

FLAME RETARDANT ELECTRICAL WIRE

CROSS REFERENCE TO RELATED APPLICATIONS

This application claims priority to United States Provisional Application Serial Nos. 60/637,406, 60/637,419, and 60/637,412 filed on December 17, 2004, which are incorporated in their entirety by reference herein.

BACKGROUND OF INVENTION

Automotive electrical wire located under the hood in the engine compartment has traditionally been insulated with a single layer of high temperature insulation that is disposed over an uncoated copper conductor. Thermoplastic polyesters, cross linked polyethylene and halogenated resins such as fluoropolymers, polyvinyl chloride have long filled the need for the high temperature insulation needed in this challenging environment that requires not only heat resistance, chemical resistance, flame retardance, and flexibility.

Thermoplastic polyester insulation layers have outstanding resistance to gas and oil, are mechanically tough and resistant copper catalyzed degradation but can fail prematurely due to hydrolysis. The insulation layers in thermoplastic polyester insulated electrical wires have also been found to crack when exposed to hot salty water and have failed when subjected to humidity temperature cycling.

There is an increasing desire to reduce or eliminate the use of halogenated resins in insulating layers due to their negative impact on the environment. In fact, many countries are beginning to mandate a decrease in the use of halogenated materials. However, as much of the wire coating extrusion equipment was created based upon the specifications of halogenated resins such as polyvinyl chloride, any replacement materials must be capable of being handled in a manner similar to polyvinyl chloride.

Cross linked polyethylene has largely been successful in providing high temperature insulation but this success may be difficult to sustain as the requirements for automotive electrical wire evolve. The amount of wiring in automobiles has increased exponentially, as more electronics are being used in modern vehicles. The dramatic

increase in wiring has motivated automobile manufacturers to reduce overall wire diameter by specifying reduced insulation layer thicknesses and specifying smaller conductor sizes. For example, ISO 6722 specifies, for a conductor having a cross sectional area of 2.5 square millimeters, that the thin wall insulation thickness be 0.35 millimeters and the ultra thin wall insulation thickness be 0.25 millimeters.

The reductions in insulation wall thickness pose difficulties when using crosslinked polyethylene. For crosslinked polyethylene the thinner insulation layer thickness result in shorter thermal life, when aged at oven temperatures between 150°C and 180°C. This limits their thermal rating. For example, an electrical wire having a copper conductor with an adjacent crosslinked polyethylene insulation layer having a 0.75 millimeter wall thickness is flexible and the insulation layer does not crack when bent around a mandrel after being exposed to 150°C for 3,000 hours. But with a similar electrical wire having a crosslinked polyethylene insulation layer with a 0.25 millimeter wall thickness, the insulation layer becomes brittle after being exposed to 150°C for 3,000 hours. The deleterious effects created by these extremely thin wall requirements have been attributed to copper catalyzed degradation, which is widely recognized as a problem in the industry.

It is possible to coat the copper core with, e.g., tin, in order to prevent the copper from contacting the crosslinked polyethylene but the additional cost of the coating material and the coating process are expensive. In addition, many automotive specifications require that the copper conductor be uncoated. It is also possible to add stabilizers, also known as metal deactivators, to the insulation material but it is recognized that stabilizers yield only partial protection for electrical wire having thin wall thicknesses.

It has been proposed to employ bilayer or trilayer insulation materials wherein a protective resin based layer is disposed between the crosslinked polyethylene and the copper conductor. However, manufacture of bilayer and trilayer insulation materials is complex, requires increased capital expenditure and the multi layer material presents new issues of inter layer adhesion.

In addition, flame retardance becomes increasingly difficult as the insulation wall thickness decreases, due, at least in part, to the insulation layer having a larger surface area to volume ratio.

Accordingly, there exists a need for electrical wires useful in the automotive environment.

BRIEF DESCRIPTION OF THE INVENTION

The above described need is met by an electrical wire comprising:

a conductor, and

a covering disposed over the conductor wherein the covering comprises a thermoplastic composition and the thermoplastic composition comprises:

- (i) a poly(arylene ether);
- (ii) a high density polyethylene;
- (iii) a block copolymer; and
- (iv) an organic phosphate ester flame retardant,

wherein the electrical wire has an average flame out time less than or equal to 10 seconds based on ten test wires having a conductor size of 0.2 square millimeters and a covering thickness of 0.2 millimeters tested according to ISO 6722 for conductor sizes less than or equal to 2.5 millimeters and all ten test wires have a flame out time less than 70 seconds.

In another embodiment, an electrical wire comprises

a conductor, and

a covering disposed over the conductor wherein the covering comprises a thermoplastic composition and the thermoplastic composition comprises:

- (i) a poly(arylene ether);

- (ii) a high density polyethylene;
- (iii) a block copolymer; and
- (iv) an organic phosphate ester flame retardant, wherein the block copolymer has a weighted average aryl alkylene content greater than or equal to 15 weight percent.

In another embodiment, a thermoplastic composition useful in a covering disposed over a conductor in an electrical wire comprises:

- (i) a poly(arylene ether);
- (ii) a high density polyethylene;
- (iii) a block copolymer; and
- (iv) an organic phosphate ester flame retardant,

wherein the electrical wire has an average flame out time less than or equal to 10 seconds based on ten test wires having a conductor size of 0.2 square millimeters and a covering thickness of 0.2 millimeters tested according to ISO 6722 for conductor sizes less than or equal to 2.5 millimeters and all ten test wires have a flame out time less than 70 seconds.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a schematic representation of a cross-section of electrical wire.

Figures 2 and 3 are perspective views of an electrical wire having multiple layers.

Figures 4 and 5 are graphs showing the flexural modulus and flame out time of Examples 2-4 and Examples 5-7.

DETAILED DESCRIPTION

In this specification and in the claims, which follow, reference will be made to a number of terms which shall be defined to have the following meanings.

The singular forms “a,” “an,” and “the” include plural referents unless the context clearly dictates otherwise.

“Optional” or “optionally” means that the subsequently described event or circumstance may or may not occur, and that the description includes instances where the event occurs and instances where it does not.

The endpoints of all ranges reciting the same characteristic are independently combinable and inclusive of the recited endpoint. Values expressed as “greater than about” or “less than about” are inclusive the stated endpoint, e.g., “greater than about 3.5” encompasses the value of 3.5.

Conductor size refers to the cross sectional area of the conductor. ISO 6722 referred to herein is the December 15, 2002 version of this standard.

As briefly discussed before, electrical wires must meet a wide range of requirements depending upon their application. The requirements for automotive electrical wires are difficult to achieve, particularly in the absence of halogenated materials. In particular, robust flame retardance (also known as fire retardance) for an electrical wire is difficult to achieve when the covering disposed over the conductor comprises polyolefin, poly(arylene ether), block copolymer and organic phosphate ester flame retardant. Typically flame retardance is achieved in similar thermoplastic compositions by adding sufficient flame retardant to achieve the desired level fire retardance. However, increased amounts of organic phosphate esters can have a negative impact on other physical properties.

