

DESCRIPTION**«METHOD AND APPARATUS FOR OPTICALLY MEASURING BY
INTERFEROMETRY THE THICKNESS OF AN OBJECT»**

5

Technical field

The present invention relates to a method and an apparatus
for optically measuring by interferometry the thickness of
10 an object.

The present invention can be advantageously applied for
optically measuring by interferometry the thickness of
slices, or wafers, made of semiconductor material
(typically silicon), to which reference will be explicitly
15 made in the specification without loss of generality.

Background art

A slice of semiconductor material is machined, for example,
20 to obtain integrated circuits or other electric components
in the semiconductor material. In particular, when the
slice of semiconductor material is very thin, the slice of
semiconductor material is placed on a support layer
(typically made of plastic material or glass) that serves
25 to provide a higher mechanical sturdiness and thus an ease
in handling.

In general it is necessary to mechanically machine the
slice of semiconductor material by grinding and polishing
to obtain a thickness that is uniform and equal to a
30 desired value. In this phase of the mechanical machining of
the slice of semiconductor material the thickness needs to
be measured for ensuring that the desired value is
accurately obtained.

For measuring the thickness of a slice of semiconductor
35 material it is known to use gauging heads with mechanical
feelers touching an upper surface of the slice of
semiconductor material being machined.

This measuring technology can cause damage to the slice of semiconductor material during the measurement owing to the mechanical contact with the mechanical feelers, and does not enable to measure very thin thicknesses (typically
5 lower than 100 micron).

For measuring the thickness of a slice of semiconductor material it is known to use capacitive probes, inductive probes (eddy current probes or other types), or ultrasound probes. These measuring technologies are of the contactless
10 type and thus do not damage the slice of semiconductor material during the measurement and can measure the thickness of the slice of semiconductor material even when there is the support layer. However, these technologies are limited both in the dimensions they can measure and in the
15 highest resolution they can achieve.

For overcoming the limits of the measuring technologies above described, optical probes and interferometric measurements are used. For example, the international patent application published with No. WO2009013231A1, the
20 US patent No. US6437868A1 and the Japanese patent application published with No. JP082160016A describe apparatuses for optically measuring the thickness of a slice of semiconductor material.

Some of the known apparatuses include a source of light radiations, that are mostly infrared radiations as the
25 currently used semiconductor materials are silicon based and the silicon is sufficiently transparent to the infrared radiations, or have a wider spectrum for enabling the measurement of particularly thin thicknesses. The emitted
30 radiation beam features a low coherence and a plurality of wavelengths within a determined band. Such apparatuses further include a spectrometer and an optical probe that is connected to the source of light radiations and to the spectrometer by means of optical fibres, faces the slice of
35 semiconductor material to be measured, and is provided with lenses for focusing the radiations emitted by the radiation source on the slice of semiconductor material to be

measured and for collecting the radiations reflected by the slice of semiconductor material to be measured. A spectral analysis of the combinations resulting from the interference of the radiations that are reflected by the external surface and by possible optical discontinuity surfaces inside the slice of semiconductor material to be measured is carried out by means of the spectrometer. From such a spectral analysis of the combinations resulting from the interference of the radiations reflected by the slice of semiconductor material it is possible to determine the measure of the thickness of one or more layers of optically homogeneous material that have been crossed by the radiations.

But the above-mentioned analysis does not enable to determine the path followed by the reflected radiations that are combined. In other words, the combinations are the end result of a plurality of reflections occurring on the external surface of the slice of semiconductor material and inside the latter at each optical discontinuity surface. But in the known apparatuses it is not possible to use information that could be present in the combinations of reflected radiations to directly or indirectly measure the distance between the optical probe and each of the discontinuity surfaces causing the reflections. As a consequence, the analysis of the combinations of radiations reflected by the slice of semiconductor material enables to determine the measure of the thickness of the layers placed between couples of optical discontinuity surfaces, but it is not possible to determine the part of the slice of semiconductor material to which the measure of the thickness has to be assigned (that is to determine whether the measure of the thickness has to be assigned to a first layer that has been crossed twice, to the first layer that has been crossed n times, to a second or third layer, or to the first layer added to the second layer, etc.).

At each reading it is not only a single radiation reflected by the slice of semiconductor material that is analyzed but

a beam of radiations reflected by the slice of semiconductor material. Therefore, the measures of a plurality of different thicknesses are determined, but it is not possible to assign each measure of thickness to a specific part or layer of the slice of semiconductor material. However, for each reading it is possible to determine a corresponding quality factor on the basis, for example, of the ratio between the specific luminous power and the overall luminous power. Indeed, the quality factor is one of the clues suggesting that the associated reading corresponds to the thickness to be measured.

A known apparatus for optically measuring by interferometry the thickness of a slice of semiconductor material provides at each reading rough thickness values and associated quality factors on the basis of which they are generally arranged. In order to succeed in identifying, among all the rough thickness values provided by the apparatus, which rough thickness values correspond to the first layer of the slice of semiconductor material (i.e. the most external layer that is made of semiconductor material, is subject to grinding or polishing, and the thickness of which is to be measured) the known apparatuses use a recognition algorithm analyzing a relatively high number of consecutive readings (typically at least some tens of consecutive readings). Such known recognition algorithm considers, for each reading, only the rough thickness value with the highest quality factor. Then, all the rough thickness values with a quality factor lower than a minimum quality threshold and all the rough thickness values being lower than a minimum reject threshold or higher than a maximum reject threshold - the reject thresholds define the range within which the wanted thickness value has to lie - are rejected. Finally, the wanted thickness value (that is the measure of the thickness of the most external layer made of semiconductor material) can be determined by averaging the remaining rough thickness values.

However, some known recognition algorithms, as the one described above, have several inconveniences.

First of all, the accuracy of the known recognition algorithm described above is not optimal and extremely variable over time: the recognition algorithm is accurate when there are no foreign thickness values that are similar to the wanted thickness value, but it is much less accurate when there are foreign thickness values that are similar to the wanted thickness value.

Moreover, to obtain an acceptable accuracy, a special attention has to be paid in choosing both the minimum quality threshold and the reject thresholds serving to cut the thickness values provided by the readings. In other words, there are no minimum quality thresholds and reject thresholds that apply to all situations, but every time it is necessary to adapt the minimum quality thresholds and the reject thresholds to the specific current situation. Hence, the choice of the minimum quality thresholds and the reject thresholds requires every time the intervention of an experienced operator who is able to analyze the rough thickness values provided by the readings beforehand.

The intervention of an experienced operator is normal and thus acceptable in laboratory measurements but is not possible in measurements carried out in a production line during the serial production.

