

DEVICE AND METHOD FOR INTERFEROMETRIC MEASURING OF AN OBJECT

Description

5 The invention relates to a device for the interferometric measuring of an object according to the preamble of claim 1 as well as a method for the interferometric measuring of an object according to the preamble of claim 12

10 Devices and methods for the interferometric measuring of an object are known in various embodiments: for example a typical design of a laser Doppler – vibrometer is known which comprises a laser as the light source for generating an emitted beam, a beam splitting device to split the emitted beam into a measuring and a reference beam, an optic interference device, and a first detector.

15 The measuring beam is guided to a measuring point on an object, and the measuring beam, at least partially reflected, is interfered together with the reference beam on a detector area of the detector so that by assessing the interference signal for example a movement of the object surface at the measuring point in the direction of the optic axis of the measuring beam can be concluded.

Furthermore, arrangements are known comprising a heterodyne design so that by phase modulations in the measuring light the direction of deflection by the surface to be measured can be concluded.

20 In order to obtain information about oscillations in two or three dimensions it is known to guide the measuring beams of three laser Doppler – vibrometers such that the measuring beams each impact the measuring point on the object diagonally in reference to each other.

25 The present invention is based on the objective to provide a device for the interferometric measuring of an object and a method for the interferometric measuring of an object so that the determination of additional information is possible in reference to single-beam laser Doppler – vibrometers of prior art. Simultaneously a robust construction and high measuring precision should be provided.

30 This objective is attained in a device for the interferometric measuring of an object according to claim 1 as well as by a method for the interferometric measuring of an object according to claim 12. Preferred embodiments of the device according to the invention are discernible from claims 2 through 11; preferred embodiments of the method according to the invention are described in claims 13 through 15. Hereby the wording of all claims is explicitly included in the description by way of reference.

The device according to the invention for the interferometric measuring of an object comprises a radiation source for generating an emitted beam, a beam splitter device for dividing the emitted beam into a measuring beam and a reference beam, an optic interference device, and a first detector.

- 5 The interference device and the first detector are embodied cooperating such that the measuring beam, at least partially reflected by the object, and the first reference beam are interfered at least on a detector area of the first detector.

10 With regards to this basic design the device according to the invention is therefore equivalent to interferometers of prior art; in particular typical laser Doppler – vibrometers of prior art show such a design.

It is essential that in the device according to the invention the beam splitter device is embodied to divide the emitted beam into a measuring beam, a first reference beam, and at least one second reference beam. Furthermore, the device according to the invention comprises at least one second detector and the interference device and the second detector are embodied cooperating
15 such that the measuring beam, at least partially scattered by the object, and the second reference beam are interfered on at least one detector area of the second detector.

The device according to the invention therefore comprises at least two detectors, on which beams are respectively interfered for an interferometric assessment. Contrary to devices of prior art the device according to the invention comprises however at least one measuring beam, which is
20 assessed on the one side by the first detector with regards to the at least partially reflected measuring beam and on the other side with regards to the measuring beam at least partially scattered by the object at the second detector.

The device according to the invention therefore exhibits a design different in principle, because the devices of prior art include one separate measuring beam for each detector.

- 25 In particular, the invention is based on the following acknowledgement of the applicant:

In the devices of prior art, in which several laser Doppler – vibrometers are combined, so that for example when three vibrometers are used, three measuring beams impact the object, here optimally the focuses of the measuring beams should be precisely overlapping because otherwise a measuring error develops during the rotation of the object about the center of the measuring
30 point.

When interfering measuring beams on the object, i.e. a precise accordance of the measuring points of several vibrometers, here the measuring light of the other two vibrometers is also received by each individual sensor because scattered light is not only collected from the measuring light of the observed channel but also measuring light from other channels, and made
35 to interfere on the detector (optic disturbance). Due to the fact that typically the frequencies of

lasers used within a frequency separation coincide, which is defined by the total of a demodulation band width and a heterodyne frequency shift, a considerable disturbing effect develops, which can lead to a total failure of the sensors to measure.

5 If this problem is circumvented by the measuring points being located slightly locally off-set, the above-stated disturbing effect is reduced, however not eliminated completely.

The above-mentioned method using several vibrometers with one measuring beam each generally show the problem of an optic interference of the detectors due to coupled measuring light of the measuring beams of the other vibrometers.

