui est couplée à la borne d'entrée d'un deuxième circuit multiplicateur de courant qui présente une borne de sortie pour l'amenée du courant d'entrée multiplié et une borne de somme pour l'amenée de la somme des courants à la borne d'entrée et la borne de sortie, cette borne de somme étant couplée à la deuxième borne d'alimentation, caractérisé en ce que la borne de sortie du deuxième multiplicateur de courant est connectée à la première extrémité de la première résistance par l'intermédiaire d'une deuxième résistance et en ce que la sortie du montage amplificateur est connectée à l'extrémité de la deuxième résistance opposée à la première extrémité, et en ce que la borne de sortie du premier circuit multiplicateur de courant est connectée à la première borne d'alimentation.

2. Montage amplificateur muni d'une entrée et d'une sortie et comportant, entre une première et une deuxième borne d'alimentation, un premier transistor présentant une borne de commande couplée à l'entrée du montage amplificateur, d'une première borne principale connectée à une première extrémité d'une première résistance dont la deuxième extrémité est couplée à la première borne d'alimentation, et d'une deuxième borne principale couplée à une borne d'entrée d'un premier circuit multiplicateur de courant, circuit multiplicateur de courant qui présente une borne de sortie pour l'amenée du courant d'entrée multiplié et une borne de somme pour l'amenée de la somme des courants à la borne d'entrée et la borne de sortie, borne de somme qui est couplée à la borne d'entrée du deuxième circuit multiplicateur de courant qui présente une borne de sortie pour l'amenée du courant d'entrée multiplié et une borne de somme pour l'amenée de la somme des courants à la borne d'entrée et la borne de sortie, cette borne de somme étant couplée à la deuxième borne d'alimentation, caractérisé en ce que la borne de sortie du deuxième circuit multiplicateur de courant est connectée à l'extrémité de la première résistance par l'intermédiaire d'une deuxième résistance et la sortie du montage amplificateur est connectée à l'extrémité de la deuxième résistance opposée à la première extrémité, et en ce que la borne de sortie du premier circuit multiplicateur de courant est connectée à l'extrémité de la deuxième résistance opposée à la première extrémité.

3. Montage amplificateur muni d'une entrée et d'une sortie et comportant, entre une première et une deuxième borne d'alimentation, un premier transistor présentant une borne de commande couplée à l'entrée du montage amplificateur, d'une première borne principale connectée à une première extrémité d'une première résistance



dont la deuxième extrémité est couplée à la première borne d'alimentation, et d'une deuxième borne principale couplée à une borne d'entrée d'un premier circuit multiplicateur de courant, circuit multiplicateur qui présente une borne de sortie pour l'amenée du courant d'entrée multiplié et une borne de somme pour l'amenée de la somme des courants à la borne d'entrée et la borne de sortie, borne de somme qui est couplée à la borne d'entrée d'un deuxième circuit multiplicateur de courant qui présente une borne de sortie pour l'amenée du courant d'entrée multiplié à la première extrémité de la première résistance et une borne de somme pour l'amenée de la somme des courants à la borne d'entrée et la borne de sortie, cette borne de somme étant connectée à la deuxième borne d'alimentation par l'intermédiaire d'une troisième résistance et la sortie du montage amplificateur est connectée à l'extrémité de la troisième résistance reliée à la borne de somme du deuxième

circuit multiplicateur de courant, caractérisé en ce que la borne de sortie du premier circuit multiplicateur de courant est connectée à l'aide d'un condensateur à l'extrémité de la troisième résistance reliée à la borne de somme du deuxième circuit multiplicateur de courant et à l'aide d'une deuxième résistance à la deuxième borne d'alimentation.

4. Montage amplificateur selon l'une des revendications précédentes, caractérisé en ce qu'au moins un troisième circuit multiplicateur de courant est disposé entre la deuxième borne principale du premier transistor et la borne d'entrée du premier circuit multiplicateur de courant, ce troisième circuit multiplicateur de courant présentant une borne de sortie à laquelle est amené le courant multiplié dans la borne d'entrée et une borne de somme à laquelle apparaît la somme des courants à la borne d'entrée et la borne de sortie et qui est couplée à la borne d'entrée du premier circuit multiplicateur de courant.

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