Disclosure of the invention

Object of the present invention is to provide a method and an apparatus for optically measuring by interferometry the thickness of an object that overcome the above described inconveniences and can be easily and cheaply implemented at the same time.

The present invention provides a method and an apparatus for optically measuring the thickness of an object according to what is claimed in the accompanying claims.

Brief description of the drawings

The present invention is now described with reference to the enclosed sheets of drawings, given by way of non
5 limiting examples, wherein:

- figure 1 is a simplified view, with some parts removed for the sake of clarity, of a machine tool that mechanically machines a slice of semiconductor material and includes an apparatus for optically
10 measuring by interferometry the thickness of a slice of semiconductor material;
- figure 2 is a simplified cross-section of the slice of semiconductor material of figure 1 while the measurement of the thickness is carried out;
- 15 - figure 3 is a graph showing the distribution of a plurality of rough thickness values that are read as part of the measuring process of the thickness of the slice of semiconductor material;
- figure 4A is a curve representing the distribution of
20 the frequencies of the rough thickness values of the graph in figure 3;
- figure 4B is a histogram showing the rough thickness values of the graph in figure 3 divided up into a number of thickness classes, and relative frequencies,
25 substantially indicating how many occurrences of the rough thickness values fall within each of such thickness classes;
- figure 5 is a view showing in an enlarged scale a detail of the histogram in figure 4B;
- 30 - figure 6 is a graph showing the evolution over time of a lower reject threshold and a higher reject threshold that are used during the measurements of the thickness of the slice of semiconductor material;
- figures 7a to 7d display the evolution over time of a
35 histogram that shows a series of thickness classes and relative frequencies.

Best mode for carrying out the invention

In figure 1, the reference number 1 indicates, on the whole, a machine tool that mechanically machines an object
5 2, such as a slice of semiconductor material, for carrying out on the slice of semiconductor material 2 a grinding operation that causes a gradual superficial removal of material. As illustrated in figure 2, the slice 2 of semiconductor material is placed on a support layer 3
10 (typically made of plastic material or glass) that serves to provide a higher mechanical sturdiness and thus an ease in handling. According to a different embodiment, herein not illustrated, the support layer 3 is omitted.

The machine tool 1 includes a support device 4 with a
15 motorized, rotary table 5 that is mounted so as to rotate about a vertical rotation axis 6. The slice 2 of semiconductor material is arranged on the rotary table 5 and it keeps contact with the latter e.g. by means of suction. Moreover, the machine tool 1 includes a machining
20 head 7 with an actuating device 8 that supports a grinding tool 9 in such a way to rotate the grinding tool 9 about a vertical rotation axis 10 and to vertically move the grinding tool 9 along the rotation axis 10.

The machine tool 1 includes a measuring device 11 for
25 optically measuring by interferometry the thickness T of the slice of semiconductor material (shown in figure 2). The measuring device 11 is, for example, a measuring device of the type described in the international patent application published with No. WO2009013231A1 to which
30 reference is made for a more detailed description of the measuring device 11. The measuring device 11 includes a source of light radiations, a spectrometer and an optical probe, which is connected by means of optical fibres to the source of light radiations and to the spectrometer, faces
35 the slice 2 of semiconductor material to be checked, and is provided with lenses for focusing a beam 12 of light radiations on the slice 2 of semiconductor material to be

checked, the latter being placed on the rotary table 5, and for collecting the radiations reflected by the slice 2 of semiconductor material to be checked. By means of the spectrometer the spectrum of the combinations resulting from the interference between the light radiations reflected by the slice 2 of semiconductor material is analyzed, and from such spectral analysis it is possible to determine the measure of the thickness of the material that has been crossed by the reflected radiations.

The light radiations emitted by the radiation source are mostly infrared, as the currently used semiconductor materials are silicon based and the silicon is sufficiently transparent to the infrared radiations, or have a wider spectrum for measuring particularly thin thicknesses. The emitted radiation beam features a low coherence and a plurality of wavelengths within a determined band.

The machine tool 1 comprises a processing unit 13 that is connected to the measuring device 11 for receiving from the measuring device 11 the readings of the thickness T of the slice 2 of semiconductor material and using the readings of the thickness T of the slice 2 of semiconductor material provided by the measuring device 11 to determine the actual value of the thickness T of the slice of semiconductor material according to the method hereinafter described.

Therefore, the measuring device 11 and the processing unit 13 form an apparatus for optically measuring by interferometry the thickness of the slice 2 of semiconductor material.

Finally, the machine tool 1 includes a control unit 14 that receives from the processing unit 13 the actual value of the thickness T of the slice 2 of semiconductor material and controls, by controlling the support device 4 and the machining head 7, the grinding of the slice 2 of semiconductor material by adjusting the rotational speed of the rotary table 5, the rotational speed of the grinding tool 9, and the vertical position of the grinding tool 9. In particular, the control unit 14 controls the grinding of

the slice 2 of semiconductor material for following a predefined and per se known machining process according to which, in general, the material removal rate (that is the thickness of removed material in the time unit) is gradually reduced as the thickness T of the slice 2 of semiconductor material approaches the wanted value. An example of how the thickness T of the slice 2 of semiconductor material varies over time owing to the grinding is illustrated in figure 6 that shows how the thickness T of the slice 2 of semiconductor material decreases faster in the first instants of the machining and decreases much more slowly in the last instants of the grinding.

At each reading of the thickness T of the slice 2 of semiconductor material, the spectrum of the combination resulting from the interference between radiations reflected by the external surface of the slice 2 of semiconductor material and by possible optical discontinuity surfaces inside the slice 2 of semiconductor material is analyzed by means of the spectrometer. From such spectral analysis it is possible to determine the measure of the thickness of one or more layers of optically homogeneous material that have been crossed by the radiations. In particular, starting from such analysis of the spectrum of the combination resulting from the interference between the reflected radiations the measuring device 11 determines a plurality of rough thickness values RTW generally differing from one another.

Indeed, starting from the analysis of a combination resulting from the interference between radiations reflected by the slice 2 of semiconductor material the measuring device 11 can determine the measure of the thickness of a material that has been crossed by the reflected radiation, but it can not determine the path that the reflected radiation has actually followed.

In other words, said combinations are generated by radiations that are the end result of a plurality of

reflections occurring on the external surface of the slice 2 of semiconductor material and inside the slice 2 of semiconductor material at each optical discontinuity surface, but in the known apparatuses it is not possible to use information that could be present in the combinations of reflected radiations to directly or indirectly measure the distance between the optical probe and each of the discontinuity surfaces causing the reflections. As a consequence, the analysis of the combinations of radiations reflected by the slice 2 of semiconductor material enables to determine the measure of the thickness of the layers placed between couples of optical discontinuity surfaces, but it is not possible to determine the layer or part of the slice 2 of semiconductor material to which the measure of the thickness has to be assigned (that is to determine whether the measure of the thickness has to be assigned to a first layer that has been crossed twice, to the first layer that has been crossed n times, to a second or third layer, or to the first layer added to the second layer, etc.).

