

DESCRIPTION

TITLE OF INVENTION

TRAVELING VEHICLE SYSTEM

TECHNICAL FIELD

5 [0001]

The present invention relates to a traveling vehicle system, particularly a traveling vehicle system in which electric power is fed to the traveling vehicle using a contactless power feed arrangement.

10 BACKGROUND ART

[0002]

15 There is a known technology for a conveying vehicle contrived to travel along a path for carrying articles in a cleanroom (e.g., in a semiconductor manufacturing plant), where dust production is a problem. An electric motor is typically used as a drive source for such a conveying vehicle. Electric power is supplied to the motor by electromagnetic induction from two power feed cables provided along the path of the conveying vehicle.

[0003]

20 A method by which electromagnetic induction is utilized to conduct contactless power feeding will now be explained.

The two power feed cables are held in a power feed cable holder of a power feed rail provided along the path. A core that is made

of ferrite and has a generally E-shaped cross sectional shape is fixed to an electric power receiving unit of the conveying vehicle.

A coil is wound onto a middle protruding piece of the core and the protruding piece is arranged between the two power feed cables

5 such that it does not contact the power feed cables. When a high-frequency electric current is passed through the power feed cables, a magnetic field is generated and the magnetic field acts

on the coil wound onto the core, causing an electric current to be induced in the coil. In this way, electric power is supplied

10 from the power feed cables to the electric power receiving unit of the conveying vehicle in a contactless manner and the electric power is used by the motor and control devices (e.g., see Patent Document 1).

A semiconductor manufacturing plant has various apparatuses for
15 processes such as inspection, exposure, impurity injection, etching, etc., and a traveling vehicle moves semiconductor wafers between loading ports of the processing apparatuses.

CITATION LIST

PATENT LITERATURE

20 [0004]

Patent Literature 1: Japanese Laid-open Patent Publication No. 2002-234366

SUMMARY OF INVENTION

TECHNICAL PROBLEM

[0005]

As explained above, the power feed cables used to supply electric power to the traveling vehicle system in a contactless manner generate a magnetic field and a portion of the magnetic field leaks to the outside from the power feed rail. The inventor has discovered that there is a possibility that magnetic field leakage from the power feed rail will affect processing equipment used in a semiconductor manufacturing plant where the traveling vehicle system is used, particularly inspection equipment. For example, when a semiconductor wafer having a line gap of 45 nm is inspected with a laser in an electron beam inspection apparatus, a magnetic field from the power feed cables sometimes affects a positioning function of the inspection apparatus and causes an incorrect measurement to occur. In particular, as semiconductor design rules progress toward smaller nodes, the problem of incorrect measurements becomes more of a concern.

[0006]

The object of the present invention is to provide a contactless power feed type traveling vehicle system that can suppress a leakage of the magnetic field from a power feed cable.

SOLUTION TO PROBLEM

[0007]

A contactless power feed system according to one aspect of the present invention comprises an AC power source, a power feed cable, a power reception pickup, and a magnetic field reducing section. The power feed cable is connected to the AC power source. The power
5 reception pickup is provided on a traveling vehicle and contrived to receive electric power through the power feed cable in a contactless fashion. The magnetic field reducing section has a coil antenna and a capacitor. An induced electric current flows in the coil antenna due to a magnetic field generated by an electric current
10 flowing in the power feed cable. A resonance relationship is established between the coil antenna and the capacitor such that the induced electric current in the coil antenna is out of phase or in opposite phase with the electric current flowing in the power feed cable.

15 In this system, the capacitor serves to make the induced current in the coil antenna out of phase with the current in the power feed cable. That is, a magnetic field generated from the coil antenna is out of phase with the magnetic field generated through the power feed cable. As a result, the leaked magnetic field from the power
20 feed cable can be canceled out by the magnetic field having a reversed phase. Here, "cancel out" means that at least a portion of the magnetic field can be canceled out such that the effect imposed on other apparatuses is reduced.

With this system, a power source or a pickup coil is not required to generate a current in the coil antenna.

[0008]

In another aspect of the present invention, the coil and the capacitor are not in a perfect resonance relationship and, instead, a frequency close but not equal to a resonance frequency is used. Thus, the phase of the electric current induced in the coil antenna is not completely out of phase with the current flowing in the power feed cable. By using a state that is offset from a perfect resonance state, a magnetic field that is out of phase to an appropriate degree for canceling out the leaked magnetic field can be generated from the coil antenna.