Surprisingly, the selection of the polyolefin can play an important role in obtaining excellent flame retardance in an electrical wire. Electrical wires having a covering comprising a thermoplastic composition that comprises high density polyethylene show surprisingly better flame retardance than comparable electrical wires having coverings comprising a thermoplastic composition that comprise other polyolefins such as polypropylene. Additionally compositions comprising high density polyethylene show lower flexural modulus in relation to comparable compositions comprising polypropylene which can translate into desirable properties when used in

an electrical wire. Flexural modulus values are inversely related to flexibility so that a low flexural modulus value would indicate a high flexibility.

Flexibility is an important property for a covering as the electrical wire must be capable of being bent and manipulated without cracking the covering. A crack in the covering can result in a voltage leak. In addition, several tests included in ISO 6722, the international standard for 60V and 600V single core cables in road vehicles, require that the electrical wire be subjected to a prescribed set of conditions and then wound around a mandrel. After being wound around a mandrel the covering of the electrical wire is examined for cracks and defects. Electrical wires using thermoplastic compositions that are minimally flexible prior to being subjected to conditions such as heat aging or chemical resistance testing frequently have insufficient flexibility, after being subjected to testing conditions, to be wound around a mandrel without cracks developing in the covering.

In addition the choice of polyolefin, the aryl alkylene content of the block copolymer can also play a role in the flame retardance properties of the electrical wire. In one embodiment, the block copolymer has a weighted average aryl alkylene content greater than or equal to 15 weight percent. The weighted average aryl alkylene content is calculated based upon the amount of each block copolymer when more than one block copolymer is used and the aryl alkylene content of the block copolymer or block copolymers. For instance, if a single block copolymer is used then the weighted average aryl alkylene content is the aryl alkylene content of the single block copolymer. If two block copolymers are used then the weighted average aryl alkylene content is determined by:

$$\text{weighted average aryl alkylene content} = \left(\frac{A1}{A1+A2} \times C1 \right) + \left(\frac{A2}{A1+A2} \times C2 \right)$$

where A1 = the amount of first block copolymer in weight percent based on the combined weight of poly(arylene ether), high density polyethylene, block copolymers and organic phosphate ester, C1 = the amount of aryl alkylene in the first block

copolymer, based on the total weight of the first block copolymer, A2 = the amount of second block copolymer in weight percent, based on the combined weight of poly(arylene ether), high density polyethylene, block copolymers and organic phosphate ester and C2 = the amount of aryl alkylene in the second block copolymer, based on the total weight of the second block copolymer. If more than two block copolymers are used then the weighted average aryl alkylene content is calculated similarly using a term for each block copolymer.

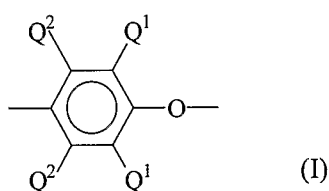
The thermoplastic composition described herein comprises at least two phases, a high density polyethylene phase and a poly(arylene ether) phase. The high density polyethylene phase is a continuous phase. In one embodiment the poly(arylene ether) phase is dispersed in the high density polyethylene phase. Good compatibilization between the phases can result in improved physical properties including higher impact strength at low temperatures and room temperature, better heat aging, better flame retardance, as well as greater tensile elongation. It is generally accepted that the morphology of the thermoplastic composition is indicative of the degree or quality of compatibilization. Small, relatively uniformly sized particles of poly(arylene ether) evenly distributed throughout an area of the thermoplastic composition are indicative of good compatibilization.

The thermoplastic compositions described herein are essentially free of an alkenyl aromatic resin such as polystyrene or rubber-modified polystyrene (also known as high impact polystyrene or HIPS). Essentially free is defined as containing less than 10 weight percent (wt%), or, more specifically less than 7 wt%, or, more specifically less than 5 wt%, or, even more specifically less than 3 wt% of an alkenyl aromatic resin, based on the combined weight of poly(arylene ether), high density polyethylene and block copolymer(s). In one embodiment, the thermoplastic composition is completely free of an alkenyl aromatic resin. Surprisingly the presence of the alkenyl aromatic resin can negatively affect the compatibilization between the poly(arylene ether) phase and the high density polyethylene phase.

In one embodiment the thermoplastic composition has a flexural modulus of 6,000 to 18,000 kilograms/centimeter (kg/cm^2) (600 to less than 1800 Megapascals (MPa))

when determined by ASTM D790-03 using a speed of 1.27 millimeters per minute and samples molded as described in the Examples below. Within this range the flexural modulus may be greater than or equal to $8,000 \text{ kg/cm}^2$, or, more specifically, greater than or equal to $10,000 \text{ kg/cm}^2$. Also within this range the flexural modulus may be less than or equal to $16,000 \text{ kg/cm}^2$, or, more specifically, less than or equal to $15,000 \text{ kg/cm}^2$.

As used herein, a “poly(arylene ether)” comprises a plurality of structural units of the formula (I):



wherein for each structural unit, each Q^1 and Q^2 is independently hydrogen, halogen, primary or secondary lower alkyl (e.g., an alkyl containing 1 to 7 carbon atoms), phenyl, haloalkyl, aminoalkyl, alkenylalkyl, alkynylalkyl, hydrocarbonoxy, aryl and halohydrocarbonoxy wherein at least two carbon atoms separate the halogen and oxygen atoms. In some embodiments, each Q^1 is independently alkyl or phenyl, for example, C_{1-4} alkyl, and each Q^2 is independently hydrogen or methyl. The poly(arylene ether) may comprise molecules having aminoalkyl-containing end group(s), typically located in an ortho position to the hydroxy group. Also frequently present are tetramethyl diphenylquinone (TMDQ) end groups, typically obtained from reaction mixtures in which tetramethyl diphenylquinone by-product is present.

The poly(arylene ether) may be in the form of a homopolymer; a copolymer; a graft copolymer; an ionomer; or a block copolymer; as well as combinations comprising at least one of the foregoing. Poly(arylene ether) includes polyphenylene ether containing 2,6-dimethyl-1,4-phenylene ether units optionally in combination with 2,3,6-trimethyl-1,4-phenylene ether units.

The poly(arylene ether) may be prepared by the oxidative coupling of monohydroxyaromatic compound(s) such as 2,6-xyleneol and/or 2,3,6-trimethylphenol.

Catalyst systems are generally employed for such coupling; they can contain heavy metal compound(s) such as a copper, manganese or cobalt compound, usually in combination with various other materials such as a secondary amine, tertiary amine, halide or combination of two or more of the foregoing.

