

Process for manufacturing a purified aqueous hydrogen peroxide solution

This application claims priority to European application No. 13187128.7 filed on October 2, 2013 and to European application N° 14175503.3 filed on July 13, 2014, the whole content of these applications being incorporated herein by reference for all purposes.

5 The present invention relates to a process for manufacturing a purified aqueous hydrogen peroxide solution.

Hydrogen peroxide is one of the most important inorganic chemicals to be produced worldwide. Its industrial applications include textile, pulp and paper bleaching, organic synthesis (propylene oxide), the manufacture of inorganic
10 chemicals and detergents, environmental and other applications.

Synthesis of hydrogen peroxide is predominantly achieved by using the Riedl-Pfleiderer process, also called anthraquinone loop process or AO (auto-oxidation) process.

This well known cyclic process makes use typically of the auto-oxidation
15 of at least one alkylanthrahydroquinone and/or of at least one tetrahydroalkylanthrahydroquinone, most often 2-alkylanthraquinone, to the corresponding alkylanthraquinone and/or tetrahydroalkylanthraquinone, which results in the production of hydrogen peroxide.

The first step of the AO process is the reduction in an organic solvent of
20 the chosen quinone (alkylanthraquinone or tetrahydroalkylanthraquinone) into the corresponding hydroquinone (alkylanthrahydroquinone or tetrahydroalkylanthraquinone) using hydrogen gas and a catalyst. The mixture of organic solvents, hydroquinone and quinone species (working solution, WS) is then separated from the catalyst and the hydroquinone is oxidized using
25 oxygen, air or oxygen-enriched air thus regenerating the quinone with simultaneous formation of hydrogen peroxide. The organic solvent of choice is typically a mixture of two types of solvents, one being a good solvent of the quinone derivative (for instance a mixture of aromatic compounds) and the other being a good solvent of the hydroquinone derivative (for instance a long chain
30 alcohol). Hydrogen peroxide is then typically extracted with water and recovered in the form of a crude aqueous hydrogen peroxide solution, and the quinone is returned to the hydrogenator to complete the loop.

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It is known to use hydrogen peroxide in the presence of a heterogeneous catalyst to convert an olefin into an oxirane, more particularly to convert propylene into propylene oxide (1,2-epoxypropane) by reaction with hydrogen peroxide. Such a process is generally performed in huge plants which consume huge amounts of hydrogen peroxide. Like many other (catalytic) organic oxidation processes, it requires pure reagents with no risk of process precipitation, i.e. a metal content of the order of 10 ppb. In the case of propylene oxide manufacture, it has namely been observed that if metals are present, like Fe (coming from the material of construction of the apparatus used) or Al (coming from the catalyst) and even in low amounts of between 50 and 200 ppb, these react with the reactives fed to the reactor and lead to the precipitation of insolubles which in turn leads to filter clogging.

Patent applications EP 529723 and EP 965562 in the name of the Applicant describe a process for manufacturing a purified aqueous hydrogen peroxide solution, in which a crude aqueous hydrogen peroxide solution is subjected to a washing operation with at least one organic solvent. In such a process, washing is intended to remove from the peroxide, working solution residuals, i.e. quinones and their degradation products. The solvents are generally those of the AO process in question used normally for dissolving the quinones in order to make working solution (the solvents being generally circulated from crude washing to main loop). The purpose of this traditional crude washing is to reduce TOC (organic matter) in the peroxide, and it has no effect on inorganic impurities (Al, Fe etc.).

On the other hand, various techniques (membrane filtration, distillation etc) are available when ultrapure peroxides are needed, but they are either too costly or not suitable for high volume (>100000 t per year) applications.

The purpose of the present invention is hence to provide an improved process for the preparation of hydrogen peroxide, in particular a new method for producing hydrogen peroxide with a low concentration of easily precipitating metals (Al, Fe, Cr...) which is not expensive and is suitable for high volumes.

