

MICROSTRUCTURED FILTER

This invention relates to microstructured filters for fluids.

5 Various filters are known, in which the filter medium has micropores down into the submicrometre range, the pore size being statistically distributed in dependence on the material. The external dimensions of filter media of this kind are powers of ten greater than the mean pore diameter and experience has shown that they cannot readily be made as small as may be desired.

10 Micro-apertured metal strips which are used for screen printing are also known, up to a thickness of 100 μm , comprising for example nickel, provided with holes which are uniformly distributed over the strip, the diameter of the holes being some micrometres. These strips are produced for example galvanically. Metal strips of this kind cannot be assembled with microstructured components.

15 European Patent Specification No. 0 231 432 describes a cross-flow microfilter to which the fluid to be filtered is fed and out of which a concentrate flow and a filtrate flow are taken. Disposed between the chamber into which the fluid flows and the collecting chamber for the filtrate is a row of webs or lands between which there are passages. The row of webs and passages forms the microfilter. The direction of
20 the passages is inclined through an angle of 90° to 135° with respect to the direction of flow of the fluid/concentrate. The supplied fluid which goes into the concentrate flows past the row of webs. The filtrate is collected in a plurality of chambers and leaves the filter either perpendicularly to the filter surface or in the filter surface in a plurality of passages which extend between the passages for the concentrate.

25 International Patent Specification No. WO 93/11862 discloses a micromechanical filter which is constructed from three layers. Disposed on the closed base layer in given regions is an intermediate layer and disposed thereon is a cover layer with openings that are elongate in a region-wise manner. The intermediate layer is missing in parallel relationship to one or both longitudinal sides of the openings.
30 In those regions, the cover layer is arranged in a cantilever or overhung configuration. Disposed under the cantilever part of the cover layer, adjoining the opening, is a shallow slot which is as thick as the intermediate layer and as long as the elongate

opening. The filtrate flows through that slot into the filtrate collection chamber which is thicker than the intermediate chamber. The cover layer contains a large number of the elongate openings which are arranged in row-wise manner parallel to each other. The rows of slots can be arranged in a meander configuration in the cover layer. The fluid flows through a plurality of openings perpendicularly to the filter surface into a plurality of inlet chambers and is removed from a plurality of filtrate collecting chambers through a plurality of openings perpendicularly to the filter surface. The layers of that filter can be made from silicon, plastic material or metal and are structured by etching, embossing or mechanical processing or machining, while methods involving thin film technology and metal deposition out of the vapour phase can be included.

These, and other, previously proposed devices suffer from a number of problems. For example, it has been noted that at least some of the previously proposed devices are unduly susceptible to blockage whereupon the device can then cease to function. In an effort to alleviate this problem it has been proposed to provide a larger filter, but these larger filters have an undesirably large dead volume. Also, some of the previously proposed devices are unduly complicated, and thus expensive and time consuming to manufacture. In addition, some of the previously proposed devices are such that they cannot easily be assembled with other microstructured components.

Accordingly it is an object of the invention is to provide a microstructured filter for a fluid that alleviates at least some of the problems associated with previously proposed devices.

According to an aspect of the invention there is provided a microstructured filter for a fluid having an inlet for the unfiltered fluid and an outlet for the filtered fluid, wherein the direction of flow of the fluid through the entire filter is in a surface, characterised by

- a plurality of projections which are arranged in rows in mutually juxtaposed relationship and which project out of a base plate and which are an integral component of the base plate,
- a plurality of passages between the projections,
- a cover plate which is disposed over the projections and which covers over



the passages, wherein

- the passages form a through path from the inlet side of the filter to the outlet side thereof, and

- an elongate inlet slot for the unfiltered fluid, which extends over approximately the entire filter width and which is approximately as high as the projections projecting out of the base plate, on the inlet side of the filter, and

- an elongate outlet slot for the filtered fluid, which extends over approximately the entire filter width and which is approximately as high as the projections projecting out of the base plate, on the outlet side of the filter.