In one embodiment, the poly(arylene ether) comprises a capped poly(arylene ether). The terminal hydroxy groups may be capped with a capping agent via an acylation reaction, for example. The capping agent chosen is preferably one that results in a less reactive poly(arylene ether) thereby reducing or preventing crosslinking of the polymer chains and the formation of gels or black specks during processing at elevated temperatures. Suitable capping agents include, for example, esters of salicylic acid, anthranilic acid, or a substituted derivative thereof, and the like; esters of salicylic acid, and especially salicylic carbonate and linear polysalicylates, are preferred. As used herein, the term "ester of salicylic acid" includes compounds in which the carboxy group, the hydroxy group, or both have been esterified. Suitable salicylates include, for example, aryl salicylates such as phenyl salicylate, acetylsalicylic acid, salicylic carbonate, and polysalicylates, including both linear polysalicylates and cyclic compounds such as disalicylide and trisalicylide. In one embodiment the capping agents are selected from salicylic carbonate and the polysalicylates, especially linear polysalicylates, and combinations comprising one of the foregoing. Exemplary capped poly(arylene ether) and their preparation are described in United States Pat. Nos. 4,760,118 to White et al. and 6,306,978 to Braat et al.

Capping poly(arylene ether) with polysalicylate is also believed to reduce the amount of aminoalkyl terminated groups present in the poly(arylene ether) chain. The aminoalkyl groups are the result of oxidative coupling reactions that employ amines in the process to produce the poly(arylene ether). The aminoalkyl group, ortho to the terminal hydroxy group of the poly(arylene ether), can be susceptible to decomposition at high temperatures. The decomposition is believed to result in the regeneration of primary or secondary amine and the production of a quinone methide end group, which may in turn generate a 2,6-dialkyl-1-hydroxyphenyl end group. Capping of poly(arylene ether) containing aminoalkyl groups with polysalicylate is

believed to remove such amino groups to result in a capped terminal hydroxy group of the polymer chain and the formation of 2-hydroxy-N,N-alkylbenzamine (salicylamide). The removal of the amino group and the capping is believed to provide a poly(arylene ether) that is more stable to high temperatures, thereby resulting in fewer degradative products during processing of the poly(arylene ether).

The poly(arylene ether) can have a number average molecular weight of 3,000 to 40,000 grams per mole (g/mol) and a weight average molecular weight of 5,000 to 80,000 g/mol, as determined by gel permeation chromatography using monodisperse polystyrene standards, a styrene divinyl benzene gel at 40°C and samples having a concentration of 1 milligram per milliliter of chloroform. The poly(arylene ether) or combination of poly(arylene ether)s has an initial intrinsic viscosity greater than or equal to 0.35 dl/g, as measured in chloroform at 25°C. Initial intrinsic viscosity is defined as the intrinsic viscosity of the poly(arylene ether) prior to melt mixing with the other components of the thermoplastic composition. As understood by one of ordinary skill in the art the viscosity of the poly(arylene ether) may be up to 30% higher after melt mixing. The percentage of increase can be calculated by (final intrinsic viscosity after melt mixing – initial intrinsic viscosity before melt mixing)/initial intrinsic viscosity before melt mixing. Determining an exact ratio, when two initial intrinsic viscosities are used, will depend somewhat on the exact intrinsic viscosities of the poly(arylene ether) used and the ultimate physical properties that are desired.

The poly(arylene ether) used to make the thermoplastic composition can be substantially free of visible particulate impurities. In one embodiment, the poly(arylene ether) is substantially free of particulate impurities greater than 15 micrometers in diameter. As used herein, the term “substantially free of visible particulate impurities” when applied to poly(arylene ether) means that a ten gram sample of a poly(arylene ether) dissolved in fifty milliliters of chloroform (CHCl_3) exhibits fewer than 5 visible specks when viewed in a light box with the naked eye. Particles visible to the naked eye are typically those greater than 40 micrometers in diameter. As used herein, the term “substantially free of particulate impurities greater than 15 micrometers” means that of a forty gram sample of poly(arylene ether)

dissolved in 400 milliliters of CHCl_3 , the number of particulates per gram having a size of 15 micrometers is less than 50, as measured by a Pacific Instruments ABS2 analyzer based on the average of five samples of twenty milliliter quantities of the dissolved polymeric material that is allowed to flow through the analyzer at a flow rate of one milliliter per minute (plus or minus five percent).

The thermoplastic composition may comprise the poly(arylene ether) in an amount of 30 to 65 weight percent (wt%), based on the combined weight of the poly(arylene ether), high density polyethylene, organic phosphate ester flame retardant and block copolymer. Within this range the amount of poly(arylene ether) may be greater than or equal to 40 wt%, or, more specifically, greater than or equal to 45 wt%. Also within this range the amount of poly(arylene ether) may be less than or equal to 60 wt%.

The high density polyethylene can be homo polyethylene or a polyethylene copolymer. Additionally the high density polyethylene may comprise a combination of homopolymer and copolymer, a combination of homopolymers having different melting temperatures, or a combination of homopolymers having a different melt flow rate. The high density polyethylene may have a density of 0.941 to 0.965 g/cm^3 .

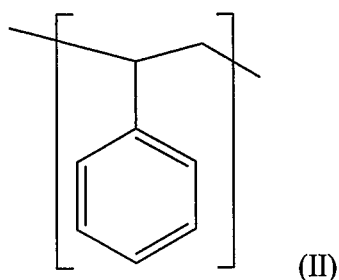
In some embodiments the high density polyethylene has a melting temperature greater than or equal to 124°C, or, more specifically, greater than or equal to 126°C, or, even more specifically, greater than or equal to 128°C.

The high density polyethylene has a melt flow rate (MFR) greater than or equal to 0.29 grams per 10 minutes and less than or equal to 15 grams per ten minutes (g/10 min). Within this range the melt flow rate may be greater than or equal to 1.0 g/10 min. Also within this range the melt flow rate may be less than or equal to 10, or, more specifically, less than or equal to 6, or, more specifically, less than or equal to 5 g/10 min. Melt flow rate can be determined according to ASTM D1238 using either powdered or pelletized polyethylene, a load of 2.16 kilograms and a temperature of 190°C.

The thermoplastic composition may comprise the high density polyethylene in an amount of 12 to 40 weight percent (wt%), based on the combined weight of the poly(arylene ether), high density polyethylene, organic phosphate ester and block copolymer. Within this range the amount of high density polyethylene may be greater than or equal to 17 wt%, or, more specifically, greater than or equal to 20 wt%. Also within this range the amount of high density polyethylene may be less than or equal to 35 wt%, or, more specifically, less than or equal to 30 wt%.

