

Description

This invention relates to a drill bit for cutting accurately-formed round holes of uniform diameter through wood and metal.

BACKGROUND ART

One of the most commonly used twist drills for drilling through metal is formed with a chisel edge, or chisel point, at the work-engaging end of the drill. The chisel edge is formed normal to the axis of the drill and usually extends equally on opposite sides of the drill axis. While the chisel edge is the first portion of the drill to engage the workpiece, the cutting lips typically taper rearwardly and from the opposite ends of the chisel edge. In use, the chisel edge engages the workpiece and literally works the material in the immediate vicinity into an extrudate rather than forming chips for extraction. The worked material permits the drill to begin to move into the material of the workpiece whereby the cutting lips begin to cut the material and form removable chips.

While the chisel-edge twist drill is satisfactory for some drilling operations, it does not provide holes with accurately located centres or round holes. For example, the chisel edge drill, which includes two flutes and two cutting lips, tends to "skip" away from the desired hole location as the rotating chisel edge engages the workpiece. Further, any out-of-round characteristic of the drill or the chuck supporting the drill is transmitted to the working end during a hole-drilling operation. This results in the formation of an oversize hole. In addition, twist drills having a chisel edge typically have a relatively large web which is slightly less than the length of the chisel edge. Drills with larger webs require significant thrust in order to urge the drill into the workpiece. The larger webs also limit the effective space for chip removal through the flutes, the radial depth of which is determined by the web thickness.

Other types of drills or hole-forming bits are available which have a self-centring capability. These drills or bits have a variety of centre-point tips which provide some degree of drill bit centring followed by the actual hole cutting facility. Some examples of these are split-point bits, spade bits, solid-centre auger bits, power bore bits and brad-point bits.

In the wood drilling art it is known to use augers which have cutting lips in the form of a fishtail and a centring piece which may be formed by, for example a brad-point or a threaded point as disclosed in AU-B-528 398. Such augers are totally unsuitable for use in metal and would either not cut the metal or break.

In the metal drilling art it is known to use a stepped drill to cut two bores of different diameters, for example to accommodate the head and shank of a bolt. A typical stepped drill is described on page 144 of the Sixth Edition of the Metal Cutting Tool Handbook published by the Metal Cutting Tool Institute in 1969.

Two of the problems associated with stepped drills such as shown in Figure 1 of this reference are that they cut irregular holes and require substantial thrust to drill.

It is an object of the present invention to provide a drill bit for cutting holes through wood and metal which is self-centring, requires relatively low thrust, does not jam or form burrs at breakthrough, will not develop transient loading or wobble and thereby avoid breaking of corners, does not stall while drilling, will penetrate the workpiece with ease, is less susceptible to breakage, will produce a thicker chip for heat dissipation from the cutting edge and powderless full waste removal, will generate a self feeding capability to enhance the lower thrust characteristic, will develop a burr-free accurately-formed round hole and will provide comparatively longer drill life.

In order to achieve these objectives the present invention is characterized in that the second section of the drill body is provided with a split point with minor cutting lips for cutting a secondary hole in the workpiece preceding the cutting of the primary hole and in that the major cutting lips are arranged in a "fishtail" configuration.

Preferably, said split point has two cutting edges which, in use, engage with workpiece in advance of the engagement of the workpiece by said minor cutting lips to initiate drilling by the drill bit, and said cutting edges are spaced apart but connected at the extreme tip of the split point cutting tip by a slight chisel edge.

Advantageously, a fillet is formed at a juncture between said outer surface and said first section, said fillet raking radially inward to provide a relief clearance.

Preferably, a forward edge of said fillet is contiguous with an associated one of said major cutting lips, and said fillet is formed with a radius which decreases as said fillet extends away from said fillet forward edge.

Advantageously, said second section has two diametrically opposed rounded outer surfaces which taper radially inwardly towards each other in the axial direction towards their respective fillets to provide an inward

back taper of said second section. Preferably, said flutes comprise a pair of diametrically opposed helical flutes with a web therebetween, and said web has a radially outward taper beginning at the free end of said tip and extending toward said shank end.

Advantageously, the lengthwise exterior of said drill body is formed with a radially inward back taper from said major cutting lips toward said shank end.

Preferably, the drill body is formed with shallow lip relief surfaces trailing major cutting lips.

Advantageously, the drill body is formed with steep lip relief surfaces trailing said shallow lip relief surfaces.

Particularly advantageously, said flutes are formed helically in said drill body at a helix angle of 22.5 degrees; said major cutting lips are formed at a point angle of 190 degrees; said minor drill diameter is thirty-seven percent of said prescribed major drill diameter; said second section extends from the first section in a direction away from the shank end by a prescribed length which is seventy percent of the minor drill diameter; said split point is formed with a pair of minor cutting lips at a point angle of 135 degrees, said second section has rounded outer side surfaces which taper toward the first section at a back taper angle of one and one-half degrees; and said outer side surfaces rake radially inwardly from a forward edge thereof to form a second relief clearance.

US-A-3 592 555 discloses a self-centring drill bit, comprising: an elongated drill body having a shank end and a working end; flutes formed in the drill body and extending to a free end of the drill body at the working end; the working end being formed with a major cutting section of a prescribed major drill diameter and including major cutting lips for cutting a primary hole in a workpiece; a pilot tip formed on the working end and being formed with minor cutting lips of a diameter smaller than the major drill diameter for cutting a leading secondary hole in the workpiece; and the pilot tip being formed with at least one outer side surface.