The present invention therefore concerns a process for manufacturing a purified aqueous hydrogen peroxide solution, in which a crude aqueous hydrogen peroxide solution is subjected to a washing operation with at least one organic solvent, and wherein an organophosphorus chelating agent is added to the organic solvent.

The term "washing" is intended to denote any treatment, which is well known in the chemical industry, of a crude aqueous hydrogen peroxide solution with an organic solvent which is intended to reduce the content of impurities in the aqueous hydrogen peroxide solution. This washing can consist, for example, in extracting impurities in the crude aqueous hydrogen peroxide solution by means of an organic solvent in apparatuses such as centrifugal extractors or liquid/liquid extraction columns, for example, operating counter-currentwise. Liquid/liquid extraction columns are preferred. Among the liquid/liquid extraction columns, columns with perforated plates are preferred.

In a preferred embodiment, the crude aqueous hydrogen peroxide solution is washed several times i.e. at least two times consecutively or even more times as required to reduce the content of impurities at a desired level.

The expression "crude aqueous hydrogen peroxide solution" is intended to denote the solutions obtained directly from a hydrogen peroxide synthesis step or from a hydrogen peroxide extraction step or from a storage unit. The crude aqueous hydrogen peroxide solution can have undergone one or more treatments to separate out impurities prior to the washing operation according to the process of the invention. It typically has an H_2O_2 concentration within the range 30-45% by weight.

It is preferred to bring the organic solvent in counter-current relative to the crude aqueous hydrogen peroxide solution. The efficacy of the washing depends on the flow rate of the organic solvent. The efficacy of the washing is improved when the flow rate of the organic solvent is increased. The volume of organic solvent used for the washing is defined as the quotient of the flow rate of solvent and of the flow rate of the hydrogen peroxide solution. The volume used in the process according to the invention is generally at least 3 l per m^3 of crude aqueous hydrogen peroxide solution. Preferably, the volume is at least 25 l per m^3 of aqueous hydrogen peroxide solution. The volume is generally not more than 100 l per m^3 of aqueous hydrogen peroxide solution. The volume is preferably not more than 75 l per m^3 of aqueous hydrogen peroxide solution. The washing temperature is generally at least 10°C. It is preferred to work at a temperature of at least 40°C. Generally, the temperature is not more than 65°C, preferably not more than 60°C. The washing time depends on the size of the apparatus chosen and on the flow rate of crude aqueous hydrogen peroxide solution introduced into the apparatus.

The metals which are removed by the process are those which easily precipitate in contact with phosphates like Al, Fe and Cr. Good results are obtained for Al and/or Fe removal. Hence, "purified" means with reduced metal content, more particularly reduced Al and/or Fe content, preferably of less than 100 ppb of Al and/or Fe (typically in the range of the 10th of ppb, preferably in the range of the ppb, even more preferably below the ppb). In preferred embodiments, the Cr content can also be reduced to the same level (i.e. less than 100 ppb, typically in the range of the 10th of ppb, in the range of the ppb or even below).

The organophosphorous chelating agent according to the invention is an organic molecule able of forming complexes with metals and in particular, with the above mentioned metals (Al and/or Fe and optionally Cr). It preferably comprises an acid group, preferably a phosphonic acid group. It is also preferably void of S (sulfur) in order namely not to influence negatively the hydrogen peroxide stability. Chelating agents which give good results are DEHPA (di-(2-ethylhexyl) phosphoric acid) and Cyanex® 272 (bis(2,4,4-trimethylpentyl)phosphinic acid). The former is preferred.

Preferably, the process of the invention comprises the following steps:

- a) hydrogenation, in the presence of a catalyst, of a working solution comprising at least one organic solvent and at least one alkylanthraquinone to obtain the corresponding alkylanthrahydroquinone,
 - b) separation of the hydrogenated working solution comprising the alkylanthrahydroquinone from the catalyst,
 - c) oxidation of the recovered hydrogenated working solution from step b) to form hydrogen peroxide,
 - d) separation, from the working solution, of said hydrogen peroxide during and/or subsequently to said oxidation step, preferably with an aqueous medium, and
 - e) recycling of the recovered working solution to step a)
- and the crude aqueous hydrogen peroxide solution separated in step d) is subjected to the washing operation.

