

MULTILAYERED CONSTRUCTION FOR RESISTOR AND CAPACITOR FORMATION

BACKGROUND OF THE INVENTION

Field of the Invention

10 This invention relates to a multilayered construction useful for forming capacitors and resistors, on printed circuit boards, other microelectronic devices, and the like. The multilayered construction comprises sequentially attached layers including a first electrically conductive layer, a first thermosetting polymer layer, a heat resistant film layer, a second thermosetting polymer layer, and a nickel-phosphorus electrical resistance material layer electroplated onto a
15 second electrically conductive layer.

Description of the Related Art

As the circuitry design of central processing units (CPU) seeks to achieve
20 increased operational speed, the performance of integrated circuits becomes ever
more important. The circuitry design of printed circuit boards, which mount
these integrated circuits, is also very important.

Capacitors and resistors are common elements on printed circuit boards and other microelectronic devices. Capacitors are used to steady the operational power supply of such devices. A capacitor is a device used for introducing capacitance into a circuit, and functions primarily to store electrical energy, block the flow of direct current, or permit the flow of alternating current. They comprise a dielectric material sandwiched between two electrically conductive

metal layers, such as copper foils. In general, the dielectric material is coupled to the electrically conductive metal layers via an adhesive layer, by lamination, or by vapor deposition.

- 5 Heretofore, capacitors arranged on the surface of printed circuit boards have been common. However, more recently, capacitors are formed of a thin, double-sided copper clad laminate within multilayered circuit board layers thus producing excellent characteristics. Of these options, it has been preferred to form printed circuit boards having embedded capacitors to maximize the surface
10 area of the circuit board for other purposes. In order to achieve increased signal transmission speed, printed circuit board manufacturers generally form printed circuit boards within such a multilayer structure. The capacitance of a capacitor depends primarily on the shape and size of the capacitor layers and the dielectric constant of the insulating material. There are various known types of dielectric
15 materials known in the art. For example, the dielectric material may be a gas, such as air, a vacuum, a liquid, a solid or a combination thereof. Each material has its own particular properties.

- The performance of conventional capacitors for use in printed circuit boards has
20 been limited by factors such as limited minimum thickness of their dielectric material, which detracts from the flexibility of the capacitor, the attainable capacitance, the effect of bond enhancers on the metal foils, low dielectric constant, and poor dielectric strength.

- 25 It is desirable to form a capacitor for circuit boards having a high dielectric constant and an extremely thin layer of dielectric material, thus increasing the capacitance and flexibility of the capacitor. To optimize the performance of a capacitor, it is important that the dielectric material employed have good material properties, exhibiting such qualities as superior adhesion, high

- dielectric strength and good flexibility. However, common problems frequently associated with extremely thin dielectric layers are the formation of microscopic voids or other structural defects and inclusion of foreign material. These lead to electrical shorts. For example, U.S. Pat. Nos. 5,155,655 and 5,161,086 describe
- 5 a method for forming a capacitor wherein a single sheet of a dielectric material is laminated together with two conductive foils. Dielectric layers of this type are highly vulnerable to the formation of voids, as well as the inclusion of foreign material, and are time consuming to detect and remedy.
- 10 U.S. Patent No. 6,693,793 relates to a structure having a pair of conductive foils, a pair of thin dielectric layers, with one dielectric layer on a surface of each of the foils. The two conductive foils are adhered together such that the dielectric layers are attached to one another via an intermediate heat resistant film layer. This capacitor offer a significant improvement in performance over
- 15 prior art capacitors and printed circuit boards. The thin dielectric layers allow for higher capacitance, greater heat conductivity and greater flexibility of the capacitor. The intermediate heat resistant film layer deters the formation of electrical shorts between the electrically conductive foils.
- 20 It would be desired to form a multilayered structure which has both capacitive and resistive elements. The present invention provides such a multilayered structure for resistor and capacitor formation. The inventive structure provides high capacitance, greater heat conductivity, and greater flexibility, while also incorporating a resistor element. The multilayered structure includes
- 25 sequentially attached layers comprising: a first electrically conductive layer, a first thermosetting polymer layer, a heat resistant film layer, a second thermosetting polymer layer, and a nickel-phosphorus electrical resistance material layer electroplated onto a second electrically conductive layer.

