

POWER SUPPLY

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This invention relates to a power supply for, for example, a television apparatus with high voltage stabilization.

5 In television receiver or monitor circuits, the ultor accelerating potential or high voltage for a picture tube is, typically, derived by rectifying a retrace pulse voltage developed in a high voltage winding horizontal output of a flyback transformer. The retrace pulse voltage is developed by a
10 horizontal deflection circuit output stage that is coupled to the high voltage winding via the primary winding of the flyback transformer. The horizontal deflection circuit output stage comprises a horizontal deflection winding, a retrace capacitor and a trace switch, comprising a damper diode and a horizontal output
15 transistor.

In typical television receiver circuits, raster size is inversely proportional to the square root of the ultor accelerating potential. Because the high voltage circuit exhibits a certain amount of source impedance, increasing the load current drawn
20 from the ultor terminal will result in a decreased ultor accelerating potential. Ultor voltage variations resulting from variation of beam current occur mainly due to a leakage inductance between the high voltage and the primary winding of the flyback transformer. Ultor voltage variations lead to reduced
25 performance. The reduced performance is manifested by undesirable raster size variations, reduced peak brightness and poor focus at high beam currents.

Because of the advent of, for example, very large picture tubes having increased resolution capability and the
30 advent of high definition television, it may be desirable to have a better stabilized or regulated ultor voltage so as to obtain better display performance over the entire beam current or brightness range. It may be further desirable to have the ultor voltage adjustable to the maximum permissible value, taking into account
35 the x-radiation limit, to obtain high brightness at low beam current and, therefore, a better spot size.

According to the invention, there is provided a high voltage power supply for a video apparatus, comprising: a source of an input signal at a frequency that is related to a deflection frequency; a first
5 flyback resonant circuit; a first flyback transformer; first switching means responsive to said input signal and coupled to said first flyback resonant circuit for generating a periodic, resonant first flyback pulse voltage that is developed across a high voltage winding
10 of said flyback transformer; a second flyback transformer; second switching means responsive to said input signal and coupled to a first terminal of a first winding of said second flyback transformer for generating a periodic, resonant second flyback pulse voltage, which
15 overlaps in time with said first flyback pulse voltage, at a controllable amplitude at a second winding of said second flyback transformer, said second winding of said second flyback transformer being coupled in series with said high voltage winding to produce across said series
20 coupled windings a high voltage pulse that is coupled to an ultor electrode of a cathode ray tube, having an amplitude that varies in accordance with said controllable amplitude of said second flyback voltage pulse, said high voltage pulse producing a beam current
25 in said ultor electrode that is transformer-coupled via said second winding of said second flyback transformer back to said first winding of said second flyback transformer; and means coupled to a second terminal of said first winding of said second flyback transformer for
30 generating at said second terminal a control voltage at a controllable magnitude to control said amplitude of said second flyback pulse voltage, said control voltage generating means forming a low impedance at said second terminal with respect to said transformer-coupled beam
35 current to prevent said transformer-coupled beam current from reducing a voltage range that said control voltage can assume.

In an embodiment of the invention, said control voltage generating means comprises a pair of transistors coupled in a push pull manner to said second terminal of first winding of said second flyback transformer.

5 The sole FIGURE illustrates a horizontal deflection circuit with ultor voltage stabilization, embodying an aspect of the invention.

 The sole FIGURE illustrates a horizontal deflection circuit 100 and a high voltage stabilization
10 circuit 102, that generates a stabilized ultor voltage U. For simplicity, east-west raster correction, horizontal linearity correction and component values, which are not relevant for explaining the invention, are omitted from the FIGURE.

 High voltage stabilization circuit 102 includes a
15 switching transistor Q2, responsive to a horizontal rate drive signal HORDRIVE, a retrace capacitor C3 and a primary winding Wa of a transformer T2. Transformer T2 has a secondary winding Wb for developing a flyback voltage V3 between terminals A and B. Winding Wb is coupled at terminal B in series with a tertiary,
20 high voltage winding W2 of a flyback transformer T1. Winding W2 is formed by, for example, four winding segments that are coupled in series via diodes D3 that form a split diode arrangement, in a well known manner.

 A switching transistor Q1 of deflection circuit 100, also
25 responsive to horizontal rate drive signal HORDRIVE, generates a horizontal rate flyback or retrace voltage V1 in a deflection retrace or flyback resonant circuit 79 that is coupled via a primary winding W1 of transformer T1 to winding W2 to form a horizontal rate retrace or flyback high voltage V2 in winding W2.
30 High voltage V2 is equal to the sum of the retrace pulse voltages in each of the four winding segments of winding W2. The waveform of voltage V2 that is shown in the FIGURE would have been obtained across winding W2 if a diode split arrangement had not been utilized but, instead, a
35 rectifying diode had been coupled between an end terminal C of such winding W2 and an ultor

electrode ULTOR of the picture tube. Such waveform of voltage V2 is equivalent to a sum of the voltages in the winding segments of winding W2. An ultor voltage U is generated in accordance with a sum of retrace voltage V2 and and flyback voltage V3. For example, the peak amplitude of voltage V2 is 27KV and that of voltage V3 is 4KV.

A beam current sampling resistor R3 and a capacitor C2 that are coupled in parallel are coupled between terminal A of winding Wb and ground. Consequently, a beam current dependent negative voltage V_{BC} is developed across resistor R3 at terminal A which serves to lower the settings of brightness or contrast or both at excessive average beam currents. Voltage V_{BC} at terminal A has no appreciable influence on stabilization circuit 102 and, therefore, is not referred to in the description that follows.

