

DATA SIGNAL CONTROLLED
OSCILLATOR FOR A VIDEO DISPLAY

The invention relates to an oscillator of a video display apparatus having a frequency that is controlled by a data signal.

5 Television displays of television signals are generated by repetitively scanning an electron beam over the surface of a picture tube viewing screen. The beam intensity is modulated by video signals to form images on the screen representative of the picture to be displayed. In order to synchronize the scanning of
10 the beam with the display information, the scanning or deflection circuits are synchronized with a synchronizing signal combined with the image information in a composite video signal. As received, the synchronizing signal may contain distortions in the form of electrical noise.

15 As transmitted, the synchronizing signal pulses recur at a rate which is stable. Because of the presence of noise it has become common practice to obtain synchronization of the horizontal deflection circuit with the horizontal synchronizing signal pulses by the use of a voltage controlled oscillator. The
20 oscillator is controlled by and is included in a phase-lock loop (PLL). The oscillator generates a signal at a frequency that is equal to the frequency of the synchronizing signal frequency f_H or its multiple. Because of the PLL operation, when, for example, one synchronizing pulse is obscured by noise, the rate of the oscillator,
25 nevertheless, remains substantially unchanged, and the deflection circuits continue to receive regular deflection control pulses.

Typically, the free-running frequency of the oscillator is determined by a capacitance. Disadvantageously, the capacitor has a wide range of tolerance spread. Therefore, the oscillator
30 free-running frequency may need to be adjusted to compensate for the wide range of tolerance spread. In one prior art arrangement, the oscillator frequency is adjusted according to data signal obtained via a bus from a microprocessor. A digital-to-analog (D/A) converter produces an analog signal at a level that
35 is determined by the data signal for controlling the free-running frequency of the oscillator.

Typically, various power supply voltages for operating stages in the television receiver are produced from retrace pulse



voltages produced in a horizontal flyback transformer. Such supply voltage is at a magnitude that is dependent on the frequency of the horizontal oscillator. Because in normal operation the horizontal oscillator frequency is constant, its effect on the supply voltage is predictable and is taken into account in the design of the power supply. However, should erroneous data signal be developed on the aforementioned bus, the horizontal frequency may become, for example, too low. Too low frequency could result in a destruction of a horizontal output transistor and/or in excessive supply voltages. Excessive supply voltages could harm the energized stages of the receiver. The erroneous data signal can occur as a result of malfunction of the microprocessor because of, for example, arcing. It may be desirable to adjust the free-running frequency of the oscillator over a wide range to compensate for the tolerance spread, during manufacturing, but to limit the frequency variation range of the oscillator, during normal operation. In this way, bit error on the bus is prevented from causing a potentially harm producing variation in the oscillator frequency.

A video display deflection, embodying an aspect of the invention, includes an oscillator for generating an output signal at a frequency related to a deflection frequency. A microprocessor develops a first data signal that is susceptible to being altered, when a fault condition occurs during operation in the microprocessor. A second data signal that cannot be altered via the microprocessor, during operation, is generated. A digital-to-analog converter having a first input responsive to the first data signal and a second input responsive to the second data signal generates an analog frequency control signal that is coupled to a control input of the oscillator to control a free-running frequency of the oscillator within a tolerance range. The free-running frequency of the oscillator is compensated partly in accordance with the first data signal and partly in accordance with the second data signal. A deflection circuit output stage is responsive to the oscillator output signal for generating a deflection current in a deflection winding.



The sole FIGURE illustrates a phase-lock-loop circuit, embodying the invention, that control the phase of a deflection current in a deflection winding.

Horizontal sync pulses S_H at a frequency f_H , having a
5 period H that in NTSC is 63.5 microseconds, are coupled,
illustratively, from a conventional sync separator of a television
receiver, not shown in the FIGURE, to an input terminal 30a of a
phase detector 30. A signal O_H that, during steady state operation,
is at the frequency f_H or its multiple is coupled to a second input
10 terminal 30b of phase detector 30. A phase difference indicative
signal PH that is indicative of the phase difference between signal
 S_H and signal O_H is generated by phase detector 30 and coupled
via a voltage-to-current converter 32 that generates a current i_0 .
Current i_0 is coupled to an input terminal 33a of a current
15 summing arrangement 33. Current summing arrangement 33
produces a sum current i_{CONT} . Sum current i_{OUT} is coupled to a
frequency control input terminal 31a of a current controlled
oscillator 31 to control its oscillation frequency. Oscillator 31
generates output signal O_H . Detector 30 and oscillator 31 form a
20 phase-lock-loop circuit (PLL) 20 that may be included in a first
integrated circuit (IC) 100. The operation of PLL 20 causes signal
 O_H to be synchronized with signal S_H .

