

- 1 -

Dielectric insulation medium

The present invention relates to a dielectric insulation medium, according to the preamble of claim 1, and to the use of a fluoroketone in such an insulation medium, according to the preamble of claim 9. The invention further relates to an apparatus for the generation, the distribution or the usage of electrical energy, according to the preamble of claim 11 and a dimensioning method of claim 23.

10 Dielectric insulation media in liquid or gaseous state are conventionally applied for the insulation of an electrical active part in a wide variety of electrical apparatuses, such as switchgears or transformers.

In medium or high voltage metal-encapsulated switchgears, for example, the electrical active part is arranged in a gas-tight housing, which defines an insulating space, said insulation space comprising an insulation gas usually with several bar pressure and separating the housing from the electrical active part without letting electrical current to pass through. Thus, metal-encapsulated switchgears allow for a much more space-saving construction than switchgears which are mounted outdoors and insulated solely by ambient air. For interrupting the current in a high voltage switchgear, the insulating gas further functions as an arc extinction gas.

Conventionally used insulation gases with high insulation and switching performance have some environmental impact when released to the atmosphere. So far, the high global warming potential (GWP) of these insulation gases has been coped with by strict gas leakage control in gas-insulated

- 2 -

apparatuses and by very careful gas handling. Conventional environmental-friendly insulation gases like e.g. dry air or CO₂ have a quite low insulation performance, so that gas pressure and/or insulation distances would have to be
5 increased.

For the reasons mentioned above, efforts have been made in the past to replace these conventional insulation gases by suitable substitutes.

For example, WO 2008/073790 discloses a dielectric gaseous
10 compound which - among other characteristics - has a boiling point in the range between about -20°C to about -273°C, which is low, preferably non-ozone depleting and which has a GWP less than about 22,200. Specifically, WO 2008/073790 discloses a number of different compounds
15 which do not fall within a generic chemical definition.

Further, US-A-4175048 relates to a gaseous insulator comprising a compound selected from the group of perfluorocyclohexene and hexafluoroazomethane, and EP-A-0670294 discloses the use of perfluoropropane as a
20 dielectric gas.

EP-A-1933432 refers to trifluoroiodomethane (CF₃I) and its use as an insulating gas in a gas-insulated switchgear. In this regard, the document mentions both the dielectric strength and the interrupting performance to be important
25 requirements for an insulating gas. CF₃I has according to EP-A-1933432 a GWP of 5 and is thus considered to cause relatively low environmental load. However, because of the relative high boiling point of CF₃I (-22°C) gas mixtures with CO₂ are taught. Additionally, pure CF₃I-gas has about
30 the same insulation performance as conventional insulation media having a high insulation and switching performance,

- 3 -

so that the proposed gas mixtures have around 80% of the specific insulation performance of a pure conventional insulation medium which would have to become compensated by increased filling pressure and/or larger insulation
5 distance.

Therefore there is an ongoing need for an insulation medium which causes even less environmental load than CF_3I and does not require an increase of the gas pressure and/or the insulation distances above today usual values.

10 In view of this, the objective of the present invention is thus to provide an insulating medium having a reduced GWP, but having at the same time comparable or even improved insulation properties in comparison to the known insulation media without an increase of the gas pressure
15 and/or the insulation distances above today applied values.

This objective is achieved by the insulation medium according to claim 1. Preferred embodiments of the invention are given in the dependent claims.

20 The invention is based on the surprising finding that by using a fluoroketone having from 4 to 12 carbon atoms an insulation medium having high insulation capabilities, in particular a high dielectric strength (or breakdown field strength), and at the same time an extremely low global
25 warming potential (GWP) can be obtained.

In general, the fluoroketone according to the present invention has the general structure



- 4 -

wherein R1 and R2 are at least partially fluorinated chains, said chains being independently from each other linear or branched and having from 1 to 10 carbon atoms. The definition encompasses both perfluorinated ketones as
5 well as hydrofluorinated ketones.

Generally, the fluoroketone used according to the present invention has a boiling point of at least -5°C at ambient pressure which is in clear contrast to the teaching of the state of the art and in particular of WO 2008/073790 which
10 teaches a boiling point of -20°C or lower to be an essential feature of a feasible dielectric compound.

Preferably, the fluoroketone has from 4 to 10 carbon atoms, more preferably from 4 to 8 carbon atoms, and most preferably 6 carbon atoms (also referred to as a C6-
15 fluoroketone). As mentioned above, said C6-fluoroketone can be a perfluorinated ketone (having the molecular formula $C_6F_{12}O$) or a hydrofluorinated ketone.

