

Description

The present invention relates to a valve for controlling the flow of fluid between inlet and outlet ports and, more particularly, to a valve having a trim arrangement which will substantially prevent leakage above the maximum shut off leakage established by ANSI Leakage Class V even though the valve experiences temperatures in excess of 450 °F (about 232 °C).

Standards exist which establish seat leakage classifications for control valves according to a valve's ability to shut off flow when it is closed. These standards specify the amount of flow allowed through the valve at shut off. This amount of flow is usually measured as a percentage of the rated valve capacity when a specified differential pressure is applied across the inlet and outlet ports of the valve. For example, ANSI standards provide that, for Leakage Class II, the maximum seat leakage through a valve shall not exceed 0.5% of its rated valve capacity at shut off. Similarly, Leakage Classes III and IV permit seat leakages of no more than 0.1% and 0.01%, respectively, of rated valve capacity to flow through the valve at shut off.

In order to determine whether or not a particular valve design meets the requirements of Leakage Classes II, III and IV, an air or water leakage test is performed on the valve while the valve is in its closed position. Typically, this air or water leakage test is performed by coupling an air or water supply to the inlet port of a closed valve and measuring the amount of leakage through the valve.

On the other hand, a valve which satisfies the requirements of Leakage Class V is tested using a water leakage test wherein a source of water is coupled to the inlet port of the valve and the amount of water flowing through the valve while it is in its closed position is measured. According to Leakage Class V, the maximum seat leakage through the valve is only 0.0005 milliliters of water per minute, per 2.5 cm (inch) of port diameter, per 6.9 kPa (psi) differential pressure from inlet port to outlet port. As an example, if the valve has 5 cm (two inch) diameter ports and the source of water connected to the inlet port is at 690 kPa (100 psi) with respect to the pressure at the outlet port, then 0.1 milliliter of water is permitted to flow through the valve per minute when the valve is in its closed position. If the flow exceeds this amount, the valve does not meet the requirements of ANSI Leakage Class V.

In addition to meeting the requirements of the desired ANSI Leakage Class, it is also advantageous for the valve to have a balanced valve plug. A balanced valve plug is one having substantially equal areas against which the internal fluid pres-

ures of the valve act so that the net forces acting on the valve plug as a result of these pressures will be minimized. By minimizing these net forces, the size of the actuator necessary to overcome these net forces and move the valve plug is also minimized.

The United States Patent US-A 4 712 769, which provides the basis for the preamble of claim 1, discloses a high temperature balanced valve trim. The trim means for controlling fluid flow between an inlet and outlet port comprise a valve cage having cage openings, a lower valve seat and a valve plug having an opening therethrough for equalizing pressure across the valve plug. A seal forming member is provided which is resiliently compressible, which is acted upon by a compressing element when the valve is closed. Upon sufficient compression, the sealing member bulges outwardly forming a tight seal around the valve plug.

Another prior art double port valve such as shown in Figure 1 is often used to balance the net forces acting on the valve plug to thereby minimize the actuator force necessary to position the plug. The double port valve shown in Figure 1 has a valve plug 11 carrying two lands 12 and 13. The land 12 cooperates with a seat ring 14 at the upper port and the land 13 cooperates with a seat ring 15 at the lower port to control the flow of fluid from an inlet 16 to an outlet 17.

The surface areas of the lands 12 and 13 cannot be made exactly equal because, when the plug 11 is inserted through the top of the valve during valve assembly, the land 13 must be small enough that it can pass through the seat ring 14. On the other hand, the land 12 must be larger than land 13 so that land 12 does not pass through the seat ring 14 but instead seats against seat ring 14. Thus, the land 12 is larger than the land 13.

Because the area of the land 12 is larger than the land 13, the fluid pressure from the inlet 16 near or at shut off will exert a greater force on the land 12 than on the land 13. The resulting net force is in a direction to oppose closing of the valve. This net force must be overcome by the actuator in order to close the valve.

The surface areas of the lands 12 and 13 are, however, nearly equal so that the net force exerted on the valve plug 11 is small. However, because it is very difficult to machine the lands and seat rings to the tight tolerances necessary to prevent leakage at shut off and to maintain thermal expansion differences at a minimum, it is consequently very difficult to manufacture this double port valve so that it will meet the maximum leakage requirements of Leakage Class V, especially at high operating temperatures.

Shown in Figure 2 is a prior art double seat valve which is designed to meet the leakage re-

quirements of Leakage Class V and to minimize the size of the valve's actuator. The valve shown in Figure 2 has a valve plug 21 positioned by a valve stem 22 which enters the valve through a typical bonnet 23 and a valve packing 24. The valve plug 21 has a two part construction which includes a pilot plug 25 and a primary plug 26. The primary plug 26 cooperates both with openings 27 in a cage 28 and with a lower valve seat in the form of a seat ring 31 to control the flow of fluid between valve ports 29 and 30. The primary plug 26 is moved away from the seat ring 31 by virtue of a washer 32 attached to the end of the pilot plug 25 by a nut 33 and is moved toward the seat ring 31 by virtue of a plurality of springs only two of which, springs 37 and 38, are shown.

The pilot plug 25 has openings 35 and 36 therein so that the fluid pressures above and below the pilot plug 25 will be equal. Thus, when the valve is to be opened, the forces acting on the pilot plug 25 caused by fluid pressure on both of its sides are relatively balanced. The valve stem 22 lifts the pilot plug 25 away from an upper valve seat 34 formed in the primary plug 26 to allow the pressure on both sides of the primary plug 26 to equalize through openings 39 in the primary plug 26.

When the valve is to be closed, the valve stem 22 drives the primary plug 26 in a direction so that it will seat against the seat ring 31. The springs 37 and 38 exert a force between the pilot plug 25 and the primary valve plug 26 to keep the port between the pilot plug 25 and the upper valve seat 34 open to maintain the pressures across the primary plug 26 balanced until the primary plug 26 is seated against the lower valve seat 31. When the primary plug 26 is seated against the lower valve seat 31, the valve stem 22 will cause the pilot plug 25 to seat against the upper valve seat 34 completing closure of the valve.

Thus, the force necessary to move the primary plug 26 to, and away from, the seat ring 31 is minimized, and minimum actuator size is needed to open and/or close the valve of Figure 2. This double seat arrangement allows the valve to achieve Leakage Class V shut off. However, the valve construction shown in Figure 2 is complicated, requires a plurality of springs, and contains numerous parts which require tight machining tolerances.

In the valve according to the present invention, a trim arrangement is provided in the valve to prevent leakage through the valve above the maximum shut off leakage established by ANSI Leakage Class V. This trim arrangement reduces the unbalanced forces which act on the valve. Furthermore, this trim arrangement also can withstand temperatures of about 450°F (about 232°C) and

above so that the valve can be used in those high temperature applications which require leakage Class V shut off.