10 A preferred embodiment of the invention provides a microstructured filter for a fluid having an inlet for the unfiltered fluid and an outlet for the filtered fluid, wherein the flow direction of the fluid through the entire filter is in a surface, having the following characterising features:

- a plurality of projections which are arranged in row-wise manner in mutually juxtaposed relationship and which project out of a preferably flat - base plate and which are an integral component of the base plate,

- a plurality of passages between the projections,

- a - preferably flat - cover plate which is disposed over the projections and which covers the passages, wherein

- the passages form a through path from the inlet side to the outlet side of the filter, and

- the spacing between the base plate in the area around the projections and the cover plate within a row of projections is approximately as large as the width of the passages on the side of the projections, on which the fluid passes into the row of passages, and

- an elongate inlet slot for the unfiltered fluid, which extends over approximately the entire width of the filter and which is approximately as high as the projections which project out of the base plate on the inlet side of the filter, and

- an elongate outlet slot for the filtered fluid, which extends over approximately the entire width of the filter and which is approximately as high as the projections which project out of the base plate, on the outlet side of the filter.

Preferably, the ratio of height to width of the inlet slot and the outlet slot is



from 1:5 to 1:1000. The inlet slot preferably retains coarse particles.

A plurality of rows of projections can be arranged in a cascade configuration. The projections arranged closer to the inlet side of the filter are preferably larger than the projections which are arranged more at the outlet side of the filter.

5 The spacing between the flat base plate and the flat cover plate in the region around each row of projections, which row is arranged in a cascade configuration, is preferably approximately as large as the width of the passages on the side of the projections, on which the fluid passes into the row of passages. The spacing is preferably between half and double the passage width. The spacing preferably
10 decreases from one row to another, as viewed in the direction of flow. The passages may therefore be of an approximately square cross-section on their entry side for the fluid.

 The spacing between the flat base plate in the area around the projections and the flat cover plate can be constant within a row of projections. In the case of rows
15 of projections which are arranged in a meander configuration or a zig-zag configuration, the spacing can be larger in the region of the end of the row which is in the proximity of the outlet side of the filter than in the region of the end of the row which is in the proximity of the inlet side of the filter. The spacing preferably approximately linearly increases from one end of the row of projections to the other.

20 The mutually facing sides of two adjacent rows of projections may define an interconnected chamber into which the fluid flows from all passages between the projections of a first row, and out of which the fluid flows into all passages between the projections of the adjacent row. Disposed upstream of the first row of projections is a collecting chamber of elongate cross-section, into which the unfiltered fluid is
25 passed and out of which the fluid flows into all passages between the projections of the first row. Disposed downstream of the last row of projections is a collecting chamber of elongate cross-section, into which the fluid flows out of all passages of the last row, and out of which the filtered fluid is passed.

30 The projections can be in the form of webs or lands which - as viewed in the flow direction - are straight or curved. The projections may also be in the form of - preferably straight - columns of any cross-section, preferably of round or polygonal cross-section.



The length of the passages extending between webs or lands is preferably at least twice as great as their height on the entry side of the fluid. The cross-section of the passages is preferably approximately square or barrel-shaped or trapezoidal; in the latter case the longer side of the trapezium can be formed by a cover plate. The passages are for example from 5 to 50 μm in length, from 2.5 to 25 μm in height and from 2.5 to 25 μm in width. The width of the passages can become greater towards the exit side.

The spacing between the rows of projections is preferably twice as great as the passage width on the entry side. The rows of projections can extend parallel to each other or in a meander configuration or a zig-zag configuration. The rows arranged in a zig-zag configuration can be inclined relative to each other through an angle of from 2° to 25° .

When the filter has rows of projections which are arranged in a meander or zig-zag configuration, the particles to be filtered out are firstly deposited in the regions on the inlet side of the fluid, which are in the proximity of the outlet side of the filter, the space between the rows of projections on the inlet side progressively increases, beginning in the region of the outlet side of the filter. The filter is only approximately completely obstructed and the filter capacity exhausted when the inlet chamber between each two rows of projections is almost entirely filled with particles to be filtered out.

The degree of separation of the filter is preferably relatively sharply defined because of minor fluctuations in the dimensions of the passages. The filter may not require a feed flow distributor for the fluid to be filtered and a filtrate collecting device for the filtered fluid.

The filter can be produced using known processes from metal, silicon, glass, ceramic or plastic material for example. The base plate can be made from the same material as, or a different material from, the cover plate. The filter is preferably suitable for the high-pressure range, for example up to 30 MPa (300 bar).

In a microstructured filter according to another embodiment of the invention, further microstructured fluidic elements are arranged on the same base plate, for example a nozzle for spraying a fluid or for producing an aerosol, also in the high-pressure range.