In use, the insulation medium can be both in liquid and gaseous state. In particular, the insulation medium can be
20 a two-phase system comprising the fluoroketone both in liquid and gaseous state. More particularly, the insulation medium can be an aerosol comprising droplets of the fluoroketone dispersed in a gas phase comprising fluoroketone in gaseous state.

For many applications, it is preferred that the insulation
25 medium comprises an insulation gas comprising the fluoroketone at operational conditions. This is in particular the case for an insulation medium used for high voltage switching in a corresponding switchgear.

- 5 -

If an insulation gas is used, it can either be a gas mixture, which apart from the fluoroketone preferably comprises air or at least one air component, in particular selected from the group consisting of carbon dioxide (CO₂),
5 oxygen (O₂) and nitrogen (N₂), as buffer or carrier gas. Alternatively, the insulation gas can substantially consist of fluoroketone.

The insulation properties of the insulation gas, and in particular its breakdown field strength, can be controlled
10 by the temperature, pressure and/or composition of the insulation medium. If a two-phase system comprising the fluoroketone both in liquid and gaseous state is used, an increase of the temperature does not only result in an increase of the absolute pressure, but also in an increase
15 of the fluoroketone's concentration in the insulation gas due to a higher vapour pressure.

It has been found that for many applications of the insulation gas, such as applications in the medium voltage range, a sufficient molar ratio, i.e. the ratio between
20 the number of molecules of the fluoroketone to the number of molecules of the remaining components of the medium (generally the carrier or buffer gas), and thus also a sufficient breakdown field strength can be achieved even at very low operational temperatures e.g. of down to about
25 -30°C or even -40°C, without additional measures such as external heating or vaporization.

If a higher concentration of the fluoroketone in the insulation gas is desired to increase the breakdown field strength, which may in particular be the case in high
30 voltage applications, the pressure, the composition and/or the temperature of the insulation medium can be adapted

- 6 -

accordingly. A way how to deduce the parameters required to obtain a desired breakdown field strength will be further exemplified in the context of the Figures below.

5 The dielectric insulation medium of the present invention can be used in any apparatus for the generation, the distribution or the usage of electrical energy, particularly in a switchgear or a part and/or component thereof.

10 For high voltage switching, for example, the interrupting capability (or arc extinction capability) of the insulation medium is of particular importance. It has surprisingly been found that the medium according to the present invention not only has a comparable or even improved insulating capability compared to the above
15 mentioned conventional insulation media, but also a sufficient arc extinction capability. Without any intention to be bound by the theory it is assumed that this arc extinction capability can at least partially be attributed to the recombination of the dissociation
20 products of the fluoroketone inside the arcing region mainly to tetrafluoromethane (CF_4) which is well known to be a highly potent arc extinction medium.

Another important aspect during arc interruption is the temperature increase of the switching gas in the whole
25 vessel which may lead to insulation failures to the grounded vessel even after successful arc interruption inside the switching gap, especially after heavy fault interruption in metal-encapsulated circuit breakers. Due to the decomposition of fluoroketones at moderate
30 temperatures (e.g. around 550°C to 570°C for C6-fluoroketone) to lower fluorocarbons, the injected heat

- 7 -

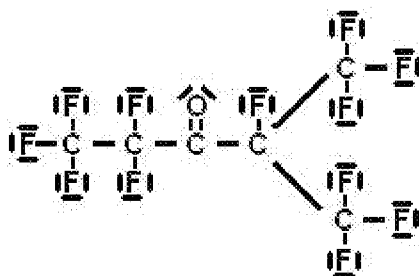
energy in the exhaust volumes does not lead to temperatures above these dissociation temperatures, until all fluoroketone is dissociated. If sufficient fluoroketone is provided, the exhaust gas temperature
5 therefore cannot exceed the above mentioned temperatures leading to a good insulation performance also shortly after the interruption of a heavy fault current in a metal-encapsulated high-voltage circuit breaker.

Among the most preferred fluoroketones having 6 carbon
10 atoms, dodecafluoro-2-methylpentan-3-one has been found to be particularly preferred for its high insulating properties and its extremely low GWP.

