

An Optical Interference Device

Background and Field

5 The invention relates to an optical interference device.

An example of an optical interference device is a grating spectrometer which is commonly used to measure the spectral properties of light over a specific portion of the electromagnetic spectrum. When used in spectroscopy, the measurement may then be analysed to determine characteristics of materials
10 exposed to the light.

However, existing spectrometers are either relatively large in size or if they are small, they suffer from low light throughput as well as low spectral resolution.

15 It is an object of the present invention to provide an optical interference device which addresses at least one of the disadvantages of the prior art and/or to provide the public with a useful choice.

20 Summary

In a first aspect, there is provided an optical interference device comprising: a phase shifter array for receiving a collimated beam of light, the phase shifter array having an array of cells for producing optical light channels from
25 respective rays of the collimated beam of light, at least some of the optical light channels having varying phase shifts; a focusing element having a focal distance and arranged to simultaneously produce, from the optical light channels, a focused beam of light in its focal plane and an image downstream the phase shifter array for detection by an optical detector; and an optical
30 spatial filter arranged at the focal distance of the focusing element and arranged to filter the focused beam of light to produce a spatially distributed interference light pattern in zeroth order for detection by the optical detector.

An advantage of the described embodiment is that this enables the components of the optical interference device to be arranged on a same optical plane and thus, a very compact optical interference device may be achieved.

5 It is envisaged that the focusing element may include a lenslet array, with each lenslet arranged to receive some of the optical light channels or a respective optical light channel. In such an embodiment, the spatial filter may include an aperture array, with each aperture arranged at the focal distance of the respective lenslet of the lenslet array.

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Preferably, at least some of the cells of the array of cells may be blank cells which do not affect the phase of the rays incident on the respective blank cells. This is particularly useful to measure source uniformity and the information may be used to compensate for non-uniform illumination.

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The phase shifter array may have various configurations and dimensions. For example, in one embodiment, at least some of the cells of the array of cells may include a lamellar structure. In one example, the lamellar structure may include alternately raised and recessed surfaces. The lamellar structure may have an even number or an odd number of the raised and recessed surfaces. In another example, the alternately raised and recessed surfaces may form a concentric pattern.

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Specifically, the focusing element may be a focusing lens or mirror. An optical collimator may form part of the optical interference device and if that's the case, then the optical interference device further comprises an optical collimator arranged to produce the collimated beam of light. The optical interference may also further comprise an entrance aperture for directing an incident light towards the optical collimator.

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Preferably, an interferogram may be derived from the spatially distributed interference light pattern, and a spectrum may be derived from the

interferogram by using a system of linear equations. The linear equations may include using matrix inversion.

The optical interference device may be used in various applications and thus,
5 the optical interference device may be adapted as a Fourier spectrometer, or a Raman spectrometer.

The optical interference device may also be adapted to detect two (or more) spectroscopic channels at the same time. Thus, the optical interference device
10 may further comprise a further phase shifter array arranged adjacent to the phase shifter array, wherein the further phase shifter array is arranged to receive a reference beam of light.

Due to its very compact size, the optical interference device may be adapted to
15 be used with handheld or portable devices for transmission or absorbance measurements. Thus, in a second aspect, there is provided a combined product in which there is the optical interference device as described above with the optical interference device including an optical housing for housing the optical collimator, the phase shifter array, the focusing lens and the spatial filter, and a
20 portable computing device having the optical detector in the form of a camera or focal plane array, the optical housing being adapted to be fitted to the camera or focal plane array wherein the camera may be configured to detect the spatially distributed interference light pattern.

25 In a third aspect, there is provided a phase shifter array for receiving a collimated beam of light, the phase shifter array having an array of cells for producing optical light channels from respective rays of the collimated beam of light, at least some of the optical light channels having varying phase shifts; wherein the array of cells includes at least some blank cells which do not affect
30 the phase of the rays incident on the respective blank cells; and a lamellar structure having cells of varying depths for producing the optical light channels having varying phase shifts.

An advantage of the described embodiment is that this enables the source uniformity to be measured simultaneously and this information may then be used to compensate for non-uniform illumination. In this way, spectral information may be computed.

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Preferably, the blank cells may be generally flat. In an embodiment, the lamellar structure may include alternately raised and recessed surfaces. The lamellar structure may include an even number or an odd number of the raised and recessed surfaces. In a described embodiment, the alternately raised and recessed surfaces may form a concentric pattern.

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In a fourth aspect, there is provided a method for producing a spatially distributed interference light pattern, comprising: receiving a collimated beam of light, producing optical light channels from respective rays of the received collimated beam of light, at least some of the optical light channels having varying phase shifts; providing a focusing element having a focal distance; simultaneously producing, by the focusing element, from the optical light channels, a focused beam of light in its focal plane and an image downstream for detection by an optical detector; and providing an optical spatial filter at the focal distance of the focusing element and filtering the focused beam of light by the optical spatial filter to produce the spatially distributed interference light pattern in zeroth order for detection by the optical detector.

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It should be appreciated that features relevant to one aspect may also be relevant to the other aspects.

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Brief Description of the Drawings

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Exemplary embodiments will now be described with reference to the accompanying drawings, in which:

Figure 1 is a schematic diagram of an optical interference device in the form of a spectrometer according to a preferred embodiment and which includes a phase shifter array;

Figure 2 is a side view of the spectrometer of Figure 1;

5 Figure 3 is an enlarged view of the phase shifter array of Figure 1;

Figure 4 is a magnified view of a cell section of the phase shifter array of Figure 3;

Figure 5 shows a single cell in the form of a blank cell as an exemplary cell of the cell section of Figure 4;

10 Figure 6 shows a single cell having a first lamellar structure as an exemplary cell of the cell section of Figure 4;

Figure 7 shows a single cell having a second lamellar structure as an exemplary cell of the cell section of Figure 4;

15 Figure 8 shows a single cell having a concentric pattern as an exemplary cell of the cell section of Figure 4;

Figure 9 shows the single cell of Figure 6 with plane light waves illustrated travelling through two facets of the cell;