[0009]

The capacitor is preferably contrived to achieve such a resonance relationship that the magnetic field generated by the electric current induced in the coil antenna cancels out the electric current flowing in the power feed cable.

[0010]

A magnetic field reducing method for a contactless power feed system according to another aspect of the present invention is a magnetic field reducing method for a contactless power feed system having an AC power source, a power feed cable connected to the AC power source, and a power reception pickup that is provided on a

traveling vehicle and contrived to receive electric power through the power feed cable in a contactless fashion. The method includes the following steps of placing a resonance circuit including a coil antenna and a capacitor to a vicinity of the power feed cable; and
5 exchanging capacitors in order to adjust a resonance relationship with respect to the coil antenna such that a magnetic field generated by an induced electric current flowing in the coil antenna cancels out a magnetic field generated by an electric current flowing in the power feed cable.

10 With this method, the resonance relationship between the capacitor and the coil antenna can be adjusted by exchanging the capacitor. More particularly, a magnetic field that is out of phase to an appropriate degree can be generated by exchanging the capacitor so as to achieve a resonance state that is offset from a perfect
15 resonance state.

[0011]

The adjusting of the resonance relationship is a step of adjusting a phase θ of the induced current in the coil antenna and a magnetic field H generated at the coil antenna by the induced current using
20 the following relationships:

Impedance Z of a circuit consisting of the coil antenna and the capacitor = $\omega L - 1/\omega C$;

Induced voltage V_c generated across coil antenna = $-N \times d\Phi/dt$

Induced current I generated in coil antenna = V_c/Z ;

Magnetic field H generated at the coil antenna by the induced current = $I/(4\pi r) \times [J(J^2 + r^2)^{-1/2}]$;

Phase θ of the induced current = $\cos^{-1} (R/Z)$, where

L is an inductance of the coil antenna, C is a capacitance of the capacitor, N is the number of windings of the coil antenna, $d\Phi/dt$ is a rate of change of a magnetic flux in the coil antenna, r is a distance from the coil antenna to a magnetic flux that is to be reduced, J is a length of the coil antenna, and R is a DC resistance of the coil antenna.

With this method, the values of the coil antenna and the capacitor can be calculated in advance.

ADVANTAGEOUS EFFECTS OF THE INVENTION

[0012]

With a traveling vehicle system according to the present invention, the magnetic field generated by a power feed cable can be cancelled out with a magnetic field having an opposite phase generated by a coil antenna.

BRIEF DESCRIPTION OF DRAWINGS

[0013]

Figure 1 is a schematic view of an overhead traveling vehicle system inside a cleanroom.

Figure 2 is a partial side view of an overhead traveling vehicle system and an overhead traveling vehicle.

Figure 3 is a vertical cross sectional view of an inside of a rail.

Figure 4 is a partial side view of an overhead traveling vehicle system and an overhead traveling vehicle.

5 Figure 5 is a vertical cross sectional view of a power feed unit.

Figure 6 is an exploded view showing the various parts of the power feed unit.

Figure 7 is a partial perspective view of a rail.

Figure 8 is a simple sketch showing a positional relationship
10 between the rail, a processing apparatus, and a noise canceling circuit.

Figure 9 is a side view of an antenna attached to a rail.

Figure 10 is an equivalent circuit of a contactless power feed section and a noise canceling circuit.

15 DESCRIPTIONS OF THE EMBODIMENTS

[0014]

An embodiment of the present invention will now be explained with reference to the drawings.

[0015]

20 (1) Overhead Traveling Vehicle System

Figure 1 is a schematic view of a contactless power feed type overhead traveling vehicle system 1 that uses a power feed cable. The overhead traveling vehicle system 1 is installed in a

semiconductor plant or other cleanroom environment and serves to transport a FOUP (front opening unified pod) that will be explained later. The overhead traveling vehicle system 1 comprises chiefly a rail 3 and an overhead traveling vehicle 5 contrived to travel
5 along the rail 3.

[0016]

The inside of the semiconductor plant will now be explained. The semiconductor plant has a plurality of bays (processes), and an inter-bay route 51 is provided to connect remote bays to one another.
10 An intra-bay route 53 is also provided within each bay. Each of the routes 51 and 53 comprises a rail 3.