The microstructured filter according to the various embodiments of the invention may exhibit some or all of the following advantages:

- because the filter has a large number of passages over a small area it can remain operational even if some passages are blocked by impurities contaminating the fluid. This can enable the useability of the filter when it is assembled with a nozzle for use in an atomiser to be improved, as when used in an atomiser for the administration of a medicament, failure of the atomiser within its specified period of use can have fatal consequences for the user;

- the passages can be defined within narrow limits in regard to shape, cross-sectional area and length (in the most preferred embodiment the dimensions of all passages within a filter are the same);

- the passage cross-section can be adapted to further conditions, for example to the cross-section of a nozzle which is connected downstream thereof;

- a large filter surface area can be disposed within a small filter volume;

- before the fluid can pass into the passages the flow of fluid may be directed between rows arranged in a meander or zig-zag configuration substantially perpendicularly to the flow in the passages;

- the open filter area (sum of the cross-sectional area of all passages) may be at least 50% of the total filter area;

- the filter may have a small dead volume; and

- the filter can be assembled in a simple fashion with other microstructured components.

The microstructured filter described herein finds particular utility when used for filtering a medicament dissolved in a solvent for producing an aerosol for inhalative application. Suitable solvents are for example water or ethanol or mixtures thereof. Suitable medicaments are for example Berotec, Atrovent, Berodual, Salbutamol, Combivent, Oxivent, Ba 679, BEA 2108 and others.

The filter according to the invention can also be used in a nebuliser, such as those described in PCT-application W091/14468 or PCT/EP96/04351.

The microstructured filter described herein may be produced in the following illustrative way: a plurality of interconnected base plates, for example of the order of magnitude of some thousand, is simultaneously microstructured on a large surface area



and connected in one step to a large flat cover plate (batch process). This combined assembly may then be divided into a number of individual pieces.

5 This mode of manufacture has some specific advantages. On the one hand batch production affords the possibility of producing particularly inexpensive individual parts with a high degree of precision with structure accuracies of a few micrometres down into the submicrometre range, which would be produced only at substantially greater cost in a serial processing procedure, while on the other hand batch production affords a uniform defined quality in respect of all parts, which can be reproducibly achieved under the same process conditions and is unlikely to slowly
10 change, as would be the case for example in serial processing procedures due to tool wear.

In addition, the position and location of the parts in the process are also predetermined by the design and do not have to be adjusted and set by means of expensive sorting and handling mechanisms as is the case with some of the previously
15 proposed arrangements.

The base plate may be produced, for example, by reactive ion etching, galvanoshaping or, in the case of plastic materials, in accordance with the LIGM process by lithography, galvanoshaping and moulding. There may be further structuring processes for producing specific passage shapes. Passages of trapezoidal or barrel-shaped cross-section can be produced by specific over-etching or under-etching. Such
20 shapes can be produced both by dry etching and also with wet etching processes. Triangular passage cross-sections can be produced with anisotropically operative etching processes in monocrystalline base plates of silicon. The base plate is preferably structured by isotropic or anisotropic wet or dry etching or a combination of those processes, particularly preferably by anisotropic dry etching.
25

The microstructured base plate and the projections thereof can be joined to the flat cover plate for example by anodic bonding of silicon and glass, for example an alkali borosilicate glass. In one example, the glass plate is laid on to the microstructured silicon plate and contacted with an electrode. The entire assembly is
30 heated to temperatures of between 200 and 500°C and a negative voltage of about 1000 V is applied between the silicon plate and the glass plate. Due to that voltage the positively charged alkali ions pass through the glass to the cathode where they are

neutralised. Formed in the glass at the transition between the glass and the silicon is a negative space charge which provides for electrostatic attraction of the two surfaces, and which in addition by way of oxygen bridge bonds results in a durable chemical bond between the glass surface and the silicon surface.

5 With the above described illustrative process a cover plate of glass is particularly advantageous for quality assurance because of, on the one hand, the quality of the bond connection and, on the other hand, because defects or included particles which result in malfunctioning of the filter can be easily recognised by optical inspection.

10 After the bonding procedure the assembly may be divided into individual filters, preferably with a high-speed rotary diamond circular saw, with the inlet side and the outlet side of each filter being exposed if they are not already previously exposed. The severing cut can be positioned with a degree of accuracy to within a few micrometers.

15 Besides using anodic bonding, the microstructured base plate can be joined to the flat cover plate by means of -ultrasonic welding, laser welding, glueing or soldering or any other means apparent to persons skilled in the art.