10 In prior art it is therefore usually necessary that the measuring points of several vibrometers used must be positioned locally side-by-side on the object in order to at least reduce any optic interference. However, here a limit develops with regards to the diameter of the measuring point, so that typically a diameter of the measuring point of 35 µm cannot be held. However it is desirable to yield multi-dimensional oscillation information for diameters of measuring points of less than 35 µm, particularly less than 15 µm, further preferred less than 5 µm.

15 In the solution according to prior art measuring occurs coaxially with each vibrometer. In a diagonal impacting of the measuring beam the primary portion of the capacity of the scattered light range is located about the reflected portion of the beam. The detection angle to the axis of the scattered light therefore amounts to twice the incident angle. Due to the fact that for a small focal diameter a high numeric aperture (NA) is required, the desired size of the measuring point
20 of each individual beam exhibits an opening angle of the measuring beam. This relationship in a homogenous lighting of the aperture of the lens of the microscope (outlet pupil) is given by the connection

$$d = 1.22 \frac{\lambda}{NA} \quad (\text{Formula 0})$$

25 with d representing the diameter of the focus in [m], λ the wavelength of the measuring beam in [m], and NA the numeric aperture of the lens.

Due to the fact that the opening angle cannot interfere, here a minimally possible angle results between the beams. Experiments of the applicant have shown that in the solutions of prior art the sensitivity of diagonally impinging vibrometer beams is no longer sufficient for most surfaces when a vertically impacting vibrometer beam is established, because then automatically
30 the incident angle of the diagonally impacting vibrometer becomes excessive. Accordingly, in both vibrometers a smaller diagonal angle must be realized, so that the incident angle keeps from being excessive in a vibrometer.

Thus, when using several vibrometers in general it is not possible to direct one of the measuring beams perpendicularly upon the surface of the sample. This would be desirable, though, with

regards to measuring technology because then a channel would directly measure the motion in the z-direction (target direction of the measuring head, which is perpendicular in reference to the intended location of the measuring surface), however due to the above-mentioned problem of diffused light in devices according to prior art it cannot be realized and/or leads to insufficient light with an excessive noise level for signal processing by diagonally measuring detectors.

In typical designs known from prior art a separate lens must be used for each measuring beam, so that there is no space available for another lens for a camera to record a spatially resolved measuring image. Typically here in devices according to prior art a camera may be coupled using a dichroitic beam splitter via a lens of a vibrometer used, in order to allow displaying the measuring point to the user for adjustment purposes. Due to the fact that, for the above-mentioned reasons, the lens exhibits a diagonal incident angle in reference to the surface of the object in devices of prior art, the image of the camera is also distorted and particularly not focused homogenously (with regards to different local positions). This way it is particularly difficult to perform a scanning measurement using a x-y – table, displacing the object.

The device according to the invention and the method according to the invention described in the following avoid all of the above-mentioned disadvantages. Due to the fact that only one measuring beam, starting at the device, is pointed from the device to the surface of the object to be measured, and on the one side a reflective portion of the measuring beam and on the other side at least one scattered portion of the measuring beam are assessed by one detector each, here oscillation information can be determined over various dimensions without several measuring beams need to be focused on the object, as in devices of prior art.

This way the above mentioned problems are corrected, caused by optical interference and the respective difficulties in signal processing, space problems with regards to objects used for focusing the measuring beam to the object, as well as the limitations regarding potential incident angles of the measuring beam upon the object.

The above-stated objective is also attained in the method according to the invention for an interferometric measuring of the object, which comprises the following processing steps:

In a processing step A an emitted beam is generated by a light source, in a processing step B a splitting of the emitted beam occurs via a beam splitting device into a measuring beam and a first reference beam. In a processing step C an interference of the first reference beam and the measuring beam occurs, at least partially reflected by the object in claim 12, to at least one detector area of a first detector.

It is essential that in the processing step B the emitted beam is additionally split into at least a second reference beam and the second reference beam is interfered with the measuring beam, at least partially reflected by the object in reference to the measuring beam in order to interfere on the first detector, here with a measuring beam scattered at a different angular range at the object on at least one detector area of a second detector. This light scattered into the different angular

range, which is interfered on the other detector area by a second reference beam, is called the reception light in the following, and the allocated optic radiation path the reception beam.

The method according to the invention exhibits the above-mentioned advantages of the device according to the invention.

- 5 The device according to the invention is preferably embodied to perform the method according to the invention and/or a preferred embodiment thereof. The method according to the invention is preferably implemented using a device according to the invention and/or a preferred embodiment thereof.