The term "alkylanthraquinones" is intended to denote 9,10-anthraquinones substituted in position 1, 2 or 3 with at least one alkyl side chain of linear or branched aliphatic type comprising at least one carbon atom. Usually, these alkyl chains comprise less than 9 carbon atoms and, preferably, less than 6 carbon atoms. Examples of such alkylanthraquinones are 2-ethylanthraquinone, 2-

isopropylanthraquinone, 2-sec- and 2-tert-butylanthraquinone, 1,3-, 2,3-, 1,4- and 2,7-dimethylanthraquinone, 2-iso- and 2-tert-amylanthraquinone and mixtures of these quinones.

5 The term "alkylanthrahydroquinones" is intended to denote the 9,10-hydroquinones corresponding to the 9,10-alkylanthraquinones specified above.

In this embodiment of the invention, the alkylanthraquinones can be dissolved in various types of solvents, especially in the solvents typically used in the working solution of the well known AO process. For instance, the alkylanthraquinones can be dissolved in a single solvent or in a mixed solvent
10 comprising at least one aromatic solvent and at least one aliphatic or alicyclic alcohol, particularly in a mixed solvent. Aromatic solvents are for instance selected from benzene, toluene, xylene, tert-butylbenzene, trimethylbenzene, tetramethylbenzene, naphthalene, methylnaphthalene mixtures of polyalkylated benzenes, and mixtures thereof. Aliphatic or alicyclic alcohols are for example
15 selected from amyl alcohol, nonyl alcohol, isoheptyl alcohol, diisobutylcarbinol, methylcyclohexanol, and mixtures thereof. Useful single solvents are, among others, a ketone, an ester, an ether, or mixtures thereof. Often used solvents are S-150 and/or diisobutylcarbinol (DiBC), preferably a mixture of both. S-150 means a commercially available aromatic hydrocarbon solvent of type 150 from
20 the Solvesso[®] series. S-150 (Solvesso[®]-150; CAS no. 64742-94-5) is known as an aromatic solvent of high aromatics which offer high solvency and controlled evaporation characteristics that make them excellent for use in many industrial applications and in particular as process fluids. The Solvesso[®] aromatic hydrocarbons are available in three boiling ranges with varying volatility, e.g. with a
25 distillation range of 165-181 °C, of 182-207 °C or 232-295 °C. They may be obtained also naphthalene reduced or as ultra-low naphthalene grades. Solvesso[®] 150 (S-150) is characterized as follows: distillation range of 182-207 °C; flash point of 64 °C; aromatic content of greater than 99 % by wt; aniline point of 15 °C; density of 0.900 at 15 °C; and an evaporation rate (nButAc=100) of 5.3.

30 In a first sub-embodiment of the invention, the organic solvent used for the washing operation is a part of the working solution used in the alkylanthraquinone process.

This sub-embodiment makes it possible to modify the feed flow rate of organic solvent in the operation for washing the crude aqueous hydrogen
35 peroxide solution obtained according to the alkylanthraquinone process. It is in fact desirable to provide a flow rate of organic solvent which is sufficient to feed

the operation for washing an aqueous hydrogen peroxide solution. It is particularly desirable to be able to adjust the flow rate of organic solvent as a function of the desired washing efficacy and as a function of the amount of crude aqueous hydrogen peroxide solution to be subjected to the washing operation.

- 5 In the alkylanthraquinone process, the working solution is available in an amount which is large enough to make it possible to take an amount of organic solvent which is required to reach the desired feed flow rate of organic solvent.

10 The process according to this sub-embodiment of the invention has economic and technical advantages since it avoids the use of large amounts of fresh organic solvent to feed the washing step. Fresh organic solvents are more expensive than purified solvents. Large amounts are difficult to generate since it is necessary to ensure a continuous feed of fresh organic solvent and its destruction after the washing operation.