Embodiments of the inventions will now be described by way of example only, with reference to the accompanying figures, in which:

20 Figure 1 illustrates a schematic representation of an embodiment of the filter;

Figure 2 is a view on an enlarged scale showing the arrangement of projections in rows of the filter of Figure 1;

Figure 3 is a cross-sectional view along the line A--A of Figure 2;

Figure 4 is a schematic illustration of a variety of different projections;

25 Figure 5 is a schematic illustration of further projections;

Figure 6 is a schematic illustration of a number of illustrative patterns in which the projections might be arranged;

Figure 7 shows one illustrative example of the orientation of the projections; and

30 Figure 8 is an image produced in a scanning electron microscope of a filter at the end of its useful life.

As mentioned above, Figure 1 shows an illustrative embodiment of a filter,

viewed from the initially open side, which is then covered with the cover plate (not shown). A base plate 1 of the filter is microstructured between the edge regions 2a and 2b. The microstructuring provides, in this example, rows 3 of projections which are arranged in a zig-zag configuration. It may also be seen that the rows 3 are inclined relative to each other through an angle α .

In this example, the base plate is provided, in addition to the filter and upstream thereof, with a further row of projections 4 which form a very coarse filter and which serve to agitate the fluid flowing therethrough. Disposed upstream of the projections 4 is an inlet slot 5 through which the unfiltered fluid passes into the filter. In this embodiment, arranged adjoining the filter is a nozzle 6 out of which the filtered fluid can exit. The nozzle 6 has been formed, in this illustrative example, as an integral component of the base plate 1. It will be appreciated that the filter can be formed without the nozzle 6 and coarse filter 4.

Figure 2 is an enlarged view of a portion of Figure 1 showing an illustrative arrangement of projections in the rows 3. In this case the projections 7 are rectangular webs or lands but, as will be described later, they may have an alternative configuration. It can be seen that the rows 3 comprise a plurality of projections 7 which upstand from the base plate 1 and which are spaced from one another to provide a fine fluid filter.

Figure 3 is a cross-sectional view through a row of projections taken along line A-A in Figure 2. In this illustrative embodiment, the projections 7 have concavely curved longitudinal sides, between which there are passages 8 of barrel-shaped cross-section.

Figure 4 shows a plurality of embodiments of projections, each viewed from the initially open side of the filter (i.e. from above). Any of, or any combination of, the illustrated projections (or any other projection) may be employed in the filter described herein. Figure 4 shows a rectangular land 11, an elongate land 12 of constant width with rounded narrow sides, a wing-shaped land 13, a land 14 of constant width and with an inclinedly extending narrow side, and a land 12 which is curved in the shape of a segment of a circle. Also illustrated are a square column 16, a triangular column 17, a round column 18 and an octagonal column 19. As mentioned above, any of or any combination of these lands are suitable for use in the

filter.

Figure 5 shows various cross-sectional views through a variety of different projections, more specifically a projection of a rectangular cross-section 21, a projection of a cross-section 22 with concavely curved longitudinal sides, a projection of trapezoidal cross-section 23 in which the long side of the trapezium is connected to the base plate 1, a projection of trapezoidal cross-section 24 in which the short side of the trapezium is connected to the base plate 1, and a projection 25 with two rounded-off longitudinal edges.

Figure 6 shows various arrangements of projections wherein the projections - irrespective of the form thereof - are indicated by dots of different sizes. The projections can be arranged in a matrix form 31 or linearly in a row 32 or in a meander configuration 33 or in a zig-zag configuration 34. A plurality of projections arranged in a row configuration 35 or in a meander or zig-zag configuration 36 can be arranged in succession in cascade relationship.

Figure 7 shows an illustrative orientation of lands in relation to the intake flow direction 41 of the fluid. As shown, some of the lands (indicated with reference numeral 42) are arranged parallel to the intake flow direction, others of the lands (indicated with reference numeral 43) are arranged perpendicularly to the intake flow direction and the remainder of the lands (indicated with reference numeral 44) are arranged inclined at different angles to the intake flow direction. It should be understood from Figure 7 that the lands do not have to have the same orientation with respect to the intake flow direction. In fact, the provision of differently orientated lands is a distinct advantage as the differing orientation serves to improve the degree of fluid agitation as the fluid moves through the filter.

Figure 8 shows an image produced in a scanning electron microscope of a microstructured filter such as that shown in Figure 1 at the end of its useful service life. The image was recorded through the cover plate (not visible) of glass. The image shown illustrates a filter having rows of projections arranged in a zig-zag configuration; however the projections themselves cannot be seen at the selected magnification.