- 10 Preferably, via the first detector essentially portions of the measuring beam are measured reflected by the object, i.e. coaxially in reference to the optic axis of the measuring beam, light beams and/or light beam bundles. However, scattered portions of the measuring beam (of the reception beam) are measured by the second detector, i. e. preferably portions not aligned parallel in reference to the optic axis of the measuring beam and/or respective bundles of beams.

- 15 The invention is further based on the acknowledgement of the applicant that the scattered light, which is collected at a diagonal angle for example by a lens and is displayed on the second detector, is displaced by a moved surface of the object Doppler frequency. However, the method used in the above-mentioned devices cannot be applied here without changes to evaluate the measuring signal of the detector. However, a formula is known from literature, which has not been applied in the past within the scope of the device according to the invention or the method
20 according to the invention for a direction-dependent Doppler effect in order to correctly describe the phase and/or frequency shift based on the following formula 1:

$$\dot{\phi}_D = \frac{2\pi}{\lambda} (v_x \sin \beta_1 + v_x \sin \beta_2 + v_z \cos \beta_1 + v_z \cos \beta_2) \quad (\text{Formula 1})$$

- The geometric parameters are discernible from the schematic illustration according to Fig. 1. The remaining parameters are defined as follows: v_x is the speed of the measuring object in the x-direction in [m/s], v_z is the speed of the measuring object in the z-direction in [m/s], and $\dot{\phi}_D$ is the derivative of the phase in [2 π rad/s].
25

If the measuring beam impinges perpendicular in the coordinate system discussed, the formula 1 simplifies to the formula 2:

$$\dot{\phi}_D = \frac{2\pi}{\lambda} (v_x \sin \beta_2 + v_z + v_z \cos \beta_2) \quad (\text{Formula 2})$$

- 30 For the above-mentioned reasons, preferably the measuring beam impacts approximately perpendicular the area of the measuring object to be measured.

As described above, the device according to the invention preferably comprises a first lens, which is arranged in the radiation path of the measuring beam and the first reference beam between the object and a first detector.

5 This way, particularly the measuring beam can be focused on a measuring point on the object. Preferably the lens comprises a numeric aperture greater than 0.05, preferably greater than 0.1, particularly preferred equivalent or greater than 0.2. This leads to the advantage that according to the formula 0 a small measuring focus develops, which particularly amounts to considerably less than 5 μm in the green wavelength used, even if the aperture of the lens is illuminated with a Gauss-shaped beam. Due to the fact that no additional laser beams impact the measuring surface
10 the focal diameter of the measuring beam is equivalent to the size of the measuring point of the entire system. Due to the circumstance that only one laser beam impacts the objects an extremely small measuring point is achieved and any optic interference cannot occur. This essential knowledge has led to the concept of the present invention.

15 Furthermore it is advantageous that the first lens is also arranged in the radiation path of the reception beam between the lens and the second detector. This way, only one lens is necessary in order to display the reflected measuring beam on the first detector, on the one side, and the scattered measuring beam (reception beam) on the second detector, on the other side.

In another preferred embodiment the device comprises a second lens, which is arranged in the radiation path of the reception beam between the lens and the second detector. This way, by the
20 second lens the optic illustration of the scattered measuring beam on the second detector can be selected in a targeted fashion. In particular it is advantageous that the numeric aperture of the second lens is lower than 0.15, preferably lower than 0.1, further preferred lower than 0.06. The numeric aperture can be selected smaller because the size of the measuring point is not influenced by the numeric aperture of the reception beam. This way the advantages develop that
25 a smaller detection angle can be selected which must be equivalent to at least the sum of half the opening angle of the measuring beam and half the opening angle of the reception beam. Furthermore, this leads to a greater area overlapped in the z-direction, which is equivalent to a greater range of depth measurement.

30 In another preferred embodiment the device according to the invention for a heterodyne measurement via the first detector is embodied such that a device is provided for a frequency shift between the measuring beam and a first reference beam, which can preferably be achieved by an optic frequency shifter, such as a Bragg-cell, e.g. This way, here in a manner known per se the direction of motion of the surface of the object measured can be determined as well. In particular it is advantageous that in all reference beams one frequency displacement device each
35 is arranged between the measuring beam and the reference beam so that the heterodyne design is therefore given with regards to all reference beams. A particularly simple design results from the preferred embodiment in which only the measuring beam is frequency modulated, so that the

measuring beam is displaced in reference to all reference beams with regards to frequency and thus here a completely heterodyne design is given with regards to all detectors.