A horizontal deflection circuit output stage 99
produces in a winding 34 of a flyback transformer T_0 a retrace
25 pulse at a high voltage that is used for generating an ultor voltage
 U . Voltage U is coupled to an ultor electrode of a cathode ray
tube, not shown in the FIGURE, of the television receiver. A
supply voltage $V+$ is generated in a similar manner and energizes
a utilization circuit 98. A phase-controlled-loop, not shown, is
30 used in such a way that a deflection current i_Y in a deflection
winding L_Y is maintained in a constant phase relationship relative
to signal O_H despite varying beam current loading that loads
winding 34, in a well known manner. It may be desirable to
prevent the frequency of oscillator 31 from becoming, for
35 example, too low, to prevent harm to elements of stage 99 or of
circuit 98.

The free-running frequency of oscillator 31 is
determined, in part, by a capacitor C that is internal to IC 100 and



that is produced using IC technology. Capacitor C is subject to wide range of spread values or tolerances. To partially compensate for the wide range of tolerances of capacitor C, a microprocessor 35 that is included in a separate, second IC 200 produces a 3-bit parallel binary data signal DATA1 on a bus BUS that is coupled to IC 100. Signal DATA1 is programmable, during operation.

A D/A converter 41 produces a D.C. current i_1 that is coupled to summing arrangement 33 and summed there to form current i_{CONT} . Current i_1 varies in a range 0-15 μ A, in accordance with signal DATA1. The maximum value of current i_1 is determined by a reference current i_{41} of D/A converter 41. Current i_1 is capable of varying the free-running frequency of oscillator 31 in a narrow range of, for example, 5% of the horizontal frequency f_H .

In accordance with an inventive feature, the range of adjustment of current i_1 is narrower than ultimately used for tolerances compensation purposes. Because current i_1 can vary the frequency of oscillator 31 only in the narrow range, an error in transmission on bus BUS, advantageously, cannot cause the aforementioned harm producing change in the frequency of oscillator 31.

A D/A converter 40, that may be located in IC 100, produces a current i_2 that is coupled to arrangement 33. Current i_2 is in a range of values of 0-40 μ A that is determined by a reference current i_{40} of D/A converter 40. The sum of currents i_2 and i_1 that are included in current i_{CONT} is capable of varying the free-running frequency of oscillator 31 in a wide range of values and with sufficient accuracy for tolerance compensation purposes.

In accordance with another inventive feature, a 3-bit binary input data signal DATA2 that is applied to D/A converter 40 is programmed in hardware in a non-alterable manner, prior to packaging a wafer that includes oscillator 31. The 3-bit signal DATA2 controls the magnitude of current i_2 . A least significant bit LSB2 of signal DATA2 has a greater contribution or weight with respect to current i_{CONT} than a most significant bit MSB1 of signal DATA1.



The value of the three bits at terminals 40a, 40b and 40c of signal DATA2 are determined by the states of programmable elements Z1, Z2 and Z3 that are coupled to terminals 40a, 40b and 40c, respectively. Prior to the

5 programming, each of elements Z1, Z2 and Z3 operates as a zener diode to produce a logical level "TRUE" at terminals 40a, 40b and 40c, respectively. Programming of a given element Z1, Z2 or Z3 establishes a logical level FALSE at the corresponding terminal 40a, 40b or 40c.

10 To determine which of elements Z1, Z1 or Z3 should be programmed, signal DATA1 is applied to D/A converter 41 at a value that produces current i_1 equal to, for example, $7.5\mu\text{A}$, or mid-range value of its entire range, $0-15\mu\text{A}$. The $7.5\mu\text{A}$ value of current i_1 is obtained when the most significant bit of signal
15 DATA1 is "TRUE" and the other two bits are at "FALSE". With current i_1 at its mid-range value, zener diodes Z1, Z2 and Z3 are selected to be programmed such that current i_2 causes a free-running frequency of oscillator 31 to be equal to the nominal frequency f_H .

20 When, for example, a logical level FALSE is required to be programmed at terminal 40a, a high level programming current produced in a factory programmer unit 60 is applied via a corresponding contact needle, not shown, that is bonded to terminal 40a. The programming current is applied prior to
25 packaging a wafer that includes zener diodes Z1, Z2 and Z3, D/A converter 40 and oscillator 31. The current applied via the contact needle transforms permanently zener diode Z1 to a passive element acting as a short circuit. Thus, the logical level FALSE that is developed at terminal 40a is non-alterable, during
30 operation. After the programming operation, the contact needles are withdrawn and are no longer bonded to the wafer. Then, the wafer that includes oscillator 31 is packaged into an IC package. During the packaging process, the wafer may be stressed mechanically. This can cause a change that is too large in the
35 free-running frequency of oscillator 31.

In accordance with another inventive feature, to maintain at least 5-bit bit resolution from the combination of signals DATA1 and DATA2 over the entire tolerance range after



the packaging, reference current i_{41} is selected to have a magnitude that enables signal DATA1 to compensate for the packaging process induced frequency change. The value of current i_{41} is such that most significant bit MSB1 has a greater weight than one-half the weight of least significant bit LSB2 of signal DATA2, with respect to current i_{CONT} . In this way, the frequency tolerance range correction is, advantageously, maintained after the packaging of the wafer.