A second aspect of the invention is characterized in that said one outer side surface is integrally joined to the major cutting section; a fillet is formed at a juncture of said outer side surface; and the major cutting section rakes radially inwardly as the fillet extends away from a forward edge of said outer side surface to provide a radial relief clearance on the fillet.

Preferably, the fillet comprises a radiused surface between a forward edge and a trailing corner thereof which is contiguous with and curves between said outer side surface and a relief surface of a respective one of said major cutting lips said radiused surface having a radius of curvature which decreases as the fillet extends away from said forward edge to said trailing corner.

For a better understanding of the invention reference will now be made, by way of example, to the accompanying drawings, in which:-

FIG. 1 is a side view showing a drill bit embodying certain principles of the invention;

FIG. 2 is a perspective view of a working end of a drill bit of FIG. 1 showing various surfaces and edges of the drill bit embodying certain principles of the invention;

FIG. 3 is an end view of the working end of the drill bit of FIG. 2 showing a general arrangement of the surfaces and edges of the working end;

FIG. 4 is a perspective view of the working end of the drill bit of FIG. 2 showing additional surfaces and edges of the working end embodying certain principles of the invention;

FIG. 5 is a section view taken along line 5-5 of FIG. 3 and along a major cutting lip at the working end of the drill bit showing particularly the contour of portions of the cutting lip and certain other edges of the working end;

FIG. 6 is a partial side view of the drill bit showing the working end in particular alignment;

FIG. 7 is a partial side view of the drill bit showing the working end in an alignment which is rotated ninety degrees from the alignment shown in FIG. 6;

FIG. 8 is a partial side view of the drill bit similar to FIG. 7 which illustrates a variety of significant parameters of the working end of the drill bit in accordance with certain principles of the invention;

FIG. 9 is a section view taken along line 9-9 of FIG. 7 showing radial relief of a pilot tip of the working end in accordance with certain principles of the invention; and

FIGS. 10 through 13 are partial side views showing the drill bit of FIG. 1 forming a hole in a workpiece.

BEST MODE FOR CARRYING OUT THE INVENTION

As illustrated in FIG. 1, a stepped drill bit 20 for cutting a variety of materials such as metal, wood, plastics, laminates, piping and tubing is formed with an elongated drill body 22 having an elongated axis and which is composed of high speed steel. Drill body 22 is formed with a shank end 24, a working end 26 and a fluted section 28 interposed between the shank end and the working end. Shank end 24 includes a

round shank 30 which extends from the end of drill body 22 to one end of fluted section 28. Working end 26 includes a "fishtail" cutting section 32 of a major diameter and a pilot tip cutting section 34 of a minor diameter which is smaller than the major diameter. Fluted section 28 is formed with a pair of helical flutes 36 formed at a prescribed helix angle and which begin at the inward end of shank 30 and extend to the outward end of working end 26.

Referring to FIGS. 2 and 3, pilot tip cutting section 34 of drill body 22 is formed with a pilot tip 38 which is formed integrally with and extends a short distance axially beyond "fishtail" cutting 32. Further, pilot tip 38 is formed at its tip end with a conventional split point having spaced cutting edges 40 and 42 with a slight chisel edge 44 extending therebetween.

Minor cutting lips 46 and 48 are formed on pilot tip 38 with lip relief surfaces 50 and 52 formed behind cutting edges 40 and 42, respectively, and behind cutting lips 46 and 48, respectively, to provide necessary clearance. Steep surfaces 54 and 56 are formed forward of cutting edges 40 and 42, respectively, to provide for the formation of the cutting edges. Pilot tip 38 is formed with rounded outer surfaces 58 (FIG. 2) and 60 (FIG. 4) in an axial direction on opposite sides of the pilot tip. As viewed in FIG. 2 outer surface 58 is formed with a forward edge 62 and a trailing edge 64. As illustrated in FIG. 4, outer surface 60 is formed with a forward edge 66 and a trailing edge 68.

Referring to FIGS. 2 and 4, outer surfaces 58 and 60 are generally rounded but are curved radially inwardly as the outer surfaces extend from forward edges 62 and 66 to trailing edges 64 and 68, respectively. This is more clearly illustrated in FIG. 9 where outer surfaces 58 and 60 are depicted as curving radially inwardly of a true circle represented by dashed line 70 as represented by radial relief "RR". In this manner, radial relief surfaces for forward edges 62 and 66 are formed by outer surfaces 58 and 60, respectively.

FIG. 8 is an outline of the profile of working end 26 and illustrates various parameters of drill bit 20. As viewed in FIG. 8, each of the outer surfaces 58 and 60 are relieved in the axial direction by the formation of a tapered slope, or radially inward pilot back taper "BT", from the tip end of working end 26 to the base of pilot tip 38.

Referring to FIG. 2, "fishtail" cutting section 32 is formed with a pair of major cutting lips 72 and 74 and with lip relief surfaces 76 and 78, respectively, to form the cutting section with a "fishtail" configuration (FIG. 7) of the type typically used for drilling holes in thin sheet metal. Steep relief surfaces 80 and 82 are also formed on "fishtail" cutting section 32 during the period when steep forward surfaces 54 and 56 are being formed on pilot tip 38. Formation of shallow relief surfaces 76 and 78 result in the formation of trailing edges 84 and 86 respectively.