In one embodiment the amount of high density polyethylene by weight is less than the amount of poly(arylene ether) by weight. Notably, the high density polyethylene remains the continuous phase even when the amount of high density polyethylene by weight is less than the amount of poly(arylene ether) by weight based on the total amounts of high density polyethylene and poly(arylene ether) in the thermoplastic composition.

As used herein and throughout the specification and claims, "block copolymer" refers to a single block copolymer or a combination of block copolymers. The block copolymer comprises (A) at least one block comprising repeating aryl alkylene units and (B) at least one block comprising repeating alkylene units. The arrangement of blocks (A) and (B) may be a linear structure or a so-called radial teleblock structure having branched chains. A-B-A triblock copolymers have two blocks A comprising repeating aryl alkylene units. A-B diblock copolymers have one block A comprising repeating aryl alkylene units. The pendant aryl moiety of the aryl alkylene units may be monocyclic or polycyclic and may have a substituent at any available position on the cyclic portion. Suitable substituents include alkyl groups having 1 to 4 carbons. An exemplary aryl alkylene unit is phenylethylene, which is shown in Formula II:



Block A may further comprise alkylene units having 2 to 15 carbons as long as the quantity of aryl alkylene units exceeds the quantity of alkylene units. Block B comprises repeating alkylene units having 2 to 15 carbons such as ethylene, propylene, butylene or combinations of two or more of the foregoing. Block B may further comprise aryl alkylene units as long as the quantity of alkylene units exceeds the quantity of aryl alkylene units. Each occurrence of block A may have a molecular weight which is the same or different than other occurrences of block A. Similarly each occurrence of block B may have a molecular weight which is the same or different than other occurrences of block B. The block copolymer may be functionalized by reaction with an alpha-beta unsaturated carboxylic acid.

In one embodiment, the B block comprises a copolymer of aryl alkylene units and alkylene units having 2 to 15 carbons such as ethylene, propylene, butylene or combinations of two or more of the foregoing. The B block may further comprise some unsaturated non-aromatic carbon-carbon bonds.

The B block may be a controlled distribution copolymer. As used herein "controlled distribution" is defined as referring to a molecular structure lacking well-defined blocks of either monomer, with "runs" of any given single monomer attaining a maximum number average of 20 units as shown by either the presence of only a single glass transition temperature (T_g), intermediate between the T_g of either homopolymer, or as shown via proton nuclear magnetic resonance methods. When the B block comprises a controlled distribution copolymer, each A block may have an average molecular weight of 3,000 to 60,000 g/mol and each B block may have an average molecular weight of 30,000 to 300,000 g/mol as determined light scattering techniques. When the B block is a controlled distribution copolymer, each B block comprises at least one terminal region adjacent to an A block that is rich in alkylene units or conjugated alkene units and a region not adjacent to the A block that is rich in aryl alkylene units. The total amount of aryl alkylene units is 15 to 75 weight percent, based on the total weight of the block copolymer. The weight ratio of alkylene units to aryl alkylene units in the B block may be 5:1 to 1:2. Exemplary block copolymers are further disclosed in U.S. Patent Application No. 2003/181584 and are

commercially available from Kraton Polymers under the trademark KRATON. Exemplary grades are A-RP6936 and A-RP6935.

The repeating aryl alkylene units result from the polymerization of aryl alkylene monomers such as styrene. The repeating alkylene units result from the hydrogenation of repeating unsaturated units derived from a diene such as butadiene. The butadiene may comprise 1,4-butadiene and/or 1,2-butadiene. The B block may further comprise some unsaturated non-aromatic carbon-carbon bonds.

Exemplary block copolymers include polyphenylethylene-poly(ethylene/propylene) which is sometimes referred to as polystyrene-poly(ethylene/propylene), polyphenylethylene-poly(ethylene/propylene)-polyphenylethylene (sometimes referred to as polystyrene-poly(ethylene/propylene)-polystyrene) and polyphenylethylene-poly(ethylene/butylene)-polyphenylethylene (sometimes referred to as polystyrene-poly(ethylene/butylene)-polystyrene).

In one embodiment, the block copolymer comprises two block copolymers. The first block copolymer has an aryl alkylene content greater than or equal to 50 weight percent based on the total weight of the first block copolymer. The second block copolymer has an aryl alkylene content less than or equal to 50 weight percent based on the total weight of the second block copolymer. An exemplary combination of block copolymers is a first polyphenylethylene-poly(ethylene/butylene)-polyphenylethylene having a phenylethylene content of 15 weight percent to 40 weight percent, based on the total weight of the block copolymer and a second polyphenylethylene-poly(ethylene-butylene)-polyphenylethylene having a phenylethylene content of 55 weight percent to 70 weight percent, based on the total weight of the block copolymer may be used. Exemplary block copolymers having an aryl alkylene content greater than 50 weight percent are commercially available from Asahi under the trademark TUFTEC and have grade names such as H1043, as well as some grades available under the tradename SEPTON from Kuraray. Exemplary block copolymers having an aryl alkylene content less than 50 weight percent are commercially available from Kraton Polymers under the trademark KRATON and

have grade names such as G-1701, G-1702, G-1730, G-1641, G-1650, G-1651, G-1652, G-1657, A-RP6936 and A-RP6935.

In one embodiment, the block copolymer comprises a triblock copolymer and a diblock copolymer. In one embodiment the ratio of the triblock copolymer to the diblock copolymer is 0.3 to 3.0.

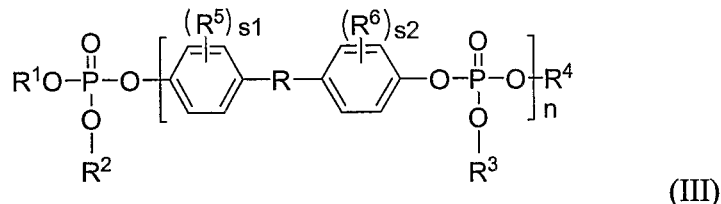
In some embodiments the block copolymer(s) have a number average molecular weight of 5,000 to 1,000,000 grams per mole (g/mol), as determined by gel permeation chromatography (GPC) using polystyrene standards. Within this range, the number average molecular weight may be at least 10,000 g/mol, or, more specifically, at least 30,000 g/mol, or, even more specifically, at least 45,000 g/mol. Also within this range, the number average molecular weight may preferably be up to 800,000 g/mol, or, more specifically, up to 700,000 g/mol, or, even more specifically, up to 650,000 g/mol.

The block copolymer is present in an amount of 2 to 20 weight percent, based on the combined weight of the poly(arylene ether), high density polyethylene ether, organic phosphate ester and block copolymer. Within this range the block copolymer may be present in an amount greater than or equal to 4, or, more specifically, greater than or equal to 6 weight percent based on the combined weight of the poly(arylene ether), high density polyethylene, organic phosphate ester and block copolymer. Also within this range the block copolymer may be present in an amount less than or equal to 18, or, more specifically, less than or equal to 16, or, even more specifically, less than or equal to 14 weight percent based on the combined weight of the poly(arylene ether), high density polyethylene, organic phosphate ester and block copolymer.