SUMMARY OF THE INVENTION

The invention provides a multilayered construction suitable for forming resistors and capacitors, which multilayered construction comprises sequentially attached
5 layers comprising: a first electrically conductive layer, a first thermosetting polymer layer, a heat resistant film layer, a second thermosetting polymer layer, and a nickel-phosphorus electrical resistance material layer electroplated onto a second electrically conductive layer.

10 The invention also provides a capacitor which comprises sequentially attached layers comprising: a first electrically conductive layer, a first thermosetting polymer layer, a heat resistant film layer, a second thermosetting polymer layer, and a nickel-phosphorus electrical resistance material layer electroplated onto a second electrically conductive layer.

15 The invention further provides a method of forming a multilayered construction which comprises attaching a first thermosetting polymer layer to a surface of a first electrically conductive layer; electroplating a nickel-phosphorus electrical resistance material layer onto a surface of a second electrically conductive layer;
20 attaching a second thermosetting polymer layer to a surface the electrical resistance material layer; and then attaching the first and second thermosetting polymer layers to opposite surfaces of a heat resistant film layer.

BRIEF DESCRIPTION OF THE DRAWINGS

25 FIG. 1 is a schematic representation of a multilayered construction according to the invention, including the following sequentially attached layers: a first electrically conductive layer, a first thermosetting polymer layer, a heat resistant film layer, a second thermosetting polymer layer, and a nickel-phosphorus
30 electrical resistance material layer electroplated onto a second electrically

conductive layer.

FIG. 2 is a schematic representation of a multilayered construction according to FIG. 1, wherein an additional nickel-phosphorus electrical resistance material layer has been electroplated onto the first electrically conductive layer such that the additional nickel-phosphorus electrical resistance material layer is attached between the first thermosetting polymer layer and the first electrically conductive layer.

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DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

The invention relates to a multilayered construction suitable for forming resistors, capacitors, and the like. As shown in FIG. 1, the multilayered construction 1 comprises a sequentially attached layers comprising a first electrically conductive layer 2, a first thermosetting polymer layer 4, a heat resistant film layer 6, a second thermosetting polymer layer 8, and a nickel-phosphorus electrical resistance material layer 10 electroplated onto a second electrically conductive layer 12. The first and second thermosetting polymer layers 4, 8 may be the same or a different material, and the first and second electrically conductive layers 2, 12 may be the same or a different material.

In another preferred embodiment, shown in FIG. 2, the multilayered construction 1 further comprises an additional nickel-phosphorus electrical resistance material layer 14 electroplated onto the first electrically conductive layer 2 such that the additional nickel-phosphorus electrical resistance material layer 14 is attached between the first thermosetting polymer layer 4 and the first electrically conductive layer 2. Thus, as shown in Fig. 2, the layers are sequentially attached as: a first electrically conductive layer 2, an additional nickel-phosphorus electrical resistance material layer 14 electroplated onto the

first electrically conductive layer 2, a first thermosetting polymer layer 4, a heat resistant film layer 6, a second thermosetting polymer layer 8, and a nickel-phosphorus electrical resistance material layer 10 electroplated onto a second electrically conductive layer 12.

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For purposes of this invention, attaching means any method of appending one layer to the next layer, non-exclusively including coating, laminating, sputtering, vapor depositing, electrodeposition, plating, or evaporating, either simultaneously or sequentially.

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The first electrically conductive layer 2 and the second electrically conductive layer 12 are preferably present in the form of a conductive layer or foil or the like. In a most preferred embodiment, they are each present in the form of a foil. Each electrically conductive layer may comprise either the same metal or may comprise different metals. The conductive metals appropriate for the purposes of the present invention may vary depending on the desired application. Preferably, the electrically conductive layers 2, 12 comprise a material selected from the group consisting of copper, zinc, brass, chrome, nickel, tin, aluminum, stainless steel, iron, gold, silver, titanium, platinum and combinations and alloys thereof. Most preferably, the electrically conductive layers comprise copper. The electrically conductive layers preferably have a thickness of from about 0.5 to about 200 microns, more preferably from about 9 to about 70 microns. The conductive materials used in the capacitors of this invention may be manufactured with a shiny side surface and a matte surface.