During formation of various relief surfaces, each of the major cutting lips 72 and 74 is formed with a section which slopes in the direction of working end 26 as the lip approaches pilot tip 38. For example, as more clearly shown in FIG. 4, cutting lip 74 begins at an outer point 88 and progresses toward pilot tip 38. Between outer point 88 and pilot tip 38, lip 74 begins to curve toward the working end 26 to eventually form a large radius at a forward edge 90 of a fillet 92 where the lip merges with forward edge 66 of outer surface 60 of the tip. This can be readily viewed in FIG. 5 where tangent lines 94 illustrate the upwardly curving cutting lip 74 and forward edge 66. Note that a portion of the cross-hatching in FIG. 5 has been removed to clearly reveal tangent lines 94 and the manner in which cutting lip 74 curves upwardly.

Referring to FIG. 2, cutting lip 72 extends from an outer point 96 and eventually curves in an identical manner into a large radius at a forward edge 98 of a fillet 100 where the lip merges with forward edge 62 of outer surface 58 of pilot tip 38.

Referring to FIGS. 2 and 4, each of the fillets 92 and 100 begin at forward edges 90 and 98, respectively, with the large radius such as the radius illustrated in FIG. 5. As the fillets 92 and 100 rake rearwardly from forward edges 90 and 98, respectively, the radius becomes progressively smaller until the fillets terminate in nearly-squared trailing corners 102 and 104, respectively. In addition, each of the fillets 92 and 100, rake radially inwardly from forward edges 90 and 98 to trailing corners 102 and 104, respectively, in the same manner as the outer surfaces 58 and 60, respectively. In this manner, fillets 92 and 100 are radially relieved with respect to the axis of drill body 22 to provide relief for forward edges 90 and 98, respectively.

Thus, continuous trailing relief is provided behind all forward working-engaging edges. For example, all surfaces of drill body 22 which trail major cutting lip 74, fillet forward edge 90 and pilot tip forward edge 66, are relieved in the manner described above so that, when drill bit 20 is used to drill a hole in a workpiece, these trailing surfaces do not engage and rub against the walls of the hole. Similarly, all surfaces which trail cutting lip 72, fillet forward edge 98 and pilot tip forward edge 62 are relieved as described so that, when drill bit 20 is used to drill a hole in a workpiece, these trailing surfaces do not engage and rub against the walls of the hole.

Referring to FIGS. 1 and 2, drill body 22 is formed with margins 106 in a conventional manner on lands 108 of the drill body where the lands are contiguous with flute 36.

Referring to FIGS. 6, 8 and 9, working end 26 is formed as illustrated with the various surfaces and cutting elements being dimensionally configured to produce the enhanced drip bit 20 for superior performance in the formation of a hole in a workpiece. The parameters of the illustrated portions of drill bit 20 combine to provide for efficient cutting ability of the drill bit with superior relief from the cutting action to preclude any rubbing of the walls of the hole.

Referring to FIG. 8, pilot tip 38 is formed with a point angle "TA" which, in the preferred embodiment, is 2.36 radians (135 degrees). The diameter "d" of pilot tip 38 is thirty-seven percent of the major diameter "D" of the drill body 22 while the height or length "L" of the pilot tip is seventy percent of the pilot tip diameter "d". For example, referring to the table of parameters below, a 1.27 cm (1/2 inch) drill bit will be formed with a pilot tip diameter of 0.4699 cm (0.185 inch) and a pilot tip length of 0.3276 cm (0.129 inch). Because of the small major diameter of the 0.3175 cm (1/8 inch) to 0.4762 cm (3/16 inch) drill bits, the pilot tip diameter "d" and pilot tip length "L" of these drill bits are based on larger percentage factors than the remaining drill bit sizes in the table.

DIA	LENGTH	FLUTE LENGTH	RELIEF DIA	WEB POINT	MARGIN	LAND	d	L	f
0.3175	6.985	4.1148	0.2921	.0508	.0381	.1778	.1600	.127	.244
0.3571	7.3152	4.445	0.3302	.0558	.0406	.2032	.1600	.127	.209
0.3967	7.9248	5.08	0.3708	.0609	.0431	.2286	.1600	.127	.209
0.4366	8.255	5.3848	0.4064	.0660	.0457	.254	.1600	.127	.209
0.4762	8.89	5.8674	0.4470	.0711	.0457	.2794	.1752	.127	.209
0.5158	9.1948	6.1976	0.4851	.0762	.0482	.3048	.1905	.1320	.209
0.5557	9.8298	6.35	0.5257	.0812	.0482	.3175	.2032	.1422	.209
0.5953	10.16	6.6548	0.5638	.0863	.0508	.3302	.2209	.1549	.209
0.635	10.4648	6.985	0.6045	.0889	.0508	.3429	.2336	.1625	.209
0.6746	10.795	7.3152	0.6426	.0965	.0533	.3556	.2489	.1727	.209
0.7142	11.0998	7.4676	0.6832	.1041	.0533	.381	.2641	.1854	.209
0.7541	11.43	7.7724	0.7213	.1117	.0558	.4064	.2794	.1955	.209
0.7937	11.7348	8.1026	0.762	.1193	.0558	.4318	.2921	.2032	.209
0.8333	12.065	8.4074	0.8026	.127	.0584	.4572	.3073	.2159	.209
0.8732	12.3698	8.7376	0.8407	.1346	.0609	.4826	.3225	.2260	.209
0.9128	12.7	8.89	0.8813	.1371	.0609	.508	.3378	.2362	.209
0.9525	12.7	9.1948	0.9220	.1397	.0635	.5334	.3530	.2463	.209
0.9921	12.7	9.1948	0.9550	.1473	.0635	.5334	.3657	.2565	.209
1.0312	12.7	9.1948	0.9982	.1549	.0660	.5588	.381	.2667	.209
1.0716	12.7	9.1948	1.0388	.1625	.0660	.5842	.3962	.2768	.209
1.1112	12.7	9.1948	1.0795	.1701	.0685	.6096	.4114	.2870	.209
1.1508	12.7	9.1948	1.1176	.1778	.0685	.635	.4267	.2971	.209
1.1907	12.7	9.1948	1.1303	.1854	.0711	.6604	.4394	.3073	.209
1.2430	12.7	9.1948	1.2090	.1879	.0736	.6858	.4546	.3175	.209
1.27	12.7	9.1948	1.2369	.1905	.0762	.7112	.4699	.3276	.209