According to the present invention, a valve is provided as defined in claim 1. Embodiments of the valve arrangement are given in the claims 2 to 19. The valve of the present invention includes a valve body having inlet and outlet ports and a valve stem extending through the valve body. A trim arrangement is provided within the valve for controlling flow of fluid between the inlet and outlet ports. The trim arrangement includes a valve cage having cage openings therein, a lower valve seat and a valve plug attached to the valve stem. The valve plug prevents fluid flow between the inlet and outlet ports when the valve plug is positioned by the valve stem against the lower valve seat. On the other hand, the valve plug allows flow between the inlet and outlet ports when the valve plug is positioned by the valve stem away from the lower valve seat. The valve plug has an opening therethrough for equalizing pressure across the valve plug when positioned against the lower valve seat.

Seal means are provided to seal against leakage between the valve plug and the valve cage, where the seal is adapted to provide a mechanical spring force when the valve plug is positioned approximate to or against the lower valve seat.

The valve plug according to the invention further comprises first and second plug perimeters. In addition the valve cage has first and second cage perimeters substantially commensurate with the first and second plug perimeters respectively. An upper valve seat is formed by either the valve plug or the valve cage by means of these perimeters. The seal means are arranged to cooperate with the upper valve seat when the valve is closed.

The seal means are advantageously arranged to prevent fluid leakage through the valve above the maximum leakage allowed by ANSI Leakage Class V. The seal is preferably a ring seal, more preferably a C-ring, a V-ring or an S-ring.

In one embodiment, the seal may be captured at a cage ledge formed by the cage perimeters. Alternatively, the plug perimeters can form a plug ledge so that the seal is captured at the plug ledge by a retainer. In a further embodiment, the valve plug may have first, second and third plug parameters forming a recess in which the seal is located. In a still further embodiment, the valve plug can have two plug parts for clamping the seal therebetween.

Preferably, the seal material comprises a metal for withstanding temperatures of about 450°F (about 232°C) or higher. These high temperature seals may be a C-ring, a V-ring or an S-ring. The mechanical spring force of these types of seals compensates for the machining tolerances and di-

mensional variations caused by temperature changes.

In another embodiment of the invention, the trim arrangement includes a valve cage having an inner surface area defined by the two cage perimeters. The inner surface also comprises a slope which forms the upper valve seat. In this arrangement, the seal is preferably in the form of a ring having a ring opening oriented in the direction of travel of the valve stem and valve plug. A retainer may be included to retain the seal to the valve plug.

These and other advantages will become more apparent from the following description of embodiments taken in conjunction with the drawings in which:

Figure 1 is a cross-sectional view of a prior art double port valve;

Figure 2 is a cross-sectional view of a prior art double seat valve;

Figure 3 is cross-sectional view of a valve and a trim arrangement having a C-ring seal according to one embodiment of the invention;

Figure 3A is an enlarged cross-sectional view of a part of the trim arrangement shown in Figure 3;

Figure 3B is a top view of the valve plug shown in Figures 3 and 3A, and illustrates that the unbalance area of the valve is annular;

Figure 4 shows the trim arrangement of Figure 3 except that the C-ring has an orientation in order to accommodate flow through the valve in an opposite direction;

Figure 5 shows a trim arrangement having a V-ring seal instead of the C-ring seal shown in Figures 3 and 4;

Figure 6 shows a trim arrangement having an S-ring seal instead of the C-ring seals shown in Figures 3 and 4 or the V-ring seal shown in Figure 5;

Figure 7 shows an alternative trim arrangement for retaining a C-ring seal; and,

Figures 8 and 8A show an alternative trim arrangement having a C-ring seal arranged to further minimize the unbalance area of the valve.

Detailed Description

As shown in Figure 3, a valve 40 includes a valve body 41 having ports 42 and 43 either of which may be designated as an inlet port and the other of which may be designated as an outlet port depending upon the direction of flow through the valve. For the flow direction shown by arrows 44 in Figure 3, the port 42 is the inlet port and the port 43 is the outlet port. A trim arrangement 45 controls the flow of fluid between the ports 42 and 43. The trim arrangement 45 includes a valve plug 47,

a valve cage 48, and a lower valve seat in the form of a seat ring 46. The seat ring 46 has an opening 49 and the valve cage 48 has a plurality of openings 50 through which fluid can flow when the valve is in its open position.

A bonnet 51 is affixed to the valve body 41 by suitable means such as bolts 52 and nuts 53. A gasket 54 is located between the valve body 41 and the seat ring 46 and a gasket 55 is located between the bonnet 51 and both the valve cage 48 and the valve body 41. When the bonnet 51 is affixed to the valve body 41, the bonnet 51 compresses the gasket 55 between the bonnet 51 and both the valve body 41 and the cage 48 and also compresses the gasket 54 between the seat ring 46 and the valve body 41 in order to contain fluid within the valve body 41. The bonnet 51 also compresses the cage 48 against the seat ring 46 for retaining the seat ring 46 within the valve body 41.

A valve stem 56 extends through the bonnet 51 and into the valve body 41. Conventional valve packing and seals (not shown) may be provided around the valve stem 56. Affixed to the valve stem 56, such as by suitable threads, is the valve plug 47 which cooperates with the seat ring 46 for controlling the flow of fluid through the valve 40. As shown in Figure 3, when the valve plug 47 is closed, the valve plug 47 seats against the seat ring 46, covers the openings 50 through the cage 48, and closes on a C-ring 63 (to be further described hereinbelow) in order to shut off the flow of fluid from the port 42 to the port 43. When the valve plug 47 is open, the valve plug 47 is withdrawn from the seat ring 46 by the valve stem 56 and fluid is allowed to flow from the port 42, through the openings 50 in the cage 48, through the opening 49 in the seat ring 46, and to the port 43. The valve plug 47 may include a conventional piston ring 57 to minimize leakage between the cage 48 and the valve plug 47 while the valve plug 47 is throttling flow through the valve 40.

The cage 48 has a first cage perimeter 58 and a second cage perimeter 59 forming a cage ledge 60. The valve plug 47 has a first plug perimeter 61 substantially commensurate with the first cage perimeter 58 and a second plug perimeter 62 substantially commensurate with the second cage perimeter 59. The difference between the first plug perimeter 61 and the second plug perimeter 62 forms a plug ledge or upper valve seat 65. Thus, when the valve 40 is closed, the lower portion of the valve plug 47 seats against the lower valve seat in the form of the seat ring 46 and the C-ring seal 63 is pressed against the upper valve seat 65 and the cage ledge 60 in order to shut off flow through the valve 40. The C-ring seal 63 is held against the cage ledge 60 by a retainer 64. The retainer 64,

which may be a wire snap ring, will maintain the C-ring seal 63 against the cage ledge 60 as the valve plug 47 is stroked by the valve stem 56. Accordingly, the C-ring seal 63 remains substantially stationary as the valve plug 47 travels. It is to be noted that the C-ring seal 63 is in compression only when the valve plug 47 is in its closed position. As a result, wear on the C-ring seal 63 and on the upper valve seat 65 is minimized or prevented.