Examples of such conductive materials are disclosed in U.S. Pat. No. 5,679,230, which is incorporated herein by reference.

The electrically conductive layers 2, 12 may be provided with a bond enhancing treatment on one or both sides. One or both sides of the layers may optionally

be roughened, such as by micro-etching, by being electrolytically treated to form a roughened copper deposit, and/or by being electrolytically treated with a deposition of micro-nodules of a metal or metal alloy on or in the surface. Such include a treatment with nickel, chromium, chromates, zinc, and a silane
5 coupling agent or combinations thereof. The nodules may comprise the same, or a different metal as the electrically conductive layers. The nodules are preferably copper or a copper alloy, and increase adhesion to the polymer film. Such nodules may be applied according to a technique described in U.S. Pat. No. 5,679,230, which is incorporated herein by reference. In a preferred
10 embodiment, at least one of the first electrically conductive layer and the second electrically conductive layer are provided with a bond enhancing treatment on one or both sides thereof.

The surface microstructure of the electrically conductive layers may be
15 measured by a profilometer, such as a Perthometer model M4P or S5P, which is commercially available from Mahr Feinpruef Corporation of Cincinnati, Ohio. Topography measurements of the surface grain structure of peaks and valleys are made according to industry standard IPC-TM-650 Section 2.2.17 of the Institute for Interconnecting and Packaging Circuits of 2115 Sanders Road,
20 Northbrook, Ill. 60062. The surface treatments are carried out to produce a surface structure having peaks and valleys which produce roughness parameters wherein the arithmetic average roughness (Ra) ranges from about 0.2 to about 1 microns and the ten point height of irregularities according to ISO 64287-1 (Rz) surface roughness may range from about 0.5 μm to about 7 μm , more preferably
25 from about 0.5 μm to about 5 μm , and most preferably from about 0.5 μm to 3 μm .

The first thermosetting polymer layer 4 and the second thermosetting polymer layer 8 may independently comprise an epoxy, a combination of epoxy and a

material which polymerizes with an epoxy, a melamine, an unsaturated polyester, a urethane, alkyd, a bis-maleimide triazine, a polyimide, an ester, an allylated polyphenylene ether (or allyl-polyphenylene ether) or combinations thereof. The thermosetting polymer layers 4, 8 are typically in dry, solid form, and may comprise about 100% of any of the above compounds, or may comprise mixtures of these compounds, or may contain other additives. Other acceptable materials include aromatic thermosetting co-polyesters such as those described in U.S. Pat. Nos. 5,439,541 and 5,707,782. Of these materials, the most preferred dielectric is an epoxy having a glass transition temperature (T_g) from about 100°C to about 250°C, preferably from about 150°C to about 200°C.

The thermosetting polymer layers 4, 8 may also optionally comprise a filler material. Preferred fillers non-exclusively include powdered ferroelectric materials, barium titanate (BaTiO_3), boron nitride, aluminum oxide, strontium titanate, barium strontium titanate, and other ceramic fillers and combinations thereof. If incorporated, a filler is preferably present in the thermosetting polymer layers in an amount of from about 5% to about 80% by volume of the layer, more preferably from about 10% to about 50% by volume of the layer. Preferably at least one of the first thermosetting polymer layer 4, the heat resistant film layer 6, and the second thermosetting polymer layer 8 comprises such a powdered filler having a dielectric constant of about 10 or higher. In addition, either one or both of the thermosetting polymer layers 4, 8 may contain a dye or pigment to impart color, alter dielectric opacity or affect contrast.

In one preferred embodiment, the thermosetting polymer layers 4, 8 are applied to the electrically conductive layers or heat resistant film layer as liquid polymer solutions to allow for control and uniformity of the polymer thickness. The solution will typically have a viscosity ranging from about 50 to about 35,000 centipoise with a preferred viscosity in the range of 100 to 27,000 centipoise.

The polymer solution will include from about 10 to about 80% and preferably 15 to 60 wt % polymer with the remaining portion of the solution comprising one or more solvents. Useful solvents include acetone, methyl-ethyl ketone, N-methyl pyrrolidone, N, N dimethylformamide, N, N dimethylacetamide and
5 mixtures thereof. A most preferred single solvent is methyl-ethyl ketone.