TABLE OF PARAMETERS OF DRILL BIT 30 IN CENTIMETERS AND RADIANS

The radially inward back taper angle "BT" of pilot tip 38 is 0.026 radian (one and one-half degrees) with a tolerance of plus or minus 0.009 radian (one-half degree). Referring to FIG. 9, the radial relief dimension "RR" at the trailing edges 64 and 68 of outer surfaces 58 and 60, respectively, is 0.0193 cm (0.0076 inch) with a tolerance of plus or minus 0.0063 cm (0.0025 inch).

Referring again to FIG. 8 the point angle "FA" of major cutting lips 72 and 74 exceeds 3.142 radians (180 degrees) to provide the "fishtail" configuration. In the preferred embodiment, point angle "FA" is 3.316 radians (190 degrees). Referring to FIG. 6, the lip relief angle "f" of the relief surfaces 76 and 78 for major

cutting lips 72 and 74, respectively, is 0.209 radians (12 degrees) except for the 0.3175 cm (1/8 inch) drill which has a lip relief angle "f" OF 0.2441 radians (14 degrees).

Referring to FIG. 1, drill bit 20 is formed with a comparatively shallow or low helix angle "HA." In the preferred embodiment, the helix angle "HA" for drill bit 20 is 0.393 radian (22.5 degrees) with a tolerance of plus or minus 0.026 radian (1.5 degrees). The shallow or low helix angle permits drill bit 20 to be used in drilling wood as well as metal. Drill bits typically used for drilling in metal have higher helix angles. When metal-drilling drill bits are used for drilling wood, the higher helix angle causes the rotating bit to periodically enter an excessive self-feeding process whereafter the drill operator experiences a "jumping" sensation. With the low helix angle of drill bit 20, the operator experiences a smooth feed, particularly in wood, without excessive self feeding.

Further, when a drill bit breaks through the opposite side of a workpiece in the drilling of a hole, there is a tendency for the bit to begin to rapidly self-feed the bit through the drilled hole. This is particularly so for drill bits having high helix angles. With drill bit 20 having a low helix angle, the undesirable self-feeding of the bit at breakthrough is reduced significantly.

As shown in FIGS. 10 and 11, the split point end of pilot tip 38 is moved into a workpiece 110 to form a centering or secondary hole 112 which provides stabilization for bit 20 in the ultimate formation of the larger or primary hole 114 by cutting lips 72 and 74. Thus, pilot tip 38 has all of the advantages of a split point tip which enhances centering of the bit 20 and provides a means for chip formation and removal particularly when compared to a conventional chisel edge which tends initially to work the immediate area of the workpiece and form an extrudate of the workpiece material rather than form chips. Further, a chisel edge tends to "skip" or "run" laterally on the workpiece surface, particularly if there is no center-punched hole to guide a chisel-edge bit. Therefore, the split-point end of tip 38 provides significant initial centering and stabilizing of bit 20 in the drilling of hole 114.

Further, if the drive unit or drill for rotating drill bit 20 has a drill chuck which is out of round, the pilot tip 38 will wobble before the pilot tip engages the workpiece 110. It would appear that the wobble of drill bit 20 would be transmitters in the formation of the hole 114 which would also be out of round. However, as pilot tip 38 enters workpiece 110, the pilot tip immediately stabilizes working end 26 of drill bit 20 to provide a stabilized formation of holes 112 and 114.

Once pilot tip 38 becomes stabilized in workpiece 110, there is no wobble in working end 26 and in major cutting lips 72 and 74. With no wobble in major cutting lips 72 and 74, there is no transient loading experienced by the corners or points 96 and 88, respectively, of the cutting lips and, consequently, no breakage of the corners.

Since pilot tip 38 has stabilized drill bit 20, the pilot tip and the fishtail cutting section 32 will form a true round hole. Since there is no wobble in this area of drill bit 20, the corners of pilot tip 38 and fishtail section 32 travel through the shortest distance necessary in drilling holes 112 and 114, respectively. This increase the life of drill bit 20 when compared to a drill bit which is not stabilized wherein the points of such a drill bit must travel a greater distance to drill the same desired hole size which actually is drilled larger because of the out-of-round wobble effect.

Some drill bits are formed with a radially inward back taper on the lands and margins which begins at the working end of the bit and extends along the fluted section to the shank of the bit. Typically, drill bits have a back taper of 0.0020 cm per 2.54 cm (0.0008 inch per inch) of drill bit length. This taper provides relief from any wobble which may be experience along intermediate portions of the bit as the bit passes through the formed portions of the hole and which does not wobble beyond the established back taper. In the preferred embodiment of drill bit 20, the radially inward back taper for the fluted section 28 is 0.00254 cm per 2.54 cm (0.001 inch per inch) of drill bit length with a tolerance of plus or minus 0.000254 cm (0.0001 inch). This further decreases any opportunity for wobble in an intermediate part of the drill bit 20 to engage and rub against the walls of the formed portions of hole 114. Effectively, then, lower power is required to move drill bit 20 through hole 114.