Figure 10 is a cross sectional view of the two facets of Figure 9;

20 Figure 11 is a schematic diagram of an alternative spectrometer arrangement to that shown in Figures 1 and 2 and which includes a plurality of lenslet;

Figure 12 is a top cross sectional view of the alternative spectrometer arrangement of Figure 11;

25 Figure 13 is a schematic diagram of yet another alternative spectrometer arrangement to that shown in Figures 1 and 2 and which includes a plurality of lenslet;

Figure 14 is a graph comparing requirements for a collimation angle for an exemplary spectrometer and the spectrometer of Figure 1 for a spectral resolution ranging from 10nm to 0.5nm at 350nm wavelength;

30 Figure 15 is a graph which plots ratio of the collimation angle requirement of the exemplary spectrometer and the spectrometer of Figure 1;

Figure 16 illustrates an enlarged exemplary size of the spectrometer of Figure 1 in relation to a 2 mm scale to illustrate possibility of reducing size of the spectrometer as suggested in Figure 15;

Figure 17 illustrates the spectrometer of Figure 16 attached to a camera of a smart phone;

Figure 18 is a graph which plots ratio of throughput ratio of $T_{MCFTS}/T_{Grating}$ as a function of spectral resolution at $\lambda_{min} = 350$ nm wavelength, where T_{MCFTS} is the throughput of the spectrometer 100 of Figure 1 and $T_{Grating}$ is the throughput of an exemplary grating device; and

Figures 19 to 23 illustrate alternative exemplary shapes and structures of the phase shifter array of Figure 1.

Detailed Description of Preferred Embodiments

Figure 1 is a schematic diagram of an optical interference device in the form of a spectrometer 100 according to a preferred embodiment. The spectrometer 100 includes an entrance optical spatial filter 102 having an entrance aperture 104, a collimating lens 106, a phase shifter array 108, a focusing element in the form of a focusing lens 110, and an exit optical spatial filter 112 having an exit aperture 114.

The entrance optical spatial filter 102 is arranged to receive light from a light source (not shown) and the entrance optical spatial filter 102 is arranged to limit and direct the light from the light source to the collimating lens 106. The collimating lens 106 collimates the light into a collimated beam of light for the phase shifter array 108 which produces optical light channels from respective rays of the collimated beam of light. It should be appreciated that at least some of the optical light channels have varying phase shifts.

The focusing lens 110 receives the optical light channels from the phase shifter array 108 and is arranged to produce a focused beam of light in its focal plane. The exit optical spatial filter 112 (and thus, the exit aperture 114) is arranged at a focal distance of the focusing lens 110, and is arranged to receive the focused

beam of light from the focusing lens 110 and to produce a spatially distributed interference light pattern in zeroth order for detection by an optical detector 116.

It should be noted that in addition to the focused beam of light, the focusing lens 110 is also arranged to produce an image of the phase shifter array 108 simultaneously and projecting the image for detection by the optical detector 116.

The optical detector 116 records a pixelated interference pattern and may send this pixel information to a processing module for computing spectral composition of the light.

Figure 3 is a close up view of the phase shifter array 108 of the spectrometer of Figure 1 and the phase shifter array 108 is made of micro-structured (and thus, quite appropriately termed as micro-phase shifter array or MPSA), transparent material such as glass or plastic. In this embodiment, the phase shifter array 108 includes a plurality of blank cells 118 which is arranged as a grid structure which forms five vertical and horizontal stripes 120, 122 across the phase shifter array 108. As shown in Figure 3, the grid structure of the blank cells 118 divides the phase shifter array 108 into 6 x 6 array sections 124 (although the number may change accordingly) with each array section 124 comprising a number of cell sections 126.

Figure 4 is a magnified view of one of the cell sections 126 having N x M cells or cell elements. In this embodiment, the cell section 126 is made up of 4 x 4 cells 128 adjacent some of the blank cells 118. Each cell differs from its neighbouring cell by its individual structural depth between its top and bottom ridges. This results in a changing or varying structure depth (see the steps in Figure 4) and thus each individual cell 128 exhibits different optical phase characteristics. When the collimated beam of light from the collimated lens 106 is directed onto the phase shifter array 108, the cells 128 produce respective optical light channels (or measurement channels). The blank cells 118 (or "zero depth" cells when compared to the other cells 128) are used to record spatial

intensity distribution of the light source across the phase shifter array. It should be appreciated that these blank cells 118 do not affect the phase of the rays of the collimated beam incident on these blank cells 118 but rather, these blank cells 118 are used to measure intensity (without affecting the phase of the rays).

5 It should be mentioned that for computation or measurement of spectral information, the information needed are:

- a) interference pattern generated by the phase shifter array 108; and
- b) non-uniformity of illumination of the phase shifter array 108 of the spectrometer 100.

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With the blank cells 118, it is possible to measure the source uniformity and use this information to compensate for non-uniform illumination. The combination of cells 128 which cause phase shifts of the incident light ray and the blank cells 118 of the phase shifter array 108 allows monitoring of the source distribution
15 illuminating the phase shifter array at the same time.

Again, the spatial intensity distribution is useful to compensate for non-uniform illumination. Arranging hundreds of the individual cells 128 in one or two perpendicular directions including the blank cells 118 make up the phase shifter
20 array 108 of Figure 3 for spectral calculations. This is particularly useful as it avoids the need for a separate blank sheet to be used to detect the source uniformity.

Figure 4 illustrates a 4 x 4 cell section 126 which means the cell section 126 is
25 made up of sixteen individual cells 128, arranged adjacent a number of the blank cells 118. Figure 5 illustrates a structure of one of the blank cells 118 which is planar or generally flat on all the surfaces 118a.

It should be appreciated that the cells 128 may come in different shapes, sizes
30 and structures depending on the measurements to be obtained. Figure 6 shows a first exemplary cell 130 having an illumination surface 130a with a lamellar structure 130b disposed on the illumination surface 130a. In this first exemplary cell 130, the lamellar structure 130b has a same number of alternately raised

surfaces 130c and recessed surfaces 130d, which have substantially equal widths. In this case, there are four alternately raised and recessed surfaces 130c,130d which is an even number. Needless to say, the number of recessed surfaces 130c,130d may also be odd.