The thermosetting polymer layers may be also applied to the electrically conductive layers 2, 12 or heat resistant film layer 6 in the form of solid sheets. In such an embodiment, the attaching of the first and second thermosetting
10 polymer layers to opposite surfaces of the heat resistant film layer is done by lamination. Lamination may be conducted in a press at a temperature of from about 150°C to about 310°C, more preferably from about 160°C. to about 200°C. Lamination may be conducted for from about 30 minute to about 120 minutes, preferably from about 40 minutes to about 80 minutes. Preferably, the
15 press is under a vacuum of at least 70 cm (28 inches) of mercury, and maintained at a pressure of about from about 3.5 kgf/cm² (50 psi) to about 28 kgf/cm² (400 psi), preferably from about 4.9 kgf/cm² (70 psi) to about 14 kgf/cm² (200 psi).

20 Preferably, the thermosetting polymer layers 4, 8 have a thickness of from about 2 to about 200 microns, more preferably from about 2 to about 100 microns. Preferably the thermosetting polymer layers have a dielectric strength of at least about 19,685 volts/mm (500 volts/mil) thickness.

25 The heat resistant film layer 6 preferably comprises a polyethylene terephthalate, a polyethylene naphthalate, a polyvinyl carbazole, a polyphenylene sulfide, an aromatic polyamide, a polyimide, a polyamide-polyimide, a polyether nitrile, a polyether-ether-ketone, or combinations thereof. It has a preferred thickness of about 12.5 μ m or less. The combined thickness of the first thermosetting

polymer layer 4, the heat resistant film layer 6, and the second thermosetting polymer layer 8 is about 25 μm or less. The heat resistant film layer 6 has a VICAT softening point of about 150°C or higher as determined by ISO 306. The heat resistant film layer 6 preferably has a Young's modulus of about 300
5 kgf/mm^2 or more, a tensile strength of about 20 kgf/mm^2 or more, an elongation of about 5% or more, and a higher softening temperature than the laminating temperature of the first thermosetting polymer layer 4 and the second thermosetting polymer layer 8. The dielectric constant of each of the first thermosetting polymer layer 4, the heat resistant film layer 6, and the second
10 thermosetting polymer layer 8 is about 2.5 or more. The heat resistant film layer 6 preferably has a dielectric breakdown voltage of at least about 50 volts, more preferably at least about 250 volts, and most preferably at least about 500 volts.

Prior to attaching the layers to form the multilayered construction, the heat
15 resistant film layer 6 may have undergone a bond enhancing treatment which may comprise a plasma treatment, a corona treatment, a chemical treatment or combinations thereof.

The nickel-phosphorus electrical resistance material layer 10 is preferably
20 electroplated, using a conventional electroplating process, onto the second electrically conductive layer. Electroplating is a technique well known in the art which is typically conducted by placing a substrate in a liquid electrolyte solution, and applying an electrical potential between a conducting area on the substrate and a counter electrode in the liquid. A chemical process takes place
25 resulting in the formation of a layer of material on the substrate.

Electroplating baths used for the deposition of resistive films typically operate at a temperature significantly greater than room temperature, that is, at a temperature in excess of 100° F (38°C). In fact, most baths previously used to

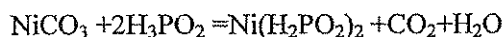
deposit resistive alloy films operate at a temperature of 150° F (65°C) to about 212° F (100°C). The thickness of the electro-deposited electrical resistance layer deposited on the conductive layer in known processes is a function of plating efficiency which is, in turn, a function of temperature.

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An example of a suitable electro-plating bath comprises an aqueous solution of hypophosphite ions, and in particular, hypophosphite ions formed from nickel hypophosphite ($\text{Ni}(\text{H}_2\text{PO}_2)_2$). Nickel hypophosphite is easily prepared by the reaction of nickel carbonate (NiCO_3) with hypophosphorous acid (H_3PO_2). That is, nickel hypophosphite suitable for electro-deposition of a nickel-phosphorous electrical resistance layer on a conductive layer is prepared by forming an aqueous solution of about one-half mole of nickel carbonate and one mole of hypophosphorous acid with a limited amount of water thus producing a crystalline reaction product which completely dissolves when diluted with water to a concentration of about 0.67 moles per liter. The reaction is believed, without intending to limit the present invention, to proceed according to the following equation:

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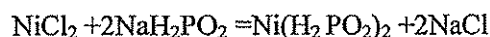
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Alternatively, an electroplating bath comprising hypophosphite ions formed from nickel hypophosphite can be produced by the reaction of nickel chloride (NiCl_2) and sodium hypophosphite (NaH_2PO_2). The reaction equation is hypothesized to be:

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Nonetheless, it may be preferred to employ an electro-plating bath formed from nickel carbonate and hypophosphorous acid with nickel-hypophosphite as a

reaction product since the reaction produces by-products of carbon dioxide and water; whereas, an electro-plating bath formed from nickel chloride and sodium hypophosphite to produce nickel hypophosphite often produces a by-product of sodium chloride which must be removed to prevent undue concentration build
5 up over time in a continuous process. An electro-plating bath comprising hypophosphite ions formed from nickel hypophosphite has been found to be operable at temperatures from about 20°C to 50° C. It may be desirable to operate the baths at room temperature (20°C to 25°C). Such baths are effectively temperature insensitive.

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In one preferred embodiment, the formed electrical resistance material layer contains up to about 50 percent by weight of phosphorus. In another preferred embodiment, the electrical resistance material layer contains up to about 30 percent by weight of phosphorus. In another embodiment, the electrical
15 resistance material comprises from about 30 to about 50 percent by weight of phosphorus. Another embodiment of the invention includes an electroplating of the second electrically conductive layer in a bath comprising an aqueous solution of a nickel ion source, H_3PO_3 and H_3PO_4 , wherein the bath is substantially sulfate and chloride free.

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It is known in the art the resistance of the electrical resistance layer of a circuit board material is dependent on both the thickness of the electrical resistance layer and the resistivity of the material employed therein. As the thickness of the electrical resistance layer decreases, the resistance of said layer increases.

25 The electrical resistance material layer 10 preferably has a resistance ranging from about 5 ohms/square to about 500 ohms/square, more preferably, ranging from about 10 ohms/square to about 300 ohms/square, and most preferably ranging from about 25 ohms/square to about 250 ohms/square. The nickel-phosphorus electrical resistance material layer preferably has a thickness

ranging from about 0.02 μm to about 0.2 μm more preferably from about 0.03 μm to about 1 μm , and most preferably from about 0.04 μm to about 0.4 μm .

5 In an additional preferred embodiment, at least the top about ten atomic layers of the electrical resistance material layer are free of sulfur. In another preferred embodiment, the surface of the electrical resistance material layer is substantially pit free.

10 The optional additional nickel-phosphorus electrical resistance material layer 14 may be the same or different from the nickel-phosphorus electrical resistance material layer 10. Preferably these two layers 10, 14 are substantially the same.

15 The multilayered construction of the invention comprises sequentially attached layers of a first electrically conductive layer, a first thermosetting polymer layer, a heat resistant film layer, a second thermosetting polymer layer and a second electrically conductive layer. By sequentially attached is meant that the layers must be present in the indicated order; however, other intermediate layers may optionally be present between the specified layers. For example, in a preferred embodiment the multilayered construction further comprises an additional
20 nickel-phosphorus electrical resistance material layer electroplated onto the first electrically conductive layer such that the additional nickel-phosphorus electrical resistance material layer is attached between the first thermosetting polymer layer and the first electrically conductive layer.

25 In an additional embodiment of the invention (not shown), the multilayered construction further comprises a barrier layer adhered between said electrical resistance material layer 10 and said second electrically conductive layer 12, wherein said barrier layer has a thickness of less than about 0.1 μm , is different in composition from said electrical resistance material layer, and is capable of