Dodecafluoro-2-methylpentan-3-one (also named 1,1,1,2,2,4,5,5,5-nonafluoro-4-(trifluoromethyl)-3-
15 pentanone, perfluoro-2-methyl-3-pentanone or $\text{CF}_3\text{CF}_2\text{C}(\text{O})\text{CF}(\text{CF}_3)_2$) has previously only been considered useful for completely different applications, namely the processing of molten reactive metals (as referred to in WO 2004/090177), for the cleaning of a vapour reactor (as
20 referred to in WO 02/086191) and in fire extinction systems, or in liquid form for cooling of electronic systems, or for the Rankine-process in small power plants (as referred to in EP-A-1764487).

Dodecafluoro-2-methylpentan-3-one is clear, colorless and
25 almost odourless. Its structural formula is given in the following:

- 8 -



Dodecafluoro-2-methylpentan-3-one has an average lifetime in the atmosphere of about 5 days and its GWP is only about 1. In addition, its ozone depletion potential (ODP) is zero. Thus, the environmental load is much lower than the one of conventional insulation gases.

In addition, dodecafluoro-2-methylpentan-3-one is non-toxic and offers outstanding margins of human safety. This is in contrast to fluoroketones having less than 4 carbon atoms, such as hexafluoroacetone (or hexafluoropropanone), which are generally toxic and very reactive.

Dodecafluoro-2-methylpentan-3-one has a boiling point of 49.2°C at 1 bar. Its vapour pressure, i.e. the pressure of the vapor in equilibrium with its non-vapor phases, is about 40 kPa at 25°C. Given the high vapour pressure of dodecafluoro-2-methylpentan-3-one, an insulation gas having a breakdown field strength sufficient for many applications, in particular in the medium voltage range, can in general also be achieved at very low temperatures down to -30°C.

If the insulation medium is an insulation gas, as it is for example preferably the case in a circuit breaker of a high voltage switchgear, dodecafluoro-2-methylpentan-3-one can either be provided in a gas mixture, which preferably

- 9 -

further comprises air or at least one air component functioning as a carrier or buffer gas. Alternatively, the insulating gas can substantially consist of dodecafluoro-2-methylpentan-3-one.

- 5 Based on the finding that at a temperature of 550°C or higher, dodecafluoro-2-methylpentan-3-one is decomposed to very reactive fluorocarbon compounds having a lower number of carbon atoms, it is preferred that the insulating gas comprises sufficient oxygen (O₂) with which the
10 fluorocarbon compounds formed can react to form inert compounds, such as e.g. CO₂.

According to a particularly preferred embodiment of the present invention, the molar ratio of the fluoroketone, in particular of dodecafluoro-2-methylpentan-3-one, in the
15 insulation gas is at least 1%, preferably at least 2%, more preferably at least 5%, more preferably at least 10%, most preferably at least 15%. These preferred molar ratios refer to a given standard or prescribed operating condition. Under deviating conditions, the molar ratio may
20 still vary from these preferred values.

The significance of an insulating medium comprising dodecafluoro-2-methylpentan-3-one in a molar ratio of at least 1%, or 2% respectively, is based on the finding that an insulation gas having this molar ratio can also be
25 obtained at very low temperature conditions down to -30°C for 2% and down to -40°C for 1% and that this insulation gas has a sufficient dielectric strength for e.g. medium voltage apparatuses, such as medium voltage gas-insulated switchgears, which are operated at an insulation gas
30 pressure of around 1 bar and in particular below 1.5 bar.

- 10 -

As will be further illustrated by way of the examples, the insulating capability of an insulating gas having a molar ratio of dodecafluoro-2-methylpentan-3-one of at least 15% is (at 1 bar) even higher than that of conventional
5 insulating gases. This embodiment is thus particularly preferred.

It is a further objective of the present invention to provide improved dielectric insulation and improved electrical apparatuses comprising the insulation medium
10 described above. This objective is achieved according to claim 9 by the use of the above-described fluoroketone for dielectric insulation and, in particular, for arc extinction, and according to claim 11 by an apparatus comprising the above-described fluoroketone. Preferred
15 embodiments are disclosed and claimed in the dependent claims.

Therefore, in addition to the insulation medium described above, the present invention further relates to an apparatus for the generation, the distribution and the
20 usage of electrical energy, said apparatus comprising a housing defining an insulating space and an electrical active part arranged in the insulating space. This insulating space comprises the insulation medium described above.

25 The term "or" in the expression "apparatus for the generation, the distribution or the usage of electrical energy" is in this context not to be understood as excluding combinations but is to be read as "and/or".