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Figure 7 shows a second exemplary cell 132 having an illumination surface 132a also with a lamellar structure 132b disposed on the illumination surface 132a. Unlike the first exemplary cell 130, the lamellar structure 132b has different numbers of alternately raised surfaces 132c and recessed surfaces 132d and the widths of these alternately raised and recessed surfaces 132c,132d are also different from each other.

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It is envisaged that a lamellar structure of a cell may have different structures and dimensions and an example is shown in Figure 8, which is a third exemplary cell 134 having a concentric lamellar structure 134a with alternately raised and recessed surfaces 134b,134c.

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The use of the blank cells 118 disposed among the cells 128 allows monitoring of source distribution illuminating the phase shifter array at the same time. This would enable non-uniform illumination to be compensated.

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Next, it would be appropriate to discuss how the phase shifter array 108 refracts the light rays as the rays transmit through the phase shifter array 108. For simplicity, Figure 9 shows the single cell 130 of Figure 6 with plane light waves u_{1j}, u_{2j} illustrated travelling through first and second facets 136,138 of the cell 130. For ease of explanation, the first facet 136 being one of the raised surfaces 130c and the second facet 138 being one of the recessed surfaces 130d, thus creating a depth between the two facets 136,138. Figure 10 is a cross sectional view of the two facets 136,138 of Figure 9 with X and Y axes drawn in.

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To appreciate dispersion of the refractive index over the spectral range, it is assumed that the plane waves u_{1j}, u_{2j} travel in the X-axis direction through the

two facets 136,138 of the cell 130 and with the two facets 136,138 having respective thicknesses L , d_j (i.e. cell lengths).

At thickness L of Figure 10, reduced amplitudes of the two light waves or beams
5 may be computed as:

$$\hat{u}_{1j}(k_0, L, t) = e^{ik_0 n(k_0) L} \quad (\text{Eq: 1-1})$$

$$\hat{u}_{2j}(k_0, L, t) = e^{ik_0 n(k_0) d_j} e^{ik_0 (L - d_j)} = e^{ik_0 ((n(k_0) - 1) d_j + L)} \quad (\text{Eq: 1-2})$$

10 where,

k_0 = vacuum wave number (the subscript "0" denoting vacuum);

L = maximum thickness of the first facet 136;

d_j = thickness of the second facet 138;

j = a natural number counting each individual cell 128 of the phase shifter

15 array 108; and

t = time.

Using the definition:

$$n(k_0) = n'(k_0) + iK(k_0) \quad (\text{Eq: 1-3})$$

20 where,

n' = real refractive index; and

K = extinction constant.

With these, the interference between the two light beams u_{1j}, u_{2j} is computed by:

$$25 \quad \hat{u}_{1j} + \hat{u}_{2j} = e^{-k_0 K(k_0) L} e^{ik_0 n'(k_0) L} + e^{-k_0 K(k_0) d_j} e^{ik_0 ((n'(k_0) - 1) d_j + L)} \quad (\text{Eq: 1-4})$$

From equation Eq:1-4, absolute square of the sum of the amplitudes of the two light beams u_{1j}, u_{2j} that is proportional to power are calculated from:

$$|\hat{u}_{1j} + \hat{u}_{2j}|^2 = (\hat{u}_{1j} + \hat{u}_{2j})(\hat{u}_{1j} + \hat{u}_{2j})^* \quad (\text{Eq: 1-5})$$

It follows for a simplified case of non-absorbing material, $K=0$:

$$|\hat{u}_{1j} + \hat{u}_{2j}|^2 = 2(1 + \cos(k_0(n'(k_0) - 1)(L - d_j))) \quad (\text{Eq: 1-6})$$

As a consequence, spectral power for $\bar{N} = N \times M$ wave number values within the design spectral range (k_{0l} , $l = 1, 2, \dots, \bar{N}$; and $\bar{N}$ is number of cells) of the j^{th} cell can be computed by:

$$\hat{I}_j = 2 \sum_{l=1}^{\bar{N}} g^2(k_{0l})(1 + \cos(k_{0l}(n'(k_{0l}) - 1)(L - d_j))) \quad (\text{Eq: 1-7})$$

where,

$$j = 1, 2, \dots, \bar{N}.$$

And $g^2(k_{0l})$ is the spectral power distribution of the light source.

From equation Eq. 1-7, a system of linear equations may be computed that can be solved using matrix inversion to obtain the interference pattern generated by the cell 130. In the case of evaluation of the interferogram by means of Fourier transformation, additional corrections of the frequency spectrum may be required to compensate for a wave number dependent peak position shift.

Although the above explanation is based on the cell 130, it should be apparent that the explanation similarly applies to the entire phase shifter array 108.

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It should be apparent that the focusing element may take other forms, not just the focusing lens 110 illustrated in Figures 1 and 2. For example, instead of using the single focusing lens 110 to image the entire phase shifter array 108, each phase shifter array cell 128 may be imaged by an individual lenslet and this first alternative spectrometer arrangement 200 is shown in Figure 11 (with some of the other components omitted for ease of explanation), and Figure 12 is a top cross sectional view of the arrangement of Figure 11.

The first alternative spectrometer arrangement 200 includes an alternative phase shifter array 202 similar to that shown in Figure 1 but comprising an

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array of the cells 130 of Figure 6 (i.e. with the lamellar structure 130b) and the blank cells 118. Instead of the single focusing lens 110, the alternative spectrometer arrangement 200 includes a lenslet array 204 comprising a plurality of lenslets 206 with each lenslet 206 arranged to receive an optical light channel 208 from a respective cell 130 (or blank cell 118, as the case may be). This optical light channel 208 is shown as shaded in Figure 11. In the alternative, it is also envisaged that each lenslet 206 may be arranged to receive some of the optical light channels produced by respective cells 130 (or blank cell 118 as the case may be).