In one embodiment the weighted average aryl alkylene content of the block copolymer is 15 to 70. Within this range the weighted average aryl alkylene content can be greater than or equal to 17, or, more specifically, greater than or equal to 20. Also within this range the weighted average aryl alkylene content can be less than or equal to 67, or, more specifically, less than or equal to 65.

Exemplary organic phosphate ester flame retardants include, but are not limited to, phosphate esters comprising phenyl groups, substituted phenyl groups, or a combination of phenyl groups and substituted phenyl groups, bis-aryl phosphate esters based upon resorcinol such as, for example, resorcinol bis-diphenylphosphate, as well as those based upon bis-phenols such as, for example, bis-phenol A bis-diphenylphosphate. In one embodiment, the organic phosphate is selected from tris(alkylphenyl) phosphate (for example, CAS No. 89492-23-9 and/or 78-33-1), resorcinol bis-diphenylphosphate (for example, CAS No. 57583-54-7), bis-phenol A bis-diphenylphosphate (for example, CAS No. 181028-79-5), triphenyl phosphate (for example, CAS No. 115-86-6), tris(isopropylphenyl) phosphate (for example, CAS No. 68937-41-7) and mixtures of two or more of the foregoing organic phosphate esters.

In one embodiment the organic phosphate ester comprises a bis-aryl phosphate of Formula III:



wherein R, R⁵ and R⁶ are independently, at each occurrence, an alkyl group having 1 to 5 carbons and R¹-R⁴ are independently an alkyl, aryl, arylalkyl or alkylaryl group having 1 to 10 carbons; n is an integer equal to 1 to 25; and s₁ and s₂ are independently an integer equal to 0 to 2. In some embodiments OR¹, OR², OR³ and OR⁴ are independently derived from phenol, a monoalkylphenol, a dialkylphenol or a trialkylphenol.

As readily appreciated by one of ordinary skill in the art, a bis-aryl phosphate is derived from a bisphenol. Exemplary bisphenols include 2,2-bis(4-hydroxyphenyl)propane (so-called bisphenol A), 2,2-bis(4-hydroxy-3-methylphenyl)propane, bis(4-hydroxyphenyl)methane, bis(4-hydroxy-3,5-

dimethylphenyl)methane and 1,1-bis(4-hydroxyphenyl)ethane. In one embodiment, the bisphenol comprises bisphenol A.

Organic phosphate esters can have differing molecular weights making the determination of the amount of different organic phosphate esters difficult. In one embodiment the amount of phosphorus, as the result of the organic phosphate ester, is 0.6 wt% to 1.5 wt% based on the combined weight of poly(arylene ether), high density polyethylene, block copolymer and organic phosphate ester.

In one embodiment, the organic phosphate ester is present in an amount of 5 to 18 weight percent, based on the combined weight of poly(arylene ether), high density polyethylene, block copolymer and organophosphate ester. Within this range the amount of organophosphate ester can be greater than or equal to 7, or more specifically, greater than or equal to 9. Also within this range the amount of organophosphate ester can be less than or equal to 16, or, more specifically, less than or equal to 14.

Additionally, the thermoplastic composition may optionally also contain various additives, such as antioxidants; fillers and reinforcing agents having an average particle size less than or equal to 10 micrometers, such as, for example, silicates, TiO₂, fibers, glass fibers, glass spheres, calcium carbonate, talc, and mica; mold release agents; UV absorbers; stabilizers such as light stabilizers and others; lubricants; plasticizers; pigments; dyes; colorants; anti-static agents; blowing agents, foaming agents, metal deactivators, and combinations comprising one or more of the foregoing additives.

In one embodiment the electrical wire comprises a conductor and a covering disposed over the conductor. The covering comprises a thermoplastic composition. The thermoplastic composition consists essentially of poly(arylene ether) having an initial intrinsic viscosity greater than 0.35 dl/g, as measured in chloroform at 25°C; a high density polyethylene having a melting temperature greater than or equal to 125°C and a melt flow rate of 0.7 to 15; an organic phosphate ester and a combination of two block copolymers having different aryl alkylene contents. The first block copolymer has an aryl alkylene content greater than or equal to 50 weight percent based on the

total weight of the first block copolymer. The second block copolymer has an aryl alkylene content less than or equal to 50 weight percent based on the total weight of the second block copolymer. The poly(arylene ether) is present in an amount by weight greater than the amount of high density polyethylene by weight, and the weighted average aryl alkylene content of the block copolymers is greater than or equal to 20 weight percent. The thermoplastic composition has a flexural modulus less than or equal to 1500 Mpa as determined by ASTM D790-03 using a speed of 1.27 millimeters per minute and samples molded as described in the Examples. The electrical wire has an average flame out time less than or equal to 10 seconds based on ten samples, when tested according to the flame propagation procedure contained in ISO 6722 for electrical wires with conductor sizes less than or equal to 2.5 square millimeters using test wires having a conductor size of 0.2 square millimeters and a covering thickness of 0.2 millimeters. Additionally, none of the 10 samples used to determine the average flame out time has an individual flame out time greater than 70 seconds. As used herein "consists essentially of" permits the inclusion of additives as described herein but excludes additional polymeric resins such as polystyrene, polyamide, polyetherimide, polycarbonate, polysiloxane and the like.

The components of the thermoplastic composition are melt mixed, typically in a melt mixing device such as a compounding extruder or Banbury mixer. In one embodiment, the poly(arylene ether), polymeric compatibilizer, and polyolefin are simultaneously melt mixed. In another embodiment, the poly(arylene ether), polymeric compatibilizer, and optionally a portion of the polyolefin are melt mixed to form a first melt mixture. Subsequently, the polyolefin or remainder of the polyolefin is further melt mixed with the first melt mixture to form a second melt mixture. Alternatively, the poly(arylene ether) and a portion of the polymeric compatibilizer may be melt mixed to form a first melt mixture and then the polyolefin and the remainder of the polymeric compatibilizer are further melt mixed with the first melt mixture to form a second melt mixture.

The aforementioned melt mixing processes can be achieved without isolating the first melt mixture or can be achieved by isolating the first melt mixture. One or more melt mixing devices including one or more types of melt mixing devices can be used in

these processes. In one embodiment, some components of the thermoplastic composition that forms the covering may be introduced and melt mixed in an extruder used to coat the conductor.