- 15 In this sub-embodiment of the invention, the organic solvent, after washing, can be subjected to a regeneration treatment. It can then be recycled into the washing step. If necessary, it can be recycled into the working solution used in the alkylanthraquinone process.

- 20 In a second sub-embodiment of the invention, the organic solvent used for the washing operation is a dedicated solvent, not part of the working solution. This sub-embodiment has the advantage that the nature of the solvent can be chosen so that it shows a synergistic effect (metal extraction) with the organophosphorus chelating agent (in other words: it improves the metal extraction by the organophosphorus chelating agent). In that regard, solvents comprising other organophosphorus compounds (i.e. at least an
- 25 organophosphorus compound different from the organophosphorus chelating agent) like alkyl-phosphates or alkyl-phosphonates are preferably used as solvents. Especially when the organophosphorus chelating agent is di-(2-ethylhexyl) phosphoric acid (DEHPA or HDEHP), good results are obtained with solvents comprising TOP (trioctylphosphate) or TEHP
- 30 (triethylhexylphosphate). Solvents comprising dibutyl phosphoric acid (DBPA), tributyl phosphate (TBP) or Cyanex® 923 (trialkylphosphine oxides) can also be used.

- 35 In this sub-embodiment, the dedicated solvent is not recycled/recirculated in the main loop (of peroxide production) but instead, is regenerated and recycled in the washing step or disposed in order to avoid soluble metal accumulation in the process.

The regeneration treatments mentioned above consist, for example, in
subjecting the solvent to one or more extractions, and to one or more treatments
with a chemical reagent which is compatible with the organic solvent, in order to
remove the impurities. The solvent regeneration is preferably done using an
5 aqueous acidic solution for instance an aqueous nitric acid solution (HNO_3).
This solvent regeneration is in fact also an extraction, the acid transforming the
organic metal complexes in inorganic salts (nitrates in the case of nitric acid) of
said metals which are water soluble and hence are extracted from the solvent
(organic phase) in an aqueous phase namely consisting of water in which the
10 metal salts are dissolved. Hence, this regeneration can be done using classical
industrial extraction equipment like a column, a centrifugal decanter etc.

Besides the nature of the chelating agent and of the solvent, several other
parameters may be adapted in order to optimize the process of the invention,
namely: the pH, the amount of chelating agent, the ratio peroxide to solvent and
15 the temperature. Preferably, the pH is acidic because this limits hydrogen
peroxide decomposition and also, the solubility of the chelating agent in said
hydrogen peroxide.

Figure 4 attached shows a bloc diagram of a preferred embodiment of the
invention, according to which a crude hydrogen peroxide aqueous solution (1) is
20 submitted to a washing operation (first extraction step 2) with an organic solvent
to which an organophosphorus chelating agent has been added, and which
actually is a mixture of fresh extraction solvent (3) and of regenerated solvent (8).
This washing operation is in fact an extraction, the organic phase (solvent +
chelating agent) being first mixed with the crude hydrogen peroxide solution in
25 order to be able of forming complexes with the metals it contains and thereafter,
two phases are separated to provide respectively a purified aqueous hydrogen
peroxide solution (4) and an organic phase charged with metal complexes (5).
The latter is then at least partly regenerated in a second extraction step (6) using
an aqueous HNO_3 solution (7) as explained above. At the issue of this
30 regeneration step (6), there is provided an aqueous phase comprising metal
nitrates (9) and a purified extraction solvent of which part (8) is recycled to the
first extraction step (washing operation 2) and part (10) is removed to balance
the process.

In one aspect, the present invention relates to a process for manufacturing
35 propylene oxide (1,2-epoxypropane) by reaction of propylene with hydrogen
peroxide, said process using a hydrogen peroxide solution containing less than

100 ppb of Al and/or Fe and less than 100 ppb of Cr. The present invention also relates to a process for manufacturing propylene oxide (1,2-epoxypropane) by reaction of propylene with hydrogen peroxide, said process using a hydrogen peroxide purified with a process as described above.