During operation, currents i_0 , i_1 , i_2 , i_3 and a bias D.C. current i_4 are summed to produce current i_{CONT} . The effect of Data signal DATA1 on the free-running frequency of oscillator 31 that is controlled by current i_{CONT} is only, for example, 5%. Advantageously, because data signal DATA2 is non-alterable and the effect of a data error in signal DATA1 is relatively small, a transmission error on bus BUS, cannot cause a significant change in the frequency of oscillator 31 that could harm stage 99 or circuit 98. Such harm might have occurred if signal DATA2 were also coupled from microprocessor 35 to D/A converter 40 via bus BUS and a transmission error occurred in data bits associated with D/A converter 40.

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WHAT IS CLAIMED IS:

1. A video display deflection comprising:
an oscillator (31) for generating an output signal (O_H) at a frequency (f_H) related to a deflection frequency (HORIZONTAL);
a microprocessor (35) for developing a first data signal (DATA) that is susceptible to being altered during operation;
a source (Z_1, Z_2, Z_3) of a second data signal (DATA 2) that cannot be altered, during operation;
a digital-to-analog converter (41,40) having a first input (MSB1-LSB1) responsive to said first data signal and a second input (MSB2-LSB2) responsive to said second data signal for generating an analog, frequency control signal (iCONT) that is coupled to a control input (33) of said oscillator to control a free-running frequency of said oscillator within a tolerance range, said free-running frequency of said oscillator being compensated partly in accordance with said second data signal such that variation of said free running frequency via said second input is prevented by said second data signal being unalterable during operation; characterized by
a deflection circuit output stage (99) responsive to said oscillator output signal for generating a deflection circuit (iy) in a deflection winding.
2. An apparatus according to Claim 1 characterized in that said second data signal (DATA 2) causes the free-running frequency of said oscillator to vary substantially less, when a fault condition occurs, than if said second data signal were susceptible to being altered via said microprocessor (31).
3. An apparatus according to Claim 1 characterized in that said oscillator (31) comprises a horizontal oscillator and said deflection circuit output stage (99) comprises a horizontal deflection circuit output stage.
4. An apparatus according to Claim 1 characterized in that said microprocessor (31) develops said first data signal





(DATA 1) on a bus (BUS) coupled to said digital-to-analog converter (41).

5. An apparatus according to Claim 1 characterized in that said second data signal (DATA 2) is developed by an operation of a passive element (Z1, Z2, Z3).

6. An apparatus according to Claim 1 characterized in that said digital-to-analog converter (40,41) comprises a first digital-to-analog converter (41) portion that is responsive to said first data signal (DATA 1) and a second digital-to-analog (40) portion that is responsive to said second data signals (DATA 2) to produce corresponding first (i1) and second (i2) portion signals that are combined to form said control signal (iCONT).

7. A video display deflection apparatus comprising:
an oscillator (31) for generating an output signal (O_H) at a frequency (f_H) related to a deflection frequency;
a microprocessor (35) for developing a first data signal (DATA 1) that is susceptible to being altered, when a fault condition occurs during operation in said microprocessor;
a source (Z1, Z2, Z3) of a second data signal (DATA 2) that cannot be altered via said microprocessor, during operation;
a digital-to-analog converter (41,40) having a first input responsive to said first data signal and a second input responsive to said second data signal for generating an analog, frequency control signal (iCONT) that is coupled to a control input of said oscillator to control a free-running frequency of said oscillator within a tolerance range, said free-running frequency of said oscillator being compensated partly in accordance with said first data signal and partly in accordance with said second data signal wherein a least significant data bit (LSB2) of said second data signal has a weight, with respect to said control signal, that is larger than a most significant data bit (MSB1) of said first data signal and all the bits of said first data signal have a combined weight that is larger than the weight of the least significant bit of said second data signal; characterized by



a deflection circuit output stage (99) responsive to said oscillator output signal for generating a deflection current (iy) in a deflection winding.

8. A video display deflection apparatus comprising:
an oscillator (31) for generating an output signal (O_H) at a frequency related to a deflection frequency;
a microprocessor (35) for developing a first data signal (DATA 1) that is susceptible to being altered, when a fault condition occurs during operation in said microprocessor;
a source of a second data signal (DATA 2) that cannot be altered via said microprocessor, during operation;
a digital-to-analog converter (40,41) having a first input responsive to said first data signal and a second input responsive to said second data signal for generating an analog, frequency control signal (iCONT) that is coupled to a control input of said oscillator to control a free-running frequency of said oscillator being compensated partly in accordance with said first data signal and partly in accordance with said second data signal wherein said oscillator is included in an integrated circuit and wherein said second data signal is programmable during the manufacturing of said integrated circuit and is non-alterable, afterwards; characterized by
a deflection circuit output stage (99) responsive to said oscillator output signal for generating a deflection current (iy) in a deflection winding.