When the block copolymer comprises two block copolymers, one having an aryl alkylene content greater than or equal to 50 weight percent and a second one having an aryl alkylene content less than 50 weight percent, the poly(arylene ether) and the block copolymer having an aryl alkylene content greater than or equal to 50 weight percent can be melt mixed to form a first melt mixture and the polyolefin and a block copolymer having an aryl alkylene content less than or equal to 50 weight percent can be melt mixed with the first melt mixture to form a second melt mixture.

The method and location of the addition of the optional flame retardant is typically dictated by the identity and physical properties, e.g., solid or liquid, of the flame retardant as well understood in the general art of polymer alloys and their manufacture. In one embodiment, the flame retardant is combined with one of the components of the thermoplastic composition, e.g., a portion of the polyolefin, to form a concentrate that is subsequently melt mixed with the remaining components.

The poly(arylene ether), block copolymer, high density polyethylene and flame retardant are melt mixed at a temperature greater than or equal to the glass transition temperature of the poly(arylene ether) but less than the degradation temperature of the high density polyethylene. For example, the poly(arylene ether), polymeric compatibilizer, high density polyethylene and flame retardant may be melt mixed at an extruder temperature of 240°C to 320°C, although brief periods in excess of this range may occur during melt mixing. Within this range, the temperature may be greater than or equal to 250°C, or, more specifically, greater than or equal to 260°C. Also within this range the temperature may be less than or equal to 310°C, or, more specifically, less than or equal to 300°C.

After some or all the components are melt mixed, the molten mixture can be melt filtered through one of more filters having openings with diameters of 20 micrometers to 150 micrometers. Within this range, the openings may have diameters less than or

equal to 130 micrometers, or, more specifically, less than or equal to 110 micrometers. Also within this range the openings can have diameters greater than or equal to 30 micrometers, or, more specifically, greater than or equal to 40 micrometers. In one embodiment the molten mixture is melt filtered through one or more filters having openings with a maximum diameter that is less than or equal to half of the thickness of the covering on the conductor.

The thermoplastic composition can be formed into pellets, either by strand pelletization or underwater pelletization, cooled, and packaged. In one embodiment the pellets are packaged into metal foil lined plastic, e.g., polypropylene, bags or metal foil lined paper bags. Substantially all of the air can be evacuated from the pellet filled bags.

In one embodiment, the thermoplastic composition is substantially free of visible particulate impurities. As used herein, the term "substantially free of visible particulate impurities" when applied to the thermoplastic composition means that when the composition is injection molded to form 5 plaques having dimensions of 75 mm X 50 mm and having a thickness of 3 mm and the plaques are visually inspected for black specks with the naked eye the total number of black specks for all five plaques is less than or equal to 100, or, more specifically, less than or equal to 70, or, even more specifically, less than or equal to 50.

In one embodiment the pellets are melted and the composition applied to the conductor by a suitable method such as extrusion coating to form an electrical wire. For example, a coating extruder equipped with a screw, crosshead, breaker plate, distributor, nipple, and die can be used. The melted thermoplastic composition forms a covering disposed over a circumference of the conductor. Extrusion coating may employ a single taper die, a double taper die, other appropriate die or combination of dies to position the conductor centrally and avoid die lip build up.

In some embodiments it may be useful to dry the thermoplastic composition before extrusion coating. Exemplary drying conditions are 60-90°C for 2-20 hours. Additionally, in one embodiment, during extrusion coating, the thermoplastic composition is melt filtered, prior to formation of the covering, through one or more

filters having opening diameters of 20 micrometers to 150 micrometers. Within this range, the openings diameters may be greater than or equal to 30 micrometers, or more specifically greater than or equal to 40 micrometers. Also within this range the openings diameters may be less than or equal to 130 micrometers, or, more specifically, less than or equal to 110 micrometers. Alternatively, the one or more filters have openings with a maximum diameter that is less than or equal to half the thickness of the covering on the conductor.

The extruder temperature during extrusion coating is generally less than or equal to 320°C, or, more specifically, less than or equal to 310°C, or, more specifically, less than or equal to 290°C. Additionally the processing temperature is adjusted to provide a sufficiently fluid molten composition to afford a covering for the conductor, for example, higher than the melting point of the thermoplastic composition, or more specifically at least 10°C higher than the melting point of the thermoplastic composition.

After extrusion coating the electrical wire is usually cooled using a water bath, water spray, air jets or a combination comprising one or more of the foregoing cooling methods. Exemplary water bath temperatures are 20 to 85°C. After cooling the electrical wire is wound onto a spool or like device, typically at a speed of 50 meters per minute (m/min) to 1500 m/min.

In one embodiment, the composition is applied to the conductor to form a covering disposed over the conductor. Additional layers may be applied to the covering.

In one embodiment the composition is applied to a conductor having one or more intervening layers between the conductor and the covering to form a covering disposed over the conductor. For instance, an optional adhesion promoting layer may be disposed between the conductor and covering. In another example the conductor may be coated with a metal deactivator prior to applying the covering. In another example the intervening layer comprises a thermoplastic or thermoset composition that, in some cases, is foamed.

The conductor may comprise a single strand or a plurality of strands. In some cases, a plurality of strands may be bundled, twisted, braided, or a combination of the foregoing to form a conductor. Additionally, the conductor may have various shapes such as round or oblong. Suitable conductors include, but are not limited to, copper wire, aluminum wire, lead wire, and wires of alloys comprising one or more of the foregoing metals. The conductor may also be coated with, e.g., tin or silver.

The cross-sectional area of the conductor and thickness of the covering may vary and is typically determined by the end use of the electrical wire. The electrical wire can be used as electric wire without limitation, including, for example, for harness wire for automobiles, wire for household electrical appliances, wire for electric power, wire for instruments, wire for information communication, wire for electric cars, as well as ships, airplanes, and the like.

A cross-section of an exemplary electrical wire is seen in Figure 1. Figure 1 shows a covering, 4, disposed over a conductor, 2. In one embodiment, the covering, 4, comprises a foamed thermoplastic composition. Perspective views of exemplary electrical wires are shown in Figures 2 and 3. Figure 2 shows a covering, 4, disposed over a conductor, 2, comprising a plurality of strands and an optional additional layer, 6, disposed over the covering, 4, and the conductor, 2. In one embodiment, the covering, 4, comprises a foamed thermoplastic composition. Conductor, 2, can also comprise a unitary conductor. Figure 3 shows a covering, 4, disposed over a unitary conductor, 2, and an intervening layer, 6. In one embodiment, the intervening layer, 6, comprises a foamed composition. Conductor, 2, can also comprise a plurality of strands.

A color concentrate or masterbatch may be added to the thermoplastic composition prior to extrusion coating. When a color concentrate is used it is typically present in an amount less than or equal to 3 weight percent, based on the total weight of the thermoplastic composition. In one embodiment dye and/or pigment employed in the color concentrate is free of chlorine, bromine and fluorine. As appreciated by one of skill in the art, the color of the thermoplastic composition prior to the addition of color concentrate may impact the final color achieved and in some cases it may be

advantageous to employ a bleaching agent and/or color stabilization agents. Bleaching agents and color stabilization agents are known in the art and are commercially available.