Also, the term "electrical active part" in this context is
30 to be interpreted broadly including a conductor, a

- 11 -

conductor arrangement, a switch, a conductive component, a surge arrester, and the like.

In particular, the apparatus of the present invention includes a switchgear, in particular an air-insulated or gas-insulated metal (or otherwise)-encapsulated switchgear, or a part and/or component thereof, in particular a bus bar, a bushing, a cable, a gas-insulated cable, a cable joint, a current transformer, a voltage transformer, a surge arrester, an earthing switch, a disconnecter, a load-break switch, and/or a circuit breaker.

Switchgears, in particular gas-insulated switchgears (GIS), are well known to a person skilled in the art. An example of a switchgear for which the present invention is particularly well suited is for example shown in EP-A-1933432, paragraphs [0011] to [0015], the disclosure of which is incorporated herewith by reference.

It is further preferred that the apparatus is a switch, in particular an earthing switch (e.g. a fast acting earthing switch), a disconnecter, a load-break switch or a circuit breaker, in particular a medium-voltage circuit breaker, a generator circuit breaker and/or a high-voltage circuit breaker.

According to another preferred embodiment, the apparatus can be a transformer, in particular a distribution transformer or a power transformer.

According to still other embodiments, the apparatus can also be, e.g., an electrical rotating machine, a generator, a motor, a drive, a semiconducting device, a

- 12 -

computing machine, a power electronics device, and/or a component thereof.

The invention particularly relates to a medium or high voltage apparatus. The term "medium voltage" as used
5 herein refers to a voltage in the range of 1 kV to 72 kV, whereas the term "high voltage" refers to a voltage of more than 72 kV. Applications in the low voltage range below 1 kV are feasible, as well.

In order to set the respective parameters to the required
10 value for achieving a desired breakdown field strength, the apparatus can comprise a control unit (also referred to as "fluid management system") for controlling individually or in combination the composition - in particular the chemical composition or the physical phase
15 composition, such as a gas/liquid two-phase system - and/or the temperature of the insulation medium as well as the absolute pressure, the gas density, the partial pressure and/or the partial gas density of the insulation medium or at least one of its components, respectively. In
20 particular, the control unit can comprise a heater and/or vaporizer in order to control the vapour pressure of the fluoroketone according to the invention. The vaporizer can e.g. be an ultrasound vaporizer, or can comprise spraying nozzles for spraying the insulation medium into the
25 apparatus.

In an exemplary embodiment for high voltage applications, a partial pressure of the fluoroketone can be provided in the insulating medium by heating and/or vaporizing, such that the partial pressure of fluoroketone is maintained at
30 a pressure level of at least 0.6 bar in gas-insulated switchgears (GIS) busbars or gas-insulated transmission

- 13 -

lines (GITL), corresponding to conventional insulation distances (with approximately required field strengths of about 300 kV/cm) and conventional pressure levels of e.g. about 4 bar. Accordingly, in a high-voltage circuit
5 breaker the heating and/or vaporizing shall be adapted such that the partial pressure of the fluoroketone is maintained at a pressure level of at least 0.9 bar, corresponding to conventional insulation distances (with approximately required field strengths of about 440 kV/cm)
10 and conventional pressure levels of e.g. about 6 bar.

If a vaporizer is used, it usually also comprises a dosing unit to set the concentration of the fluoroketone in the insulation medium according to needs of breakdown field strength. This will exemplarily be shown in more detail
15 below for a high voltage gas-insulated switchgear. Furthermore, the control unit may comprise a measuring unit for measuring the control parameters, such as temperature, pressures and/or composition - in particular the liquid phase level - and/or a monitoring unit for
20 monitoring such parameters.

The invention is further illustrated by way of the following Example in combination with the Figures of which

Figure 1a shows a graphical representation of the pressure reduced breakdown field of an
25 insulating medium according to the present invention as a function of its mole fraction of dodecafluoro-2-methylpentan-3-one in comparison to the breakdown field of conventional insulation gases;

- 14 -

Figures 1b, 1c show the absolute pressure of the insulation medium as a function of the partial pressure of dodecafluoro-2-methylpentan-3-one

5 Figure 2 shows a graphical representation of the vapour pressure of dodecafluoro-2-methylpentan-3-one as a function of the temperature;

10 Figure 3a, 3b, 3c show for various concentration levels, i.e. mole fractions, of dodecafluoro-2-methylpentan-3-one in air as carrier gas the respective pressure and temperature values at which an exemplary breakdown field strength of 440 kV/cm or 50 kV/cm is
15 achieved;

Figure 4 shows a purely schematic representation of a high voltage gas-insulated switchgear according to the present invention comprising a temperature control unit; and

20 Figure 5 shows a purely schematic representation of a high voltage gas-insulated switchgear according to the present invention comprising a fluid handling unit.