9. An apparatus according to Claim 1 characterized in that said oscillator (31) is included in a phase-lock-loop circuit (30,32,33,31).

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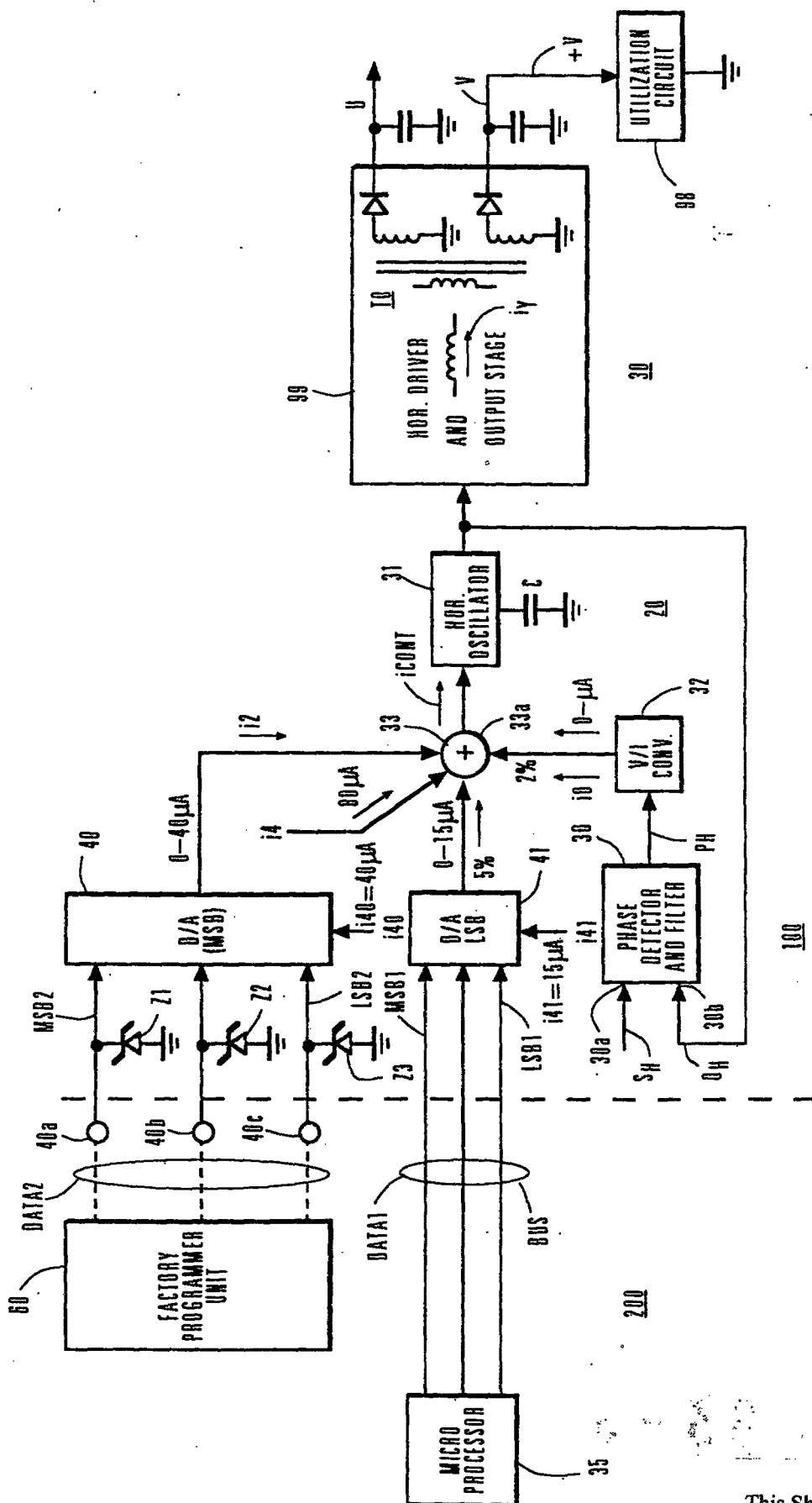
ABSTRACT

The free-running frequency of a bus controlled horizontal oscillator (31) is adjusted by programming of a first data signal (DATA 2) that is coupled to a digital-to-analog converter (40). The programming causes the first data signal to be non-alterable. The programming is done during manufacturing of a wafer that includes the oscillator. A second data signal (DATA 1) that is coupled from a microprocessor (35) via a bus (BUS) and via a second analog-to-digital converter (41) to the oscillator can vary the oscillator free-running frequency to provide for tolerance compensation. The first data signal is immune against data errors. The second data signal is not immune against data errors but can vary the oscillator frequency within only a relatively narrow range of values. Consequently, data errors are prevented from causing a significant change in the oscillator free-running frequency that might have occurred had both data signals been alterable.

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The invention relates to an oscillator of a video display apparatus having a frequency that is controlled by a data signal.