The thermoplastic composition and electrical wire are further illustrated by the following non-limiting examples.

EXAMPLES

The following examples were prepared using the materials listed in Table 1.

Table 1.

Component	Description
PPE	A poly(2,6-dimethylphenylene ether) with an intrinsic viscosity of 0.46 dl/g as measured in chloroform at 25°C commercially available from General Electric under the grade name PPO646.
KG1650	A polyphenylethylene-poly(ethylene/butylene)-polyphenylethylene block copolymer having a phenylethylene content of 30 weight percent, based on the total weight of the block copolymer and commercially available from KRATON Polymers under the grade name G 1650.
PP	A polypropylene having a melt flow rate of 1.5 g/10 min determined according to ASTM D1238 as described above and commercially available under the tradename D-105-C Sunoco Chemicals.
HDPE	A high density polyethylene having a melt flow rate of 0.8 g/10min determined according to ASTM D1238 as described above and commercially available from Mitsui Chemicals under the tradename HI-ZEX 5305E.
Tuftec H1043	A polyphenylethylene-poly(ethylene/butylene)-polyphenylethylene block copolymer having a phenylethylene content of 67 weight percent, based on the total weight of the block copolymer and commercially available from Asahi Chemical.
KG1657	A mixture of polyphenylethylene-poly(ethylene/propylene) and polyphenylethylene-poly(ethylene/butylene)-polyphenylethylene block copolymers having a phenylethylene content of 13 weight percent, based on the total weight of the block copolymers and commercially available from KRATON Polymers under the grade name G 1657.
Tuftec H1052	A polyphenylethylene-poly(ethylene/butylene)-polyphenylethylene block copolymer having a phenylethylene content of 20 weight percent, based on the total weight of the block copolymer and commercially available from Asahi Chemical.
BPADP	bis-phenol A bis-diphenylphosphate (CAS 181028-79-5)

Examples 1-7.

Examples 1-7 were made by combining the components in a twin screw extruder. The PPE and block copolymers were added at the feedthroat and the PP was added

downstream. The BPADP was added by a liquid injector in the second half of the extruder. The material was filtered in melt and pelletized at the end of the extruder and the pelletized material was injected molded into test specimens for flexural modulus, heat deflection temperature, and melt flow index testing.

Flexural modulus (FM) was determined using ASTM D790-03 at a speed of 1.27 millimeters per minute and is expressed in kilograms per square centimeter (kg/cm^2). The values given are the average of three samples. The samples for flexural modulus were formed using an injection pressure of 600-700 kilograms-force per square centimeter and a hold time of 15 to 20 seconds on a Plastar Ti-80G2 from Toyo Machinery & Metal co. LTD. The remaining molding conditions are shown in Table 2.

Heat distortion temperature (HDT) was determined using ASTM D648-04 at 4.6 kilograms per 6.4 millimeters. Values are expressed in degrees centigrade ($^{\circ}\text{C}$) and are the average of three samples. Samples were molded using the same conditions as the samples for flexural modulus.

Melt flow rate (MFR) was determined using ASTM D1238 at 280°C and 5 kilograms. Values are expressed in grams per ten minutes ($\text{g}/10 \text{ min}$) and are the average of two values. Samples were molded using the same conditions as the samples for flexural modulus.

The thermoplastic compositions of the Examples and data are listed in Table 3.

Electrical wires were produced using the thermoplastic composition of Examples 1-7. The conductor had a cross sectional area of 0.2 square millimeters (mm^2). The thermoplastic composition was dried at 80°C for 3-4 hours prior to extrusion with the conductor to form the electrical wire. During extrusion the melt was filtered prior to being applied to the conductor. The coverings had thicknesses of 0.2 millimeters. The electrical wire was cut into 80 centimeter lengths and subjected to a flame as described in ISO 6722. The average amount of time (in seconds) required for the sample to extinguish (the average flame out time) is expressed in Table 3, based on 10 test wires.

Table 2

Drying temperature (°C)	80
Dry time in hours	4
Cylinder temperature	
1	240
2	250
3	260
4	260
DH	260
Mold temperature	80

Table 3.

	1*	2	3	4	5*	6*	7*
PPE	52	52	52	52	52	52	52
HDPE	27	27	27	27	-	-	-
PP	-	-	-	-	27	27	27
KG1650	-	-	5	10	-	5	10
H1043	-	-	-	-	-	-	-
H1052	-	10	-	-	10	-	-
KG1657	10	-	5	-	-	5	-
BPADP	11	11	11	11	11	11	11
FM	9835	10424	13764	14214	10755	14855	15803
HDT	111	111	125	129	117	119	133
MFR	48	44	21	14	44	23	16
Weighted average aryl alkylene content	13	20	22	30	20	22	30
Avg flame out time	16	8	4	3	131	65	74

*Comparative Example

Examples 5-7 are comparative examples which contain polypropylene instead of high density polyethylene and have comparable weight average aryl alkylene content to Examples 2-4. Surprisingly Examples 2-4 have average flame out times that are 4-6% of the average flame out times for Examples 5-7. In addition, Examples 2-4 have flexural modulus values that are lower than the flexural modulus values for Examples 5-7. Example 1 shows that compositions having a weighted aryl alkylene content less than 20% can have an average flame out time greater than 10 seconds. Figure 4 is a graph showing the relationship between the flexural modulus of Examples 2-4 and the flexural modulus of Examples 5-7. Figure 5 is a graph showing the relationship

between the flame out times of Examples 2-4 and the flame out times of Examples 5-7.

While the invention has been described with reference to a several embodiments, it will be understood by those skilled in the art that various changes may be made and equivalents may be substituted for elements thereof without departing from the scope of the invention. In addition, many modifications may be made to adapt a particular situation or material to the teachings of the invention without departing from essential scope thereof. Therefore, it is intended that the invention not be limited to the particular embodiments disclosed as the best mode contemplated for carrying out this invention, but that the invention will include all embodiments falling within the scope of the appended claims.

All cited patents, patent applications, and other references are incorporated herein by reference in their entirety.

WHAT IS CLAIMED IS:

1. An electrical wire comprising:

a conductor, and

a covering disposed over the conductor wherein the covering comprises a thermoplastic composition and the thermoplastic composition comprises:

(i) a poly(arylene ether);

(ii) a high density polyethylene;

(iii) a block copolymer; and

(iv) an organic phosphate ester flame retardant,

wherein the electrical wire has an average flame out time less than or equal to 10 seconds based on ten electrical wire samples having a conductor size of 0.2 square millimeters and a covering thickness of 0.2 millimeters tested according to ISO 6722 for conductor sizes less than or equal to 2.5 millimeters.