[0017]

A plurality of processing apparatuses 55 and 55, e.g., semiconductor processing apparatuses, are arranged along the
15 intra-bay routes 53. Additionally, a loading port 57 is provided near each of the processing apparatuses 55 and 55. The loading ports 57 are provided directly under the intra-bay routes 53. Thus, the overhead traveling vehicle 5 travels along the rail 3 and transports FOUPs between loading ports 57.

20 [0018]

(2) Rail

As shown in Figure 2, the rail 3 is suspended from a ceiling 9 with a plurality of columns 7. The rail 3 comprises chiefly a

traveling rail 11 and an electric power supply rail 13 provided on a bottom portion of the traveling rail 11.

[0019]

(a) Traveling rail

5 The traveling rail 11 is made of, for example, aluminum. As shown in Figure 3, the traveling rail 11 is shaped like an inverted U in a cross sectional view and has an upper face section 11a and two side face sections 11b. A pair of inwardly extending first traveling surfaces 11c is formed below the side face sections 11b.

10 A second traveling surface 11d is formed on an inside surface of an upper portion of each of the side face sections 11b, and a third traveling surface 11e is formed on an underside surface of the upper face section 11a.

[0020]

15 (b) Electric power supply rail

 The electric power supply rail 13 comprises chiefly a pair of power feed cable holders 15 and 15 provided on both sides of a lower portion of the traveling rail 11. Arranged on the power feed cable holders 15 and 15 is a pair of power feed cables 17 and 17, each

20 comprising a litz wire made of a copper wire or other conductive wire covered with an insulating material. An electric power supply device (not shown) is provided at one end of the power feed cables 17 and serves to supply a high-frequency electric current to the

pair of power feed cables 17 and 17.

[0021]

(3) Overhead Traveling Vehicle

The overhead traveling vehicle 5 comprises chiefly a traveling section 21, an electric power receiving section 23, and a hoist driving section 25. The traveling section 21 is a mechanism arranged inside the traveling rail 11 for traveling along the rail 3. The electric power receiving section 23 is a mechanism arranged inside the electric power supply rail 13 for receiving electric power from the pair of power feed cables 17 and 17. The hoist driving section 25 is a mechanism arranged below the electric power supply rail 13 for holding and hoisting a FOUP 4 up and down.

[0022]

(a) Traveling section

The traveling section 21 is arranged inside the traveling rail 11 and has a pair of first guide wheels 18 and 18, a pair of second guide wheels 19 and 19, a travel driving wheel 20, and a motor 22. The two first guide wheels 18 and 18 are arranged on both sides of a lower portion of the traveling section 21 and rotatably supported on an axle extending in a left-and-right direction, with respect to the traveling direction of the vehicle. The first guide wheels 18 and 18 are arranged on the first traveling surfaces 11c of the traveling rail 11.

[0023]

The second guide wheels 19 and 19 are arranged on both sides of an upper portion of the traveling section 21 and rotatably supported on an axle extending in a vertical direction. The second guide wheels 19 and 19 use the second traveling surfaces 11d of the traveling rail 11 as guide surfaces and prevent the position of the vehicle from drifting in a transverse direction (left-and-right direction with respect to an advancement direction).

[0024]

The travel driving wheel 20 is arranged in an approximate center of the traveling section 21 and is pressed against the third traveling surface 11e of the traveling rail 11 with a spring or other pressing means. The travel driving wheel 20 is driven with the motor 22. As a result, the overhead traveling vehicle 5 travels along the rail 3.

[0025]

(b) Electric power receiving section

The electric power receiving section 23 has a pair of pickup units 27 for obtaining electric power from the pair of power feed cables 17 and 17. More specifically, the two pickup units 27 and 27 are arranged transversely adjacent to each other inside the electric power supply rail 13. Each of the pickup units 27 has a generally E-shaped cross sectional shape and comprises a core 29 made of ferrite

and a pickup coil 31 wound onto the core 29. The core 29 has two protruding sections 29a and a middle protruding section 29b arranged in between. The pickup coil 31 is wound onto the middle protruding section 29b.