- protecting said electrical resistance material layer 10 from attack by alkaline ammoniacal copper etchants. The barrier layer preferably has a thickness of less than about 0.1 μm , more preferably ranging from about 50 angstroms to about 0.1 μm , and most preferably from about 150 angstroms to about 600 angstroms.
- 5 In a preferred embodiment, the barrier layer is electrodeposited using conventional techniques. The barrier layer can be an inorganic material which has good etchant selectivity. It is also important that the material used as the barrier layer have no substantial detrimental effect on the uniformity of the resistivity and other functional properties of the underlying electrical resistance
- 10 layer. The barrier layer preferably comprises a material selected from the group consisting of Ni-Sn, Co-Sn, Cd-Sn, Cd-Ni, Ni-Cr, Ni-Au, Ni-Pd, Ni-Zn, Sn-Pb, Sn-Zn, Ni, Sn, and combinations thereof. A preferred barrier layer comprises Ni-Sn.
- 15 The multilayered construction of the invention is preferably used in the formation of a resistor or capacitor. Such may be used in the formation of printed circuit boards, electronic devices, and the like.
- In a preferred embodiment of the invention, the preferred capacitance of a
- 20 capacitor according to the invention is at least about 100 pF/cm², more preferably from about 100 pF/cm² to about 4,000 pF/cm². Capacitors of this invention may be used in a variety of printed circuit applications. For example, an electrical connection may be present on the first electrically conductive layer and another electrical connection to the second electrically conductive layer.
- 25 The capacitor may be connected to or be incorporated into a printed circuit board or other electronic device or the electronic device may comprise a printed circuit board comprising the capacitor. They may be coupled with or embedded within rigid, flexible or in rigid/flexible electrical circuits, printed circuit boards or other microelectronic devices such as chip packages. Generally, they are

used by creating a first circuit pattern on one or both electrically conductive material layers. A second circuit pattern may be applied to the polymer surface either in the form of a conductive foil, by electrodeposition, by sputtering, by vapor phase deposition or some other means. In addition, it may be necessary to
5 generate vias in the capacitor to electrically connect opposing circuit layers.

Once a capacitor has been formed, circuit patterns may also be created in the electrically conductive material layer using known etching techniques. In etching, a layer of a photo-imageable resist, dry-film or liquid material is
10 applied to the conductive foil layer. Using a negative photo pattern, which is overlaid on the resist, the photoresist is exposed to actinic radiation such as UV radiation creating a desired circuit pattern. The imaged capacitor is then exposed to film developing chemistry that selectively removes the unwanted unexposed portions. The capacitor with circuit image is then contacted with
15 known chemical etchant baths to remove the exposed conductive layer, leaving the final desired conductive patterned capacitor. Also, each of the conductive material layers may optionally be electrically connected by forming a hole through the entire capacitor and filling it with a conductive metal. Lamination steps are preferably conducted at a minimum of 150°C.

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The multilayered construction of the present invention offers a significant improvement in performance over prior art capacitors and printed circuit boards. This construction offers better uniformity, higher capacitance, greater heat conductivity, and greater flexibility, while also incorporating a resistor element.

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The following non-limiting examples serve to illustrate the invention.

EXAMPLE 1

A 35 μm thick electrodeposited (ED) copper foil is provided, which foil has a surface roughness of 3 microns and has been electroplated with a layer of nickel-phosphorous. The thickness and composition of the nickel-phosphorous layer is such to result in an electrical resistance layer of 25 ohms/square. A layer of epoxy resin is applied to one side of a 12 micron polyamide film with a thickness of 6 microns. On another 35 micron ED copper foil a layer of epoxy resin is applied to a thickness of 6 microns. The two coated foils are laminated together with a sheet of 12 micron polyamide film between the foils with the resistance layer coming in contact with the resin coated side of the film. Lamination occurs in a hydraulic press under 250 psi at 350 °F for 1 hour. The press chamber is also under a vacuum of 25 mm Hg. After lamination the combined product is High Potential Tested to 500 volts to check for possible shorts. A pattern is etched into the copper surfaces using industry standard techniques using an alkaline etchant. This chemistry will etch the copper without attacking the resistance (Ni-P) layer. A second imaging process is conducted to form the resistor pattern by vacuum laminating a photoresist, exposing and developing it. The photoresist remains on the Ni-P layer that defines the resistor pattern. The background Ni-P is removed using an acid etchant (such as cupric chloride or copper sulfate). The photoresist is stripped and the circuits are inspected using automated optical inspection and or electrical test (including High Potential testing). The circuitized product goes through a process to prepare the copper for relamination. This process is a black oxide or an alternative. The circuitized product is laminated into a multilayer circuit board and completed using industry standard techniques.

EXAMPLE 2

Example 1 is repeated except that both sides of the polyamide film are applied with a copper layer and an electrical resistance layer, resulting in a two sided resistor product.