2. The electrical wire of Claim 1, wherein the block copolymer has a weighted average aryl alkylene content greater than or equal to 15 weight percent.

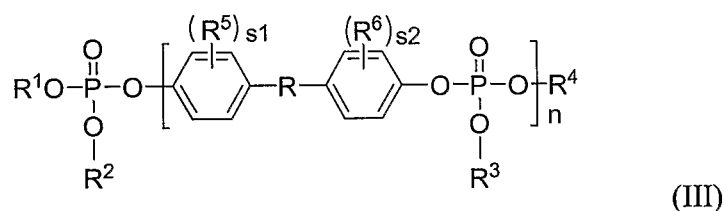
3. The electrical wire of Claim 1, wherein the thermoplastic composition is essentially free of an alkenyl aromatic resin.

4. The electrical wire of Claim 1, wherein the thermoplastic composition has a flexural modulus of 6000 to less than 18000 kilograms per square centimeter as determined by ASTM D790-03 using a speed of 1.27 millimeters per minute.

5. The electrical wire of Claim 1, wherein the poly(arylene ether) has an initial intrinsic viscosity greater than 0.35 deciliters per gram, as measured in chloroform at 25°C.

6. The electrical wire of Claim 1, wherein the poly(arylene ether) is present in an amount of 30 to 65 weight percent, the high density polyethylene is present in an amount of 12 to 40 weight percent, and the block copolymer or combination of block copolymers is present in an amount of 2 to 20 weight percent based on the combined weight of poly(arylene ether), high density polyethylene, block copolymer and organic phosphate ester flame retardant.

7. The electrical wire of Claim 1, wherein the organic phosphate ester flame retardant comprises a bis-aryl phosphate of formula III



wherein R, R⁵ and R⁶ are independently an alkyl group having 1 to 5 carbons and R¹-R⁴ are independently an alkyl, aryl, arylalkyl or alkylaryl group having 1 to 10 carbons; n is an integer equal to 1 to 25; and s1 and s2 are independently an integer equal to 0 to 2.

8. The electrical wire of Claim 1, wherein the thermoplastic composition comprises a continuous high density polyethylene phase and a dispersed poly(arylene ether) phase.

9. The electrical wire of Claim 1, wherein the thermoplastic composition further comprises one or more additives selected from the group consisting of antioxidants, fillers having an average particle size less than or equal to 10 micrometers, reinforcing agents having an average particle size less than or equal to 10 micrometers, silicates, TiO₂, fibers, glass fibers, glass spheres, calcium carbonate, talc, mica, mold release agents, UV absorbers, stabilizers, light stabilizers, lubricants, plasticizers, pigments, dyes, colorants, anti-static agents, blowing agents, foaming agents, metal deactivators, and combinations comprising one or more of the foregoing additives.

10. The electrical wire of Claim 1, wherein the thermoplastic composition comprises a high density polyethylene having a melt flow rate of 0.29 grams per 10 minutes to 15 grams per 10 minutes when determined according to ASTM D1238 using powdered or pelletized high density polyethylene, a load of 2.16 kilograms and a temperature of 190°C.

11. The electrical wire of Claim 1, wherein the thermoplastic composition comprises phosphorus in amount of 0.6 to 1.5 weight percent based on the combined weight of poly(arylene ether), high density polyethylene, block copolymer and organic phosphate ester flame retardant.

12. The electrical wire of Claim 1, wherein the amount of high density polyethylene by weight is less than the amount of poly(arylene ether) by weight based on the total amounts of high density polyethylene and poly(arylene ether) in the thermoplastic composition.

13. The electrical wire of Claim 1, wherein the high density polyethylene has a melting temperature greater than or equal to 124°C.

14. The electrical wire of Claim 1, wherein the block copolymer comprises a block that is a controlled distribution copolymer.

15. The covered of Claim 1, wherein the block copolymer comprises:

a first block copolymer having an aryl alkylene content greater than or equal to 50 weight percent, based on the total weight of the first block copolymer; and

a second block copolymer having an aryl alkylene content less than 50 weight percent based on the total weight of the second block copolymer.

16. The electrical wire of Claim 1, wherein the block copolymer comprises a diblock copolymer and a triblock copolymer.

17. An electrical wire comprising:

a conductor, and

a covering disposed over the conductor wherein the covering comprises a thermoplastic composition and the thermoplastic composition comprises:

- (i) a poly(arylene ether);
- (ii) a high density polyethylene;
- (iii) a block copolymer; and
- (iv) an organic phosphate ester flame retardant, wherein the block copolymer has a weighted average aryl alkylene content greater than or equal to 15 weight percent.

18. An electrical wire comprising:

a conductor, and

a covering disposed over the conductor wherein the covering comprises a thermoplastic composition and the thermoplastic composition consists essentially of:

- (i) a poly(arylene ether);
- (ii) a high density polyethylene;
- (iii) a first block copolymer;
- (iv) a second block copolymer;
- (v) an organic phosphate ester flame retardant,

wherein the poly(arylene ether) has an initial intrinsic viscosity greater than 0.35 dl/g, as measured in chloroform at 25°C,

wherein the high density polyethylene having a melting temperature greater than or equal to 125°C and a melt flow rate of 0.7 to 15,

wherein the first block copolymer has an aryl alkylene content greater than or equal to 50 weight percent based on the total weight of the first block copolymer,

wherein the second block copolymer has an aryl alkylene content less than or equal to 50 weight percent based on the total weight of the second block copolymer.

19. The electrical wire of Claim 18 wherein the thermoplastic composition has a flexural modulus less than or equal to 1500 Mpa as determined according to ASTM D790-03 using a speed of 1.27 millimeters per minute.

20. The electrical wire of Claim 18, wherein the electrical wire has an average flame out time less than or equal to 10 seconds based on ten test wires tested according to ISO 6722 for cables with conductor sizes less than or equal to 2.5 square millimeters using test wires having a conductor size of 0.2 square millimeters and a covering with a thickness of 0.2 millimeters and further wherein all ten test wires have a flame out time less than 70 seconds.

21. A thermoplastic composition useful in a covering disposed over a conductor in an electrical wire comprises:

- (i) a poly(arylene ether);
- (ii) a high density polyethylene;
- (iii) a block copolymer; and
- (iv) an organic phosphate ester flame retardant,

wherein the electrical wire has an average flame out time less than or equal to 10 seconds based on ten test wires having a conductor size of 0.2 square millimeters and a covering thickness of 0.2 millimeters tested according to ISO 6722 for conductor sizes less than or equal to 2.5 millimeters and all ten test wires have a flame out time less than 70 seconds.