As illustrated in FIG. 3, a thickness "W" of a web 116 of drill bit 20 is located where the wall of one of the flutes 36 is closest to the wall of the other flute. Drill bits with thick webs require significant thrust force or bias to move the drill bit through a workpiece because of the required drill chisel length. In the preferred embodiment of the drill bit 20, the web has been designed with a relatively thin web 116 at the tip or working end 26 of the bit. The thickness "W" of web 116 at the pilot of bit 20 is approximately fifteen percent of the major drill diameter with a tolerance of plus or minus 0.0051 cm (0.002 inch). For example, as indicated in the above table of parameters, the web thickness at the pilot of the 0.4366 cm (11/64 inch) drill bit is 0.066 cm (0.026 inch) which is fifteen percent of the major drill diameter of 0.4366 cm (0.1719 inch). Also in the preferred embodiment of drill bit 20, web 116 increases in thickness from working end 26 toward the shank 30 by a radially outward back taper of 0.061 cm (0.024 inch) per inch of drill bit length

with a tolerance of plus or minus 0.0076 cm (0.003 inch). This taper permits web 116 to be thinner at the working end 26, thereby reducing the thrust or bias requirement, while providing strengthening substance in trailing portions of drill bit 20.

Referring to FIG. 11, as drill bit 20 is moved into workpiece 110, outer points 96 and 88 (Fig. 4) of lips 72 and 74, respectively are the first portions of "fishtail" cutting section 22 to engage the workpiece and the outer points begin to cut a circular scribe in the workpiece. Eventually cutting lips 72 and 74 cut and form chips from the workpiece material remaining between hole 112 formed by pilot tip 38 and the scribe formed by points 96 and 88 of the cutting lips. As drill bit 20 progresses through workpiece 110, the working end 26 of drill bit 20 remains stabilized by the self-centering capability of pilot tip 38. Further, points 96 and 88 of cutting lips 72 and 74, respectively, are always axially ahead of remaining portions of "fishtail" cutting section 32 and are, therefore, cutting and forming a smooth-walled hole rather than a rough-burred hole of the type typically formed by most conventional twist drills.

Also, due to the various relief clearances and minimum web thickness on pilot tip 38 and "fishtail" cutting section 32, continued drilling of holes 112 and 114 still requires only a low thrust force or bias. This is further enhanced by the radially inward back taper of margins 106 and lands 108 in the fluted section 28.

Because points 96 and 88 are leading the remainder of "fishtail" section 32, a trepanning slug 118 (FIG. 12) is cut from the last portion of material of the workpiece 110 in the formation of the hole. The trepanning effect results in the formation of a relatively burr-free opening at the bottom of hole 114 compared to the typically burred-hole openings formed by conventional twist drills having point angles of less than 3.142 radians (180°). In addition, the low helix angle "HA" and the "fishtail" configuration of cutting section 32 preclude jamming and hang-up of drill bit 20 at the time when the bit "breaks through" workpiece 110 to form the lower opening of hole 114. Since outer surfaces 58 and 60 of pilot tip 38 are formed with the radially inward back taper relief as indicated by angle "BT" (Fig. 8), and are formed with the radial relief represented by dimension "RR" (FIG. 9), forward edges 62 and 66 are the only portions of the pilot tip which tend to support trepanning plug 118 after the plug has been cut from workpiece 110. By virtue of the radii of fillets 92 and 100 and the above-noted relief, plug 118 readily separates from drill bit 20 as illustrated in FIG. 13 and is not carried with the drill bit as the bit is withdrawn through newly formed hole 114.

When using a conventional chisel edge drill, a relatively large thrust force is required in order to move the drill through a workpiece. This is due, in part, to a back force which has to be overcome when the relatively long cutting lips of the conventional chisel edge drill cut into the workpiece.

In comparison with the conventional chisel-edge drill, less thrust force is required when using drill bit 20 because, in part, the effective combined length of cutting lips 46, 48, 72 and 74 is less than the effective combined length of the cutting lips of the chisel-edge drill. Thus, relatively less back force is developed by use of drill bit 20 and thereby requires relatively less thrust force to be applied by an operator. This is a clear advantage of drill bit 20 over the conventional chisel-edge drill.

In summary, drill bit 20 is designed to optimize use of a relatively low thrust or bias, for example low hand bias by an operator, to penetrate a workpiece comparatively faster than the drill bits. This minimizes the time that drill bit 20 is working in the drilling of a hole thereby increasing the comparative life of the bit. The life of drill bit 20 is also increased by the formation of thick continuous chips which carry away heat from the work area and by a pilot tip design which eliminates transient edge loading as noted above.

The various design features also result in no stall at breakthrough and provide for an essentially burr-free, true-round hole having superior hole-wall finish.

Thus, drill bit 20 is geometrically designed to be self-centering, require low thrust, does not jam or form burrs at breakthrough, will not develop transient loading or wobble at working end 26 which avoids breaking of corners, does not hang up while drilling, will penetrate the workpiece with ease, is less susceptible to breakage, will produce thicker chips for heat dispersal and full waste removal, will generate a balanced self-feeding capability to enhance the lower thrust characteristic, will develop a burr-free accurately-formed round hole and will provide comparatively longer drill life.