In another preferred embodiment the device is embodied as a confocal microscope with regards to the beam path of the measuring beam and a first reference beam. This way, the advantage results that non-focal radiation is not displayed on the detector. A typical confocal design can be realized by providing an optic pinhole in the radiation path of the measuring beam and the first reference beam. Preferably the confocal design is yielded by embodying the detector as an optic pinhole.

In another preferred embodiment the beam splitting device is embodied to split the emitted beam into a measuring beam, a first reference beam, a second reference beam, and at least one third reference beam. Furthermore, the device comprises at least one third detector, and the interference device and the third detector are embodied cooperating such that the beam at least partially scattered by the object and the third reference beam are interfered at least on a detector area of the third detector. This way a measuring of an oscillation or deflection of the surface of the object is possible in three dimensions.

In particular it is advantageous that the device is embodied such that a first plane, which is defined by the measuring beam and the reception beam, forms an angle greater than 45° , preferably greater than 85° with a second plane, which is formed by the measuring beam and the third reference beam. This way it is ensured that a sufficiently precise separation of the information about motions is possible in three dimensions.

Preferably, the angle between the measuring beam and at least one reception beam is less than 40° , preferably less than 30° . In particular it is advantageous that in all reception beams the angle between the measuring beam and the reception beam is respectively below 40° , preferably below 30° . This way a high signal-noise ratio is ensured for the reception beams and a large range of depth measurement.

Preferably the radiation source is embodied as a longitudinal single-mode laser. This way the advantage results that no disturbing interferences between the modes develop by the optic mixing effects. In particular it is advantageous to embody the radiation source additionally as a transversal single-mode laser, so that furthermore the advantage develops that the measuring laser beam can be optimally focused and a minimal measuring point – diameter is yielded. A laser with a M^2 -factor of less than 1.5 has proven sufficient for good focusing effects.

Experiments of the applicant have shown that particularly the embodiment of the radiation source as a laser with a wavelength in the visible range is advantageous, preferably as a DPSS-laser with a wavelength of 532 nm.

In order to yield a small measuring point it is advantageous for all detectors to only evaluate light of the reflected or scattered measuring beam of one measuring area on the object with a diameter

of less than 35 μm , particularly less than 15 μm , further preferred less than 5 μm . In particular the optic components and here for example one or more lenses of the device are preferably embodied such that a measuring range is displayed on the object with a diameter less than 35 μm , particularly less than 15 μm , further preferred less than 5 μm on the measuring area of the detectors.

The method according to the invention is preferably embodied such that the measuring signals of the first and the second detector are each phase modulated so that a multi-dimensional evaluation of the deflection of the surface of the object can be performed.

In another advantageous embodiment of the method according to the invention the measuring signals of the first detector are phase modulated, in order to perform a deflection of the surface of the object and the measuring signals of the second detector are amplitude modulated in order to perform an assessment of the intensity of the scattered measuring beam. This way, in a simple fashion both the deflection in the direction of the optic axis of the measuring beam as well as the intensity of the scattered light can be measured with a precision not achieved in prior art. This results in a plurality of new applications:

In particular it is possible to detect unevenness or flawed particles on an essentially smooth surface by determining from a relative motion of the measuring beam in reference to the surface any changes of the surface (in the transferred sense the “deflection”) by way of phase modulation of the measuring signals of the first detector and furthermore the light scattered by the flawed particles via amplitude modulation of the measuring signals of the second detector.

Preferably the method according to the invention is therefore embodied such that a surface topography of the object is determined, comprising the following steps:

- Moving the object in reference to the measuring beam, preferably essentially perpendicular in reference to the optic axis of the measuring beam, and
- Measuring the deflection via the first detector as well as measuring the scattered light via the second detector.

In the following additional features and preferred embodiments are described based on the figures and the exemplary embodiments. Here it shows:

Fig. 1 a schematic illustration of a typical design of a device according to the invention for illustrating the geometric parameters of the formula 1, which describes the Doppler effect depending on the direction;

Fig. 2 a schematic illustration of a first exemplary embodiment of a device according to the invention;

Fig. 3 a spatial arrangement of a light source and detectors of the first exemplary embodiment shown in Fig. 2; and

Fig. 4 schematic illustrations of the radiation paths in exemplary embodiments of the device according to the invention with one lens (detail A) and several lenses (detail B).

Fig. 1 shows the geometric arrangement for applying the above-mentioned formula 1 based on a first exemplary embodiment.

- 5 For an easier understanding here initially the first exemplary embodiment is explained based on the schematic illustration according to Fig. 2.