Stabilization circuit 102 operates as an energy flywheel. When transistor Q2 is conductive, an increasing ramp current i_1 flows through winding Wa and stores energy in winding Wa. When transistor Q2 is switched off, the stored energy is transferred into retrace capacitor C3 and develops a retrace voltage V4 across capacitor C3 and across winding Wa that forms with capacitor C3 a flyback resonant circuit 78. Voltage V4 is transformer coupled to winding Wb and appears as flyback voltage V3 across winding Wb that is in series with retrace voltage V2.

A flyback interval t_a of voltage V3 is substantially longer than a deflection retrace interval t_r of voltage V2. For example, the deflection retrace time t_r may be 11.6 microseconds, corresponding to retrace resonance frequency of 44 KHZ. In contrast, the flyback interval t_a of voltage V3 may be 24 microseconds, corresponding to flyback resonance frequency of 20.8 KHZ.

Signal HORDRIVE is coupled to a gate electrode of transistor Q2 via an inverter stage that includes a transistor Q3 and resistor R60, R61 and R62. The storage time in transistor Q1 is, for example, 6 microseconds; whereas, the storage time of the transistor Q3 is substantially smaller because of a smaller peak collector current in transistor Q3. Therefore, the

leading edge of the flyback pulse of voltage V3 will occur substantially earlier than that of voltage V2. Therefore, the entire pulse of voltage V2 will occur during the peak, flat portion of the wide pulse of voltage V3. The peak portion of the pulse of pulse voltage V3 is relatively "flat" when the peak of the pulse of voltage V2 occurs, because each pulse of voltage V3 overlaps the corresponding pulse of pulse voltage V2. Therefore, phase perturbations between the pulses of pulse voltages V2 and V3 that occur due to, for example, sudden beam current variations will not cause a significant change in ultor voltage U.

A control circuit 103 of circuit 102 provides an energizing DC voltage V_{CONT} that controls the amplitude of pulse voltage V4 and V3. The level of voltage V_{CONT} varies in accordance with a current i_2 that flows in a bleeder resistor R2 that is indicative of the level of ultor voltage U. Bleeder resistor R2 provides a focus voltage and a Grid 2 voltage, not shown, to the picture tube. Ultor voltage U is proportional to the peak value of the sum of retrace voltages V2 and V3. That peak voltage is controlled by control circuit 103. Ultor voltage U is held constant by a negative feedback loop of control circuit 103.

Control circuit 103 includes a differential amplifier 104 having an inverting terminal that is coupled to a reference voltage VZ developed in a zener diode Z. A noninverting input terminal of amplifier 104 is coupled to a low end of bleeder resistor R2 via an adjustable resistor R63 that is used for adjusting ultor voltage U. An output terminal of amplifier 104 is coupled via a signal inverting stage 64 that includes a transistor Q4 and resistors R65, R66, R67 and R68. The collector of transistor Q4 is coupled to the base electrodes of transistors Q5 and Q6 operating in a push-pull manner as emitter followers. Voltage V_{CONT} is developed at a junction terminal 69 between the emitters of transistors Q5 and Q6. A filter capacitor C70 is coupled between terminal 69 and ground. A change in ultor voltage U will produce a corresponding change in voltage V_{CONT} in a negative feedback manner to vary the peak amplitude of voltage V3 that stabilizes ultor voltage U.

Because winding Wb of transformer T2 is coupled in a current path of a beam current i_{BEAM} that flows in ultor terminal ULTOR of the picture tube, current i_{BEAM} is transformer-coupled back to winding Wa to flow in an opposite direction to the arrow associated with current i_1 . Transformer-coupled current i_{BEAM} tends to charge capacitor C70 and to make voltage V_{CONT} at terminal 69 more positive. It may be desirable to enable voltage V_{CONT} to become as low as zero volts at the high beam current, so as to maintain a large regulation range.

10 Transistor Q6 is capable of current
sinking transformer-coupled current i_{BEAM} . Therefore,
the voltage range of voltage V_{CONT} can
be as low as zero volts at the high beam current. Had transistor
Q6 been eliminated, the transformer-coupled beam current would
15 have caused voltage V_{CONT} to be positive at such high beam
current. By enabling voltage V_{CONT} to become as low as zero volts
the regulation range is, advantageously, increased.

Attention is invited to Patent Application GB-A-2243751 from which this application is derived.



CLAIMS:

1. A high voltage power supply for a video apparatus, comprising:

a source of an input signal at a frequency that is related to a deflection frequency;

5 a first flyback resonant circuit;

a first flyback transformer;

first switching means responsive to said input signal and coupled to said first flyback resonant circuit for generating a periodic, resonant first flyback pulse voltage that is developed across a high voltage winding of said flyback transformer;

10 a second flyback transformer;

second switching means responsive to said input signal and coupled to a first terminal of a first winding of said second flyback transformer for generating a periodic, resonant second flyback pulse voltage, which overlaps in time with said first flyback pulse voltage, at a controllable amplitude at a second winding of said second flyback transformer, said second winding of said second flyback transformer being coupled in series with said high voltage winding to produce across said series coupled windings a high voltage pulse that is coupled to an ultor electrode of a cathode ray tube having an amplitude that varies in accordance with said controllable amplitude of said second flyback voltage pulse, said high voltage pulse producing a beam current in said ultor electrode that is transformer-coupled via said second winding of said second flyback transformer back to said first winding of said second flyback transformer; and

25 means coupled to a second terminal of said first winding of said second flyback transformer for generating at said second terminal a control voltage at a controllable magnitude to control said amplitude of said second flyback pulse voltage, said control voltage generating means forming a low impedance at said second terminal with respect to said transformer-coupled beam current to prevent said transformer-coupled beam current from reducing a voltage range that said control voltage can assume.

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2. A power supply according to Claim 1 wherein said control voltage generating means comprises a pair of transistors coupled in a push pull manner to said second terminal of said first winding of said second flyback transformer.