Claims

1. A drill bit for cutting accurately formed round holes through wood and metal having a step drill configuration and comprising an elongated drill body (22) having a shank end (24), an intermediate section (28) and a working end (26); the shank end (24), the intermediate section (28) and the working end (26) being all formed integrally in the drill body (22); flutes (36) formed in the drill body (22), each and every flute (36) having a continuous uninterrupted surface extending from a juncture of the shank end (24) and the intermediate section (28) to a free end tip (38) of the drill body (22) at the working end

with a tolerance of plus or minus 0.0076 cm (0.003 inch). This taper permits web 116 to be thinner at the working end 26, thereby reducing the thrust or bias requirement, while providing strengthening substance in trailing portions of drill bit 20.

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Because points 96 and 88 are leading the remainder of "fishtail" section 32, a trepanning slug 118 (FIG. 12) is cut from the last portion of material of the workpiece 110 in the formation of the hole. The trepanning effect results in the formation of a relatively burr-free opening at the bottom of hole 114 compared to the typically burred-hole openings formed by conventional twist drills having point angles of less than 3.142 radians (180°). In addition, the low helix angle "HA" and the "fishtail" configuration of cutting section 32 preclude jamming and hang-up of drill bit 20 at the time when the bit "breaks through" workpiece 110 to form the lower opening of hole 114. Since outer surfaces 58 and 60 of pilot tip 38 are formed with the radially inward back taper relief as indicated by angle "BT" (Fig. 8), and are formed with the radial relief represented by dimension "RR" (FIG. 9), forward edges 62 and 66 are the only portions of the pilot tip which tend to support trepanning plug 118 after the plug has been cut from workpiece 110. By virtue of the radii of fillets 92 and 100 and the above-noted relief, plug 118 readily separates from drill bit 20 as illustrated in FIG. 13 and is not carried with the drill bit as the bit is withdrawn through newly formed hole 114.

When using a conventional chisel edge drill, a relatively large thrust force is required in order to move the drill through a workpiece. This is due, in part, to a back force which has to be overcome when the relatively long cutting lips of the conventional chisel edge drill cut into the workpiece.

In comparison with the conventional chisel-edge drill, less thrust force is required when using drill bit 20 because, in part, the effective combined length of cutting lips 46, 48, 72 and 74 is less than the effective combined length of the cutting lips of the chisel-edge drill. Thus, relatively less back force is developed by use of drill bit 20 and thereby requires relatively less thrust force to be applied by an operator. This is a clear advantage of drill bit 20 over the conventional chisel-edge drill.

In summary, drill bit 20 is designed to optimize use of a relatively low thrust or bias, for example low hand bias by an operator, to penetrate a workpiece comparatively faster than the drill bits. This minimizes the time that drill bit 20 is working in the drilling of a hole thereby increasing the comparative life of the bit. The life of drill bit 20 is also increased by the formation of thick continuous chips which carry away heat from the work area and by a pilot tip design which eliminates transient edge loading as noted above.

The various design features also result in no stall at breakthrough and provide for an essentially burr-free, true-round hole having superior hole-wall finish.

Thus, drill bit 20 is geometrically designed to be self-centering, require low thrust, does not jam or form burrs at breakthrough, will not develop transient loading or wobble at working end 26 which avoids breaking of corners, does not hang up while drilling, will penetrate the workpiece with ease, is less susceptible to breakage, will produce thicker chips for heat dispersal and full waste removal, will generate a balanced self-feeding capability to enhance the lower thrust characteristic, will develop a burr-free accurately-formed round hole and will provide comparatively longer drill life.

Claims

1. A drill bit for cutting accurately formed round holes through wood and metal having a step drill configuration and comprising an elongated drill body (22) having a shank end (24), an intermediate section (28) and a working end (26); the shank end (24), the intermediate section (28) and the working end (26) being all formed integrally in the drill body (22); flutes (36) formed in the drill body (22), each and every flute (36) having a continuous uninterrupted surface extending from a juncture of the shank end (24) and the intermediate section (28) to a free end tip (38) of the drill body (22) at the working end