In the first exemplary embodiment a light source 1 is embodied as a laser with a wavelength of 532 nm. An emitted beam 2, which is generated by the laser, is split by the beam splitting device into a measuring beam 3 and a first reference beam 4a, a second reference beam 4b, and a third
10 reference beam 4c.

For this purpose, the beam splitting device comprises several beam splitters 5a, 5b, and 5c. The measuring beam 3 is displayed via a first lens 6a on a measuring point A on an object 7 to be measured. The measuring beam reflected by the surface of the object 7 at the measuring point A in turn enters the beam path of the first lens 6a and is displayed via an optic interference device
15 on a first detector 8a, which first detector 8a comprises two photo-detectors 8a' and 8a''. The optic interference device comprises the mirror M, the polarization beam splitter PBS. The detector comprises an additional beam splitter 8a''' for interfering the radiation on the two photo-detectors 8a' and 8a''.

The design of the first photo-detector is therefore equivalent to the design of the so-called
20 "balanced detector" arrangement known per se.

A confocal design is realized via a pinhole A in the radiation path of the measuring beam and a first reference beam.

Furthermore, a frequency displacement device 9 is arranged in the radiation path of the measuring beam 3, embodied as a Bragg-cell, in order to embody a heterodyne design with
25 regards to the measuring beam and all reference beams. Alternatively the frequency displacement device 9 may be arranged in the radiation path of one or both reference beams.

The first measuring beam is displayed in a manner known per se via a telescope T and Lambda quarter wavelength plates QWP on the measuring point A on the object 7 and accordingly the recoupled, reflected measuring beam is displayed via this optic design on the first detector 8a.

30 The device according to Fig. 2 also comprises a second detector 8b similar to the first detector 8a, which comprises two photo-detectors 8b' and 8b'' as well as a beam splitter 8b''' for a balanced-detector arrangement. The portion of the measuring light scattered at the measuring point A on the object 7 is collected as the first reception beam 4b', partially via a second lens 6b, and interfered with the second reference beam 4c via the mirror M and another telescope T on
35 the second detector 8b.

Similarly, a third lens 6c is provided, which collects portions of the measuring beam scattered in another spatial angle at the point A of the object 7 as a second reception beam 4c' and displays it via the mirror M on a third detector 8c, which third detector 8c comprising in an analog design two photo-detectors 8c' and 8c'' as well as a beam splitter 8c'''. Similarly, the scattered light
 5 portions of the measuring beam, collected by the lens 6c, are interfered with a third reference beam 4c on the measuring area of the photo detectors 8c' and 8c''.

The device is preferably arranged and embodied such that the measuring beam 3 impacts the measuring point A approximately perpendicular in reference to the area normal of the object 7.

The measuring point generated by the first lens 6a exhibits a diameter of less than 5 μm .

10 For this purpose, the first lens exhibits a numeric aperture of approximately 0.2. The numeric apertures of the second and third lens 6b and 6c amount to approximately 0.1, however.

The three detectors 8a, 8b, and 8c are connected to an assessment unit (not shown) which is embodied in a manner known per se, in order to perform amplitude modulations and/or phase demodulations of the measuring signals of the photo-detectors.

15 This way, it is possible to measure for example a motion of the measuring point A on the surface of the object 7 in three dimensions. Here, it is possible for the first time to perform this with a measuring point showing a diameter of 5 μm , without here the disturbing effects occur that are reported in prior art.

20 In order to assess the three-dimensional oscillation information the Doppler effect, depending on the direction, is considered, preferably according to formula 1.

The importance of the geometric parameters of formula 1 is illustrated in the schematic representation according to Fig. 1:

25 The light source embodied as a laser, with its emitted beam being split into a measuring beam 3 and several reference beams, is arranged such that the measuring beam 3 impacts the measuring point A on the area normal of the object 7 at an angle β_1 . The area normal furthermore defines the xy plane and the z-axis arranged perpendicular in reference thereto.

The second detector 8b is arranged at an angle β_2 .

30 As already stated, Fig. 2 shows a schematic illustration of an exemplary embodiment of a device according to the invention, in which for a simplified illustration all radiation paths are shown two-dimensionally.

Fig. 3 shows the actual spatial arrangements of the light source 1, the first detector 8a, the second detector 8b, and the third detector 8c in a spatial illustration particularly with regards to the x, y, and z-coordinates defined by the area normal of the measuring object 7 at the measuring point A. In particular, the angles φ_{det} are marked, which are preferably less than 40°

Fig. 4 shows two details of exemplary embodiments of the device according to the invention:

The detail A shows an exemplary embodiment in which via only one lens both the measuring beam 3 is displayed on the measuring point A on the measuring object 7 as well as a first reference beam 4a, aligned at a spatial angle φ_{det} in reference thereto, is displayed by the very
 5 same lens on the second detector via additional components.