The orientation of the C-ring seal 63 shown in Figure 3 accommodates flow through the valve 40 from the port 42 to the port 43. The C-ring seal 63 provides a substantially fluid tight seal between the valve plug 47 and the cage 48 when the valve plug 47 is positioned against the seat ring 46. That is, when the valve 40 is closed so that the valve plug 47 is positioned against the seat ring 46, the C-ring seal 63 provides a seal against any leakage through the valve 40 between the valve plug 47 and the cage 48. Any fluid attempting to leak through the valve 40 between the valve plug 47 and the cage 48 will enter the opening of the C-ring seal 63 and press the C-ring seal 63 more tightly against the upper valve seat 65 and the cage ledge 60 to increase the seal between the valve plug 47 and the cage 48. The mechanical spring force of the C-ring seal 63 compensates for the machining tolerances and dimensional variations caused by temperature changes.

The valve plug 47 has openings 66 in order to balance the pressures acting across it. Thus, because of the openings 66, the pressures in volume 67 above the valve plug 47 and in volume 68 below the valve plug 47 will be equal and would result in generally equal but opposite internal fluid forces being applied to the valve plug 47 except for the unbalance area of the valve plug 47. This unbalance area can best be seen from Figure 3A.

Figure 3A is an enlarged cross-sectional view of that part of the trim arrangement 45 which includes the C-ring seal 63, the upper valve seat 65, and the lower valve seat provided by the seat ring 46. The dimensions of Figure 3A are exaggerated for clarity. As shown in Figure 3A, when the valve 40 is closed, the lower portion of the valve plug 47 is seated against the seat ring 46 and the C-ring seal 63 is pressed against the upper valve seat 65. However, because of the openings 66 through the valve plug 47, outlet pressure is applied against both the upper and lower sides of the valve plug 47. These upper and lower sides have generally equal areas except for the area of the valve stem which can be minimized but must be present. Since the pressures in the volumes 67 and 68 are thus equal and act against generally equal areas, these pressures will exert generally equal but opposite forces on the valve plug 47. These generally equal but opposite forces will off-

set one another. However, there will be an area of the valve plug 47 which will be exposed to different pressures resulting in non-offsetting forces being applied to the valve plug 47. This area is unbalance area 69 and, as best shown in Figure 3B, is annular.

This unbalance area 69 has an outer radius defined by the point at which the C-ring seal 63 contacts the upper valve seat 65 and an inner radius defined by the point at which the lower portion of the valve plug 47 contacts the seat ring 46. (The annular area 111 of the valve plug 47 between the annular area 69 and the point of contact between the piston ring 57 and the first cage perimeter 58 does not contribute to the unbalance area. The pressure above the valve plug 47 exerts a downward force against the area 111. This pressure also leaks down passed piston ring 57 to the area between ledges 60 and 65 outside the C-ring seal 63 and exerts an upward force upon the area 111 of the plug 47 to counter the downward force.) The lower side of this unbalance area 69 is exposed to inlet pressure because of the leakage between valve plug 47 and cage 48 which will fill the C-ring seal 63. The upper side of this unbalance area, at the top of the valve plug 47, is exposed to the outlet pressure in the volume 67. If these pressures are different, as they will most often be, a resulting net force will be applied to the valve plug 47 which must be overcome by the valve actuator when the valve is to be closed. This net force is proportional to the difference between these pressures multiplied by the unbalance area. As can be seen from Figures 3 and 3A, because the size of this unbalance area is small, the net force acting on the valve plug 47 due to this unbalance area is also small so that a smaller actuator is required to close the valve plug 47 against the seat ring 46 than would be the case with prior art valves. This trim arrangement allows Leakage Class V shut off when the valve plug 47 is positioned against the seat ring 46. Furthermore, the C-ring seal 63 may be made of a suitable material, such as Inconel X750 or 718 metal, so that the valve 40 can withstand high temperatures, such as those in the neighborhood of about 232°C (450°F) and above. (It is also necessary, of course, to suitably select materials for the other parts of valve 40.)

The trim arrangement of Figure 3 is shown in Figure 4 (wherein like reference numerals are used to depict like elements) except for the orientation and retaining of the C-ring seal. Accordingly, the C-ring seal 70 of Figure 4 has an orientation to accommodate flow in the direction of the arrow, i.e. in the opposite direction through the valve 40. As shown in Figure 4, the C-ring seal 70 has its opening directed in the opposite direction to the

opening of the C-ring seal 63 shown in Figure 3. In the case of Figure 4, any fluid attempting to leak through the valve 40 when it is closed will tend to flow between the valve plug 47 and the cage 48 (with this flow direction, the cage ledge 60 now becomes the upper valve seat) from the volume 67 to the port 42. This fluid will fill the C-ring seal 70 through its outwardly directed opening and will press the C-ring seal 70 more tightly against the cage ledge 60 of the cage 48 and the plug ledge 65 thus increasing the seal between the valve plug 47 and the cage 48. With the trim arrangement of Figure 4, the unbalance area is defined as the area of the valve plug 47 between the point where the C-ring seal 70 contacts the upper valve seat (i.e. the cage ledge 60 for the flow direction shown in Figure 4) and the point where the lower portion of the valve plug 47 contacts the seat ring 46. This trim arrangement also allows the valve to achieve Leakage Class V shut off at high temperatures.

Moreover, whereas the retainer 64 retains the C-ring seal 63 against the cage ledge 60 in Figure 3 so that the C-ring seal 63 does not move with the valve plug 47, the retainer 71 of Figure 4 retains the C-ring seal 70 to the valve plug 47. Accordingly, the C-ring seal 70 moves with the valve plug 47.

The trim arrangement of Figure 4 is shown in Figure 5 (with like reference numerals used for like elements) except that, instead of the C-ring seal 70 of Figure 4, a V-ring seal 72 is provided in the arrangement of Figure 5. The V-ring seal 72 is held to the valve plug 47 by a retainer 73. Although the arrangement shown in Figure 5 accommodates flow through the valve 40 from the port 43 to the port 42 (in the direction of the arrow), it should be apparent that flow from the port 42 to the port 43 can also be accommodated by reversing the orientation of the V-ring seal 72 shown in Figure 5 so that the opening of the V-ring seal 72 points inwardly instead of outwardly. Furthermore, as in the case of the C-ring seals shown in Figures 3 and 4, the V-ring seal 72 may be made of a suitable metal so that the valve 40 can operate in high temperature environments with Leakage Class V shut off.

The trim arrangement shown in Figure 6 is similar to the trim arrangement of Figure 3 (like reference numerals being used to depict like elements). However, as shown in Figure 6, an S-ring seal 74 is used instead of the C-ring seal 63 shown in Figure 3. In Figure 6, the valve plug 75 has a two-part construction. Accordingly, a first plug part 76 and a second plug part 77 are suitably attached (such as by threads) to the valve stem 56. The first plug part 76 of the valve plug 75 has a first plug perimeter 78 commensurate with the first cage perimeter 58 of the cage 48. Similarly, the second plug part 77 of the valve plug 75 has a second

plug perimeter 79 commensurate with the second cage perimeter 59. The S-ring seal 74 is clamped between the first plug part 76 and the second plug part 77 of the valve plug 75 so that the S-ring seal 74 will travel along with the valve plug 75 when the valve plug 75 is stroked by the valve stem 56.