The first alternative spectrometer arrangement 200 further includes an optical spatial filter in the form of an aperture array 210 arranged at a focal distance of the lenslet array 204. The aperture array 210 comprising a plurality of slit apertures 212 with each slit aperture 212 arranged at a focal distance of a corresponding lenslet 206. Further, downstream of the lenslet array 204 and the aperture array 210, the first alternative spectrometer arrangement 200 also includes a secondary lenslet array 214 comprising a plurality of secondary lenslets 216, and an optical detector in the form of a detector array 218.

As shown in Figure 12, the secondary lenslets 216 are arranged to refocus the light beam from the aperture array 210 as a single pixel or a group of binned pixels for detection by respective detectors 220 of the detector array 218.

With the use of the lenslet array 204, it is possible to achieve a very compact spectrometer. It should be appreciated that the lenslet array 204 (and the secondary lenslet array 214) may be formed by two or more individual lens array combined together such as two crossed cylindrical lenslet arrays instead of a singular lenslet array shown in Figure 11. Needless to say, the alternative phase shifter array 202 may take other forms and a further example is shown in Figure 13, which illustrates a second alternative spectrometer arrangement 300.

The second alternative spectrometer arrangement 300 includes an alternative phase shifter array 302 similar to that shown in Figure 11 but comprising an

array of the cells 134 of Figure 8 (i.e. with the concentric structure 134a) and the blank cells 118. Similarly, a lenslet array 304 is arranged downstream and also an aperture array 306 arranged at a focal distance of the lenslet array 304, a secondary lenslet array 308, and a detector array 310.

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In view of the concentric structure of the phase shifter array 302, unlike the arrangement of Figure 11, the aperture array 306 includes a number of circular or pinhole apertures 312 which receives the (refracted) light beam from the phase shifter array 302.

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The described embodiment and alternative arrangements have many advantages and solve numerous problems. For example:

Broader Free Spectral Working Range:

15 Dispersive elements like gratings or prisms tend to limit the spectral bandwidth of a device, referred to as free spectral range. For instance, the dispersion formula of a grating at normal incidence is described by the formula:

$$d(\sin \theta_m + \sin \alpha) = m\lambda \quad (\text{Eq.:2-1})$$

where

20 d = slit spacing, the so-called grating constant;

m = the diffraction order;

θ_m = diffraction angle of the m^{th} diffraction order;

α = incidence angle with reference to the grating normal; and

λ = wavelength.

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Thus, for $\alpha=0$, a given diffraction grating of fixed grating spacing d, and a diffraction order such as the first ($m=1$), diffracted beam θ_m forms a maximum for an angle $\theta_{m=1} = \sin^{-1} (\lambda/d)$. The same applies for the case of $m=2$ and a wavelength of $\lambda/2$, implying that the free spectral range for diffraction gratings is
30 limited to one octave working band ($\lambda_{\text{max}} / \lambda_{\text{min}} < 2$). As a result, conventional grating spectrometers require filtering of wavelengths beyond the working band of the grating.

In contrast, the optical interference device described in the embodiment does not require the filtering of wavelengths and can be tailored to work throughout the spectral bandwidth set by the optical detector and this may be typically an order of magnitude.

Lower Manufacturing Tolerances:

Gratings may be produced by mechanical ruling or by holography. In case of mechanical ruling, the manufacturing requirements of a grating are tremendous. It is known that each groove facet of a grating should be flat with smooth straight edges and free from irregularities on a scale of less than $\lambda_{\min}/10$. The groove spacing should be maintained within about 1% of the wavelength. For a grating of a size of 10 by 10 mm² for example, and $\lambda_{\min}$ of 300 nm such a requirement necessitates a manufacturing tolerance of 30 nm over the entire length of a groove of 10 mm. This equals an angular tolerance along a facet of 3 μ rad and a surface roughness well below the 30 nm. The requirement of the high degree of planarity makes low cost replication techniques difficult since the grating must not distort in the process.

In case of holographic production, requirements are more naturally fulfilled as the grating pattern are generated via interference of two coherent laser beams, however, holographic gratings cannot be easily blazed and have a considerably lower efficiency than ruled gratings.

In the described embodiment, it is proposed that individual cells 130,132,134 are used to form the phase shifter array 108 and thus, the entire surface can be considered as being divided into small surface elements and requires much lower tolerance levels in terms of surface planarity. Comparing both types for a wavelength of 300 nm, the tolerance on surface planarity for the described embodiment may only be in the range of 30 mrad, which may be four orders of magnitude less stringent while maintaining a similar requirement on surface roughness.

On-optical-axis system:

Gratings are generally used off-axis in either transmission (refraction) or reflection modes. In comparison, the described embodiment offers a transmission setup (as described above) offering an advantage of having all optical components on a common optical axis. This results in low optical aberrations and thus a compact device with minimum number of optical elements could be achieved. It is envisaged that the described embodiment may similarly extend to reflection setups.

With a very compact optical interference device, it is possible to adapt the device for use with portable electronic devices such as smart phones. Indeed, in doing so, by ubiquitous presence and ready availability of smart phone-integrated spectrometers, the invention drastically lowers the threshold for using spectroscopy in daily life, commercial, industrial, scientific, medical, cosmetics, biological field while providing all the advantages of spectroscopy over other conventional spectroscopic approaches.

Compact device size:

The spectrometer 100 described in the embodiment may not require a high degree of collimation thus allowing for compact short focal length collimators and size.

In a conventional grating spectrometer having a collimator, the focal length of the collimator and an entrance aperture size may have a significant influence on the spectral resolution.

The collimation angle ϕ is given by:

$$\phi = \tan^{-1}(\phi/2f) \quad (\text{Eq.:2-2})$$

where

ϕ = diameter of the source point, and
f = focal length of the collimator.

To separate two wavelengths in a spectrum, the grating must disperse the incoming beam to angles larger than the collimation angle e.g. ($\Delta\theta = \theta_{m,\lambda_2} - \theta_{m,\lambda_1} > \varphi$). See Eq.:2-1 for definitions of λ , θ_m etc.