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More generally, the present invention also relates to the use of a purified H₂O₂ solution for manufacturing propylene oxide, wherein "purified" is as defined above i.e. having an Al and/or Fe (and optionally also a Cr content) of less than 100 ppb, typically in the range of the 10th of ppb, preferably in the range of the ppb, even more preferably below the ppb of these elements.

Should the disclosure of any patents, patent applications, and publications which are incorporated herein by reference conflict with the description of the present application to the extent that it may render a term unclear, the present description shall take precedence.

The present invention is illustrated in a non limitative way by the Examples below and Figures 1 to 3 attached which relate to preferred embodiments thereof.

Figure 1 is schematic diagram of the apparatus (installation) used for the continuous trial of Example 7.

Figure 2 shows the evolution of aluminium and iron content in the aqueous phase at the outlet of this installation.

Figure 3 shows the buildup of aluminium and iron in the organic phase inside said installation.

Examples 1 to 4

DEHPA has been tested as a chelant to remove Al and Fe from a crude H₂O₂ solution having a peroxide concentration of 40% and the following metal content:

- Al = 220 ppb
- Fe = 110 ppb

Example 1: pH optimization

A sample of hydrogen peroxide at 40% concentration is treated either with a nitric acid solution or with sodium hydroxide solution to obtain the desired pH. Then the hydrogen peroxide is mixed with the organic solution containing the solvent and the chelating agent in a plastic decanting funnel. The funnel was then shaken during 30 min and let to decant until a good separation is obtained between the organic and the aqueous phases. The treated hydrogen peroxide was recovered and analyzed for metal concentration by ICP. The ratio peroxide on organic phase (TOP+DEHPA) was set equal to 5.0. The amount of DEHPA in TOP was set equal to 2 % by weight.

The results obtained are shown in table 1 below.

Table 1

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pH	Al in H ₂ O ₂ crude ppb	Fe in H ₂ O ₂ crude ppb	P in H ₂ O ₂ crude ppm	Al removed (%)	Fe removed (%)
	180	24	8,3	5	76
2,0	170	17	12	26	85
2,5	150	14	20	35	87
3,0	140	26	36	36	76
1,5	150	54	77	35	55
4,0	180	74	81	22	33
4,5	180	80	83	22	27

These tests show that:

- the optimum pH range for Al and Fe removal is between 2.0 and 2.5 which is close to the natural pH of crude peroxide
 - when the pH increases (especially above 3.5), the chelant (complexing agent)
- 5 has a tendency to dissolve in the hydrogen peroxide as can be seen by the evolution of the P content.

Example 2: Optimization of the ratio peroxide / organic and amount of DEHPA

- 10 The same conditions as in Example 1 were used except that the pH was not adjusted before the test.

The results obtained are shown in table 2 below.

Table 2

pH of H ₂ O ₂	H ₂ O ₂ /TOP ratio	DEHPA in TOP (%)	Al in H ₂ O ₂ crude ppb	Fe in H ₂ O ₂ crude ppb	P in H ₂ O ₂ crude ppm	Al removed (%)	Fe removed (%)
2	1	0	220	46	11	4	58
2	1	2	120	5	15	48	95
2	1	5	41	< 5	25	82	> 95
2	5	0	200	43	10	13	61
2	5	2	170	17	12	26	85
2	5	5	66	< 5	16	71	> 95
2	10	0	200	42	10	13	62
2	10	2	180	18	12	22	84
2	10	5	120	< 5	12	48	> 95

These tests show that the optimum metal removal is obtained with a low ratio peroxide to organic phase (1 to 1) and with a concentration of DEHPA of 5 % by weight in TOP.

Example 3: Influence of solvent: Solvesso®/DiBC compared to TOP

- 5 As the solvent combination Solvesso®150/DiBC is often used on crude H₂O₂ production sites, it was interesting to check the efficiency of DEHPA in this type of solvent.

The tests performed at lab scale (again using the same procedure as in the previous examples) are shown in Table 3 below.