The trim arrangement shown in Figure 6 will accommodate flow (in the direction of the arrow) from the port 43 to the port 42 of the valve 40 shown in Figure 3. Any fluid tending to leak between the valve plug 75 and the cage 48 will force S-ring 74 more tightly against the cage ledge 60 in order to increase the seal against such leakage. Accordingly, the design shown in Figure 6 can also attain Leakage Class V shut off. Furthermore, as in the case of the C-ring seals shown in Figures 3 and 4 and the V-ring seal shown in Figure 5, the S-ring seal 74 may be made of a suitable metal to allow the valve 40 to operate in high temperature environments. A conventional piston ring 80 may be included in the first plug part 76 of the valve plug 75 to minimize leakage between the cage 48 and the valve plug 75 while the valve plug 75 is throttling flow through the valve.

The trim arrangement shown in Figure 7 is similar to, and can be used in place of, the trim arrangement 45 of Figure 3 (like reference numerals being used to depict like elements). However, as shown in Figure 7, the valve plug 81 has a two part plug construction in order to form a recess within which the C-ring seal 82 may be retained. Thus, a first plug part 83 of the valve plug 81 has a first plug perimeter 84 commensurate with the inner cage perimeter 58 and a second plug part 85 of the valve plug 81 has a second plug perimeter 86 commensurate with the inner cage perimeter 59. The first plug part 83 of the valve plug 81 also has a third plug perimeter 87. The third plug perimeter 87 is smaller than either the first plug perimeter 84 or the second plug perimeter 86 in order to form a recess within which to retain the C-ring seal 82. Thus, a wire snap ring or other suitable retainer is not necessary for retaining the C-ring seal 82.

The trim arrangement shown in Figure 7, like the trim arrangement of Figure 4, will accommodate flow (in the direction of the arrow) from the port 43 to the port 42 of the valve 40. Flow from the port 42 to the port 43 can be accommodated by reversing the orientation of the C-ring seal 82. As shown in Figure 7, any fluid tending to leak between the valve plug 81 and the cage 48 will press the C-ring seal 82 more tightly against the cage ledge 60 and the plug ledge 65 in order to increase the seal against such leakage. Accordingly, the design shown in Figure 7 can also attain Leakage Class V shut off. Furthermore, as in the case of the C-ring seals shown in Figures 3 and 4, the V-ring seal shown in Figure 5, and the S-ring

seal of Figure 6, the C-ring seal 82 may be made of a suitable metal so that valve 40 can operate in high temperature environments. A conventional piston ring 88 may be included in the first plug part 83 of the valve plug 81 to minimize leakage between the cage 48 and the valve plug 81 while the valve plug 81 is throttling flow through the valve.

The unbalance areas of the valve plugs shown in Figures 5, 6 and 7 may be defined in the same manner as the unbalance areas of the valve plugs 47 shown in Figures 3, 3A and 3B were defined.

The trim arrangement shown in Figure 8 can be used in the valve 40 in place of the trim arrangement shown in Figure 3. The trim arrangement of Figure 8, however, further reduces the unbalance area of the valve plug. The trim arrangement of Figure 8 includes a valve cage 90, a valve plug 92, a C-ring seal 101, a seal retainer 102, and a lower valve seat 93 in the form of a seat ring. The valve cage 90 of Figure 8 has openings 91 to allow fluid to flow between the inlet and outlet ports of the valve 40 when the valve plug 92 is withdrawn from the lower valve seat 93. A valve stem 94 positions the valve plug 92 with respect to the lower valve seat 93 in order to control the flow of fluid through the valve. The valve plug 92 may be suitably attached to the valve stem 94 such as by threads.

The valve plug 92 has a first plug perimeter 95 substantially commensurate with a first cage perimeter 96 and a second plug perimeter 97 which is smaller than the first plug perimeter 95 to form a groove 98 between the valve plug 92 and the cage 90.

The cage 90 has a second cage perimeter 99. The inner surface of the cage 90 has a slope 100 to accommodate the difference between the first cage perimeter 96 and the somewhat larger second cage perimeter 99. The slope 100 forms an upper valve seat for the valve. The C-ring seal 101 is located within the groove 98 and has its opening either pointed downwardly (as shown in Figure 8) or upwardly (not shown) depending upon the direction of flow through the valve 40. Thus, the opening of the C-ring seal 101 is substantially parallel to the axis of travel of the valve stem 94. If fluid flow is from the port 42 to the port 43, the C-ring seal 101 is oriented with its opening pointed downward as shown in Figure 8 in order to provide a fluid tight seal at shut off. The seal retainer 102 is suitably attached, such as by threads, to the valve stem 94 and is arranged for retaining the C-ring seal 101 within the groove 98 of the valve plug 92. The seal retainer 102 has a retainer perimeter 103 which is substantially commensurate with the second cage perimeter 99, and the seal retainer 102 has a conventional piston ring 104. When the valve plug 92 is positioned against the lower valve seat 93 at

shut off, any fluid attempting to leak through the valve 40 between the valve plug 92 and the valve cage 90 will fill the C-ring seal 101. This fluid will tend to press the C-ring seal 101 more tightly against both the upper valve seat formed by the slope 100 of the cage 90 and the second plug perimeter 97 to increase the seal between the valve plug 92 and the cage 90. Again, as noted above, the C-ring seal 101 is in compression only when the valve plug 92 is in its closed position. As a result, wear on the C-ring seal 101 and on the upper valve seat 100 is minimized or prevented. Also, the mechanical spring force of this seal compensates for the machining tolerances and dimensional variations caused by temperature changes.

Openings 105 are provided in the valve plug 92 to equalize the pressures in volume 106 above the valve plug 92 and volume 107 below the valve plug 92. Thus, because of the openings 105, the pressures in the volume 106 above the valve plug 92 and in the volume 107 below the valve plug 92 will be equal and, but for the unbalance area across the valve plug 92, would result in generally equal but opposite forces being applied to the valve plug 92. This unbalance area can best be seen from Figure 8A.

Figure 8A is an enlarged cross-sectional view of that part of the trim arrangement shown in Figure 8 which includes the C-ring seal 101, the upper valve seat formed by the slope 100, and the lower valve seat 93. The retainer 102 has been omitted from Figure 8A for clarity. Also for clarity, the dimensions of the trim arrangement have been exaggerated. As shown in Figure 8A, when the valve 40 is closed, the lower portion of the valve plug 92 seats against the lower valve seat 93 at point 110 and the C-ring seal 101 is pressed against the upper valve seat formed by the slope 100 at point 109. Because of the openings 105 through the valve plug 92, the outlet pressure is applied against both the upper and lower sides of the valve plug 92/retainer 102 combination. Since the pressures in the volumes 106 and 107 are thus equal, these pressures will exert generally equal but opposite forces on the valve plug 92. These generally equal but opposite forces will offset one another. However, the valve plug 92 will have an annular unbalance area 108 which will be exposed to different pressures resulting in non-offsetting forces being applied to the valve plug 92.