5 [0026]

The two power feed cables 17 and 17 held in a power feed cable holder 15 are arranged between the middle protruding section 29b and the respective protruding sections 29a. When a high-frequency current is passed through the pair of power feed cables 17 and 17, a magnetic field is generated which acts on the pickup coil 31 and generates an induced current in the pickup coil 31. In this way, electric power is supplied from the pair of power feed cables 17 and 17 to the pickup unit 27 in a contactless manner such that the travel motor 22 is driven and electric power is supplied to control devices. The pair of power feed cables 17 and 17 of the electric power supply rail 13 and the electric power receiving section 23 of the overhead traveling vehicle 5 constitute a contactless power feed section 33.

[0027]

20 (c) Hoist driving section

As shown in Figure 2, the hoist driving section (hoist) 25 comprises chiefly a main body frame 35, a lateral feeding section 37, a drive 39, a hoist body 41, and a hoist table 43.

[0028]

The main body frame 35 is a member fixed to a bottom portion of the electric power receiving section 23. A frontward frame 45 and a rearward frame 47 are provided respectively on front and rear
5 sides of the main body frame 35.

[0029]

The lateral feeding section 37 feeds the θ drive 39, the hoist body 41, and the hoist table 43 in, for example, a sideways direction and can transfer a FOUP 4 to and from a side buffer (non shown)
10 provided on a side of the rail 3. The θ drive 39 turns the hoist body 41 within a horizontal plane to make it easier to transfer a FOUP 4. A hoisting means (not shown) is provided inside the hoist body 41 to raise and lower the hoist table 43. The hoisting means comprises, for example, four sets of winding drums and a belt 59
15 arranged around the winding drums. The hoist table 43 is attached to an end portion of the belt 59. Figure 4 depicts a state in which the belt 59 has been reeled out from the drums such that the hoist table 43 is lowered along with a FOUP 4.

[0030]

20 The FOUP 4 houses a plurality of semiconductor wafers inside and has a removable lid provided on a front face thereof. A flange 49 is provided on an upper portion of the FOUP 4 and the flange 49 is held by the hoist table 43.

[0031]

(4) Power Feed Cable Holder

The structure of the power feed cable holders 15 will now be explained using Figures 5 to 7. Since the structures of both of
5 the power feed cable holders 15 and 15 are generally the same, the structure of only one will be explained.

[0032]

○ The power feed cable holder 15 comprises an outside holder 61,
a plate member 62, and a plurality of inside holders 63. The outside
10 holder 61 and the plate member 62 have prescribed corresponding lengths, and the inside holders 63 are provided with respect to the assembled pair comprising the outside holder 61 and the plate member 62.

[0033]

○ 15 The outside holder 61 is formed as a one piece integral unit made of a resin and has a main face section 65 and a pair of side face sections 67 and 68 that extend laterally from edge portions of the main face section 65. The main face section 65 extends perpendicularly to the plane of the paper in Figures 5 and 6 and
20 extends vertically in a cross section. The side face sections 67 and 68 also extend in the direction perpendicular to the plane of the paper along side the main face section 65 and in a rightward horizontal direction from the edge portions of the main face section

65. The side face section 67 has a first portion 67a on a near-base side and a second portion 67b that extends from the first portion 67a. The second portion 67b is thinner than the first portion 67a and has a high degree of flexibility. A bent section 67c that is bent inward into a hook-like shape is formed on a tip end of the second portion 67b. The side face section 68 has a first portion 68a on a near-base side and a second portion 68b that extends from the first portion 68a. The second portion 68b has a high degree of flexibility compared to the first portion 68a. A bent section 68c that is bent inward into a hook-like shape is formed on a tip end of the second portion 68b.

[0034]

An engaging section 67d is formed on the side face section 67 of the outside holder and engages with an engaging section 11f (Figure 3) formed on a bottom surface of the traveling rail 11. With this structure, the power feed rail 13 is fixed to the traveling rail 11.