EXAMPLE 3

A roll of one ounce copper foil is cut into foil samples of predetermined sizes. A predetermined amount of foil samples are electroplated with a nickel-phosphate electrical resistance material layer, and a predetermined amount foil samples do not receive such electroplating.

For those foil samples to be electroplated, a batch process is employed with the plating cell remaining constant. Mild agitation is provided in the plating cell by a recirculating pump to maintain uniform bath composition. The cathode employed is electro-deposited one ounce copper foil which is plated on the matte side. The shiny or drum side of the foil is masked by a rubber coated backing fixture. The cathode size is 11.5 inches by 14.25 inches. The anode is platinum clad columbium with an anode to cathode ratio of 1.3:1. Prior to passing into the plating cell, the copper foil is immersed in an aqueous hydrochloric acid solution (equal volume) for one minute. The copper foil is then passed through an activating solution comprising an aqueous solution of benzotriazole for 30 seconds prior to passing through the plating cell.

A plating bath is formed which comprises 0.5 moles per liter of nickel hypophosphite. The plating bath is made by reacting 20 moles of nickel carbonate (2508 grams of basic nickel carbonate, $\text{NiCO}_3 \cdot 2\text{Ni}(\text{OH})_2 \cdot 4\text{H}_2\text{O}$, mol. wt. 376.24) with 40 moles of hypophosphorous acid (8.6 liters of 50% H_3PO_2 at

9.3 M/L diluted with an equal volume of water) and subsequently diluting the reaction product to 40 liters. The temperature of the plating bath, after cooling to room temperature, is 23°C, the current is 10 amperes, and the plating bath dwell time is 30 seconds.

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Next the electroplated foil samples and non-electroplated foil samples each receive a layer of epoxy resin. A liquid epoxy resin is adjusted to 30% solids, a viscosity of about 500 centipoises, with MEK in a stainless steel mixing vat. A doctor blade is adjusted to produce a wet film of 15 microns in thickness, resulting in a flexible composite having a dried polymer film in thickness of about 5 microns. A continuous liquid head height and volume of dammed material is maintained on the upstream side of the doctor blade to maintain a constant flexible composite film thickness and a film free of included air bubbles.

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The solvent is evaporated off and the epoxy resin is cured in an oven. As the coated foil first enters the oven, an initial temperature drop should be anticipated. Once steady state temperatures are achieved in the oven, film thickness is checked by taking a foil sample and comparing the coated weight to the base weight of the foil using the epoxy resin density to convert from weight to film thickness. Adjustments to the rate of epoxy resin dispensed and or doctor blade height over the foil are corrected based on this measurement. This process is repeated until the desired film thickness is attained to produce first and second thermosetting polymer layers on first and second copper foil layers.

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A capacitor is formed by laminating two pieces of epoxy coated foil to an intermediate heat resistant sheet of an aromatic polyamide having a thickness of 4 μm , Young's modulus of 1500 kg/mm^2 , a tensile strength of 40 kg/mm^2 and an elongation of about 20% in 25°C. One of the coated copper foils has been

electroplated with a nickel-phosphorus electrical resistance material layer. Lamination is done in a hydraulic press at 165°C and 10 kgf/cm² (150 psi) for 60 minutes. The press is under vacuum of 71 cm (28 inches) of mercury. The capacitor is cut to size and processed to impart a pattern in the copper. The
5 resulting capacitor is visually inspected and then electrically tested for shorting at 500 volts. Resulting capacitor layers have a capacitance of at least 300 pF/cm² and a dielectric breakdown voltage of at least 7.87 x 10⁴ volts/mm (2000 volts/mil.).

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EXAMPLE 4

Example 3 is repeated except both of the copper foils laminated to the heat resistant sheet have been electroplated with a nickel-phosphorus electrical resistance material layer.

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While the present invention has been particularly shown and described with reference to preferred embodiments, it will be readily appreciated by those of ordinary skill in the art that various changes and modifications may be made without departing from the spirit and scope of the invention. It is intended that
20 the claims be interpreted to cover the disclosed embodiment, those alternatives which have been discussed above and all equivalents thereto.