- 5 Thus, the spectral resolution (the difference between two neighbouring resolved spectral lines $\Delta\lambda = \lambda_2 - \lambda_1$) is inevitably limited by the collimation angle φ . It may be estimated by differentiating Eq.: 2-1:

$$\Delta\lambda / \Delta\theta = d \cos(\theta_m) / m \quad (\text{Eq.:2-3})$$

- 10 Assuming $\Delta\theta \geq \varphi$ results in:

$$\Delta\lambda \geq \varphi d \cos(\theta_m) / m = \tan^{-1}(\varnothing/2f) d \cos(\theta_m) / m \cong (\varnothing/2f) d \cos(\theta_m) / m \quad \text{for small collimation angles} \quad (\text{Eq.:2-4})$$

or

$$\varphi \leq \Delta\lambda m / (d \cos(\theta_m))$$

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As a result of Eq. 2-4, grating spectrometers must keep φ at minimum to obtain higher resolution (smaller values of $\Delta\lambda$) and thus require either small entrance apertures (small $\varnothing$) or optically long collimator arrangements (large focal length f) with low acceptance angles.

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- In the described embodiment of Figure 1, the spectral resolution is dependent on the maximum optical path difference generated between interfering beams. The collimation angle φ places a resolution limit either when interfering beams of a phase shifter array cell are π out of phase (condition 1) due to inclined angles or when collimation angle is large enough to overlap zeroth diffraction order of the longest wavelength and the first diffraction order of the shortest wavelength (condition 2).

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It follows:

$\varphi = \min[\text{condition 1, condition 2}]$ with:

- 30 Condition 1: $\varphi = \cos^{-1}(1 - \lambda/2\delta_{\max})$ (Eq.:2-5)

with $\Delta\lambda = \lambda^2/(2\delta_{\max})$ it follows:

$$\varphi = \cos^{-1}(1 - \Delta\lambda / \lambda)$$

$$\Delta\lambda = (1 - \cos(\varphi)) \lambda$$

$$\text{Condition 2: } \varphi = \cos^{-1}(\sqrt{((P/\lambda_{\min})^2 / (1 + P/\lambda_{\min})^2))) \quad (\text{Eq.:2-6})$$

where

- 5 P = period of the phase shifter array; and
 $\lambda_{\min}$ = minimum wavelength in the spectrum.

Accordingly, P may be chosen in the range of $P = 3$ to $10 \lambda_{\max}$ to avoid or minimise polarization effects of the phase shifter array 100. It should be mentioned that purposely-designed phase shifter arrays with periods below $3 \lambda_{\max}$ offer polarization sensitive measurements and polarization dependent detection and are part of the scope of the described embodiment.

Figure 14 is a graph which compares requirements for a collimation angle for an exemplary spectrometer and the spectrometer 100 of the described embodiment (MC FTS in Figure 14) for a spectral resolution ranging from 10 nm to 0.5 nm at 350 nm wavelength. The exemplary spectrometer has a typical grating of 1200 lines per millimeter and line AA marks the requirements of the collimation angle for such a spectrometer. As it can be appreciated from Figure 14, for a resolution of 10 nm the grating of such a spectrometer requires collimation angles smaller than 0.013 rad. In contrast, the spectrometer 100 of the described embodiment is limited by condition 2 to 0.16 rad at a period of $P = 3 \lambda_{\max}$ (i.e. maximum wavelength which is 700 nm in this example), a factor of 12 less stringent, and this is shown by line BB in Figure 14. For the spectrometer 100 of the described embodiment, the collimation angle is given by either condition 1 or 2 (Eq.: 2-5 or 2-6) whichever is smaller.

To compare the exemplary spectrometer and the spectrometer 100 of the described embodiment, Figure 15 is a graph which plots ratio of the collimation angle requirement of the spectrometer of Figure 1 to the exemplary spectrometer for a spectral resolution ranging from 10 nm to 0.1 nm at a wavelength of 350 nm. The graph of Figure 15 demonstrates the potential of the spectrometer 100 in terms of size reduction as well as throughput advantage. It

should be seen that particularly at higher resolution the spectrometer 100 outperforms the exemplary spectrometer by one to two orders of magnitude. As an example: For a resolution of 1 nm at a minimum wavelength of 350 nm, the spectrometer 100 with a period of $10 \lambda_{\max}$ allows a 40-fold larger collimation angle ϕ . According to Eq.: 2-2, this allows a 40-fold reduction of the collimator focal length when the aperture size is kept constant between both spectrometers. It should be apparent that the reduction in collimator length reduces the overall system size while it greatly improves the overall acceptance angle for radiation entering the spectrometer and thus the light collection ability at the same time. This is an important advantage for scarce light applications such as Raman spectroscopy or when the detectors are less sensitive as in the case of CMOS detectors in smartphones emphasizing the throughput advantage.

Figure 16 illustrates an enlarged exemplary physical size of the spectrometer 100 in relation to a 2 mm scale to illustrate a dimensional advantage of the described embodiment. Also, Figure 17 illustrates the spectrometer 100 of Figure 16 being housed in an optical housing and attached to a camera of a typical smart phone 400 with a main optical axis 140 of the spectrometer 100 substantially perpendicular to a longitudinal axis 142 of the smart phone 400. It is envisaged that this may not be so, and the spectrometer 100 may also be attached with its main optical axis 140 substantially parallel to the longitudinal axis 142 of the smart phone 400. It is also envisaged that the size of the spectrometer 100 may be further reduced, in particular with the lenslet array 204 as suggested in Figure 11, such that the spectrometer 100 may be integrated within smart phone's housing.

High light throughput:

It is well known that throughput (T) or geometrical extent of an optical system is given by product of the cross-sectional area (A) of a beam and its projected solid angle (Ω):

$$T = A \Omega$$

$$(Eq.: 2-7)$$

The projected solid angle is given by:

$$\Omega = \pi \sin^2(\Theta) \quad (\text{Eq.: 2-8})$$

- 5 whereby Θ describes a half angle of the largest cone of meridional rays that can pass through the optical system.