[0035]

The plate member 62 is a plate made of thin copper sheet metal and comprises chiefly a main face section 69 and a pair of side face sections 71 and 73 that extend laterally from edge portions of the main face section 69. The thickness of the plate member 62 is, for example, 0.3 mm and the thickness is preferably in a range

from 0.2 to 0.4 mm. The main face section 69 extends perpendicularly to the plane of the paper in Figures 5 and 6 and extends vertically in a cross section. The side face sections 71 and 73 also extend in the direction perpendicular to the plane of the paper along side the main face section 69 and in a rightward horizontal direction from the edge portions of the main face section 69. The plate member 62 has a same shape as an inside surface of the outside holder 61 and is held in close contact with the inside surface of the outside holder 61. Thus, the main face section 69 of the plate member 62 is in close contact with the inside surface of the main face section 65 of the outside holder 61. Similarly, the side face section 71 of the plate member 62 is in close contact with the inside surface of the side face section 67 of the outside holder 61, and the side face section 73 of the plate member 62 is in close contact with the inside surface of the side face section 68 of the outside holder 61. Once installed, tip ends of the side face sections 71 and 73 of the plate member 62 are respectively arranged inside the bent sections 67c and 68c.

[0036]

Each of the inside holders 63 is formed as a one-piece integral member made of resin. As shown in Figure 7, the inside holders 63 are arranged at prescribed intervals in the assembled unit of the outside holder 61 and the plate member 62. The inside holders 63

are arranged at a pitch of, for example, 250 to 300 mm. Each of the inside holders 63 comprises a main face section 75, two power feed cable holding sections 77 and 79 provided such that they extend laterally from two intermediate locations on the main face section 75, and two side face sections 81 and 83 extending laterally from edge portions of the main face section 75. An outside surface of the inside holder 63 has generally the same shape as the inside surface of the outside holder 61. Thus, the inside holders 63 fit into the outside holder 61. The tip ends of the side face sections 81 and 83 touch against or are in close proximity to the bent tip end faces of the bent sections 67c and 68c of the outside holder 61. Once installed, the inside holders 63 are in a state of slight elastic deformation and are secured in place in the outside holder 61 by their own elastic forces. The inside holders 63 not only secure themselves in the outside holder 61 but also secure the plate member 62 in the outside holder 61 because the plate member 62 is sandwiched between the outside holder 61 and the inside holders 63.

[0037]

As shown in Figure 3, the two power feed cables 17 are held by the tip ends of the power feed cable holding sections 77 and 79 and arranged deep inside the respective spaces between the protruding sections 29a and the protruding section 29b of the core 29.

[0038]

Since a plurality of inside holders 63 are arranged in a dispersed manner, a large portion of the main face section 69 of the plate member 62 remains exposed. Consequently, it is difficult for the inside holders 63 to impose a reducing effect on magnetic flux.

5 [0039]

As is clear in Figure 5, the distance L1 from one of the power feed cables 17 and 17 to the closer side face section 71 of the plate member 62 is equal to the distance L2 from the other of the power feed cables 17 and 17 to the closer side face section 73.

10 In the figure, L1 and L2 are the shortest distances between said parts. The magnetic fields emanating from the power feed cables 17 and 17 do not readily leak to the outside because the plate member 62 is non-magnetic. As a result, processing apparatuses are less likely to be adversely affected by magnetic field leakage. More
15 specifically, since the plate member 62 is made of copper (which has a high conductivity), it has a strong effect of reducing magnetic flux leakage. Also, providing the plate member 62 improves a power feeding efficiency because a magnetic circuit of the core 29 forms a closed loop when electric power is fed by means of electromagnetic
20 induction.

[0040]

Since the distances L1 and L2 between the respective power feed cables 17 and 17 and the closer of the two side face sections 71

and 73 of the plate member 62, respectively, are equal, a balance can be maintained between the magnetic fields generated by the two power feed cables 17 and 17. As a result, the effect of suppressing adverse effects on other apparatuses caused by magnetic field leakage is strengthened.

[0041]

The length L3 by which the side face section 71 of the plate member 62 extends from the main face section 69 is the same as the length L4 by which the side face section 73 extends from the main face section 69, and the two side face sections 71 and 73 extend to such a position that tip end portions thereof cover the power feed cables 17. Here, "the side face sections 71 and 73 cover the power feed cables 17 and 17" means that the tip ends of the side face sections 71 and 73 extend farther toward the outside in a lateral direction than the laterally outermost portions of the power feed cables 17 and 17. Since the lengths by which the two side face sections 67 and 68 extend from the main face section 69 are the same, a balance can be maintained between the magnetic fields generated by the two power feed cables 17 and 17. As a result, the effect of suppressing adverse effects on other apparatuses caused by magnetic field leakage is strengthened. Also, since the tip ends of the side face sections 71 and 73 of the plate member 62 extend to such positions that they cover the power feed cables 17 and 17, the magnetic fields emanating

from the two power feed cables 17 and 17 do not readily leak to the outside.