According to a preferred embodiment, the measuring device 11 can provide for each rough thickness value RTW a corresponding quality factor MF on the basis, for example, of the ratio between the specific luminous power and the overall luminous power. Indeed, the quality factor is one of the clues suggesting that the associated reading corresponds to the thickness to be measured. At the end of each reading the measuring device 11 arranges all the determined rough thickness values RTW as a function of the corresponding quality factors MF that are available, and provides the processing unit 13 only with the three rough thickness values RTW that have the highest quality factors. For determining the actual value of the thickness T of the slice 2 of semiconductor material, the processing unit 13 uses a plurality of consecutive readings (typically the number of readings corresponding to a complete rotation of the slice 2 of semiconductor material) carried out by the

measuring device 11, and thus considers a plurality of rough thickness values RTW (each readings carried out by the measuring device 11 can provide, for example and as mentioned above, three rough thickness values RTW with the associated quality factors MF). As an example, figure 3 is a graph showing the distribution of a plurality of rough thickness values RTW that have been provided by a plurality of consecutive readings carried out by the measuring device 11 (in figure 3 the ordinate represents the thickness value expressed in micron and the abscissa represents the time expressed in milliseconds).

As an example again, in an application where the slice 2 rotates at a speed of about 300 RPM and the measuring device has a data capture frequency of 4 KHz, the number of processed readings is 800 that correspond - in the above mentioned case where three values RTW are provided for each reading - to 2400 rough thickness values RTW.

The processing unit 13 can determine the actual value of the thickness T of the slice 2 of semiconductor material by analyzing the plurality of rough thickness values RTW provided by a plurality of consecutive readings carried out by the measuring device 11.

The processing unit 13 evaluates the frequencies (number of occurrences) of the rough thickness values RTW and the distribution of such frequencies. According to a first implementation procedure, first of all a variability interval of rough thickness values RTW is determined so that it is wide enough to include a significant part of such values RWT. Then, the processing unit 13 provides and processes a continuous function $F(RTW)$ representing the frequency density of the values within the above-mentioned variability interval, and calculates the relative frequency density function. Figure 4A shows, for example, a curve relating to such a function $F(RTW)$ of the rough thickness values RTW of the graph in figure 3.

According to a different, preferred implementation procedure to which reference is made for the most part in

the subsequent description, in an early stage the processing unit 13 defines the above-mentioned variability interval of the rough thickness values RTW by determining a plurality of thickness classes C that is large enough to include a significant part of the rough thickness values RTW. The resolution of the thickness classes C (that is the wideness of each thickness class C) is preferably of the order of magnitude of micron.

Subsequently, the processing unit 13 evaluates the frequencies by means of a classification of the rough thickness values RTW so as to determine for each thickness class C the corresponding frequency F with which the rough thickness values RTW fall within that thickness class C, i.e. how often the rough thickness values (RTW) fall within that thickness class (C). In other words, for each thickness class C the processing unit 13 determines how many occurrences of the rough thickness values RTW are included in that thickness class C: the number of occurrences of rough thickness values RTW included in that thickness class C represents the frequency F with which the rough thickness values RTW fall within that thickness class C. As an example, figure 4B is a histogram that shows the frequency F indicating how many of the rough thickness values RTW of the graph in figure 3 fall within a series of thickness classes C with a resolution of 1 micron (in figure 4B the ordinate represents the frequency F and the abscissa represents the thickness classes C). Instead of the absolute frequency F (number of occurrences), it is possible to use a specific frequency or density (that is one frequency per unit of length) that is achieved by dividing the absolute frequency F by the wideness of the thickness class C.

According to a preferred embodiment, the processing unit 13 determines the frequencies F with which the rough thickness values RTW fall within the thickness classes C by considering the quality factors MF so that the weight assigned to each rough thickness value RTW provided by the

measuring device 11 is greater than the one corresponding to a simple occurrence, and increases as the quality factor MF increases. In other words, a rough thickness value RTW with a high quality factor MF has more weight in calculating the frequency F of the corresponding thickness classe C than a rough thickness value RTW with a low quality factor MF. In this way, more importance is given to the rough thickness values RTW with higher quality factors MF and thus to the rough thickness values RTW that more probably refers to the thickness to be measured.

A similar weighting procedure of the frequencies of the values RTW with the relative quality factors MF can be carried out in case of using the continuous function that has been mentioned with reference to figure 4A.

According to said first implementation procedure, the subsequent step consists in determining among different, limited intervals of the function $F(RTW)$ - on the abscissa axis of figure 4A - i.e. limited sets of adjacent rough thickness values RTW, the limited interval at which a frequency integration or summation, in particular the integral of the function $F(RTW)$, represents an absolute maximum, and determining the actual value of the thickness T of the slice 2 of semiconductor material as a function of the values RTW of said limited set of adjacent values.

Likewise, in the preferred implementation procedure to which figure 4B refers, once the rough thickness values have been classified, the processing unit 13 determines a preponderant group G_{MAX} of thickness classes C that is composed of one or more adjacent thickness classes C, for which the sum of the corresponding frequencies F represents an absolute maximum (as shown in the histogram of figure 4B). In substance, according to said preferred implementation procedure, the preponderant group G_{MAX} of thickness classes C comprises and defines the limited set of adjacent rough thickness values RTW whose frequency integration or summation represents an absolute maximum, and thus the processing unit 13 determines the actual value

of the thickness T of the slice 2 of semiconductor material as a function of the preponderant group G_{MAX} of thickness classes C . In other words, among all the frequencies F (that is the frequencies inside the histogram) the processing unit 13 determines all the existing groups G (that is all the sets of adjacent thickness classes C whose relative frequencies F are significantly not null) and recognizes the preponderant group G_{MAX} of thickness classes C by comparing all the existing groups G . For recognizing the preponderant group G_{MAX} of thickness classes C the processing unit 13 calculates the sum of the frequencies F of all the groups G and searches the highest sum of the frequencies F (that is the absolute maximum of the frequency integration or summations).

Generally, the preponderant group G_{MAX} of thickness classes C includes a plurality of adjacent thickness classes C , but it can even include just a single thickness class C .