- (26); the working end (26) of the drill body being formed with a first section (32) of a prescribed major drill diameter (D) and including major cutting lips (72, 74) for cutting a primary hole (114) through a workpiece (110); the working end (26) of the drill body (22) being formed with a second section (34) which is formed integrally with and extends from the first section (32) in a direction away from the shank end (24) of the drill body, said second section (34) having an outer surface (60, 58) with edges (62, 66) extending integrally from the inward ends of the major cutting lips (72, 74); the second section (34) of the drill body being formed with a minor drill diameter (d) smaller than the prescribed major drill diameter (D); characterized in that the second section (34) of the drill body is provided with a split point with minor cutting lips (46, 48) for cutting a secondary hole in the workpiece (110) preceding the cutting of the primary hole (114) and in that the major cutting lips (72, 74) are arranged in a "fishtail" configuration.
2. A drill bit as claimed in Claim 1, characterized in that said split point has two cutting edges (40,42) which, in use, engage with workpiece (110) in advance of the engagement of the workpiece (110) by said minor cutting lips (46, 48) to initiate drilling by the drill bit (20), and said cutting edges (40, 42) are spaced apart but connect at the extreme tip of the split point cutting tip (38) by a slight chisel edge (44).
 3. A drill bit as claimed in Claim 1 or 2, characterized in that a fillet (92; 100) is formed at a juncture between said outer surface (60; 58) and said first section (32), said fillet (92; 100) raking radially inward to provide a relief clearance.
 4. A drill bit as claimed in Claim 3, characterized in that a forward edge (90; 98) of said fillet (92; 100) is contiguous with an associated one of said major cutting lips (74: 72), and said fillet (92; 100) is formed with a radius which decreases as said fillet (92; 100) extends away from said fillet forward edge (90; 98).
 5. A drill bit as claimed in Claim 3 or 4, characterized in that said second (34) has two diametrically opposed rounded outer surfaces (60, 58) which taper radially inwardly towards each other in the axial direction towards their respective fillets (92; 100) to provide an inward back taper (BT) of said second section (34).
 6. A drill bit as claimed in any preceding Claim, characterized in that said flutes (36) comprise a pair of diametrically opposed helical flutes (36) with a web (116) therebetween, and said web (116) has a radially outward taper beginning at the free end of said tip (38) and extending toward said shank end (24).
 7. A drill bit as claimed in any preceding Claim, characterized in that the lengthwise exterior of said drill body (22) is formed with a radially inward back taper from said major cutting lips (72, 74) toward said shank end (24).
 8. A drill bit as claimed in any preceding Claim, characterized in that said drill body (22) is formed with shallow lip relief surfaces (76,78) trailing major cutting lips (72,74).
 9. A drill bit as claimed in Claim 8, characterized in that said drill body (22) is formed with steep lip relief surfaces (80,82) trailing said shallow lip relief surfaces (76, 78).
 10. A self-centring drill bit as claimed in any preceding Claim, characterized in that said flutes (36) are formed helically in said drill body (22) at a helix angle of 22.5 degrees; said major cutting lips (72,74) are formed at a point angle of 190 degrees; said minor drill diameter (d) is thirty-seven percent of said prescribed major drill diameter (D); said second section (38) extends from the first section (32) in a direction away from the shank end (24) by a prescribed length which is seventy percent of the minor drill diameter (d); said split point is formed with a pair of minor cutting lips (46,48) at a point angle of 135 degrees, said second section (34) has rounded outer side surfaces (58,60) which taper toward the first section (32) at a back taper (BT) angle of one and one-half degrees; and said outer side surfaces (58,60) rake radially inwardly from a forward edge (62,66) thereof to form a second relief clearance (RR).



11. A self-centring drill bit, as claimed in any preceding Claim, characterized in that said one outer surface (58,60) is integrally joined to the first section (32); and a fillet (92,100) is formed at a juncture of said outer surface (58,60) and the first section (32) which fillet (92,100) rakes radially inwardly as the fillet (92,100) extends away from a forward edge (62,66) of said outer surface (58,60) to provide a radial relief clearance (RR) on the fillet (92,100).
12. A drill bit as claimed in Claim 11, characterized in that said fillet (92,100) comprises a radiused surface between a forward edge (90,98) and a trailing corner (102,104) thereof which is contiguous with and curves between said outer side surface (58,60) and a relief surface (76, 78) of a respective one of said major cutting lips (72,74), said radiused surface having a radius of curvature which decreases as the fillet (92, 100) extends away from said forward edge (90,98) to said trailing corner (102,104).
13. A drill bit as claimed in any preceding Claim, characterized in that the radially outer surface (58, 60) of said second section (34) is substantially smooth.

Patentansprüche

1. Bohrwerkzeug zum Schneiden genau geformter, runder Löcher durch Holz und Metall, das eine Stufenbohrer-Anordnung hat und einen länglichen Bohrkörper (22) mit einem Schaftende (24), einem Zwischenabschnitt (28) und einem Arbeitsende (26) aufweist; wobei das Schaftende (24), der Zwischenabschnitt (28) und das Arbeitsende (26) im Bohrkörper (22) integriert ausgebildet sind; wobei im Bohrkörper (22) Nuten (36) ausgebildet sind, wobei jede einzelne Nut (36) eine durchgehende, ununterbrochene Fläche hat, die sich von einem Übergang zwischen dem Schaftende (24) und dem Zwischenabschnitt (28) bis zu einem freien Endschnidteil (38) am Arbeitsende (26) des Bohrkörpers (22) erstreckt; wobei das Arbeitsende (26) des Bohrkörpers mit einem ersten Abschnitt (32) eines vorgeschriebenen Hauptbohrdurchmessers (D) ausgebildet ist und Hauptschneidkanten (72, 74) aufweist, um ein erstes Loch (114) durch ein Werkstück (110) zu schneiden; wobei das Arbeitsende (26) des Bohrkörpers (22) mit einem zweiten Abschnitt (34) versehen ist, der mit dem ersten Abschnitt (32) integriert gebildet ist und sich davon in eine Richtung entgegen dem Schaftende (24) des Bohrkörpers erstreckt, wobei der zweite Abschnitt (34) eine äußere Fläche (60, 58) mit Kanten (62, 66) aufweist, die sich von den nach innen gerichteten Enden der Hauptschneidkanten (72, 74) integriert erstrecken; wobei der zweite Abschnitt (34) des Bohrkörpers mit einem Vorbohrdurchmesser (d) ausgebildet ist, der kleiner ist als der vorgeschriebene Hauptbohrdurchmesser (D); **dadurch gekennzeichnet**, daß der zweite Abschnitt (34) des Bohrkörpers mit einer Querschneide mit Vorschneidkanten (46, 48) ausgebildet ist, um ein zweites Loch in das Werkstück (110) zu schneiden, bevor das erste Loch (114) geschnitten wird, und daß die Hauptschneidkanten (72, 74) in einer "Fischschwanz"-Konfiguration angeordnet sind.
2. Bohrwerkzeug nach Anspruch 1, **dadurch gekennzeichnet**, daß die Querschneide zwei Schneidkanten (40, 42) aufweist, die bei Benutzung am Werkstück (110) angreifen, bevor die Vorschneidkanten (46, 48) am Werkstück (110) angreifen, um das Bohren des Bohrwerkzeugs (20) einzuleiten, und daß die Schneidkanten (40, 42) voneinander beabstandet, jedoch an der äußersten Spitze des Querschneiden-Schneidteils (38) durch eine kleine Meißelkante (44) verbunden sind.
3. Bohrwerkzeug nach Anspruch 1 oder 2, **dadurch gekennzeichnet**, daß an einem Übergang zwischen der äußeren Fläche (60; 58) und dem ersten Abschnitt (32) eine Kehle (92; 100) ausgebildet ist, wobei die Kehle (92; 100) radial nach innen geneigt ist, um eine Hinterschliff-Fläche auszubilden.
4. Bohrwerkzeug nach Anspruch 3, **dadurch gekennzeichnet**, daß eine vordere Kante (90; 98) der Kehle (92; 100) an eine der zugehörigen Hauptschneidkanten (74; 72) angrenzt, und daß die Kehle (92; 100) mit einem Radius ausgebildet ist, der abnimmt, wenn sich die Kehle (92; 100) entgegen der vorderen Kante (90; 98) der Kehle erstreckt.
5. Bohrwerkzeug nach Anspruch 3 oder 4, **dadurch gekennzeichnet**, daß der zweite Abschnitt (34) zwei diametral gegenüberliegende, abgerundete, äußere Flächen (60, 58) hat, die sich in axialer Richtung auf ihre zugehörigen Kehlen (92; 100) radial zueinander nach innen verjüngen, um eine nach innen gerichtete Profilverjüngung (BT) des zweiten Abschnitts (34) auszubilden.