[0042]

Since the plate member 62 is arranged on a side of the outside
5 holder 61 where the two power feed cables 17 and 17 are arranged,
i.e. on the inside of the outside holder 61, dust from the plate
member 62 is not likely to escape to the outside even if another
object collides against the overhead traveling vehicle system 1.
As a result, an overhead traveling vehicle system according to this
10 embodiment of the present invention is not likely to cause a problem
when it is used in a cleanroom.

[0043]

Since the inside holders 63 function both to hold the plate member
62 and to hold the pair of power feed cables 17 and 17, the number
15 of components of the system can be reduced.

[0044]

Assembly and disassembly of the power feed cable holder 15 will
now be explained. First, the plate member 62 is fitted into the
inside of the outside holder 61. When this is done, the second portion
20 67b of the side face section 67 and the second portion 68b of the
side face section 68 of the outside holder 61 are flexed outward
and the tip ends of the plate member 62 are fitted inside the bent
sections 67c and 68c. In this state, the plate member 62 is loosely

secured in the outside holder 61. Next, the inside holders 63 are fitted inside the outside holder 61, i.e., inside the plate member 62. This completes the assembly of the power feed cable holder 15. Disassembly is accomplished by reversing the steps of assembly
5 described above.

Since there are a plurality of inside holders 63, the work of assembling and disassembling the holder can be accomplished more easily. More specifically, since the inside holders 63 are smaller than the outside holder 61 and the plate member 62, they can be
10 installed without having to be positioned precisely with respect to the outside holder 61 and the plate member 62. Removal of the inside holders 63 can also be accomplished more easily because the smaller members can be removed one at a time.

[0045]

15 (5) Noise Canceling Circuit

As shown in Figures 8 to 10, a noise canceling circuit 85 is installed in the rail 3. The noise canceling circuit 85 functions to reduce a magnetic field emanating from the power feed rail 13.

[0046]

20 As shown in Figure 10, the noise canceling circuit 85 is a resonance circuit comprising a coil antenna 87 and a capacitor 89. The coil antenna 87 comprises a plurality of elongated windings that extend parallel to a lengthwise direction of the rail 3. As shown in Figures

8 and 9, the coil antenna 87 is arranged on an outside portion of the power feed cable holder 15, i.e., in a position outward of the power feed cables 17 but close to the power feed cables 17. In Figures 8 and 9, the coil antenna 87 is fixed to the power feed cable holder 15 through a mounting member 93. The capacitor 89 serves to reverse the phase of the induced current flowing in the coil antenna 87 with respect to the phase of the current flowing in the power feed cables 17.

[0047]

It is acceptable to provide the coil antenna 87 throughout the entire rail 3 or only in locations corresponding to processing apparatuses 55 for which it is necessary. Providing the coil antenna "in locations corresponding to processing apparatuses 55 for which it is necessary" means arranging the coil antenna such that the length of the coil antenna in a traveling direction corresponds to at least 70% of the length of the processing apparatus in the traveling direction.

[0048]

When a high-frequency electric current is supplied to the power feed cables 17 from an AC power source 91 shown in Figure 10, a magnetic field is generated around the power feed cables 17. This magnetic field causes a current to be induced in the pickup coil 31 wound onto the core 29. In short, electric power is transferred in a

contactless manner.

[0049]

Meanwhile, the magnetic field emanating from the power feed cables 17 induces an electric current in the coil antenna 87 of the noise canceling circuit 85 and the induced current causes a magnetic field to emanate from the coil antenna 87. With this noise canceling circuit 85, the interaction of the capacitor 89 and the coil antenna 87 causes the induced current flowing in the coil antenna 87 to be out of phase with the current flowing in the power feed cables 17. Consequently, the magnetic field emanating from the coil antenna 87 is out of phase with the magnetic field emanating from the power feed cables 17. The out-of-phase magnetic field acts to cancel out the magnetic field emanating from the power feed cables 17. Here, "cancel out" means that at least a portion of the magnetic field generated by the electric current flowing in the power feed cables 17 is canceled out. As a result, the magnetic field emanating from the power feed cables 17 has less of an adverse effect on the processing apparatus 55 (e.g. an inspection apparatus).