As illustrated in figure 5, for determining a group G of thickness classes C (and thus the preponderant group G_{MAX} of thickness classes C , too) the processing unit 13 determines, at the beginning, the thickness class C_{MAX} that has the highest frequency F_{MAX} in a local area (i.e. that locally represents a relative maximum within a relatively high interval of thickness classes C), and thus joins to such thickness class C_{MAX} the adjacent thickness classes C (which are the thickness classes C "on the left" and "on the right") that have a relatively high frequency F . For example, a group G of thickness classes C is formed by joining to the thickness class C_{MAX} with the highest frequency F_{MAX} all the adjacent thickness classes C with a frequency F that is equal at least to the 10% of the frequency F_{MAX} of the thickness class C_{MAX} (or to a different preset percentage, for example 12.5% or 6.25%). What has been described hereinbefore is illustrated, as an example, in figure 5 showing in an enlarged scale a detail of the histogram of the figure 4B. Figure 5 shows the thickness class C_{MAX} with the highest frequency F_{MAX} and a horizontal

dashed line indicates the frequency limit that is equal, for example, to the 10% of the frequency F_{MAX} of the thickness class C_{MAX} . The thickness classes C that are adjacent to the thickness class C_{MAX} and have a frequency F higher than the 10% of the frequency F_{MAX} of the thickness class C_{MAX} (marked with grey colour) are joint to the thickness class C_{MAX} , whereas the thickness classes C that are adjacent to the thickness class C_{MAX} and have a frequency F lower than the 10% of the frequency F_{MAX} of the thickness class C_{MAX} are not joint to the thickness class C_{MAX} .

It is to be noted that, according to the above-mentioned first implementation procedure (figure 4A), the limited intervals of the function $F(RTW)$, or limited sets of adjacent rough thickness values RTW , can be determined in a similar manner, i.e. by detecting highest frequencies $F_{MAX}(RTW)$ and defining intervals or "windows" ΔRTW (figure 4A) delimited by rough thickness values RTW whose frequency is equal to about 10 % (for instance) of the relative highest frequencies $F_{MAX}(RTW)$.

In the histogram of the preferred implementation procedure to which figure 4B refers it is possible to identify more thickness classes C_{MAX} that have locally the highest frequency F_{MAX} (that is a series of "relative maxima"). In this case the processing unit 13 determines for each thickness class C_{MAX} that has locally the highest frequency F_{MAX} the corresponding group G of thickness classes C , calculates for each group G of thickness classes C the frequency integration or summation, more specifically the sum of the corresponding frequencies F (that is the sum of the frequencies F of all the thickness classes C belonging to the group G of thickness classes C), and finally identifies the preponderant group G_{MAX} of thickness classes C that has the highest sum of the corresponding frequencies F .

According to a preferred embodiment, the processing unit 13 determines the actual value of the thickness T of the slice

2 of semiconductor material by averaging the rough thickness values RTW belonging to the thickness classes C of the preponderant group G_{MAX} of thickness classes C.

According to a different embodiment, the processing unit 13
5 determines, in the preponderant group G_{MAX} of thickness classes C, the thickness class C_{MAX} that has the highest frequency F_{MAX} , and defines that the actual value of the thickness T of the slice 2 of semiconductor material is equal to the average of all the rough thickness values RTW
10 belonging to the thickness class C_{MAX} that has the highest frequency F_{MAX} .

It should be noted that the slice 2 of semiconductor material is in continuous motion during the readings of the measuring device 11 owing to the rotation of the rotary
15 table 5 about the rotation axis 6. Therefore, the rough thickness values RTW that are read by the measuring device 11 and are considered in the processing algorithm do not refer to the same point of the slice 2 of semiconductor material but to a series of points of the slice 2 of
20 semiconductor material placed along a circumference arc (whose angle has generally a size of at least 36° , corresponding to a tenth of a round angle, and can reach even 360° that is a round angle). Within said circumference arc the thickness T of the slice 2 of semiconductor
25 material is not generally constant owing to, for example, the possible unevenness of the material. As a consequence, the reading of the rough thickness values RTW along a circumference arc enables to determine not only the actual value of the thickness T representing an average of the
30 thickness T along the circumference arc but also a minimum T_{min} and a maximum T_{max} of the actual value of the thickness T of the slice 2 of semiconductor material along the circumference arc that represent how the actual value of the thickness T can vary along the circumference arc.

35 In general, the processing unit 13 determines the minimum T_{min} and the maximum T_{max} of the actual value of the thickness T of the slice 2 of semiconductor material, i.e.

it determines the amplitude ΔT of the variation range of the actual value of the thickness T of the slice 2 of semiconductor material, because such data can be useful to correctly control the machining carried out by the grinding tool 9. The minimum $T_{\min}$ and the maximum $T_{\max}$ of the actual value of the thickness T of the slice 2 of semiconductor material represent the two extremes delimiting the variation range of the actual value of the thickness T of the slice 2 of semiconductor material that has an amplitude ΔT (where $\Delta T = T_{\max} - T_{\min}$).

According to a first embodiment the processing unit 13 determines the minimum $T_{\min}$ and the maximum $T_{\max}$ of the actual value of the thickness T of the slice 2 of semiconductor material, i.e. it determines the amplitude ΔT of the variation range of the actual value of the thickness T of the slice 2 of semiconductor material as a function of a minimum and a maximum of the rough thickness values RTW belonging to the preponderant group $G_{\max}$ of thickness classes C . Said minimum and maximum can be estimated, for example, on the basis of processing on the standard deviation in the distribution of such rough thickness values RTW. In other words, the rough thickness value that is estimated to be the lowest among the rough thickness values RTW belonging to the preponderant group $G_{\max}$ of thickness classes C represents the minimum $T_{\min}$ of the actual value of the thickness T of the slice 2 of semiconductor material, whereas the rough thickness value that is estimated to be the highest among the rough thickness values RTW belonging to the preponderant group $G_{\max}$ of thickness classes C represents the maximum $T_{\max}$ of the actual value of the thickness T of the slice 2 of semiconductor material. Such a method is typically applied when the rough thickness values RTW used for a single measurement of the thickness T of the slice 2 of semiconductor material are read along a long circumference arc (whose length is close or equal to the round angle).