Fluid has flowed through the filter in the direction of the arrows during use of the filter, and particles suspended in the fluid have become trapped by adjacent

projections. As shown, the rows of projections are covered with filtered-out particles, more specifically to a greater degree in the proximity of the edge regions 2a and 2b than in the central region of the filter. There are almost no particles in the space between the rows of projections, which is at the intake flow side of the filter; and thus the filter is fully operational in that region (i.e. fluid can still pass therethrough). As can be seen from Figure 8, the limit line between the free filter region and the obstructed filter region extends in an approximately parabolic shape. As seen from Figure 8, fluid can still pass through the filter even though a considerable part of the filter surface area has already been obstructed.

It can be seen therefore that the filter described herein is less prone to blockage than previously proposed filters, as it can still function adequately even when a relatively large proportion of the filter surface has been obstructed. As a result of this improvement, the useful life of the filter (and thus any devices including the filter) may be greatly increased. This is in direct contrast to previously proposed arrangements where a relatively small amount of filter obstruction causes the device to cease functioning correctly.

Example: Microstructured filter for an atomiser

As mentioned above, the filter described herein finds great utility in atomisers, and in particular in atomisers for producing an aerosol of a medicament-bearing fluid.

An illustrative example of one such atomiser will now be described. In this illustrative example, the filter is formed on a base plate together with a number of other microstructured components. The base plate is 2.6 mm wide and about 5 mm long. On a width of about 2 mm it contains 40 rows of projections, with the rows arranged in a zig-zag configuration. Each row is 1.3 mm long. The projections are rectangular lands which are 10 μm long and 2.5 μm wide; and they project out of the base plate by 5 μm . Provided between the lands are passages which are 5 μm high and 3 μm wide.

Disposed on the fluid entry side of the filter is a row of 10 rectangular lands which are 200 μm long and 50 μm wide; and they project out of the base plate by 100 μm . Provided between those lands are passages which are 100 μm high and 150 μm wide. The ten rectangular lands provide a coarse filter and a means for

agitating the fluid flowing therethrough. At a spacing of about 300 μm in front of the row of lands there is provided a fluid entry gap which is about 2 mm wide and 100 μm high.

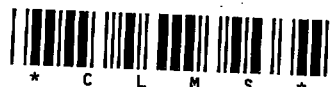
5 A filtrate collecting chamber is provided behind the rows of lands arranged in a zig-zag configuration. The filtrate collecting chamber is 5 μm high and gradually narrows from a 2 mm width and which communicates with a nozzle of rectangular cross-section which is 5 μm high and 8 μm wide. In this example, the nozzle opening was produced at the same time as the microstructuring of the base plate.

10 The base plate which is 1.5 mm thick comprises nickel and is produced by galvano-shaping of a plastic moulding insert which contains the complementary structures for 1083 filters. It is covered with a 0.8 mm thick, flat nickel plate which is soldered to the base plate.

CLAIMS

1. A microstructured filter for a fluid, the filter having an inlet for unfiltered fluid and an outlet for filtered fluid, the filter comprising:
- 5 - a plurality of projections (7) which are arranged in at least two rows (3) in mutually juxtaposed relationship and which project out of a base plate (1) and which are an integral component of the base plate,
- a plurality of passages (8) between the projections (7), and
- a cover plate which is securable to the base plate to cover the projections (7)
- 10 b - e and the passages (8), wherein
- the passages form a plurality of through paths from the inlet to the outlet,
- said inlet comprises an elongate inlet slot (5) for the unfiltered fluid, which extends over approximately the entire filter width and which is approximately as high as the projections (7) projecting out of the base plate, on the inlet side of the filter,
- 15 and
- said outlet comprises an elongate outlet slot for the filtered fluid, which extends over approximately the entire filter width and which is approximately as high as the projections (7) projecting out of the base plate, on the outlet side of the filter.
- 20 2. A filter according to Claim 1, wherein a spacing between the base plate and the cover plate is approximately as large as the width of the passages (8) between adjacent projections (7).
3. A filter according to Claim 1, wherein:
- 25 - a plurality of rows (3) of projections (7) are arranged in cascade form,
- the cross-section of the passages (8) perpendicularly to the direction of flow of the fluid - as viewed in the direction of flow - decreases from row to row,
- the projections (3) which are arranged closer to the inlet side of the filter are larger than the projections (3) which are arranged more at the outlet side of the filter,
- 30 and
- the spacing between the base plate and the cover plate in the area around each row of projections (7), which row is arranged in a cascade form, is approximately as





large as the width of the passages on the side of the projections (7), on which the fluid passes into the row of passages.