This unbalance area 108 of the valve plug 92 is annular and has an outer radius defined by the point 109 at which the C-ring seal 101 contacts the upper valve seat formed by the slope 100 and an inner radius defined by the point 110 at which the lower portion of the valve plug 92 contacts the lower valve seat 93. The lower side of this unbalance area 108 is exposed to inlet pressure be-

cause of the leakage between the valve plug 92 and the cage 90 which will fill the C-ring seal 101. The upper side of this unbalance area (i.e. at the top of the retainer 102) is exposed to the outlet pressure in the volume 106. If these pressures are different, as they will most often be, a resulting net force will be applied to the valve plug 92 which must be overcome by the valve actuator when the valve is to be closed. Because the slope 100 can be made slight, this unbalance area 108 is smaller than is the unbalance area 69 of the trim arrangement shown in Figure 3. Thus, there is a smaller net force applied to the valve plug 92 of Figure 8 than is applied to the valve plug 47 of Figure 3 requiring a still smaller actuator to close the valve. Furthermore, the same C-ring can be used in the trim arrangement shown in Figure 8 regardless of the flow direction through the valve which is not the case of the trim arrangement of Figure 3. (That is, if the flow direction shown in Figure 8 is reversed, the C-ring 101 is simply flipped over so that its opening now points up.)

The arrangement of Figure 8 also allows Leakage Class V shut off when the valve plug 92 is positioned against the lower valve seat 93. Furthermore, the C-ring 101 may also be made of a suitable metal, such as Inconel X750 or 718, so that valve 40 can withstand high temperatures, such as those in the neighborhood of about 232 °C (450 °F) and above.

Again, as noted above, it is apparent that the C-ring seal 101 is in compression only when the valve plug 92 is in its closed position. As a result, wear on the C-ring seal 101 and on the upper valve seat formed by the slope 100 is minimized. Furthermore, the mechanical spring force of the C-ring seal 101 compensates for the machining tolerances and dimensional variations caused by temperature changes.

Claims

1. A valve comprising:
 - a valve body (41) having inlet and outlet ports (42, 43)
 - a valve stem (56) extending through said valve body;
 - trim means (45) for controlling the flow of fluid between said inlet and outlet ports (42, 43), said trim means including
 - (a) a valve cage (48) having cage openings (50) therein,
 - (b) a lower valve seat (46)
 - (c) a valve plug (47) attached to said valve stem (56), said valve plug (47) preventing fluid flow between said inlet and outlet ports (42, 43) when said valve plug (47) is positioned by said valve stem against said lower

valve seat (46), and for allowing fluid flow between said inlet and outlet ports (42, 43) when said valve plug (47) is positioned by said valve stem away from said valve lower seat (46), said valve plug (47) having an opening (66) therethrough for equalizing pressure across said valve plug (47) when said valve plug is positioned against said lower valve seat (46), and

(d) seal means (63) for providing a seal against leakage between said valve plug (47) and said valve cage (48), wherein said seal means is adapted to provide a mechanical spring force only when said valve plug (47) is positioned approximate to or against said lower valve seat (46);

characterized in that

said valve plug (47) has first and second plug perimeters (61, 62) and said valve cage (48) has first and second cage perimeters (58, 59) substantially commensurate with the first and second plug perimeters (61, 62) respectively; an upper valve seat (60, 65) is formed by one of said valve plug (47) and said valve cage (48);

said seal means (63) is arranged to cooperate with said upper valve seat (60, 65) when said valve is closed.

2. The valve according to claim 1, wherein said seal means (63) comprises a ring (70, 72, 74) having a ring opening so that fluid leaking between said valve plug (47) and said valve cage (48) will enter said ring opening and press said ring against said upper valve seat (60, 65) to increase said seal against said leakage through said valve (40) when said valve plug (47) is positioned against said lower valve seat.
3. The valve according to claim 2, wherein said seal means comprises a C-ring (70) having a C-ring opening or a V-ring (72) having a V-ring opening (47).
4. The valve according to claim 2, wherein said seal means comprises an S-ring (74), said S-ring (74) being arranged so that fluid leaking around said valve plug (47) will increase said seal against said leakage through said valve.
5. The valve according to one of the claims 1 to 4, wherein said first and second plug perimeters (61, 62) form a plug ledge (65) and said first and second cage perimeters (58, 59) form a cage ledge (60) and retainer means (64) are provided for retaining said seal means (63) substantially at said cage ledge (60) such that,



cause of the leakage between the valve plug 92 and the cage 90 which will fill the C-ring seal 101. The upper side of this unbalance area (i.e. at the top of the retainer 102) is exposed to the outlet pressure in the volume 106. If these pressures are different, as they will most often be, a resulting net force will be applied to the valve plug 92 which must be overcome by the valve actuator when the valve is to be closed. Because the slope 100 can be made slight, this unbalance area 108 is smaller than is the unbalance area 69 of the trim arrangement shown in Figure 3. Thus, there is a smaller net force applied to the valve plug 92 of Figure 8 than is applied to the valve plug 47 of Figure 3 requiring a still smaller actuator to close the valve. Furthermore, the same C-ring can be used in the trim arrangement shown in Figure 8 regardless of the flow direction through the valve which is not the case of the trim arrangement of Figure 3. (That is, if the flow direction shown in Figure 8 is reversed, the C-ring 101 is simply flipped over so that its opening now points up.)

The arrangement of Figure 8 also allows Leakage Class V shut off when the valve plug 92 is positioned against the lower valve seat 93. Furthermore, the C-ring 101 may also be made of a suitable metal, such as Inconel X750 or 718, so that valve 40 can withstand high temperatures, such as those in the neighborhood of about 232 °C (450 °F) and above.

Again, as noted above, it is apparent that the C-ring seal 101 is in compression only when the valve plug 92 is in its closed position. As a result, wear on the C-ring seal 101 and on the upper valve seat formed by the slope 100 is minimized. Furthermore, the mechanical spring force of the C-ring seal 101 compensates for the machining tolerances and dimensional variations caused by temperature changes.