According to an alternative embodiment, when the rough thickness values RTW used for a single measurement of the thickness T of the slice 2 of semiconductor material are read along a short circumference arc (whose angle size, for example, is equal to $1/10$ of the round angle, that is equal to 36°) more consecutive measures of the thickness T of the slice 2 of semiconductor material are considered for determining the minimum $T_{\min}$ and the maximum $T_{\max}$ of the actual value of the thickness T of the slice 2 of semiconductor material, that is for determining the amplitude ΔT of the variation range of the actual value of the thickness T of the slice of semiconductor material. In this case, the minimum $T_{\min}$ and the maximum $T_{\max}$ of the actual value of the thickness T of the slice 2 of semiconductor material, that is the amplitude ΔT of the variation range of the actual value of the thickness T of the slice of semiconductor material, are determined as a function of the minimum and the maximum of the actual values of the thickness T of the slice 2 of semiconductor material that are determined by the sequence of measures of the thickness T of the slice 2 of semiconductor material (i.e. the minimum $T_{\min}$ and the maximum $T_{\max}$ of the actual value of the thickness T of the slice 2 of semiconductor material are equal to the minimum $T_{\min}$ and the maximum $T_{\max}$ of the actual values of the thickness T of the slice 2 of semiconductor material, respectively). The sequence of measures of the thickness T of the slice 2 of semiconductor material that are considered to determine the minimum $T_{\min}$ and the maximum $T_{\max}$ of the actual value of the thickness T of the slice 2 of semiconductor material has to correspond to a complete rotation of the slice 2 of semiconductor material in order to provide a completely reliable result. According to a preferred embodiment, a minimum quality threshold $MT_{\min}$ that is stored in a memory of the processing unit 13 is determined. Before classifying the rough thickness values RTW, the processing unit 13 eliminates (rejects) all the rough thickness values RTW whose quality

factors MF are lower than the minimum quality threshold MT_{min} . In this way, rough thickness values RTW with too low quality factors MF (and thus possibly affected by even remarkable measuring errors) are not considered in
5 determining the actual value of the thickness T of the slice 2 of semiconductor material. If, for example, the range of the quality factors MF extends from 0 to 100, rough thickness values RTW with a quality factor MF lower than 30 or 20 can be rejected.

10 According to a preferred embodiment, the processing unit 13 sets a lower reject threshold R_{min} and a higher reject threshold R_{max} that define a searching interval including the actual value of the thickness T of the slice 2 of semiconductor material and it eliminates (rejects) all the
15 rough thickness values RTW that are lower than the lower reject threshold R_{min} and higher than the higher reject threshold R_{max} . In other words, the searching interval defined by the lower reject threshold R_{min} and the higher reject threshold R_{max} defines where the actual value of the
20 thickness T of the slice 2 of semiconductor material has to be searched so as to narrow the searching area.

During the superficial machining of the slice 2 of semiconductor material causing a gradual reduction of the thickness T of the slice 2 of semiconductor material, the
25 processing unit 13 progressively updates the lower reject threshold R_{min} and the higher reject threshold R_{max} for "following" the gradual reduction of the thickness T of the slice 2 of semiconductor material, as a function of the progress state of the surface machining of the slice 2 of
30 semiconductor material. What has been described above is illustrated in the graph of figure 6 showing the evolution over time of the thickness T of the slice 2 of semiconductor material during the surface machining, and thus the evolution over time of the lower reject threshold
35 R_{min} and the higher reject threshold R_{max} .

According to a first embodiment, the processing unit 13 determines the progress state of the surface machining of

the slice 2 of semiconductor material as a function of the machining process (which, as previously stated, controls the progress state of the surface machining), and thus progressively updates the lower reject threshold $R_{\min}$ and the higher reject threshold $R_{\max}$ as a function of the progress state of the surface machining. In particular, the machining process defines a material removal rate VA (that is, the material thickness that is removed per unit of time). Hence, knowing that the thickness T of the slice 2 of semiconductor material takes a value T_{PC} at a control instant of time t_{PC} (that typically corresponds to the last change in the material removal rate VA), it is easier to progressively update the reject thresholds $R_{\min}$ and $R_{\max}$ by using the following equations:

$$[1] \quad R_{\min}(t) = T_{PC} - VA \cdot (t - t_{PC}) - M_{SC}$$

$$[2] \quad R_{\max}(t) = T_{PC} - VA \cdot (t - t_{PC}) + M_{SC}$$

20	$R_{\min}(t)$	lower reject threshold at the instant of time t;
	$R_{\max}(t)$	higher reject threshold at the instant of time t;
	T_{PC}	value of the thickness T of the slice 2 of semiconductor material at a control instant of time t_{PC} ;
25	t_{PC}	control instant of time;
	VA	material removal rate;
	M_{SC}	maximum deviation between the theoretical removal of material and the actual removal of material (generally preset by means of experimental tests).
30		

According to a second embodiment, measurements of the thickness T of the slice 2 of semiconductor material are carried out in a sequence, and the processing unit 13 updates the lower reject threshold $R_{\min}$ and the higher reject threshold $R_{\max}$ used for the current measurement of

the thickness T as a function of the actual value of the thickness T determined at the end of the preceding measurement of the thickness T . Preferably, the processing unit 13 determines, according to the above described method, at each measurement of the thickness T of the slice 2 of semiconductor material the amplitude ΔT of the variation range of the actual value of the thickness T of the slice 2 of semiconductor material, too, and sets the lower reject threshold $R_{\min}$ and the higher reject threshold $R_{\max}$, used for the current measurement of the thickness T of the slice 2 of semiconductor material, by subtracting from and adding to, respectively, the actual value of the thickness T determined at the end of the preceding measurement half the amplitude ΔT of such variation range of the actual value of the thickness T determined at the end of the preceding measurement, to which a safety coefficient KS (in the order of 10-30%) can be added or not. In other words, the reject thresholds $R_{\min}$ and $R_{\max}$ can be updated by using the following equations:

20

$$[3] \quad R_{\min-i} = T_{i-1} - (\Delta T_{i-1}/2) * (1+KS)$$

$$[4] \quad R_{\max-i} = T_{i-1} + (\Delta T_{i-1}/2) * (1+KS)$$

25

$R_{\min-i}$ lower reject threshold used for the i -th measurement of the thickness T of the slice 2 of semiconductor material;

$R_{\max-i}$ higher reject threshold used for the i -th measurement of the thickness T of the slice 2 of semiconductor material;

30

T_{i-1} actual value of the thickness T of the slice 2 of semiconductor material determined at the end of the $(i-1)$ -th measurement;

35

ΔT_{i-1} amplitude of the variation range of the actual value of the thickness T of the slice 2 of semiconductor material determined at the end of the $(i-1)$ -th measurement;

KS safety coefficient.

According to an alternative embodiment, it is possible to choose a distance between the reject thresholds $R_{\min}$ and $R_{\max}$ that is bigger or smaller than the above mentioned amplitude ΔT of the variation range.