The detail B however shows an exemplary embodiment in which via a first lens 6a the measuring beam 3 is displayed on the measuring point A of the object 7 and a scattered light portion of the measuring beam 3, via a second lens 6b and additional optic components, is displayed on the second detector 8b.

Claims

1. A device for the interferometric measuring of an object, comprising a light source to generate an emitted beam, a beam slitting device for splitting the emitted beam into a measuring beam and a first reference beam, an optic interference device, and a first detector, with the interfering device and the first detector being embodied cooperating such that the measuring beam at least partially reflected by the object and the first reference beam are interfered on at least one detection area of the first detector, characterized in that the beam splitting device is embodied to divide the emitted beam into a measuring beam, a first reference beam, and at least a second reference beam, that the device comprises at least a second detector, and the interfering device and the second detector are embodied cooperating such that the measuring beam as a first reception beam, at least partially scattered by the object at a different angular range than the at least partially reflected measuring beam, and the second reference beam are interfered on at least one detector area of the second detector.
2. A device according to claim 1, characterized in that the device comprises a first lens, which is arranged in the radiation path of the measuring beam, and a first reference beam between the object and the first detector, that preferably the numeric aperture of the lens is greater than 0.1, preferably greater than 0.15, particularly greater than 0.2.
3. A device according to claim 2, characterized in that the first lens is further arranged in the radiation path of the second reference beam between the object and the second detector.
4. A device according to claim 3, characterized in that the device comprises a second lens which is arranged in the radiation path of the second reference beam between the object and the second detector, that preferably the numeric aperture of the second lens is less than 0.15, preferably less than 0.1.
5. A device according to one of the previous claims, characterized in that the device is embodied for a heterodyne measuring via the first detector by a frequency displacement device being provided for the frequency shift between the measuring beam and the first reference beam, that preferably the frequency displacement device is provided for the frequency displacement between the measuring beam and all reference beams.
6. A device according to one of the previous claims, characterized in that the device is embodied as a confocal microscope with regards to the radiation paths of the measuring beam and the first reference beam.
7. A device according to one of the previous claims, characterized in that the beam splitting device is embodied to split the emitted beam into a measuring beam, a first reference beam, a second reference beam, and at least a third reference beam, that the

device comprises at least a third detector, and the interference device and the third detector are embodied cooperating such that the measuring beam, at least partially scattered by the object, is interfered as a second reception beam and the third reference beam is interfered on at least one detector area of the third detector, that preferably the device is embodied such that a first level, which is defined by the measuring beam and the second reference beam, forms an angle greater than 45° , preferably greater than 85° with a second level, which is formed by the measuring beam and the third reference beam.

8. A device according to one of the previous claims, characterized in that the angle between the measuring beam and at least one receiving beam, preferably between the measuring beam and all reception beams, is less than 30° .
9. A device according to one of the previous claims, characterized in that the radiation source is embodied as a longitudinal single-mode laser, preferably is additionally embodied as a transversally single-mode laser, particular a laser with a M^2 -factor smaller than 1.5.
10. A device according to one of the previous claims, characterized in that the radiation source is embodied as a laser with a wavelength in the visible range.
11. A device according to claim 10, characterized in that the light source is embodied as a DPSS-laser with a wavelength of 532 nm.
12. A method for the interferometric measuring of an object, comprising the following processing steps:
 - A Generating an emitted beam via a light source;
 - B Splitting an emitted beam via a beam splitting device into a measuring beam and a first reference beam;
 - C Interfering a first reference beam and the measuring beam, at least partially reflected by the object, to at least one detector surface of a first detector;
 characterized in that in the processing step B the emitted beam is additionally split into at least a second reference beam and the second reference beam is interfered on at least one detector area of the second detector with the measuring beam, scattered at least partially by the object at a different angular range than the at least partially reflected measuring beam.
13. A method according to claim 12, characterized in that the measuring signals of the first and the second detector are each phase modulated for a multi-dimensional assessment of a deflection of the surface of the object.
14. A method according to one of claims 12 through 13, characterized in that the measuring signals of the first detector are phase modulated for an assessment of a deflection of the surface of the object and that the measuring signals of the second

detector are amplitude modulated for an evaluation of the intensity of the scattered measuring beam.