Examples

25 For measuring the breakdown field strength of an insulation medium according to the present invention, a test vessel comprising dodecafluoro-2-methylpentan-3-one (Novec 649, available from 3M) was evacuated down to about 140 mbar and the pressure was successively increased by
30 adding ambient air as buffer gas up to about 5 bar. For

- 15 -

selected mole fractions of dodecafluoro-2-methylpentan-3-one in the resulting insulation gas, the breakdown field strength was determined in a pin-plate electrode arrangement under dc-voltage applied.

5 As shown in Fig. 1a, the pressure-reduced breakdown field strength for the insulation medium according to the present invention increases linearly as a function of an increasing mole fraction of the fluorketone of the present invention, here selected to be dodecafluoro-2-
10 methylpentan-3-one. At a mole fraction above 15%, the insulation medium according to the present invention has a breakdown voltage higher than the most conventional insulation gas according to the state of the art.

Fig. 1b and 1c show the absolute filling pressure of the
15 insulation medium according to the present invention as a function of the mole fraction of the fluorketone of the present invention, here selected to be dodecafluoro-2-methylpentan-3-one. Fig. 1b and 1c are obtained from Fig. 1a by choosing a permissible field strength of the
20 electrical apparatus, by transforming the abscissa (y-axis) of Fig. 1a by dividing the values by the permissible field strength and inverting the resulting values to arrive at an absolute pressure scale and hence absolute pressure curve, and by multiplying the ordinate (x-axis)
25 with the absolute pressure curve to arrive at the partial pressure of the fluorketone of the invention, here preferably of dodecafluoro-2-methylpentan-3-one. The permissible field strength is chosen to be exemplarily 440 kV/cm in Fig. 1b and 50 kV/cm in Fig. 1c.

30 In Fig. 2, the vapour pressure of dodecafluoro-2-methylpentan-3-one as a function of the temperature is

- 16 -

shown. The (absolute) pressure of the insulating gas shall be chosen such that given the partial gas pressure of the fluoroketone (defined by the minimal operating temperature according to Figure 2) the desired breakdown field strength is obtained.

As well, an operating temperature can be determined for a given breakdown field strength and absolute pressure of the system. For example, a breakdown field strength of 440 kV/cm at an absolute pressure of 2.5 bar is according to Fig. 1 achieved at a molar ratio of dodecafluoro-2-methylpentan-3-one of 0.5. The partial pressure of dodecafluoro-2-methylpentan-3-one in the insulation gas is thus 1.25 bar. According to Fig. 2, this partial pressure is obtained at a temperature of 56°C.

From Figures 1b or 1c in combination with Figure 2, a method for selecting the parameters of the insulation medium, such as absolute filling pressure, molar fraction or partial pressure of fluoroketone and fluid management, in particular heating and/or vaporization of liquid phase fluoroketone, and/or fluid reserve management of liquid phase fluoroketone, can be deduced.

This method comprises the steps of:

- determining for a given electrical apparatus a permissible electrical field strength of the desired insulation medium and a minimal permissible operating temperature of the desired insulation medium,
- determining from the pressure-reduced breakdown field strength of the desired insulation medium as a function of the molar fraction of the fluoroketone of the invention (see e.g. Fig. 1a), hereinafter

- 17 -

preferably with 6 to 9 C-atoms and more preferably dodecafluoro-2-methylpentan-3-one, and from the permissible field strength the absolute pressure curve of the insulation medium as a function of the partial pressure of the fluorketone (see e.g. Fig. 1b or Fig. 1c),

- selecting a desired absolute filling pressure of the insulation medium (which is typically defined for some standard conditions and may, e.g., be based on constructive and/or operational constraints of the electrical apparatus),
- determining from the absolute pressure curve the minimal required partial pressure of the fluorketone, and from the vapour pressure curve the corresponding vaporization temperature of the fluorketone, and
- determining whether the vaporization temperature is above the minimal permissible operating temperature of the desired insulation medium, and
- only if the vaporization temperature is below the minimal permissible operating temperature of the desired insulation medium, providing a fluid management system, in particular means for heating and/or vaporization and/or fluid reserve management of liquid phase fluorketone, for maintaining the partial pressure above the minimal required partial pressure.