The throughput is the decisive figure of merit describing an ability of a device to collect and transmit radiation through the optical system. In a subsequent
10 derivation, an estimation is given for the advantage over conventional grating spectrometer devices. As stated earlier the throughput is important for scarce light applications such as Raman spectroscopy, when the detectors are less sensitive, or when integration times to capture a signal are short.

- 15 For the spectrometer 100, the throughput follows the same conditions as described for the collimation angle. Thus, Θ is limited either by collimation angle required for a given resolution (condition 1, in the previous section) or by the angle of the 1st diffraction of the shortest wavelength ($\lambda_{\min}$) emanating from the spectrometer 100 (denoted as MCFTS) (condition 2) whichever is smaller. It
20 follows:

$$T_{\text{MCFTS}} = \min [T_{\text{MCFTS},1} T_{\text{MCFTS},2}]$$

Condition 1: Combining equations 2-5, 2-7, and 2-8 and setting the requirement for $\Theta \leq \varphi$, the throughput is given by:

$$25 \quad T_{\text{MCFTS},1} \leq A\pi \frac{\Delta\lambda}{\lambda} \left(2 - \frac{\Delta\lambda}{\lambda} \right)^2 \quad (\text{Eq.:2-9})$$

$$\text{Condition 2: } \sin(\theta) = \lambda_{\min} / P \quad (\text{Eq.:2-10})$$

whereby

θ = the first order diffraction angle; and

- 30 P the period of the grating cells.

Combining equations 2-7, 2-8 and 2-10, and setting the requirement for $\Theta \leq \theta$, the throughput is given by:

$$T_{MCFTS,2} \leq A\pi\left(\frac{\lambda_{\min}}{P}\right)^2 \quad (\text{Eq.:2-11})$$

Where:

- 5 A = total area of the phase shifter array 108 (MPSA) structure in case the total system throughput is considered or it is given by the area of a single cell element in case each measurement channel is considered individually.

- 10 To derive Eq. 2-9 and Eq. 2-11, the two equations $\sin^2(\cos^{-1}(x))=1-x^2$ and $\sin^2(\sin^{-1}(x))=x^2$ are simplified for small values of x , respectively.

- 15 Comparing the throughput, T , with a conventional spectrometer such as a grating device, T_{Grating} can be estimated by combining equations 2-1,2-4,2-7, and 2-8. Using the simplification of $\cos(\sin^{-1}(x)) = \sqrt{1-x^2}$ it follows that the throughput for perpendicularly incident radiation onto such a grating device is given by:

$$T_{\text{Grating}} = A\pi \sin^2\left(\frac{\lambda m}{d\sqrt{1-\left(\frac{m\lambda}{d}\right)^2}}\right) \quad (\text{Eq.:2-12})$$

where:

- 20 A = grating area illuminated,
 $\Delta\lambda$ = wavelength resolution,
 m = diffraction order,
 λ = wavelength of the probing beam, and
 d = groove period of the grating device.

- 25 Using the same assumptions as in the discussion on collimation requirements, the throughputs $T_{MCFTS}/T_{\text{Grating}}$ of both devices are compared by plotting the throughput ratio of $T_{MCFTS}/T_{\text{Grating}}$ as a function of spectral resolution at $\lambda_{\min} = 350$ nm wavelength ($\lambda_{\max}$ is set to 700 nm) for the given case that both illuminated areas A are the same for both devices in respect of $P = 100\lambda_{\max}$.

$P = 10\lambda_{\max}$, and $P = 3\lambda_{\max}$. The result is shown in Figure 18 which demonstrates the throughput advantage of the spectrometer 100 of the described embodiment. Particularly at high resolution the spectrometer 100 may increase the light throughput up to 4 orders of magnitude compared to the 1200 lines grating device. This is a tremendous advantage in scarce light applications such as Raman spectroscopy or in cases in which the optical detector is less sensitive. Equally important for the detection of fast signals, higher light throughput improves the system's speed performance as the spectrometer 100 may gather more photons in a given period of time thus allowing shorter integration times.

Spatial filtering:

Unlike known techniques, a spatial filtering technique is combined with the phase shifter array 108. As proposed in Figure 1, the exit optical spatial filter 112 (which may have a single slit aperture or a circular aperture array) is placed in at the focal point of the focusing lens 110 to spatially filter higher diffraction orders from entering the optical detector 116. Similarly, the same may be said if the lenslet array 204 and the aperture array 210 are used. This avoids complexity of the known techniques (such as a Soller-collimator) and thus reduces optical components and system costs.

Spectroscopy may have very wide fields of application and a determining factor is the spectral range. For example, in the field of visible spectroscopy and the use of a smart phone camera as a read-out and computation tool, such applications may extend beyond industrial applications to encompass individual smart phone users. The smart phone market is ever expanding and thus, smart phone spectrometers may offer huge potentials such as detection of blood sugar levels or blood oxygen levels to the measurement of UVA (ultraviolet A) which may be used to predict or determine cancer risks and UV protection for sunbathing. Additionally, combining spectroscopy with smart phone platforms, this offers a low-cost point-of-care sensing solutions, which allows information to be sent via the web, which may include feedback, location identification and data logging utilizing cloud services.