10 Table 3

pH of H ₂ O ₂	H ₂ O ₂ /solvent ratio	DEHPA in S150/DBC (%)	Al in H ₂ O ₂ crude ppb	Fe in H ₂ O ₂ crude ppb	P in H ₂ O ₂ crude ppm	Al removed (%)	Fe removed (%)
2	1	1	180	47	11	22	57
3	1	1	190	50	14	17	55
4	1	1	190	33	15	17	70
5	1	1	220	13	27	4	88
6	1	1	12	12	80	95	89

These results indicate two main different trends in comparison with TOP
- the optimum pH is much higher (close to 6.0) and might lead to a stability issue for hydrogen peroxide

- 15 - the amount of DEHPA required for an optimum removal is lower than the one required for TOP systems (1 % instead of 5 %).

Example 4: Influence of complexing agents: CYANEX® 272 compared to DEHPA

- 20 CYANEX® 272, a phosphonated component with a different structure than DEHPA and having the chemical formula is bis(2,4,4-trimethylpentyl)phosphinic acid (CAS : 83411-71-6) was used again in the same experimental conditions. The comparative tests performed at lab scale are shown in Table 4 below.

Table 4

H2O2 /TOP ratio	CYANEX in TOP (%)	Al in H2O2 CRUDE ppb	Fe in H2O2 CRUDE ppb	P in H2O2 crude ppm	Al removed (%)	Fe removed (%)
1	0	220	46	11	4	58
1	2	160	6	15	30	95
1	5	160	6	18	30	> 95
5	0	200	43	10	13	61
5	2	170	12	12	26	89
5	5	160	5	14	30	> 95
10	0	200	42	10	13	62
10	2	170	19	11	26	83
10	5	160	9	13	30	> 95

These tests show that when using the best conditions optimized for DEHPA (pH=2, Ratio=1 and DEHPA=5%), the Al removal by CYANEX® is limited to 30 % instead of 82 % for DEHPA.

CYANEX® 272 has however a high efficiency for Fe removal (> 95 %) and similar to the one obtained with DEHPA.

Examples 5, 6 and 7:

A multi-extraction process has been tested to remove Al, Fe and Cr from a crude H2O2 solution having a peroxide concentration of 40% and the following metal content:

- Al = 76 ppb
- Fe = 92 ppb
- Cr = 23 ppb

15 Example 5: Test at ambient temperature

A crude solution of hydrogen peroxide at 40% concentration was mixed with an organic solution containing a mixture of solvents and a chelating agent in a plastic decanting funnel. The organic solution consisted of :

- 80% w/w of Solvesso®150
- 20 - 10% w/w of TOP
- 10% w/w of DEHPA

The funnel was then shaken during 60 min at ambient temperature and let to decant for 24 hours. The treated hydrogen peroxide was separated from the

organic phase, filtered on paper filters (597 ½ followed by 595) and a sample was taken for analysis.

- 5 The same sample of hydrogen peroxide was treated 5 times successively with a fresh aliquot of the organic chelating solution. At each step of the process, a sample was taken and analysed for metal concentration by ICP-MS.

The ratio peroxide on organic phase (S150+TOP+DEHPA) was the same at each step and equal to 10.

The results obtained are shown in Table 5 below:

Table 5

	ICP analysis			Yield of removal		
	Al	Fe	Cr	Al	Fe	Cr
	µg/kg	µg/kg	µg/kg	%	%	%
Initial H2O2	76	92	23			
extraction 1	5	0.29	16	93.4	99.7	30.4
extraction 2	2	0.07	11	97.4	99.9	52.2
extraction 3	1.5	0.09	8	98.0	99.9	65.2
extraction 4	1.5	0.15	5	98.0	99.8	78.3
extraction 5	1.4	0.08	3.1	98.2	99.9	86.5

10

These results show that:

- The extracting process is efficient for Al, Fe and Cr at the natural pH of crude hydrogen peroxide
- The efficiency of the extracting process goes in the order : Fe > Al > Cr

15 **Example 6: test at 50°C**

The same procedure as in Example 5 was repeated except that the temperature was set at 50°C instead of ambient.