As the reject thresholds $R_{\min}$ and $R_{\max}$ are not static (i.e. always constant) but dynamic (that is they continuously vary to follow the evolution over time of the actual value of the thickness T of the slice 2 of semiconductor material), the reject thresholds $R_{\min}$ and $R_{\max}$ are particularly effective in eliminating the rough thickness values excluded from the processing for calculating the thickness T , and thus in increasing the efficiency of said processing and the accuracy in determining the actual value of the thickness T . Such a result can be achieved because the reject thresholds $R_{\min}$ and $R_{\max}$ are dynamic and they can thus define a particularly narrow acceptability interval. When the first measurement of the thickness T of the slice 2 of semiconductor material is carried out, there are no preceding measures available to which reference can be made for determining the lower reject threshold $R_{\min}$ and the higher reject threshold $R_{\max}$. Therefore, when the first measurement of the thickness T of the slice 2 of semiconductor material is carried out, the employed values of the lower reject threshold $R_{\min}$ and the higher reject threshold $R_{\max}$ are predetermined and calculated as a function of the nominal features of the slice 2 of semiconductor material and of the tolerances of the nominal features. Typically, the initial and predetermined values of the reject thresholds $R_{\min}$ and $R_{\max}$ calculated as a function of the nominal features enclose a wide interval that is gradually reduced as more measures of the actual value of the thickness T of the slice 2 of semiconductor material are available. According to a possible, particular solution, at the beginning the initial, wide interval included between the reject thresholds $R_{\min}$ and $R_{\max}$ remains valid until a predetermined persistence of the initial

measuring value is detected. For example, the first measuring value generated by the algorithm is obtained when it persists for at least N consecutive times (where N=100 for example) featuring small variations, not extending
5 outside a limited, predetermined range (3 micron, for example), and in this phase the reject thresholds $R_{\min}$ and $R_{\max}$ continue to be determined on the basis of the original, theoretical thickness and of its tolerance. This particular solution serves to provide more reliability to the initial
10 value that is the basis on which the values of the subsequent automatic limits are determined.

According to a preferred embodiment, after rejecting the rough thickness values RTW that do not comply with the two rejection criteria (i.e. which are lower than the lower reject threshold $R_{\min}$, higher than the higher reject threshold $R_{\max}$, or have a quality factor MF lower than the minimum quality threshold $MT_{\min}$) the processing unit 13
15 determines an acceptability percentage $A\%$ representing the number of rough thickness values RTW that comply with the rejection criteria (i.e. surviving after rejections based on the rejection criteria) in comparison with the total number of available rough thickness values RTW. Moreover, the processing unit 13 determines the actual value of the thickness T of the slice 2 of semiconductor material only
20 if the acceptability percentage $A\%$ is higher than a representativeness threshold RT. Such condition ensures that the actual value of the thickness T of the slice 2 of semiconductor material is determined only if it is possible to use a significant number of rough thickness values RTW.
25 In fact, the use of a too lower number of rough thickness values RTW causes the risk of making not negligible mistakes in determining the thickness T of the slice 2 of semiconductor material.

When the actual value of the thickness T of the slice 2 of semiconductor material can not be determined as the
35 acceptability percentage $A\%$ is not higher than a representativeness threshold RT, the processing unit 13

preferably modifies at least one rejection criterion of the rough thickness values RTW for trying to increase the acceptability percentage $A\%$. Typically, if the acceptability percentage $A\%$ is lower than the representativeness threshold RT even after at least one rejection criterion has been modified, the processing unit 13 does not determine the actual value of the thickness T of the slice 2 of semiconductor material and signals a missed measurement.

According to a possible embodiment, the processing unit 13 determines, by analyzing a series of consecutive measures of the thickness T of the slice 2 of semiconductor material, at least one possible parasitic thickness value that always remains substantially constant and a relative average number of rough thickness values RTW of the parasitic thickness value that belong to the thickness class C corresponding to the parasitic thickness value. Hence, after determining the parasitic thickness value, the processing unit 13 removes from the thickness class C corresponding to the parasitic value the average number of rough thickness values RTW of the parasitic thickness value. In this way it is possible to eliminate the influence of the parasitic values that can have negative effects when the actual value of the thickness T of the slice 2 of semiconductor material crosses, when decreasing, a parasitic value.

What described before is exemplified in figures 7a to 7d: comparing the four figures 7a, 7b, 7c and 7d it can be understood that there are a preponderant group G_{MAX} of thickness classes C and two minority groups GP_1 and GP_2 of thickness classes C. The preponderant group G_{MAX} of thickness classes C gradually displaces over time toward lower values owing to the surface machining carried out by the grinding tool 9, whereas the two minority groups GP_1 and GP_2 of thickness classes C always remain substantially constant over time. The processing unit 13 recognizes that the two minority groups GP_1 and GP_2 of thickness classes C

always remain substantially constant over time, and thus they can not represent the thickness T of the slice 2 of semiconductor material that has to decrease over time owing to the surface machining carried out by the grinding tool

5 9. When the preponderant group G_{MAX} of thickness classes C crosses (i.e. overlaps) the minority group GP_2 of thickness classes C , the preponderant group G_{MAX} is "deformed" by the minority group GP_2 (as shown in figure 7b). In order to avoid such "deformation", the processing unit 13 eliminates

10 the minority group GP_2 that overlaps the preponderant group G_{MAX} (as shown in figure 7c) when the minority group GP_2 crosses the preponderant group G_{MAX} .

As stated above, for determining the actual value of the thickness T of the slice 2 of semiconductor material the

15 processing unit 13 uses a plurality of consecutive readings carried out by the measuring device 11, and thus considers a plurality of rough thickness values RTW (each reading carried out by the measuring device 11 provides, for example, a single rough thickness value RTW or, according

20 to the hereinbefore mentioned embodiment, three rough thickness values RTW). According to a preferred embodiment, each measurement of the thickness T of the slice 2 of semiconductor material uses a predetermined and constant number of readings of the thickness T within a measuring

25 time interval. Between two consecutive measurements the processing unit translates over time the measuring time interval by an extent that is smaller than the extent of the measuring time interval itself so that a number of readings of the thickness T belong to both the end part of

30 the preceding measurement and the initial part of the subsequent measurement.

The above described method for optically measuring by interferometry the thickness T of the slice 2 of semiconductor material is based on the hypothesis that the

35 rough thickness values RTW corresponding to the thickness T of the slice 2 of semiconductor material are considerably more frequent than all the other values and/or have quality

factors MF that are, on average, higher than all the other ones. Many experimental tests have proved that such hypothesis is correct, and thus the above described method is reliable.

5 In a different method according to the invention, the thickness T can be determined at the beginning in a way differing from the one hereinbefore described, for example, on the basis of the quality factor MF according to a known way, or by considering rough thickness values RTW that are
10 closer than other values detected to a theoretical, preset thickness value. In such a different method according to the invention, the minimum reject threshold $R_{\min}$ and the maximum reject threshold $R_{\max}$ are, however, defined in a dynamic way, for example by using one of the methods
15 hereinbefore described.

The above described methods for optically measuring by interferometry the thickness T of a slice 2 of semiconductor material, or of an object made of a different material that is at least partially transparent to the used
20 light radiations, provide a lot of advantages.