What is claimed is:

1. A multilayered construction suitable for forming resistors and capacitors,
5 which multilayered construction comprises sequentially attached layers
comprising: a first electrically conductive layer, a first thermosetting polymer
layer, a heat resistant film layer, a second thermosetting polymer layer, and a
nickel-phosphorus electrical resistance material layer electroplated onto a
second electrically conductive layer.
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2. The multilayered construction of claim 1 which further comprises an
additional nickel-phosphorus electrical resistance material layer electroplated
onto the first electrically conductive layer such that the additional nickel-
phosphorus electrical resistance material layer is attached between the first
15 thermosetting polymer layer and the first electrically conductive layer.
3. The multilayered construction of claim 1 wherein the electrical resistance
material layer has a resistance ranging from about 5 ohms/square to about 500
ohms/square.
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4. The multilayered construction of claim 1 wherein the first electrically
conductive layer and the second electrically conductive layer independently
comprise a material selected from the group consisting of copper, zinc, brass,
chrome, nickel, tin, aluminum, stainless steel, iron, gold, silver, titanium,
25 platinum and combinations thereof.
5. The multilayered construction of claim 1 wherein the first electrically
conductive layer and the second electrically conductive layer comprise copper.

6. The multilayered construction of claim 1 wherein the first electrically conductive layer and the second electrically conductive layer comprise copper foils having a surface roughness R_z in the range of from about 0.5 μm to about 7 μm .
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7. The multilayered construction of claim 1 wherein at least one of the first electrically conductive layer and the second electrically conductive layer are provided with a bond enhancing treatment on one or both sides thereof.
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8. The multilayered construction of claim 1 wherein at least one of the first electrically conductive layer and the second electrically conductive layer are provided with a bond enhancing treatment which comprises treatment with metal nodules, nickel, chromium, chromates, zinc, a silane coupling agent or combinations thereof.
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9. The multilayered construction of claim 1 wherein one or both of the first thermosetting polymer layer and the second thermosetting polymer layer comprise an epoxy, a melamine, an unsaturated polyester, a urethane, alkyd, a bis-maleimide triazine, a polyimide, an ester, an allyated polyphenylene ether or
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- combinations thereof.
10. The multilayered construction of claim 1 wherein the heat resistant film layer comprises a polyethylene terephthalate, a polyethylene naphthalate, a polyvinyl carbazole, a polyphenylene sulfide, an aromatic polyamide, a
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- polyimide, a polyamide-polyimide, a polyether-nitrile, a polyether-ether-ketone, or combinations thereof.
11. The multilayered construction of claim 1 wherein the electrical resistance material layer contains up to about 30 percent by weight of phosphorus.

12. The multilayered construction of claim 1 wherein at least about the top ten atomic layers of the electrical resistance material layer are free of sulfur.
13. The multilayered construction of claim 1 further comprising a barrier layer adhered between said electrical resistance material layer and said second electrically conductive layer, wherein said barrier layer has a thickness of less than about 0.1 μm , is different in composition from said electrical resistance material layer, and is capable of protecting said electrical resistance material layer from attack by alkaline ammoniacal copper etchants.
14. A capacitor which comprises sequentially attached layers comprising: a first electrically conductive layer, a first thermosetting polymer layer, a heat resistant film layer, a second thermosetting polymer layer, and a nickel-phosphorus electrical resistance material layer electroplated onto a second electrically conductive layer.
15. The capacitor of claim 14 which further comprises an additional nickel-phosphorus electrical resistance material layer electroplated onto the first electrically conductive layer such that the additional nickel-phosphorus electrical resistance material layer is attached between the first thermosetting polymer layer and the first electrically conductive layer.
16. A printed circuit board comprising the capacitor of claim 14.
17. An electronic device comprising the printed circuit board of claim 16.
18. An electronic device comprising the capacitor of claim 14.

19. A method of forming a multilayered construction which comprises attaching a first thermosetting polymer layer to a surface of a first electrically conductive layer; electroplating a nickel-phosphorus electrical resistance material layer onto a surface of a second electrically conductive layer; attaching a second
- 5 thermosetting polymer layer to a surface the electrical resistance material layer; and then attaching the first and second thermosetting polymer layers to opposite surfaces of a heat resistant film layer.
20. The method of claim 19 wherein the attaching of the first and second
- 10 thermosetting polymer layers to opposite surfaces of the heat resistant film layer is by lamination.