Claims

1. A valve comprising:

a valve body (41) having inlet and outlet ports (42, 43)

a valve stem (56) extending through said valve body;

trim means (45) for controlling the flow of fluid between said inlet and outlet ports (42, 43), said trim means including

(a) a valve cage (48) having cage openings (50) therein,

(b) a lower valve seat (46)

(c) a valve plug (47) attached to said valve stem (56), said valve plug (47) preventing fluid flow between said inlet and outlet ports (42, 43) when said valve plug (47) is positioned by said valve stem against said lower

valve seat (46), and for allowing fluid flow between said inlet and outlet ports (42, 43) when said valve plug (47) is positioned by said valve stem away from said valve lower seat (46), said valve plug (47) having an opening (66) therethrough for equalizing pressure across said valve plug (47) when said valve plug is positioned against said lower valve seat (46), and

(d) seal means (63) for providing a seal against leakage between said valve plug (47) and said valve cage (48), wherein said seal means is adapted to provide a mechanical spring force only when said valve plug (47) is positioned approximate to or against said lower valve seat (46);

characterized in that

said valve plug (47) has first and second plug perimeters (61, 62) and said valve cage (48) has first and second cage perimeters (58, 59) substantially commensurate with the first and second plug perimeters (61, 62) respectively; an upper valve seat (60, 65) is formed by one of said valve plug (47) and said valve cage (48);

said seal means (63) is arranged to cooperate with said upper valve seat (60, 65) when said valve is closed.

2. The valve according to claim 1, wherein said seal means (63) comprises a ring (70, 72, 74) having a ring opening so that fluid leaking between said valve plug (47) and said valve cage (48) will enter said ring opening and press said ring against said upper valve seat (60, 65) to increase said seal against said leakage through said valve (40) when said valve plug (47) is positioned against said lower valve seat.

3. The valve according to claim 2, wherein said seal means comprises a C-ring (70) having a C-ring opening or a V-ring (72) having a V-ring opening (47).

4. The valve according to claim 2, wherein said seal means comprises an S-ring (74), said S-ring (74) being arranged so that fluid leaking around said valve plug (47) will increase said seal against said leakage through said valve.

5. The valve according to one of the claims 1 to 4, wherein said first and second plug perimeters (61, 62) form a plug ledge (65) and said first and second cage perimeters (58, 59) form a cage ledge (60) and retainer means (64) are provided for retaining said seal means (63) substantially at said cage ledge (60) such that,



when said valve is closed, said seal means (63) is seated against said cage ledge (60) as said upper valve seat.

6. The valve according to claim 5, wherein said seal means comprises a C-ring (63) surrounding said valve plug (47) and having a C-ring opening pointing radially inward. 5
7. The valve according to claim 5, wherein said seal means comprises a V-ring (72) surrounding said valve plug (47) and having a V-ring opening pointing radially inward. 10
8. The valve according to claim 5, wherein alternatively retainer means (71, 73) are provided for retaining said seal means substantially at said plug ledge (65) such that, when said valve is closed, said seal means is seated against said plug ledge (65) as said upper valve seat. 15
9. The valve according to claim 8, wherein said seal means (63) comprises a C-ring (70) surrounding said valve plug (47) and having a C-ring opening pointing radially outward. 20
10. The valve according to claim 8, wherein said seal means (63) comprises a V-ring (72) surrounding said valve plug (47) and having a V-ring opening pointing radially outward. 25
11. The valve according to claim 1, wherein said valve plug (47) has first, second and third plug perimeters (84, 86, 87) forming a recess such that said recess retains said seal means (82) therein. 30
12. The valve according to claim 11, wherein said seal means comprises a C-ring (82) surrounding said valve plug (47) and having a C-ring opening so that fluid leaking around said valve plug (47) will enter said C-ring opening so as to increase said seal against said leakage through said valve (40). 35
13. The valve according to claim 11, wherein said seal means comprises a V-ring (72) surrounding said valve plug (47) and having a V-ring opening so that fluid leaking around said valve plug (47) will enter said V-ring opening so as to increase said seal against said leakage through said valve (40). 40
14. The valve according to claim 1, wherein said trim means (45) comprises said cage (48) having said first and second cage perimeters (58, 59) thereby forming a cage ledge (60), said cage ledge (60) acting as said upper valve 45

seat, and wherein said valve plug (85) comprises first and second plug parts (76, 77) for clamping said seal means therebetween such that, when said valve is closed, said seal means is seated against said upper valve seat.

15. The valve according to claim 14, wherein said seal means comprises an S-ring (74) surrounding said valve plug (85), said S-ring being arranged so that fluid leaking around said valve plug (47) will increase said seal against said leakage through said valve (40).
16. The valve according to claim 1, wherein said seal means comprises a seal ring (70, 72, 74) surrounding said valve plug (47) and having a ring opening pointing in a direction substantially parallel to said valve stem (56).
17. The valve according to one of the claims 1 to 16, wherein said seal means (63) comprises a material capable of allowing said valve (40) to be operated at temperatures of about 450 °F (about 232 °C) or higher, in particular wherein said material comprises metal.
18. The valve according to claim 17, wherein said metal comprises a metal C-ring (63, 70), a metal V-ring (72) or a metal S-ring (74).
19. A valve according to one of the claims 1 to 4 and 16 to 18, wherein the valve cage (90) has outer and inner surfaces, said inner surface (96, 99) having a slope (100) forming said upper valve seat.

Patentansprüche

1. Ventil, das folgendes aufweist:
- ein Ventilgehäuse (41) mit einem Einlaß- und einem Auslaßkanal (42, 43),
 - einen Ventilschaft (56), der sich durch das Ventilgehäuse erstreckt;
 - eine Trimmeinrichtung (45), um die Fluidströmung zwischen dem Einlaß- und dem Auslaßkanal (42, 43) zu steuern, wobei die Trimmeinrichtung aufweist:
- (a) einen Ventilkäfig (48), in dem Käfigöffnungen (50) vor-gesehen sind,
 - (b) einen unteren Ventilsitz (46),
 - (c) einen Ventilstopfen (47), der an dem Ventilschaft (56) angebracht ist, wobei der Ventilstopfen (47) einen Fluidströmung zwischen dem Einlaß- und dem Auslaßkanal (42, 43) verhindert, wenn der Ventilstopfen (47) von dem Ventilschaft in Anlage an dem unteren Ventilsitz (46) positioniert ist, und einen Fluidströmung zwischen dem Einlaß-