A further detailed example is shown in Fig. 1c in connection with Fig. 2 for a medium-voltage apparatus being rated to a given voltage level, from which the permissible electrical field strength of the desired

- 18 -

insulation medium can be derived (e.g. 50 kV/cm), and being rated to an ambient temperature, from which the minimal permissible operating temperature of the desired insulation medium can be derived (e.g. -25°C). According to Fig. 2 extrapolated to -25°C, the partial pressure of fluorketone of the invention, here exemplarily dodecafluoro-2-methylpentan-3-one, at -25°C is approximately 0.025 bar, which according to Fig. 1c requires approximately 0.95 bar absolute filling pressure. This is below the (e.g. apparatus-specific) permissible filling pressure of e.g. 1.2 bar, such that no active vaporization of liquid fluorketone is needed.

A further dimensioning rule relates to the maximal permissible operating temperature of the desired insulation medium, e.g. 105°C in high-voltage or medium-voltage apparatuses. According to Fig. 2, 105°C corresponds to a fluorketone partial pressure 5 bar, which may result in the absolute pressure exceeding all permissible (e.g. apparatus-specific) pressure limits. This shall be avoided by limiting the amount of available liquid fluorketon and/or limiting the temperature, e.g. by active cooling. Therefore, in the apparatus a reserve volume of liquid fluorketone and/or a maximal permissible operating temperature of the desired insulation medium shall be limited such that the absolute filling pressure is maintained below a given pressure limit of the apparatus (maximal permissible operating pressure). The apparatus shall thus have a reserve volume of liquid fluorketone and/or means for limiting a maximal permissible operating temperature of the desired insulation medium such that the absolute filling pressure is maintained below a given pressure limit of the apparatus.

- 19 -

Fig. 3a, 3b and 3c show further the relationship between the absolute filling pressure and the temperature of the insulation gas required to obtain a given breakdown field strength (=permissible electrical field strength, here exemplarily 440 kV/cm and 50 kV/cm, respectively) for various molar fractions M of the fluoroketone of the invention. As is apparent, the dielectric field strength of the insulation gas can be increased by increasing the molar ratio M of the fluoroketone, in this particular case of dodecafluoro-2-methylpentan-3-one, and/or by increasing the total or absolute filling pressure. In Fig. 3a for example, a high-voltage breakdown field strength of 440 kV/cm is achieved at a pressure of about 7 bar and a temperature of about 22°C, the molar ratio of the fluoroketone being 5%. The same breakdown field strength is achieved at a pressure of less than 2 bar, but a temperature of 60°C, the molar ratio of fluoroketone being 100%.

In Fig. 3b for example, a medium-voltage breakdown field strength of 50 kV/cm is achieved at an absolute filling pressure of about 0.8 bar and a temperature of about -20°C, the molar ratio of the fluoroketone being 5%. The same breakdown field strength is achieved at a pressure of about 0.1 bar and a temperature of about 5°C, the molar ratio M of fluoroketone being 100%.

Fig. 3c shows once more the admissible parameter range for the case of a high-voltage breakdown field strength of 440 kV/cm. The horizontal dashed line between points 1 and 2 represents the apparatus-specific maximal permissible absolute pressure, here e.g. 6 bar. The vertical dashed line between points 2 and 3 represents the maximal permissible operating temperature, here e.g. 105°C. The

- 20 -

limiting absolute pressure curve for molar ratio $M=100\%$ extends between points 4 and 3. The drawn-through curve between points 1 and 4 is the absolute pressure curve as a function of temperature and of molar ratio of fluorketone of the invention, here e.g. dodecafluoro-2-methylpentan-3-one, as taken from Fig. 3a. The encircled area, i.e. the area delimited by the lines connecting in sequence the points 1-2-3-4-1, defines the range of admissible parameters, namely absolute filling pressures, operating temperatures of the desired insulation medium, and molar ratios (or correspondingly partial pressures) of the fluorketone of the invention for a selected breakdown field strength or permissible electrical field strength.

As mentioned above, the electrical apparatus of the present invention can comprise a control unit (or "fluid management system") in order to adapt the pressure, the composition and/or the temperature of the insulating medium.