5 Television displays of television signals are generated by repetitively scanning an electron beam over the surface of a picture tube viewing screen. The beam intensity is modulated by video signals to form images on the screen representative of the picture to be displayed. In order to synchronize the scanning of
 10 the beam with the display information, the scanning or deflection circuits are synchronized with a synchronizing signal combined with the image information in a composite video signal. As received, the synchronizing signal may contain distortions in the form of electrical noise.

15 As transmitted, the synchronizing signal pulses recur at a rate which is stable. Because of the presence of noise it has become common practice to obtain synchronization of the horizontal deflection circuit with the horizontal synchronizing signal pulses by the use of a voltage controlled oscillator. The
 20 oscillator is controlled by and is included in a phase-lock loop (PLL). The oscillator generates a signal at a frequency that is equal to the frequency of the synchronizing signal frequency f_H or its multiple. Because of the PLL operation, when, for example, one synchronizing pulse is obscured by noise, the rate of the oscillator, nevertheless, remains substantially unchanged, and the deflection
 25 circuits continue to receive regular deflection control pulses.

Typically, the free-running frequency of the oscillator is determined by a capacitance. Disadvantageously, the capacitor has a wide range of tolerance spread. Therefore, the oscillator
 30 free-running frequency may need to be adjusted to compensate for the wide range of tolerance spread. In one prior art arrangement, the oscillator frequency is adjusted according to data signal obtained via a bus from a microprocessor. A digital-to-analog (D/A) converter produces an analog signal at a level that
 35 is determined by the data signal for controlling the free-running frequency of the oscillator.

Typically, various power supply voltages for operating stages in the television receiver are produced from retrace pulse

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voltages produced in a horizontal flyback transformer. Such supply voltage is at a magnitude that is dependent on the frequency of the horizontal oscillator. Because in normal operation the horizontal oscillator frequency is constant, its effect
5 on the supply voltage is predictable and is taken into account in the design of the power supply. However, should erroneous data signal be developed on the aforementioned bus, the horizontal frequency may become, for example, too low. Too low frequency could result in a destruction of a horizontal output transistor
10 and/or in excessive supply voltages. Excessive supply voltages could harm the energized stages of the receiver. The erroneous data signal can occur as a result of malfunction of the microprocessor because of, for example, arcing. It may be desirable to adjust the free-running frequency of the oscillator
15 over a wide range to compensate for the tolerance spread, during manufacturing, but to limit the frequency variation range of the oscillator, during normal operation. In this way, bit error on the bus is prevented from causing a potentially harm producing variation in the oscillator frequency.

20 A video display deflection, embodying an aspect of the invention, includes an oscillator for generating an output signal at a frequency related to a deflection frequency. A microprocessor develops a first data signal that is susceptible to being altered, when a fault condition occurs during operation in the
25 microprocessor. A second data signal that cannot be altered via the microprocessor, during operation, is generated. A digital-to-analog converter having a first input responsive to the first data signal and a second input responsive to the second data signal generates an analog frequency control signal that is coupled to a
30 control input of the oscillator to control a free-running frequency of the oscillator within a tolerance range. The free-running frequency of the oscillator is compensated partly in accordance with the first data signal and partly in accordance with the second data signal. A deflection circuit output stage is responsive to the
35 oscillator output signal for generating a deflection current in a deflection winding.

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The sole FIGURE illustrates a phase-lock-loop circuit, embodying the invention, that control the phase of a deflection current in a deflection winding.

Horizontal sync pulses S_H at a frequency f_H , having a
5 period H that in NTSC is 63.5 microseconds, are coupled,
illustratively, from a conventional sync separator of a television
receiver, not shown in the FIGURE, to an input terminal 30a of a
phase detector 30. A signal O_H that, during steady state operation,
is at the frequency f_H or its multiple is coupled to a second input
10 terminal 30b of phase detector 30. A phase difference indicative
signal PH that is indicative of the phase difference between signal
 S_H and signal O_H is generated by phase detector 30 and coupled
via a voltage-to-current converter 32 that generates a current i_0 .
Current i_0 is coupled to an input terminal 33a of a current
15 summing arrangement 33. Current summing arrangement 33
produces a sum current i_{CONT} . Sum current i_{OUT} is coupled to a
frequency control input terminal 31a of a current controlled
oscillator 31 to control its oscillation frequency. Oscillator 31
generates output signal O_H . Detector 30 and oscillator 31 form a
20 phase-lock-loop circuit (PLL) 20 that may be included in a first
integrated circuit (IC) 100. The operation of PLL 20 causes signal
 O_H to be synchronized with signal S_H .