In general, visible spectroscopy provides information about:

- electron transitions in atoms – atomic information > in addition to infrared providing molecular information
- 5 • in fluorescence spectroscopy, transitions from excited states to ground state
- in Raman spectroscopy, molecular information may be obtained > high impact.
 - Utilize laser excitation, high resolution phase shifter array tailored
 - 10 to the visible light spectrum plus smart phone to compute Raman resonances in the IR. Very low signal strength, that may be difficult to detect.
- Colorimetry: Precise determination of color, including color changes of labeling agents indicating change in concentration or acidity e.g. the change of
 - 15 methyl orange color as pH indicators. Lateral flow tests whereby a color change can be read out by the spectrometer 100 to report a certain event such as a pregnancy.
 - Concentration monitoring: The visible spectroscopy allows quantifying concentrations by passing light through unknown
 - 20 samples and computing transmittance by comparing I transmitted to I_0 sent in. From the transmittance T , the absorbance $A = \log(1/T)$ can be computed.
 - Beer's law allows computing concentrations via $A = \epsilon C l$, whereby A is absorbance, ϵ is the molar absorptivity coefficient (L/mol cm), C is
 - 25 concentration of absorbing species (mol/L), and " l " the path length (cm).
 - Chemical labeling – in the visible light spectrum, chromophores absorb highly and thus, it is possible
 - 30 to attach chromophores to molecules which need to be detected;

- Concentration rate measurements to study enzymes (proteins present in all living cells). Enzymes are measured by attaching labeling molecules reacting to UV/visible.

5

- Widest use in medicine as indicator for tissue damage. When cells are damaged by disease, enzymes leak into bloodstream and the amount present indicates the severity of tissue damage.

10

- Quantitative determination of solutions of transition metal ions highly conjugated organic compounds, and biological macromolecules.
- Solutions of transition metal ions can be colored. The color of metal ion solutions is strongly affected

15

- **Medical:**

- Pulse oximeter, measuring transmitted light through finger and monitoring blood oxygen content.
- Non-invasive detection of tumors: differentiate tumors from healthy tissue by their increased autofluorescence and differing optical properties.

20

The described embodiments should not be construed as limitative. For example, arranging the individual cells 128 of varying profile depth together results in a global phase shifter array 108 as shown in Figures 3 and 4, and the arrangement of blank elements throughout the phase shifter array 108 may be of any form: on a rectangular grid, circular or randomly distributed. The number of blank cells required depends on the expected degree of uniform illumination. The cell 128 may be a grating cell.

30

The optical detector 116 may be any device sensitive to electromagnetic radiation such as CCD or CMOS photon detectors for the light (such as UV) to be detected. MCT (Mercury cadmium telluride or HgCdTe) and/or thermal

detectors for infrared radiation may also be used. The detector material and the spectral characteristics of the optical components comprising the spectrometer 100 determine the spectral working band. In the case of a visible spectrometer, the spectrometer presented may utilize the camera system of a smart phone or other electronic devices such as tablets to read the interference pattern. Additionally, the processor of the smart phone may be utilized to compute the necessary Fourier-transformation or matrix inversion to obtain the spectral information. Such an arrangement is shown in Figure 17.

The size of the spectrometer 100 and the various components (eg. the entrance optical filter 102, the collimating lens 106, phase shifter array 108 etc) may be designed and optimized, and it is also possible that the spectrometer 100 may be integrated as part of the smart phone's optical system. It is also possible that in the smart phone 400, additional optics such as a third lens to collimate the beam coming from the exit aperture 114 of the exit optical spatial filter 112 may be utilized to further reduce the system size. In case of an additional collimating lens, the image of the phase shifter array 108 is then formed at "infinity" while the smart phone's camera optics must be locked at "infinity" focus to form the image of the phase shifter array 108 at the detector plane. Further, if the spectrometer 100 is arranged parallel to the longitudinal axis 142 of the smart phone, mirrors may be arranged along the optical path of the longitudinal axis 142 of the smart phone 400 to permit highly compact spectrometer setups. To avoid chromatic aberrations introduced by the lens system, achromatic lenses may be used.

If a smart phone (or portable electronic device such as tablet) is used to process interference pattern, the camera of the smart phone may function as the optical detector 116 and in this way, the camera may record a pixelated interference pattern generated by the spectrometer 100 and the processor of the smart phone may plots this information as an interferogram from which the spectral composition is computed via Fourier transformation or matrix inversion to present the result.

It is also possible to construct or arrange two (or more) identical phase shifter arrays 108 next to each other and this allows detecting two (or more) spectroscopic channels at the same time. This may be of particular importance for transmission or absorbance measurements. For example, one phase shifter array may be used for a sample beam of light and the other phase shifter may be used for a reference beam of light. This may be performed using the similar focusing lens and exit aperture as in Figure 1 with one phase shifter array placed next to the other phase shifter array and both phase shifter arrays are imaged onto different locations on a CCD. Alternatively, a similar measurement may be performed using the lenslet array 204 of Figure 11. In case of a transmission measurement, the sample and reference beam may then be measured at the same time by placing the sample in the collimated beam before the phase shifter array for the sample beam whereas the reference beam path would be unobstructed.

15

Some of the components of the spectrometer 100 illustrated in Figure 1 may not be necessary. For example, it is envisaged that the collimating lens 106 may not be necessary.

20 The phase shifter array 108 may be fabricated in different shapes and dimensions. For example, the phase shifter array 108 may have a triangular cross-section or diagonally extending staircase surface. Figure 19 to 23 illustrate alternative exemplary shapes and structures of the phase shifter array 108, which may have stepped front-side surfaces, stepped back-side surfaces or a combination of both. For example, Figure 19 illustrates a first phase shifter array variation 500 having a transmissive lamellar structure 502 (beams CC illustrating the transmission) having elongate front side raised members 504 interleaved by front side elongate grooves 506. The lamellar structure 502 also includes backside elongate raised members 508 and backside elongate recessed members 510. It should be appreciated that the front side elongate raised members 504 have varying heights (extending in the Y-axis) and in this variation, the height of the front side elongate raised members 504 increases along the X-axis as shown in Figure 19 i.e. perpendicular to the Y-axis. Further,

30

the lamellar structure 502 includes a backside stepped surface 512 with progressive steps along the Z-axis direction of the lamellar structure 502.

In another variation, Figure 20 shows a second phase shifter array variation 530
 5 having a reflective lamellar structure 532 including a series of front side raised elements 534 interleaved with recessed elements 536. It should be apparent that the front side raised elements 534 have varying height and this could also be observed from Figure 21 which is an end view of the second phase shifter array variation 530 in the direction DD of Figure 20. It may also be appreciated
 10 that the recessed elements 536 are arranged in a step manner 538. In this variation, surfaces of the front side raised elements 534 and the recessed elements 536 are coated with a reflective layer and when light enters via the top (as shown by light rays EE), the light rays are reflected by either the front side raised elements 534 or the recessed elements 536.