4. A filter according to any of claims 1 to 3, wherein said base plate (1) and said cover plate are substantially flat.

5. A filter according to any of claims 1 to 4, wherein said inlet slot (5) has a ratio of height to width from 1:5 to 1:1000, and said outlet slot has a ratio of height to width from 1:5 to 1:1000.

6. A filter according to any of claims 1 to 5, wherein:
- a spacing between the base plate (1) in the area around the projections (7) and the cover plate within a row (3) of projections (7) is between half and double the passage width on the side of the projections, on which the fluid passes into the row of passages (8).

7. A filter according to any of claims 1 to 6, wherein mutually facing sides of two adjacent rows of projections (7) define an interconnected space into which the fluid flows from all passages between the projections of a first row and out of which the fluid flows into all passages between the projections of the row following in the direction of flow.

8. A filter according to any of claims 1 to 7, comprising:
- a collecting chamber of elongate cross-section between the inlet slot (5) and a first row of projections (4), into which the unfiltered fluid is passed and out of which the fluid flows into all passages between the projections of the first row, and
- a collecting chamber of elongate cross-section between a last row of projections and the outlet slot, into which the fluid flows out of all passages of the last row and out of which the filtered fluid is passed.

9. A filter according to any of claims 1 to 8, wherein said projections are either in the form of lands (11, 12, 13, 14, 15) which - as viewed in the flow direction- are



straight or curved; or are in the form of columns (16, 17, 18, 19).

5 10. A filter according to any of claims 1 to 9, wherein said passages (8) are of substantially constant cross-section, and have a length that is at least twice as great as their height on the entry side of the fluid.

10 11. A filter according to any of claims 1 to 10, wherein said passages (8) are of an approximately constant cross-section over the passage length, and are of a length of 5 μm to 50 μm , a height of 2.5 μm to 25 μm and a width of 2.5 μm to 25 μm .

12. A filter according to Claim 11, wherein said passages have a substantially square cross-section.

15 13. A filter according to any of claims 1 to 11, wherein said passages have a barrel-shaped or trapezoidal cross-section.

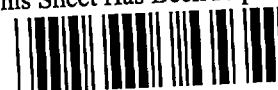
14. A filter according to Claim 13, wherein a longer side of the trapezoidal passages is formed by the cover plate.

20 15. A filter according to any of claims 1 to 11, wherein the passages (8) have an approximately square cross-section on the entry side of the filter that becomes wider towards the exit side of the filter.

25 16. A filter according to any of claims 1 to 15, wherein a spacing between the rows of projections is preferably twice as great as the passage width on the entry side.

30 17. A filter according to any of claims 1 to 16, wherein said projections are arranged in rows (31) extending parallel to each other, or in rows (33) extending in a meander configuration, or in rows (34) which extend in a zig-zag configuration and which are inclined relative to each other through an angle α of between 2° to 25° .

18. A filter according to any of claims 1 to 17, wherein the spacing between the





base plate (1) in the area around the projections (7) and the cover plate within a row (3) of projections is substantially constant.

19. A filter according to any of claims 1 to 17, wherein the spacing between the base plate (1) in the area around the projections (7) and the cover plate within a row (3) of projections (7) arranged in a meander configuration (33) or a zig-zag configuration (34) is greater in the region of the end of the row which is in the proximity of the outlet of the filter than in the region of the end of the row which is in the proximity of the inlet of the filter.

20. A filter according to Claims 1 and 17, wherein a spacing between the flat base plate (1) in the area around the projections (7) and the flat cover plate within a row of projections arranged in a meander configuration (33) or a zig-zag configuration (34), which linearly increases from the region of the end of the row which is in the proximity of the inlet side of the filter in a direction towards the region of the end of the row which is in the proximity of the outlet side of the filter.

21. A filter according to any of claims 1 to 18, wherein said base plate (1) has been structured by isotropic or anisotropic wet or dry etching or a combination of those processes, preferably by anisotropic dry etching.

22. A filter according to any of claims 1 to 21, wherein said base plate (1) is of silicon and said cover plate is of glass, said base plate being joined to said cover plate by anodic bonding.

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