A horizontal deflection circuit output stage 99
produces in a winding 34 of a flyback transformer T_0 a retrace
25 pulse at a high voltage that is used for generating an ultor voltage
 U . Voltage U is coupled to an ultor electrode of a cathode ray
tube, not shown in the FIGURE, of the television receiver. A
supply voltage $V+$ is generated in a similar manner and energizes
a utilization circuit 98. A phase-controlled-loop, not shown, is
30 used in such a way that a deflection current i_Y in a deflection
winding L_Y is maintained in a constant phase relationship relative
to signal O_H despite varying beam current loading that loads
winding 34, in a well known manner. It may be desirable to
prevent the frequency of oscillator 31 from becoming, for
35 example, too low, to prevent harm to elements of stage 99 or of
circuit 98.

The free-running frequency of oscillator 31 is
determined, in part, by a capacitor C that is internal to IC 100 and

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that is produced using IC technology. Capacitor C is subject to wide range of spread values or tolerances. To partially compensate for the wide range of tolerances of capacitor C, a microprocessor 35 that is included in a separate, second IC 200 produces a 3-bit parallel binary data signal DATA1 on a bus BUS that is coupled to IC 100. Signal DATA1 is programmable, during operation.

A D/A converter 41 produces a D.C. current i_1 that is coupled to summing arrangement 33 and summed there to form current i_{CONT} . Current i_1 varies in a range 0-15 μ A, in accordance with signal DATA1. The maximum value of current i_1 is determined by a reference current i_{41} of D/A converter 41. Current i_1 is capable of varying the free-running frequency of oscillator 31 in a narrow range of, for example, 5% of the horizontal frequency f_H .

In accordance with an inventive feature, the range of adjustment of current i_1 is narrower than ultimately used for tolerances compensation purposes. Because current i_1 can vary the frequency of oscillator 31 only in the narrow range, an error in transmission on bus BUS, advantageously, cannot cause the aforementioned harm producing change in the frequency of oscillator 31.

A D/A converter 40, that may be located in IC 100, produces a current i_2 that is coupled to arrangement 33. Current i_2 is in a range of values of 0-40 μ A that is determined by a reference current i_{40} of D/A converter 40. The sum of currents i_2 and i_1 that are included in current i_{CONT} is capable of varying the free-running frequency of oscillator 31 in a wide range of values and with sufficient accuracy for tolerance compensation purposes.

In accordance with another inventive feature, a 3-bit binary input data signal DATA2 that is applied to D/A converter 40 is programmed in hardware in a non-alterable manner, prior to packaging a wafer that includes oscillator 31. The 3-bit signal DATA2 controls the magnitude of current i_2 . A least significant bit LSB2 of signal DATA2 has a greater contribution or weight with respect to current i_{CONT} than a most significant bit MSB1 of signal DATA1.

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The value of the three bits at terminals 40a, 40b and 40c of signal DATA2 are determined by the states of programmable elements Z1, Z2 and Z3 that are coupled to terminals 40a, 40b and 40c, respectively. Prior to the programming, each of elements Z1, Z2 and Z3 operates as a zener diode to produce a logical level "TRUE" at terminals 40a, 40b and 40c, respectively. Programming of a given element Z1, Z2 or Z3 establishes a logical level FALSE at the corresponding terminal 40a, 40b or 40c.

10 To determine which of elements Z1, Z2 or Z3 should be programmed, signal DATA1 is applied to D/A converter 41 at a value that produces current i_1 equal to, for example, $7.5\mu\text{A}$, or mid-range value of its entire range, $0-15\mu\text{A}$. The $7.5\mu\text{A}$ value of current i_1 is obtained when the most significant bit of signal DATA1 is "TRUE" and the other two bits are at "FALSE". With current i_1 at its mid-range value, zener diodes Z1, Z2 and Z3 are selected to be programmed such that current i_2 causes a free-running frequency of oscillator 31 to be equal to the nominal frequency f_H .

20 When, for example, a logical level FALSE is required to be programmed at terminal 40a, a high level programming current produced in a factory programmer unit 60 is applied via a corresponding contact needle, not shown, that is bonded to terminal 40a. The programming current is applied prior to packaging a wafer that includes zener diodes Z1, Z2 and Z3, D/A converter 40 and oscillator 31. The current applied via the contact needle transforms permanently zener diode Z1 to a passive element acting as a short circuit. Thus, the logical level FALSE that is developed at terminal 40a is non-alterable, during operation. After the programming operation, the contact needles are withdrawn and are no longer bonded to the wafer. Then, the wafer that includes oscillator 31 is packaged into an IC package. During the packaging process, the wafer may be stressed mechanically. This can cause a change that is too large in the free-running frequency of oscillator 31.

35 In accordance with another inventive feature, to maintain at least 5-bit bit resolution from the combination of signals DATA1 and DATA2 over the entire tolerance range after

the packaging, reference current i_{41} is selected to have a magnitude that enables signal DATA1 to compensate for the packaging process induced frequency change. The value of current i_{41} is such that most significant bit MSB1 has a greater
5 weight than one-half the weight of least significant bit LSB2 of signal DATA2, with respect to current i_{CONT} . In this way, the frequency tolerance range correction is, advantageously, maintained after the packaging of the wafer.