[0050]

In this embodiment, although magnetic field leakage to the outside of the power feed rail 13 is reduced due to the plate member 62, as explained previously, adverse effects of the magnetic field leakage are reduced even further because the magnetic field generated

by the induced current flowing in the coil antenna 87 is out of phase with the leaked magnetic field and, thus, serves to cancel out the leaked magnetic field.

[0051]

5 Since the coil antenna 87 has a plurality of windings, the magnetic field leakage reduction is effective even if the induced current flowing in the coil antenna 87 is small. Also, since a lengthwise direction of the coil antenna 87 is parallel to the power feed cables 17, the leaked magnetic field can be reduced along a wide span of
10 the power feed cables 17.

[0052]

Since an induced current is generated in the coil antenna 87 using the power feed cables 17 as a power source, it is not necessary to prepare a separate power source or a separate pickup coil.

15 [0053]

The coil antenna 87 and the capacitor 89 are not in a perfect resonance relationship and, instead, a frequency in a range close to the resonance frequency is used. Thus, the phase of the electric current induced in the coil antenna 87 is not completely out of
20 phase with respect to the electric current flowing in the power feed cables 17. By establishing a state that is offset from a perfect resonance state, the coil antenna 87 can be made to emanate a magnetic field that is out of phase to an appropriate degree for canceling

out the leaked magnetic field.

[0054]

The work required to accomplish magnetic field reduction involves the following steps:

5 A step in which a coil antenna 87 is prepared; and

 A step in which a capacitor 89 is prepared by adjusting a resonance relationship with respect to the coil antenna 87 such that a magnetic field generated by an induced electric current flowing in the coil antenna 87 cancels out a magnetic field generated by an electric
10 current flowing in the power feed cables 17.

[0055]

 With this method, the resonance relationship between the capacitor 89 and the coil antenna 87 can be adjusted by exchanging the capacitor 89. In particular, a magnetic field that is out of phase to an
15 appropriate degree can be generated by exchanging the capacitor 89 so as to achieve a resonance state that is offset from a perfect resonance state.

[0056]

 More specifically, adjusting the resonance relationship is a step
20 in which a phase θ of the induced current in the coil antenna 87 and a magnetic field H generated at the coil antenna 87 by the induced current are adjusted using the following relationships: impedance Z of a circuit consisting of the coil antenna 87 and the capacitor

89 = $\omega L - 1/\omega C$; induced voltage V_c generated across coil antenna
87 = $-N \times d\Phi/dt$, induced current I generated in coil antenna 87
= V_c/Z ; magnetic field H generated at the coil antenna 87 by the
induced current = $I/(4\pi r) \times [J(J^2 + r^2)^{-1/2}]$; phase θ of the induced
5 current = $\cos^{-1} (R/Z)$, where L is the inductance of the coil antenna
87, C is the capacitance of the capacitor 89, N is the number of
windings of the coil antenna 87, $d\Phi/dt$ is a rate of change of the
magnetic flux in the coil antenna 87, r is the distance from the
coil antenna 87 to a magnetic flux that is to be reduced, J is the
10 length of the coil antenna 87, and R is the DC resistance of the
coil antenna 87.

With this structure, the characteristic variables of the coil
antenna 87 and the value of the capacitor 89 can be calculated in
advance.

15 [0057]

(6) Other Embodiments

An embodiment of the present invention has been explained
heretofore, but the invention is not limited to the embodiment.
Various changes can be made without departing from the scope of
20 the invention.

[0058]

Although in the previously explained embodiment the plate member
comprises a single plate formed to have three faces, it is acceptable

to make the plate member out of three separate plates attached together.

[0059]

Although in the previously explained embodiment the traveling
5 vehicle system is an overhead traveling vehicle system, the present invention can also be applied to other vehicle traveling systems having a vehicle that travels along a path, such as a vehicle that travels on the floor.

[0060]

10 Although in the previously explained embodiment the traveling vehicle system is used in a clean room of a semiconductor manufacturing plant, a system according to the present invention can also be used in other types of plant.

[0061]

15 Although in the previously explained embodiment a plate member made of copper is used in the power feed cable holder, the present invention can also be applied to a power feed cable holder that does not use a plate member. In such a case, it is possible that the amount of magnetic field leakage from the power feed cable holder
20 will be large, but the out-of-phase magnetic field emanating from the coil antenna will also be larger. Consequently, the adverse effect of the leaked magnetic field on the processing equipment can be reduced in a manner similar to the previously explained

embodiment.