- und dem Auslaßkanal (42, 43) zuläßt, wenn der Ventilstopfen (47) durch den Ventilschaft von dem unteren Ventilsitz (46) entfernt positioniert ist, wobei der Ventilstopfen (47) eine ihn durchsetzende Öffnung (66) hat, um den Druck über den Ventilstopfen (47) auszugleichen, wenn der Ventilstopfen in Anlage an dem unteren Ventilsitz (46) positioniert ist, und
- (d) eine Dichteinrichtung (63), um eine Abdichtung gegen Austreten zwischen dem Ventilstopfen (47) und dem Ventilkäfig (48) vorzusehen, wobei die Dichteinrichtung ausgebildet ist, um nur dann eine mechanische Federkraft zu liefern, wenn der Ventilstopfen (47) nahe bei oder in Anlage an dem unteren Ventilsitz (46) positioniert ist; dadurch gekennzeichnet, daß
- der Ventilstopfen (47) einen ersten und einen zweiten Stopfenumfang (61, 62) hat und der Ventilkäfig (48) einen ersten und einen zweiten Käfigumfang (58, 59) hat, die mit dem ersten bzw. dem zweiten Stopfenumfang (61, 62) im wesentlichen übereinstimmen;
- ein oberer Ventilsitz (60, 65) von einem von dem Ventilstopfen (47) und dem Ventilkäfig (48) gebildet ist;
- die Dichteinrichtung (63) angeordnet ist, um mit dem oberen Ventilsitz (60, 65) zusammenzuwirken, wenn das Ventil geschlossen ist.
2. Ventil nach Anspruch 1, wobei die Dichteinrichtung (63) einen Ring (70, 72, 74) aufweist, der eine Ringöffnung hat, so daß zwischen dem Ventilstopfen (47) und dem Ventilkäfig (48) austretendes Fluid in die Ringöffnung eintritt und den Ring gegen den oberen Ventilsitz (60, 65) preßt, um die Abdichtung gegen Austreten durch das Ventil (40) zu verstärken, wenn der Ventilstopfen (47) in Anlage an dem unteren Ventilsitz positioniert ist.
 3. Ventil nach Anspruch 2, wobei die Dichteinrichtung einen C-Ring (70), der eine C-Ringöffnung hat, oder einen V-Ring (72), der eine V-Ringöffnung (47) hat, aufweist.
 4. Ventil nach Anspruch 2, wobei die Dichteinrichtung einen S-Ring (74) aufweist, wobei der S-Ring (74) so angeordnet ist, daß um den Ventilstopfen (47) herum austretendes Fluid die Abdichtung gegen Austreten durch das Ventil verstärkt.
 5. Ventil nach einem der Ansprüche 1-4, wobei der erste und der zweite Stopfenumfang (61, 62) eine Stopfenstegfläche (65) bilden und der erste und der zweite Käfigumfang (58, 59) eine Käfigstegfläche (60) bilden und eine Festlegeeinrichtung (64) vorgesehen ist, um die Dichteinrichtung (63) im wesentlichen an der Käfigstegfläche (60) festzulegen, so daß, wenn das Ventil geschlossen ist, die Dichteinrichtung (63) an der Käfigstegfläche (60) als dem oberen Ventilsitz dicht anliegt.
 6. Ventil nach Anspruch 5, wobei die Dichteinrichtung einen C-Ring (63) aufweist, der den Ventilstopfen (47) umgibt und eine radial nach innen weisende C-Ringöffnung hat.
 7. Ventil nach Anspruch 5, wobei die Dichteinrichtung einen V-Ring (72) aufweist, der den Ventilstopfen (47) umgibt und eine radial nach innen weisende V-Ringöffnung hat.
 8. Ventil nach Anspruch 5, wobei alternativ Festlegeeinrichtungen (71, 73) vorgesehen sind, um die Dichteinrichtung im wesentlichen an der Stopfenstegfläche (65) festzulegen, so daß, wenn das Ventil geschlossen ist, die Dichteinrichtung an der Stopfenstegfläche (65) als dem oberen Ventilsitz dicht anliegt.
 9. Ventil nach Anspruch 8, wobei die Dichteinrichtung (63) einen C-Ring (70) aufweist, der den Ventilstopfen (47) umgibt und eine radial nach außen weisende C-Ringöffnung hat.
 10. Ventil nach Anspruch 8, wobei die Dichteinrichtung (63) einen V-Ring (72) aufweist, der den Ventilstopfen (47) umgibt und eine radial nach außen weisende V-Ringöffnung hat.
 11. Ventil nach Anspruch 1, wobei der Ventilstopfen (47) einen ersten, zweiten und dritten Stopfenumfang (84, 86, 87) hat, die eine Ausnehmung bilden, so daß die Dichteinrichtung (82) in der Ausnehmung festgelegt ist.
 12. Ventil nach Anspruch 11, wobei die Dichteinrichtung einen C-Ring (82) aufweist, der den Ventilstopfen (47) umgibt und eine C-Ringöffnung hat, so daß um den Ventilstopfen (47) herum austretendes Fluid in die C-Ringöffnung eintritt, um die Abdichtung gegen Austreten durch das Ventil (40) zu verstärken.
 13. Ventil nach Anspruch 11, wobei die Dichteinrichtung einen V-Ring (72) aufweist, der den Ventilstopfen (47) umgibt und eine V-Ringöffnung hat, so daß um den Ventilstopfen (47) herum austretendes Fluid in die V-Ringöffnung eintritt, um die Abdichtung gegen Austreten durch das Ventil (40) zu verstärken.



14. Ventil nach Anspruch 1, wobei die Trimmeinrichtung (45) den Käfig (48) aufweist, der den ersten und den zweiten Käfigumfang (58, 59) hat, um dadurch eine Käfigstegfläche (60) zu bilden, wobei die Käfigstegfläche (60) als der obere Ventilsitz wirkt, und wobei der Ventilstopfen (85) einen ersten und einen zweiten Stopfenteil (76, 77) aufweist, um die Dichteinrichtung zwischen diesen einzuspannen, so daß, wenn das Ventil geschlossen ist, die Dichteinrichtung dicht an dem oberen Ventilsitz anliegt. 5
15. Ventil nach Anspruch 14, wobei die Dichteinrichtung einen S-Ring (74) aufweist, der den Ventilstopfen (85) umgibt, wobei der S-Ring so angeordnet ist, daß um den Ventilstopfen (47) herum austretendes Fluid die Abdichtung gegen Austreten durch das Ventil (40) verstärkt. 10 15
16. Ventil nach Anspruch 1, wobei die Dichteinrichtung einen Dichtring (70, 72, 74) aufweist, der den Ventilstopfen (47) umgibt und eine Ringöffnung hat, die in eine Richtung weist, die zu dem Ventilschaft (56) im wesentlichen parallel ist. 20 25
17. Ventil nach einem der Ansprüche 1 bis 16, wobei die Dichteinrichtung (63) ein Material aufweist, das fähig ist, den Betrieb des Ventils (40) bei Temperaturen von ca. 232 °C (ca. 450 °F) oder höher zuzulassen, wobei das Material ins-besondere Metall aufweist. 30
18. Ventil nach Anspruch 17, wobei das Metall einen metallischen C-Ring (63, 70), einen metallischen V-Ring (72) oder einen metallischen S-Ring (74) aufweist. 35
19. Ventil nach einem der Ansprüche 1 bis 4 und 16 bis 18, wobei der Ventilkäfig (90) äußere und innere Oberflächen hat und die innere Oberfläche (96, 99) eine Schräge (100) hat, die den oberen Ventilsitz bildet. 40 45