During operation, currents i_0 , i_1 , i_2 , i_3 and a bias D.C.
10 current i_4 are summed to produce current i_{CONT} . The effect of Data signal DATA1 on the free-running frequency of oscillator 31 that is controlled by current i_{CONT} is only, for example, 5%. Advantageously, because data signal DATA2 is non-alterable and the effect of a data error in signal DATA1 is relatively small, a
15 transmission error on bus BUS, cannot cause a significant change in the frequency of oscillator 31 that could harm stage 99 or circuit 98. Such harm might have occurred if signal DATA2 were also coupled from microprocessor 35 to D/A converter 40 via bus BUS and a transmission error occurred in data bits associated with
20 D/A converter 40.

WHAT IS CLAIMED IS:

1. A video display deflection comprising:
 - an oscillator (31) for generating an output signal (O_H) at a frequency (f_H) related to a deflection frequency (HORIZONTAL);
 - a microprocessor (35) for developing a first data signal (DATA) that is susceptible to being altered during operation;
 - a source (Z_1, Z_2, Z_3) of a second data signal (DATA 2) that cannot be altered, during operation;
 - a digital-to-analog converter (41,40) having a first input (MSB1-LSB1) responsive to said first data signal and a second input (MSB2-LSB2) responsive to said second data signal for generating an analog, frequency control signal (iCONT) that is coupled to a control input (33) of said oscillator to control a free-running frequency of said oscillator within a tolerance range, said free-running frequency of said oscillator being compensated partly in accordance with said second data signal such that variation of said free running frequency via said second input is prevented by said second data signal being unalterable during operation; characterized by
 - a deflection circuit output stage (99) responsive to said oscillator output signal for generating a deflection circuit (iy) in a deflection winding.
2. An apparatus according to Claim 1 characterized in that said second data signal (DATA 2) causes the free-running frequency of said oscillator to vary substantially less, when a fault condition occurs, than if said second data signal were susceptible to being altered via said microprocessor (31).
3. An apparatus according to Claim 1 characterized in that said oscillator (31) comprises a horizontal oscillator and said deflection circuit output stage (99) comprises a horizontal deflection circuit output stage.
4. An apparatus according to Claim 1 characterized in that said microprocessor (31) develops said first data signal



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(DATA 1) on a bus (BUS) coupled to said digital-to-analog converter (41).

5. An apparatus according to Claim 1 characterized in that said second data signal (DATA 2) is developed by an operation of a passive element (Z1, Z2, Z3).

6. An apparatus according to Claim 1 characterized in that said digital-to-analog converter (40,41) comprises a first digital-to-analog converter (41) portion that is responsive to said first data signal (DATA 1) and a second digital-to-analog (40) portion that is responsive to said second data signals (DATA 2) to produce corresponding first (i1) and second (i2) portion signals that are combined to form said control signal (iCONT).

7. A video display deflection apparatus comprising:
an oscillator (31) for generating an output signal (O_H) at a frequency (f_H) related to a deflection frequency;
a microprocessor (35) for developing a first data signal (DATA 1) that is susceptible to being altered, when a fault condition occurs during operation in said microprocessor;
a source (Z1, Z2, Z3) of a second data signal (DATA 2) that cannot be altered via said microprocessor, during operation;
a digital-to-analog converter (41,40) having a first input responsive to said first data signal and a second input responsive to said second data signal for generating an analog, frequency control signal (iCONT) that is coupled to a control input of said oscillator to control a free-running frequency of said oscillator within a tolerance range, said free-running frequency of said oscillator being compensated partly in accordance with said first data signal and partly in accordance with said second data signal wherein a least significant data bit (LSB2) of said second data signal has a weight, with respect to said control signal, that is larger than a most significant data bit (MSB1) of said first data signal and all the bits of said first data signal have a combined weight that is larger than the weight of the least significant bit of said second data signal; characterized by



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a deflection circuit output stage (99) responsive to said oscillator output signal for generating a deflection current (i_y) in a deflection winding.

8. A video display deflection apparatus comprising:
an oscillator (31) for generating an output signal (O_H) at a frequency related to a deflection frequency;
a microprocessor (35) for developing a first data signal (DATA 1) that is susceptible to being altered, when a fault condition occurs during operation in said microprocessor;
a source of a second data signal (DATA 2) that cannot be altered via said microprocessor, during operation;
a digital-to-analog converter (40,41) having a first input responsive to said first data signal and a second input responsive to said second data signal for generating an analog, frequency control signal (i_{CONT}) that is coupled to a control input of said oscillator to control a free-running frequency of said oscillator being compensated partly in accordance with said first data signal and partly in accordance with said second data signal wherein said oscillator is included in an integrated circuit and wherein said second data signal is programmable during the manufacturing of said integrated circuit and is non-alterable, afterwards; characterized by
a deflection circuit output stage (99) responsive to said oscillator output signal for generating a deflection current (i_y) in a deflection winding.