As an example, a high voltage switchgear comprising a temperature control unit is shown in Fig. 4. The switchgear 2 comprises a housing 4 defining an insulating space 6 and an electrical active part 8 arranged in the insulating space 6. The switchgear 2 further comprises a temperature control unit 10a for setting the housing 4, or at least a part of the housing 4, of the switchgear and thus the insulation medium comprised in the insulating space 6 to a desired temperature. Of course, any other part in contact with the insulation medium can be heated in order to bring the insulation medium to the desired temperature. Thus, the vapour pressure of the fluoroketone - and consequently its molar ratio in the insulation gas - as well as the absolute pressure of the insulation gas can

- 21 -

be adapted accordingly. As also shown in Fig. 4, the fluoroketone is in this embodiment not homogenously distributed throughout the insulating space due to the temperature gradient given in the insulation space. The
5 concentration of the fluoroketone is thus higher in close proximity to the walls 4' of the housing 4.

An alternative control unit or fluid management system is schematically shown in Fig. 5 in which a fluid handling unit 10b is attributed to the gas-insulated switchgear as
10 the control unit. According to this control unit, the composition of the insulating medium, and in particular its concentration of the fluoroketone, is adjusted in a respective dosing unit comprised in the fluid handling unit 10b, and the resulting insulation medium is injected
15 or introduced, in particular sprayed, into the insulating space 6. In the embodiment shown in Fig. 5, the insulation medium is sprayed into the insulating space in the form of an aerosol 14 in which small droplets of liquid fluoroketone are dispersed in the respective carrier gas.
20 The aerosol 14 is sprayed into the insulating space 6 by means of nozzles 16 and the fluoroketone is readily evaporated, thus resulting in an insulating space 6 with an inhomogenous concentration of fluoroketone, specifically a relatively high concentration in close
25 proximity of the housing wall 4' comprising the nozzles 16. Alternatively, the insulation medium, in particular its concentration, pressure and temperature, can be controlled in the fluid handling unit 10b before being injected into the insulation space. In order to ensure
30 circulation of the gas, further openings 18 are provided in the upper wall 4'' of the housing 4, said openings leading to a channel 20 in the housing 4 and allowing the insulating medium to be removed from the insulating space

- 22 -

6. The switchgear with fluid handling unit 10b, as shown in Fig. 5, can be combined with the temperature control unit 10a described in connection with Fig. 4. If no temperature control unit is provided, condensation of the fluoroketone can occur. The condensed fluoroketone can be collected and reintroduced into the circulation of the insulation medium.

In the context of the switchgears shown in Fig.s 4 and 5 it is noted that nominal current load generally facilitates the vaporization of the fluoroketone by the ohmic heating of current carrying conductors.

List of reference numerals

2	switchgear
4	housing
15 4'	housing wall
4''	upper wall of the housing
6	insulating space
8	electrical active part
10a	temperature control unit
20 10b	fluid handling unit
14	aerosol
16	nozzle
18	opening
M	molar ratio of fluorketone.

Claims

1. Dielectric insulation medium, characterized in that said insulation medium comprises a fluoroketone having from 4 to 12 carbon atoms.
- 5 2. Insulation medium according to claim 1, characterized in that the fluoroketone has the general structure
$$R1-CO-R2$$
wherein R1 and R2 are at least partially fluorinated chains, said chains being independently from each other linear or branched and having from 1 to 10
10 carbon atoms.
3. Insulation medium according to claim 1 or 2, characterized in that the fluoroketone has a boiling point of at least -5°C at ambient pressure.
- 15 4. Insulation medium according to any of the preceding claims, characterized in that the fluoroketone has 6 carbon atoms.
5. Insulation medium according to claim 4, characterized in that the fluoroketone is dodecafluoro-2-methylpentan-3-one.
20
6. Insulation medium according to any of the preceding claims, characterized in that the insulation medium comprises an insulation gas comprising the fluoroketone at operational conditions.
- 25 7. Insulation medium according to claim 6, characterized in that the molar ratio of the fluoroketone in the

- 24 -

insulation gas is at least 1%, preferably at least 2%, more preferably at least 5%, more preferably at least 10%, most preferably at least 15%.