15. A method according to claim 14, characterized in that the surface topography of the object is determined, comprising the following processing steps:
- Moving the object in reference to the measuring beam, preferably essentially perpendicular in reference to the optic axis of the measuring beam, and
 - Measuring the deflection via the first detector as well as measuring the scattered light via the second detector.

Figure 1

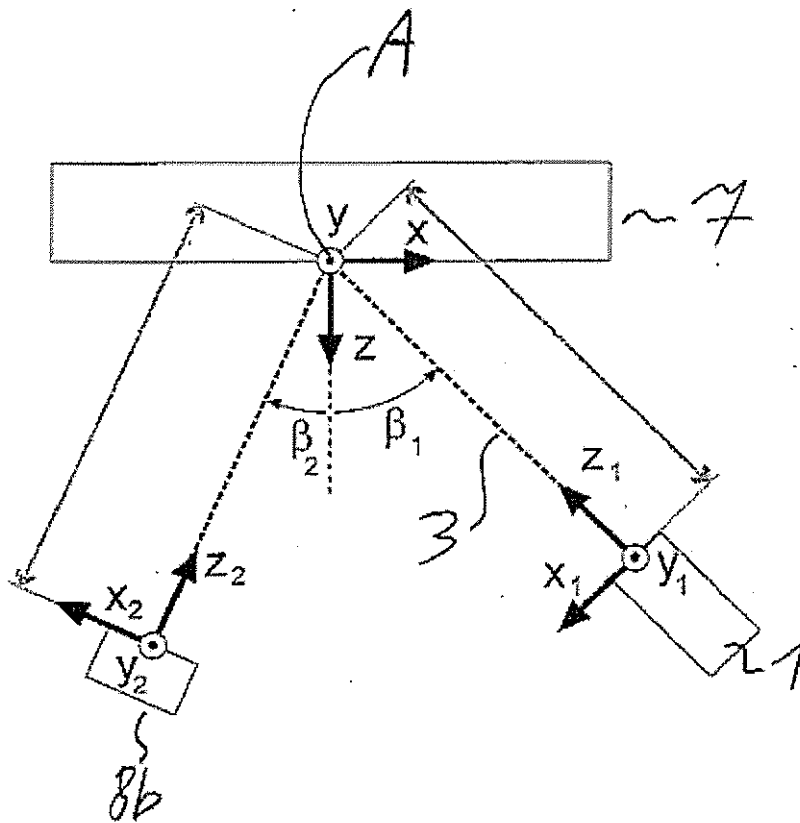


Figure 2

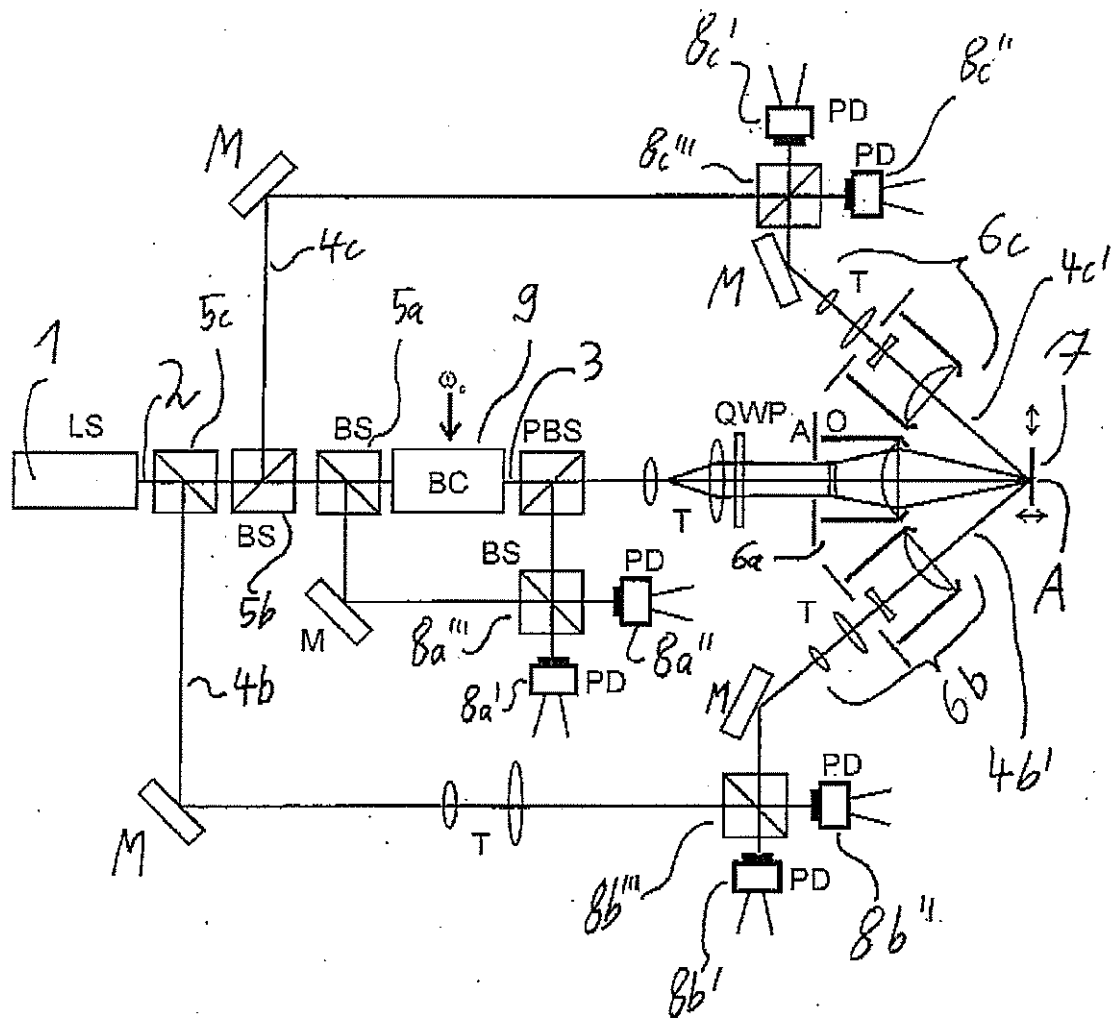


Figure 3

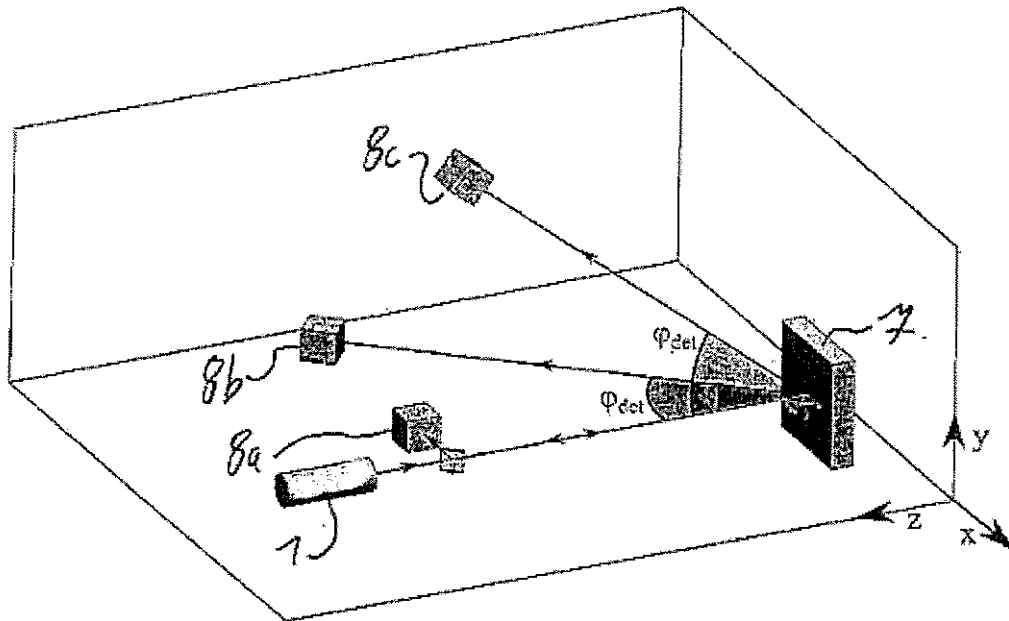
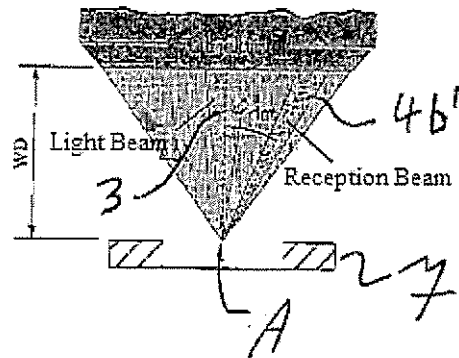


Figure 4

a)



b)