9. An apparatus according to Claim 1 characterized in that said oscillator (31) is included in a phase-lock-loop circuit (30,32,33,31).



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**DATA SIGNAL CONTROLLED
OSCILLATOR FOR A VIDEO DISPLAY**

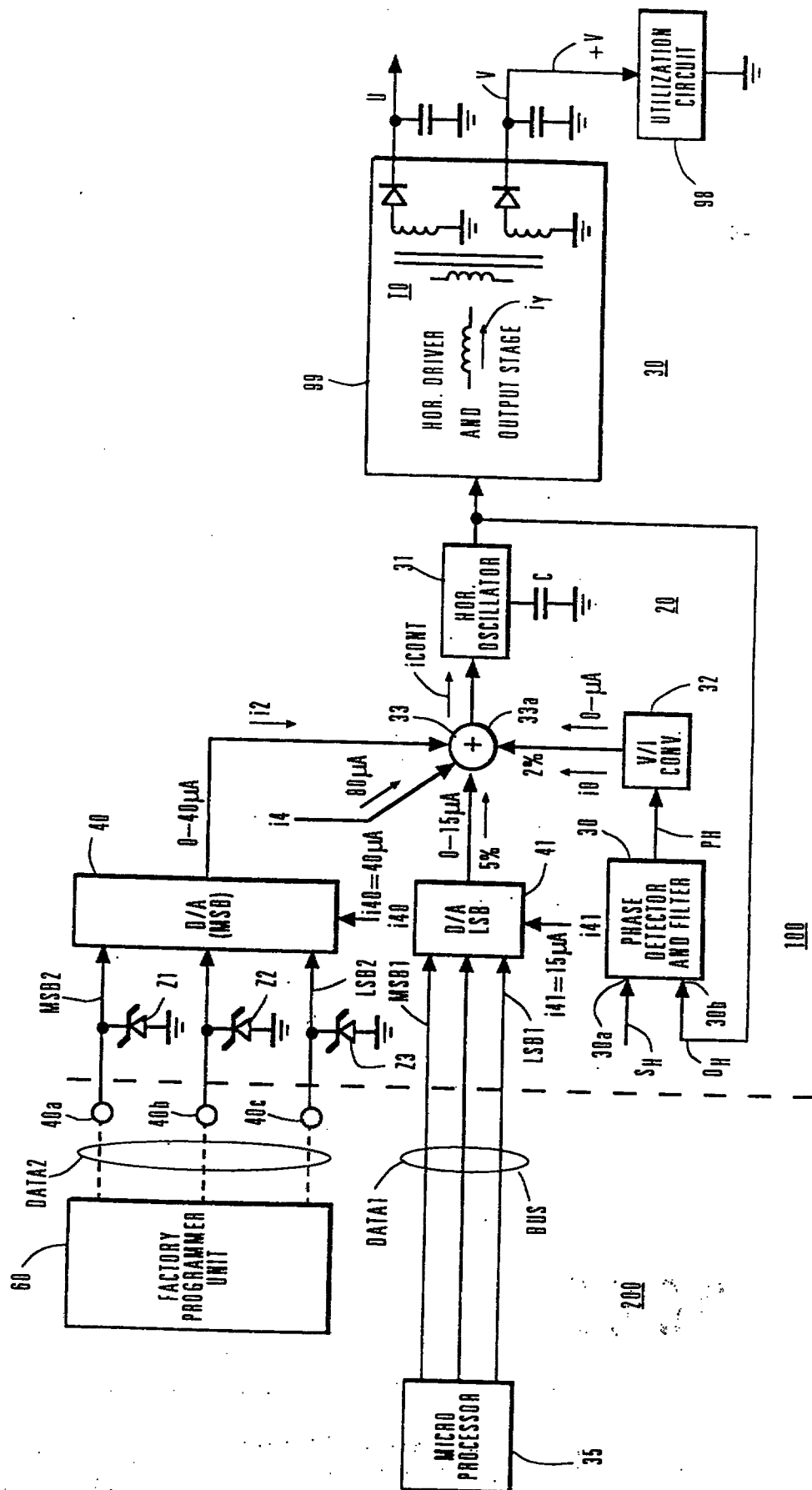
ABSTRACT

The free-running frequency of a bus controlled horizontal oscillator (31) is adjusted by programming of a first data signal (DATA 2) that is coupled to a digital-to-analog converter (40). The programming causes the first data signal to be non-alterable. The programming is done during manufacturing of a wafer that includes the oscillator. A second data signal (DATA 1) that is coupled from a microprocessor (35) via a bus (BUS) and via a second analog-to-digital converter (41) to the oscillator can vary the oscillator free-running frequency to provide for tolerance compensation. The first data signal is immune against data errors. The second data signal is not immune against data errors but can vary the oscillator frequency within only a relatively narrow range of values. Consequently, data errors are prevented from causing a significant change in the oscillator free-running frequency that might have occurred had both data signals been alterable.

FIGURE 1

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