Revendications

1. Robinet à soupape comprenant un corps (41) ayant un orifice d'entrée et un orifice de sortie (42, 43), une tige (56) traversant ce corps, une garniture (45) commandant l'écoulement de fluide entre les orifices d'entrée et de sortie (42, 43), cette garniture comprenant
 - (a) une cage (48) ayant des ouvertures (50),
 - (b) un siège inférieur de robinet (46),
 - (c) un clapet (47) fixé à la tige (56), ce clapet (47) empêchant l'écoulement de fluide entre les orifices d'entrée et de sortie (42, 43) lorsqu'il est placé par la tige contre le siège inférieur de robinet (46) et permettant l'écoulement de fluide entre ces orifices (42, 43) lorsqu'il est écarté par la tige du siège inférieur de robinet (46), ce clapet (47) étant traversé par une ouverture (66) pour l'égalisation des pressions en amont et en aval de lui lorsqu'il est placé contre le siège inférieur de robinet (46), et
 - (d) un moyen d'étanchéité (63) empêchant les fuites entre le clapet (47) et la cage (48), ce moyen d'étanchéité étant fait pour produire une force mécanique élastique seulement lorsque le clapet (47) est à proximité du siège inférieur de robinet (46) ou contre celui-ci,
 caractérisé par le fait que le clapet (47) a un premier et un deuxième périmètres (61, 62) et la cage (48) a un premier et un deuxième périmètres (58, 59) sensiblement proportionnés respectivement au premier et au deuxième périmètres (61, 62) du clapet, un siège supérieur de robinet (60, 65) est formé par le clapet (47) ou par la cage (48), le moyen d'étanchéité (63) est monté pour coopérer avec ce siège supérieur de robinet (60, 65) lorsque le robinet est fermé.
2. Robinet à soupape selon la revendication 1, dans lequel le moyen d'étanchéité (63) comprend un anneau (70, 72, 74) ayant une ouverture de façon que le fluide fuyant entre le clapet (47) et la cage (48) entre dans cette ouverture et serre l'anneau contre le siège supérieur de robinet (60, 65) pour accroître l'étanchéité vis-à-vis de cette fuite dans le robinet (40) lorsque le clapet (47) est placé contre le siège inférieur de robinet.
3. Robinet à soupape selon la revendication 2, dans lequel le moyen d'étanchéité comprend un anneau à section en C (70) ayant une ouverture ou un anneau à section en V (72) ayant une ouverture.
4. Robinet à soupape selon la revendication 2, dans lequel le moyen d'étanchéité comprend un anneau à section en S (74), cet anneau (74) étant monté de façon que le fluide fuyant autour du clapet (47) accroisse l'étanchéité vis-à-vis de cette fuite dans le robinet.
5. Robinet à soupape selon l'une des revendications 1 à 4, dans lequel les premier et deuxième périmètres (61, 62) du clapet forment un rebord (65) de celui-ci et les premier et



- deuxième périmètres (58, 59) de la cage forment un rebord (60) de celle-ci, et un moyen de retenue (64) est prévu pour retenir le moyen d'étanchéité (63) sensiblement au rebord (60) de la cage de façon que lorsque le robinet est fermé, le moyen d'étanchéité (63) soit appuyé contre ce rebord (60), qui forme le siège supérieur de robinet.
6. Robinet à soupape selon la revendication 5, dans lequel le moyen d'étanchéité comprend un anneau à section en C (63) entourant le clapet (47) et ayant une ouverture dirigée radialement vers l'intérieur. 5
 7. Robinet à soupape selon la revendication 5, dans lequel le moyen d'étanchéité comprend un anneau à section en V (72) entourant le clapet (47) et ayant une ouverture dirigée radialement vers l'intérieur. 10
 8. Robinet à soupape selon la revendication 5, dans lequel, alternativement, un moyen de retenue (71, 73) est prévu pour retenir le moyen d'étanchéité sensiblement au rebord (65) du clapet de façon que lorsque le robinet est fermé, le moyen d'étanchéité soit appuyé contre ce rebord (65), qui forme le siège supérieur de robinet. 15
 9. Robinet à soupape selon la revendication 8, dans lequel le moyen d'étanchéité (63) comprend un anneau à section en C (70) entourant le clapet (47) et ayant une ouverture dirigée radialement vers l'extérieur. 20
 10. Robinet à soupape selon la revendication 8, dans lequel le moyen d'étanchéité (63) comprend un anneau à section en V (72) entourant le clapet (47) et ayant une ouverture dirigée radialement vers l'extérieur. 25
 11. Robinet à soupape selon la revendication 1, dans lequel le clapet (47) a un premier, un deuxième et un troisième périmètres (84, 86, 87) formant un creux de façon que le moyen d'étanchéité (82) soit retenu dans ce creux. 30
 12. Robinet à soupape selon la revendication 11, dans lequel le moyen d'étanchéité comprend un anneau à section en C (82) entourant le clapet (47) et ayant une ouverture de façon que le fluide fuyant autour du clapet (47) entre dans cette ouverture afin d'accroître l'étanchéité vis-à-vis de cette fuite dans le robinet (40). 35
 13. Robinet à soupape selon la revendication 11, dans lequel le moyen d'étanchéité comprend un anneau à section en V (72) entourant le clapet (47) et ayant une ouverture de façon que le fluide fuyant autour du clapet (47) entre dans cette ouverture afin d'accroître l'étanchéité vis-à-vis de cette fuite dans le robinet (40). 40
 14. Robinet à soupape selon la revendication 1, dans lequel la garniture (45) comprend la cage (48) ayant les premier et deuxième périmètres (58, 59), qui forment un rebord (60) de celle-ci qui forme le siège supérieur de robinet, et dans lequel le clapet (74) comprend une première et une deuxième parties (76, 77) destinées à serrer le moyen d'étanchéité entre elles de façon que lorsque le robinet est fermé, le moyen d'étanchéité soit appuyé contre le siège supérieur de robinet. 45
 15. Robinet à soupape selon la revendication 14, dans lequel le moyen d'étanchéité comprend un anneau à section en S (74) entourant le clapet (85), cet anneau étant monté de façon que le fluide fuyant autour du clapet (47) accroisse l'étanchéité vis-à-vis de cette fuite dans le robinet (40). 50
 16. Robinet à soupape selon la revendication 1, dans lequel le moyen d'étanchéité comprend un joint annulaire (70, 72, 74) entourant le clapet (47) et ayant une ouverture dirigée dans une direction sensiblement parallèle à la tige (56). 55
 17. Robinet à soupape selon l'une des revendications 1 à 16, dans lequel le moyen d'étanchéité (63) est fait d'une matière permettant le fonctionnement du robinet (40) à des températures d'environ 232 °C (450 °F) ou supérieures, en particulier de métal.
 18. Robinet à soupape selon la revendication 17, dans lequel le métal constitue un anneau à section en C (63, 70), un anneau à section en V (72) ou un anneau à section en S (74).
 19. Robinet à soupape selon l'une des revendications 1 à 4 et 16 à 18, dans lequel la cage (90) a des surfaces extérieure et intérieure, la surface intérieure (96, 99) ayant une pente (100) qui forme le siège supérieur de robinet.