First of all, the above described methods enable to rapidly and accurately determine the actual value of the thickness T of the slice 2 of semiconductor material. Indeed, many experimental tests have demonstrated that the above
25 described methods enable to determine the actual value of the thickness T of the slice 2 of semiconductor material with small errors.

Moreover, the above described methods do not require any external intervention for adjusting the operational
30 parameters. On the contrary, such methods can adjust autonomously and without external intervention to the specific features of the current measurement for providing the greatest accuracy in each situation. As a consequence, the above described methods are particularly suitable to be
35 used in a production line during the serial production.

Finally, the above described methods neither require a high processing power nor take up much storage space. Therefore,

they can be easily and cheaply implemented even in an existing processing unit 13 (that can thus be easily updated), which can be even integrated into the control unit 14.

CLAIMS

1. Method for optically measuring by interferometry the thickness (T) of an object (2); the method including the steps of:
- 5 carrying out by optical interferometry a plurality of readings of the thickness (T) of the object for obtaining at least one rough thickness value (RTW) from each reading and, consequently, a plurality of rough thickness values (RTW); and
- 10 determining the actual value of the thickness (T) of the object (2) by analyzing the plurality of rough thickness values (RTW);
- the method being characterized in that it includes the steps of:
- 15 defining a variability interval of the rough thickness values (RTW) that is wide enough to comprise at least one significant part of the rough thickness values (RTW);
- 20 evaluating the frequencies of the rough thickness values (RTW) of said variability interval;
- identifying a limited set of adjacent rough thickness values (RTW) whose frequency integration or summation represents an absolute maximum;
- 25 determining the actual value of the thickness (T) of the object (2) as a function of the rough thickness values (RTW) belonging to said limited set of values.
2. Method according to claim 1 wherein
- 30 the step of evaluating the frequencies of the rough thickness values (RTW) of said variability interval comprises the processing of a continuous function (F(RTW)) representing the frequency density of the rough thickness values (RTW) and the calculation of the relative frequency density function;
- 35 said limited set of adjacent rough thickness values (RTW) defining a limited interval and said frequency

integration or summation being defined as the integral of said continuous function ($F(RTW)$) in said limited interval.

5 3. Method according to claim 1 wherein

the step of defining a variability interval of the rough thickness values (RTW) includes the determination of a plurality of thickness classes (C) that is large enough to comprise a significant part of the rough
10 thickness values (RTW);

the step of evaluating the frequencies of the rough thickness values (RTW) of said variability interval comprises a classification of the rough thickness values (RTW) so as to determine for each thickness class (C) a
15 corresponding frequency (F) indicating how often the rough thickness values (RTW) fall within that thickness class (C);

the method further comprising the step of determining a preponderant group (G_{max}) of thickness classes (C) that is composed of one or more adjacent thickness classes (C) for which the sum of the corresponding frequencies (F) defines said frequency integration or summation representing an absolute maximum, said limited set of
20 adjacent rough thickness values (RTW) being defined by said preponderant group (G_{max}) of thickness classes (C).
25

4. Method according to claim 3 and further comprising the additional steps of

determining in the preponderant group (G_{max}) of
30 thickness classes (C_{max}) the thickness class (C) that has the highest frequency (F_{max}); and

determining the actual value of the thickness (T) of the object (2) as the average of the rough thickness values (RTW) belonging to the thickness class (C_{max}) that
35 has the highest frequency (F_{max}).

5. Method according to any one of claims 1 to 3 and including the further step of determining the actual value of the thickness (T) of the object (2) by averaging all the rough thickness values (RTW) belonging to said limited set of adjacent rough thickness values (RTW).
6. Method according to any one of the preceding claims and including the further step of determining a minimum ($T_{\min}$) and a maximum ($T_{\max}$) of the actual value of the thickness (T) of the object (2), i.e. determining the amplitude (ΔT) of a variation range of the actual value of the thickness (T) of the object (2) as a function of a minimum and a maximum of the rough thickness values (RTW) belonging to said limited set of adjacent rough thickness values (RTW).
7. Method according to any one of claims 1 to 5 and including the further steps of:
- carrying out a sequence of measurements of the thickness (T) of the object (2); and
- determining a minimum ($T_{\min}$) and a maximum ($T_{\max}$) of the actual value of the thickness (T) of the object (2), i.e. determining the amplitude (ΔT) of a variation range of the actual value of the thickness (T) of the object (2) as a function of a minimum and a maximum of the actual values of the thickness (T) of the object (2) determined by the sequence of measurements of the thickness (T) of the object (2).
8. Method according to claim 7 and including the further steps of:
- rotating the object about a rotation axis (6) while carrying out the sequence of measurements of the thickness (T) of the object (2); and
- carrying out the sequence of measurements of the thickness (T) of the object (2) in such a way that the

sequence of measurements is carried out throughout a complete rotation of the object (2) about the rotation axis (6).

- 5 9. Method according to any one of the preceding claims and including the further steps of:
 having a corresponding quality factor (MF) for each reading and each rough thickness value (RTW);
 determining the frequencies (F) of the rough thickness
10 values (RTW) considering the quality factors (MF) so that the weight assigned to each rough thickness value (RTW) increases as the quality factor (MF) increases.
- 15 10. Method according to any one of the preceding claims and including the further steps of:
 having a corresponding quality factor (MF) for each reading and for each rough thickness value (RTW);
 setting a minimum quality threshold (MT_{min}); and
 eliminating all the rough thickness values (RTW) whose
20 quality factors (MF) are lower than the minimum quality threshold (MT_{min}).
- 25 11. Method according to any one of the preceding claims and including the further steps of:
 setting a lower reject threshold (R_{min}) and a higher reject threshold (R_{max}) that identify a searching interval comprising the actual value of the thickness (T) of the object (2); and
 eliminating all the rough thickness values (RTW) that
30 are lower than the lower reject threshold (R_{min}) or higher than the higher reject threshold (R_{max}).
- 35 12. Method according to claim 11 and including the further steps of:
 machining the surface of the object (2) so as to gradually reduce the thickness (T) of the object (2) according to a known machining process;

determining the progress state of the surface machining of the object (2) as a function of the machining process; and

5 progressively updating the lower reject threshold ($R_{\min}$) and the higher reject threshold ($R_{\max}$) as a function of the progress state of the surface machining of the object (2).

10 13. Method according to claim 11 and including the further steps of:

carrying out measurements of the thickness (T) of the object (2) in a sequence; and

15 updating the lower reject threshold ($R_{\min}$) and the higher reject threshold ($R_{\max}$) that are used for the current measurement of the thickness (T) of the object (2) as a function of the actual value of the thickness (T) of the object (2) determined at the end of the preceding measurement of the thickness (T) of the object (2).