15 In a further variation, Figure 22 is a third phase shifter variation 550 having a reflective lamellar structure 552 formed of different media – such as air as medium 1 and PMMA as medium 2. The lamellar structure 552 includes front side protruding members 554 arranged between front side recessed surfaces
 20 556 and the front side protruding members 554 also have varying height profiles. The third phase shifter variation 550 has a back surface 558 having a step-like structure 560 with diagonally extending progressive steps as shown in Figure 23, which is a back view of the third phase shifter variation 500 of Figure 22. Top surfaces of the front side protruding members 554 are coated with a
 25 reflective coating 562 and the back surface 558 are similarly coated with a back reflective coating 564. In this way, light rays falling on the top surfaces of the front side protruding members 554 are reflected by the reflective coating 562 (without passing through medium 2) as shown by arrow FF, whereas light rays falling on the front side recessed surfaces 556 transmit through medium 2 but
 30 are reflected by the back reflective coating 56 as illustrated by arrow GG.

It should be appreciated from these variations that other structures and configurations of the phase shifter array 108 may be used.

Having now fully described the invention, it should be apparent to one of ordinary skill in the art that many modifications can be made hereto without departing from the scope as claimed.

CLAIMS

1. An optical interference device comprising
a phase shifter array for receiving a collimated beam of light, the phase
5 shifter array having an array of cells for producing optical light channels from
respective rays of the collimated beam of light, at least some of the optical light
channels having varying phase shifts;
a focusing element having a focal distance and arranged to
simultaneously produce, from the optical light channels, a focused beam of light
10 in its focal plane and an image downstream the phase shifter array for detection
by an optical detector; and
an optical spatial filter arranged at the focal distance of the focusing
element and arranged to filter the focused beam of light to produce a spatially
distributed interference light pattern in zeroth order for detection by the optical
15 detector.
2. An optical interference device according to claim 1, wherein the focusing
element includes a lenslet array, with each lenslet arranged to receive some of
the optical light channels or a respective optical light channel.
- 20 3. An optical interference device according to claim 2, wherein the spatial
filter includes an aperture array, with each aperture arranged at the focal
distance of the respective lenslet of the lenslet array.
- 25 4. An optical interference device according to any preceding claim, wherein
at least some of the cells of the array of cells are blank cells which do not affect
the phase of the rays incident on the respective blank cells.
5. An optical interference device according to any preceding claim, wherein
30 at least some of the cells of the array of cells includes a lamellar structure.
6. An optical interference device according to claim 5, wherein the lamellar
structure includes alternately raised and recessed surfaces.

7. An optical interference device according to claim 6, wherein the lamellar structure includes an even number of the raised and recessed surfaces.
- 5 8. An optical interference device according to claim 6, wherein the lamellar structure includes an odd number of the raised and recessed surfaces.
9. An optical interference device according to claim 6, wherein the alternately raised and recessed surfaces form a concentric pattern.
- 10 10. An optical interference device according to any preceding claim, wherein the focusing element is a focusing lens or mirror.
11. An optical interference device according to any preceding claim, further
15 comprising an optical collimator arranged to produce the collimated beam of light.
12. An optical interference device according to claim 11, further comprising
20 an entrance aperture for directing an incident light towards the optical collimator.
13. An optical interference device according to any preceding claim, wherein
an interferogram is derived from the spatially distributed interference light
pattern, and a spectrum is derived from the interferogram by using a system of
25 linear equations.
14. An optical interference device according to claim 13, wherein the linear
equations include using matrix inversion.
- 30 15. An optical interference device according to any preceding claim in the form of a Fourier spectrometer.

16. An optical interference device according to any preceding claim in the form of a Raman spectrometer.

17. An optical interference device according to any preceding claim, further comprising a further phase shifter array arranged adjacent to the phase shifter array, wherein the further phase shifter array is arranged to receive a reference beam of light.

18. In combination, an optical interference device of any of the preceding claim, the optical interference device including an optical housing for housing the optical collimator, the phase shifter array, the focusing lens and the spatial filter, and a portable computing device having the optical detector in the form of a camera or focal plane array, the optical housing being adapted to be fitted to the camera or focal plane array wherein the camera is being configured to detect the spatially distributed interference light pattern.

19. A phase shifter array for receiving a collimated beam of light, the phase shifter array having an array of cells for producing optical light channels from respective rays of the collimated beam of light, at least some of the optical light channels having varying phase shifts;

wherein the array of cells includes at least some blank cells which do not affect the phase of the rays incident on the respective blank cells; and a lamellar structure having cells of varying depths for producing the optical light channels having varying phase shifts.

20. A phase shifter array according to claim 19, wherein the blank cells are generally flat.

21. A phase shifter array according to claim 19 or 20, wherein the lamellar structure includes alternately raised and recessed surfaces.

22. A phase shifter array according to claim 19 or 20, wherein the lamellar structure includes an even number of the raised and recessed surfaces.

23. A phase shifter according to claim 19 or 20, wherein the lamellar structure includes an odd number of the raised and recessed surfaces.

5 24. A phase shifter according to claim 19 or 20, wherein the alternately raised and recessed surfaces form a concentric pattern.

25. A method for producing a spatially distributed interference light pattern, comprising

10 receiving a collimated beam of light,
producing optical light channels from respective rays of the received collimated beam of light, at least some of the optical light channels having varying phase shifts;

providing a focusing element having a focal distance;

15 simultaneously producing, by the focusing element, from the optical light channels, a focused beam of light in its focal plane and an image downstream for detection by an optical detector; and

providing an optical spatial filter at the focal distance of the focusing element and filtering the focused beam of light by the optical spatial filter to
20 produce the spatially distributed interference light pattern in zeroth order for detection by the optical detector.