8. Insulation medium according to claim 6 or 7,
5 characterized in that the insulation gas is a gas mixture, which further comprises air or at least one air component, in particular selected from the group consisting of carbon dioxide, oxygen and nitrogen.
9. Use of a fluoroketone according to any of claims 1 to
10 8 in a dielectric insulation medium.
10. Use of a fluoroketone according to claim 9,
characterized in that the insulation medium is used for extinguishing an arc in an electrical switch, in particular in a low voltage switch, a medium voltage
15 switch or a high voltage switch, in particular a circuit breaker.
11. Apparatus for the generation, the distribution or the usage of electrical energy, said apparatus comprising a housing defining an insulating space and an
20 electrical active part arranged in the insulating space, said insulating space comprising an insulation medium, characterized by the dielectric insulation medium according to any of the claims 1 to 8.
12. Apparatus according to any of the preceding claims,
25 the apparatus being a medium or high voltage apparatus.
13. Apparatus according to claim 10 or 11, characterized in that the apparatus is a switchgear, in particular an air-insulated or a gas-insulated metal-
30 encapsulated switchgear, or a part or component

- 25 -

thereof, in particular a bus bar, a bushing, a cable, a gas-insulated cable, a cable joint, a current transformer, a voltage transformer, and/or a surge arrester.

- 5 14. Apparatus according to any of claims 10 to 12, characterized in that the apparatus is a switch, in particular an earthing switch, a disconnecter, a load-break switch and/or a circuit breaker.
- 10 15. Apparatus according to claim 14, characterized in that the apparatus is a high voltage circuit breaker having a heating chamber for providing a self-blasting effect, and that in a switching operation the fluoroketone is decomposed to fluorocarbon compounds having a lower number of carbon atoms in
15 the heating chamber during a back-heating phase.
16. Apparatus according to claim 15, characterized in that the fluoroketone has 6 carbon atoms, and in particular is dodecafluoro-2-methylpentan-3-one.
- 20 17. Apparatus according to any of claims 10 to 12, characterized in that the apparatus is a transformer, in particular a distribution transformer or a power transformer.
- 25 18. Apparatus according to any of claims 10 to 12, characterized in that the apparatus is an electrical rotating machine, a generator, a motor, a drive, a semiconducting device, a computing machine, a power electronics device, and/or a component thereof.
- 30 19. Apparatus according to any of the preceding claims, characterized in that it further comprises a control unit for controlling individually or in combination a

- 26 -

composition, a temperature, an absolute pressure, a partial pressure, a gas density and/or a partial gas density of the insulating medium or at least one of its components, respectively.

- 5 20. Apparatus according claim 19, characterized in that the control unit comprises a heater and/or vaporizer for controlling the partial pressure of the fluoroketone and, in particular, for maintaining it above a required partial pressure level.
- 10 21. Apparatus according to any of claims 19 to 20, characterized in that the control unit (10a, 10b) comprises a temperature control unit (10a) comprising a heating system for setting the housing (4), or at least a part of the housing (4), of the apparatus to
15 a desired temperature, and/or the control unit (10a, 10b) comprises a fluid handling unit (10b) for dosing a concentration of the fluoroketone and for injecting the resulting insulation medium into the apparatus.
- 20 22. Apparatus according to any of claims 11-21, characterized by the apparatus having a reserve volume of liquid fluorketone and/or means for limiting a maximal permissible operating temperature of the desired insulation medium such that the absolute filling pressure is maintained below a given
25 pressure limit of the apparatus.
23. Method for dimensioning an electrical apparatus according to any of claims 11 to 21, characterized by the steps of
- determining for the apparatus a permissible
30 electrical field strength of the desired insulation

- 27 -

- medium and a minimal permissible operating temperature of the desired insulation medium,
- determining from the pressure-reduced breakdown field strength of the desired insulation medium as a function of the molar fraction of the fluorketone,
5 and from the permissible field strength the absolute pressure curve of the insulation medium as a function of the partial pressure of the fluorketone,
 - selecting a desired absolute filling pressure of the
10 insulation medium,
 - determining from the absolute pressure curve the minimal required partial pressure of the fluorketone, and from the vapour pressure curve the corresponding vaporization temperature of the fluorketone, and
 - determining whether the vaporization temperature is
15 above the minimal permissible operating temperature of the desired insulation medium.
24. Method for dimensioning an electrical apparatus as claimed in claim 22, characterized by the further
20 step of, if the vaporization temperature is below the minimal permissible operating temperature of the desired insulation medium, providing a fluid management system, in particular the fluid management system claimed in any of claims 19-22, preferably
25 comprising means for heating and/or vaporization and/or fluid reserve management of liquid phase fluorketone, for maintaining the partial pressure above the minimal required partial pressure.