20

14. Method according to claim 13 and including the further steps of:

25 determining, for each measurement of the thickness (T) of the object (2), the amplitude (ΔT) of a variation range of the actual value of the thickness (T) of the object (2); and

30 setting the lower reject threshold ($R_{\min}$) and the higher reject threshold ($R_{\max}$) that are used for the current measurement of the thickness (T) of the object (2) by subtracting from and adding to, respectively, the actual value of the thickness (T) of the object (2) determined at the end of the preceding measurement of the thickness (T) of the object (2) half the amplitude (ΔT) of the variation range of the actual value of the thickness (T) of the object (2) determined at the end of the preceding measurement of the thickness (T) of the object (2).

35

15. Method for optically measuring by interferometry the thickness (T) of an object (2) during a surface machining of the object (2) that gradually reduces the thickness (T) of the object (2); the method including the steps of:

carrying out by optical interferometry a plurality of readings of the thickness (T) of the object for obtaining at least one rough thickness value (RTW) from each reading and, consequently, a plurality of rough thickness values (RTW);

determining an actual value of the thickness (T) of the object (2) by analyzing the plurality of rough thickness values (RTW);

setting a lower reject threshold ($R_{\min}$) and a higher reject threshold ($R_{\max}$) that define a searching interval comprising the actual value of the thickness (T) of the object (2); and

eliminating all the rough thickness values (RTW) that are lower than the lower reject threshold ($R_{\min}$) or higher than the higher reject threshold ($R_{\max}$);

the method being characterized in that it includes the step of:

progressively updating the lower reject threshold ($R_{\min}$) and the higher reject threshold ($R_{\max}$) as a function of the gradual reduction of the thickness (T) of the object (2).

16. Method according to claim 15, wherein the surface machining of the object (2) that gradually reduces the thickness (T) of the object (2) takes place according to a known machining process, the method including the further steps of:

determining the progress state of the surface machining of the object (2) as a function of the machining law; and

progressively updating the lower reject threshold ($R_{\min}$) and the higher reject threshold ($R_{\max}$) as a function of the progress state of the surface machining of the object (2).

5

17. Method according to claim 15 and including the further steps of:

carrying out a sequence of measurements of the thickness (T) of the object (2); and

10 updating the lower reject threshold ($R_{\min}$) and the higher reject threshold ($R_{\max}$) that are used for the current measurement of the thickness (T) of the object (2) as a function of the actual value of the thickness (T) of the object (2) determined at the end of the preceding measurement of the thickness (T) of the object (2).

15

18. Method according to claim 17 and including the further steps of:

20 determining, for each measurement of the thickness (T) of the object (2), the amplitude (ΔT) of a variation range of the actual value of the thickness (T) of the object (2); and

25 setting the lower reject threshold ($R_{\min}$) and the higher reject threshold ($R_{\max}$) that are used for the current measurement of the thickness (T) of the object (2), by subtracting from and adding to, respectively, the actual value of the thickness (T) of the object (2) determined at the end of the preceding measurement of the thickness (T) of the object (2) half the amplitude (ΔT) of the variation range of the actual value of the thickness (T) of the object (2) determined at the end of the preceding measurement of the thickness (T) of the object (2).

30

35

19. Method according to any one of claims 15 to 18 and including the further steps of:

determining a plurality of thickness classes (C) that is large enough to comprise a significant part of the rough thickness values (RTW);

5 classifying the rough thickness values (RTW) so as to determine for each thickness class (C) a corresponding frequency (F) indicating how often the rough thickness values (RTW) fall within that thickness class (C);

10 determining a preponderant group ($G_{\max}$) of thickness classes (C) that is composed of one or more adjacent thickness classes (C), for which the sum of the corresponding frequencies (F) defines an absolute maximum; and

15 determining the actual value of the thickness (T) of the object (2) as a function of the rough thickness values (RTW) belonging to the preponderant group ($G_{\max}$) of thickness classes (C).

20. Method according to claim 19 and including the further step of determining the actual value of the thickness (T) of the object (2) by averaging all the rough thickness values (RTW) belonging to the preponderant group ($G_{\max}$) of thickness classes (C).

21. Method according to any one of claims 3, 4, 19 or 20 and including the further steps of:

25 carrying out a sequence of measurements of the thickness (T) of the object (2);

30 determining, by analyzing a series of subsequent measurements, at least one possible parasitic thickness value that always remains constant in the series of subsequent measurements and a corresponding average number of rough thickness values (RTW) of the parasitic thickness value that belong to the thickness class (C) corresponding to the parasitic thickness value; and

35 eliminating from the thickness class (C) corresponding to the parasitic thickness value the average number of

rough thickness values (RTW) of the parasitic thickness value.

22. Method according to any one of claims 15 to 21 and
5 including the further steps of:
having a corresponding quality factor (MF) for each
reading and each rough thickness value (RTW);
setting a minimum quality threshold (MT_{min}); and
eliminating all the rough thickness values (RTW) whose
10 quality factors (MF) are lower than the minimum quality
threshold (MT_{min}).

23. Method according to any one of the preceding claims and
including the further steps of:
15 determining at least one rejection criterion of rough
thickness values (RTW);
eliminating all the rough thickness values that do not
comply with the rejection criterion;
determining an acceptability percentage ($A\%$)
20 representing the number of rough thickness values (RTW)
that comply with the rejection criterion in comparison
with the total number of available rough thickness
values (RTW); and
determining the actual value of the thickness (T) of
25 the object (2) only if the acceptability percentage ($A\%$)
is higher than a representativeness threshold (RT).

24. Method according to any one of the preceding claims and
including the further steps of:
30 carrying out a sequence of measurements of the
thickness (T) of the object (2), each of them using a
predetermined and constant number of readings of the
thickness (T) of the object that are carried out by
optical interferometry and are within a measuring
35 interval; and
translating over time, between two subsequent
measurements, the measuring interval by an extent which

is smaller than the extent of the measuring interval itself so that a number of readings of the thickness (T) of the object carried out by interferometry belongs to both the end part of the preceding measurement and the
5 initial part of the subsequent measurement.

25. Method according to any one of the preceding claims, wherein the object (2) is a slice of semiconductor material.

10

26. Apparatus for optically measuring by interferometry the thickness (T) of an object (2); the apparatus includes:
a measuring device (11) for thickness measurement by interferometry that carries out a plurality of readings
15 of the thickness (T) of the object for obtaining at least one rough thickness value (RTW) from each reading and, consequently, a plurality of rough thickness values (RTW); and
a processing unit (13) that carries out a measuring
20 method according to one of the preceding claims.