[0062]

Although in the previously explained embodiment the coil antenna is arranged as close as possible to the power feed cables, it is also acceptable for the coil antenna to be arranged higher or lower than the power feed cables or farther away from the power feed cables in a lateral direction.

[0063]

Although in the previously explained embodiment the coil antenna is attached to the power feed rail, it is also acceptable for the coil antenna to be attached to the traveling rail.

[0064]

Although in the previously explained embodiment the coil antenna is attached to one side of the rail, it is also acceptable if the coil antenna is attached only to the opposite side of the rail or if coil antennas are attached to both sides of the rail.

[0065]

It is acceptable for the two power feed cables to be provided on both power feed cable holders or on only one of the power feed cable holders.

INDUSTRIAL APPLICABILITY

[0066]

The present invention can be applied widely to systems having

a traveling vehicle that travels along a path.

REFERENCE SIGNS LIST

[0067]

- 1 overhead traveling vehicle system
- 5 3 rail
- 4 FOUP
- 5 overhead traveling vehicle
- 11 traveling rail
- 13 power feed rail
- 10 15 power feed cable holder
- 17 power feed cable
- 21 traveling section (conveying vehicle body)
- 23 electric power receiving section
- 27 pickup unit
- 15 29 core
- 31 pickup coil
- 33 contactless power feed section
- 61 outside holder
- 62 plate member
- 20 63 inside holder
- 65 main face section
- 67, 68 side face section
- 69 main face section

71, 73 side face section

75 main face section

77, 79 power feed cable holding section

81, 83 side face section

5 85 noise canceling circuit

87 coil antenna

89 capacitor

CLAIMS

1. A contactless power feed system, comprising:

an AC power source;

a power feed cable connected to the AC power source;

5 a power reception pickup that is provided on a traveling vehicle and contrived to receive electric power through the power feed cable in a contactless fashion; and

○ a magnetic field reducing circuit having a coil antenna and a capacitor connected to the coil antenna, the coil antenna being
10 contrived to carry an electric current induced therein by a magnetic field generated due to an electric current flowing in the power feed cable, a resonance relationship is established between the coil antenna and the capacitor such that the induced electric current in the coil antenna is out of phase with the electric current flowing
15 in the power feed cable.

○
2. The contactless power feed system according to claim 1, wherein the capacitor is adjusted to achieve the resonance relationship in which a magnetic field generated by the induced electric current
20 in the coil antenna cancels out a magnetic field generated by the electric current flowing in the power feed cable.

3. A magnetic field reducing method for a contactless power feed

system having an AC power source, a power feed cable connected to the AC power source, and a power reception pickup that is provided on a traveling vehicle and contrived to receive electric power through the power feed cable in a contactless fashion, the method includes:

5 placing a resonance circuit including a coil antenna and a capacitor to a vicinity of the power feed cable; and

 exchanging capacitors in order to adjust a resonance relationship with respect to the coil antenna such that a magnetic field generated by an induced electric current in the coil antenna cancels out a
10 magnetic field generated by an electric current flowing in the power feed cable.

4. The magnetic field reducing method for a contactless power feed system according to claim 3, wherein the adjusting of the
15 resonance relationship is a step of adjusting a phase θ of the induced current in the coil antenna and a magnetic field H generated at the coil antenna by the induced current using the following relationships:

 impedance Z of a circuit consisting of the coil antenna and the
20 capacitor = $\omega L - 1/\omega C$;

 induced voltage V_c generated across the coil antenna = $-N \times d\Phi/dt$;

 induced current I generated in the coil antenna = V_c/Z ;

 the magnetic field H generated at the coil antenna by the induced
current = $I/(4\pi r) \times [J(J^2 + r^2)^{-1/2}]$;

the phase θ of the induced current = $\cos^{-1} (R/Z)$;

where L is an inductance of the coil antenna, C is a capacitance of the capacitor, N is the number of windings of the coil antenna, $d\Phi/dt$ is a rate of change of a magnetic flux in the coil antenna,
5 r is a distance from the coil antenna to a magnetic flux that is to be reduced, J is a length of the coil antenna, and R is a DC resistance of the coil antenna.