The results obtained are shown in Table 6 below:

Table 6

	ICP analysis			Yield of removal		
	Al	Fe	Cr	Al	Fe	Cr
	µg/kg	µg/kg	µg/kg	%	%	%
Initial H ₂ O ₂	76	92	23			
extraction 1	3.8	0.9	6	95.0	99.0	73.9
extraction 2	1.3	0.16	1.3	98.3	99.8	94.3
extraction 3	0.7	0.05	0.5	99.1	99.9	97.8
extraction 4	1.2	0.08	0.22	98.4	99.9	99.0
extraction 5	0.7	< 0.05	0.13	99.1	100	99.4

These results show that:

- The efficiency of the extracting process is higher at 50°C than at ambient temperature
- Metal concentrations below 1ppb in the crude can be achieved after 3 extractions for Al, Fe and Cr
- After 5 extractions, Fe can be removed completely from the hydrogen peroxide solution.

10 **Example 7: Continuous extraction trial**

2 continuous flows of a crude solution of hydrogen peroxide at 40% concentration identical to the one used in Examples 5 and 6 above and of an organic solution containing a mixture of solvents and a chelating agent were mixed together continuously in a heated glass reactor. The organic solution consisted of:

- 80% w/w of Solvesso®150
- 10% w/w of TOP
- 10% w/w of DEHPA

The mixture between aqueous and organic phases was then fed continuously in a separating glass column filled with a packing glass in order to separate both phases. That process was then repeated in a second set of identical material. A schematic diagram of the used apparatus (installation) is set out in Figure1 attached. The mixture of solvents was permanently recycled inside this installation following a closed circuit. The flows for each solutions were:

- 50 ml/h for the aqueous hydrogen peroxide solution
- 100 ml/h for the organic extraction solution

The total amount of organic solution recycled in the system was 1250ml and the installation was fully kept at 50°C.

5 Periodically a sample of the aqueous solution was taken at the outlet of the installation and analysed by ICP. The evolution of aluminium and iron content in the aqueous phase at the outlet of the installation is shown in Figure 2 attached.

Periodically a sample of the organic solution was taken and analysed by ICP-MS. The buildup of aluminium and iron in the organic phase is shown in
10 Figure 3 attached.

These results show that:

- An aluminium concentration in the outlet crude can be maintained below 20ppb for almost 2500 hours of operation.
- A concentration below 5 ppb of iron in the outlet hydrogen peroxide can be
15 maintained on a long run.
- 1250ml of extraction solution allowed purifying 125l of hydrogen peroxide while maintaining a concentration of aluminium lower than 20ppb in the crude.

Example 8: Regeneration of exhausted chelating solution

The organic mixture of solvents and chelating agent used in the
20 continuous extraction trial (example 7) has been used to test the regeneration procedure.

During the continuous trial, the inlet and outlet hydrogen peroxide solutions have been analysed periodically by ICP. By integration of these analytical results, the amount of aluminium in the organic solution at the end of
25 the continuous test can be estimated to 10.2 mg/kg.

In a plastic fuel decanter, 100ml of that organic extracting solution have been mixed for 30 minutes with 100ml of HNO₃ 1mol/l at ambient temperature and let to decant until a good separation is obtained between both phases.

Then the nitric acid solution was recovered and its aluminium content
30 analysed by ICP. The result obtained was 9.2mg/kg of aluminium in the nitric phase.

Taking into account the density of hydrogen peroxide, the yield of aluminium regeneration was about :

$$9.2 * 100 / (10.2 * 1.15) = 78\%$$

CLAIMS

1. Process for manufacturing propylene oxide (1,2-epoxypropane) by reaction of propylene with hydrogen peroxide, said process using a hydrogen peroxide solution containing less than 100 ppb of Al and/or Fe and less than 100 ppb of Cr.
2. Process according to claim 1, wherein the hydrogen peroxide solution contains Al and/or Fe, and Cr in the range of the ppb.
3. Process according to claim 2, wherein the hydrogen peroxide solution contains below the ppb of Al and/or Fe, and Cr.