6. Bohrwerkzeug nach einem der vorhergehenden Ansprüche, **dadurch gekennzeichnet**, daß die Nuten (36) ein Paar diametral gegenüberliegende Spiralnuten (36) mit einem zwischenliegenden Kern (116) aufweisen, wobei sich der Kern (116) am freien Ende der Spitze (38) beginnend in Richtung auf das Schaftende (24) radial nach außen ausweitet.
7. Bohrwerkzeug nach einem der vorhergehenden Ansprüche, **dadurch gekennzeichnet**, daß das längsgerichtete Äußere des Bohrkörpers (22) von den Hauptschneidkanten (72, 74) in Richtung auf das Schaftende (24) mit einer radial nach innen gerichteten Profilverjüngung ausgebildet ist.
8. Bohrwerkzeug nach einem der vorhergehenden Ansprüche, **dadurch gekennzeichnet**, daß der Bohrkörper (22) mit flachen, den Hauptschneidkanten (72, 74) nachfolgenden Hinterschliff-Flächen (76, 78) ausgebildet ist.
9. Bohrwerkzeug nach Anspruch 8, **dadurch gekennzeichnet**, daß der Bohrkörper (22) mit steilen Hinterschliff-Flächen (80, 82) ausgebildet ist, die den flachen Hinterschliff-Flächen (76, 78) folgen.
10. Selbstzentrierendes Bohrwerkzeug nach einem der vorhergehenden Ansprüche, **dadurch gekennzeichnet**, daß die Nuten (36) im Bohrkörper (22) spiralförmig mit einem Spiralwinkel von $22,5^\circ$ ausgebildet sind; wobei die Hauptschneidkanten (72, 74) mit einem Spitzenwinkel von 190° ausgebildet sind; wobei der Vorbohrdurchmesser (d) 37% des vorgeschriebenen Hauptbohrdurchmessers (D) beträgt; wobei sich der zweite Abschnitt (38) vom ersten Abschnitt (32) in einer Richtung entgegen dem Schaftende (24) über eine vorgeschriebene Länge erstreckt, die 70% des Vorbohrdurchmessers (d) beträgt; wobei die Querschneide mit einem Paar Vorschneidkanten (46, 48) mit einem Spitzenwinkel von 135° ausgebildet ist, wobei der zweite Abschnitt (34) abgerundete, äußere Seitenflächen (58, 60) aufweist, die sich mit einem Verjüngungs (BT)-Winkel von $1,5^\circ$ in Richtung auf den ersten Abschnitt (32) erstrecken; und wobei die äußeren Seitenflächen (58, 60) von deren vorderen Kante (62, 66) radial nach innen gerichtet abgeschrägt sind, um einen zweiten Hinterschliff (RR) auszubilden.
11. Selbstzentrierendes Bohrwerkzeug nach einem der vorhergehenden Ansprüche, **dadurch gekennzeichnet**, daß eine äußere Fläche (58, 60) mit dem ersten Abschnitt (32) integriert verbunden ist; und wobei eine Kehle (92, 100) an einem Übergang zwischen der äußeren Fläche (58, 60) und dem ersten Abschnitt (32) ausgebildet ist, wobei sich die Kehle (92, 100) radial nach innen gerichtet abschrägt, wenn sich die Kehle (92, 100) entgegen der vorderen Kante (62, 66) der äußeren Fläche (58, 60) erstreckt, um in der Kehle (92, 100) einen radialen Hinterschliff (RR) auszubilden.
12. Bohrwerkzeug nach Anspruch 11, **dadurch gekennzeichnet**, daß die Kehle (92, 100) eine gerundete Fläche zwischen einer vorderen Kante (90, 98) und einer darauf folgenden Ecke (102, 104) enthält, die sich an die äußere Seitenfläche (58, 60) und eine Hinterschliff-Fläche (76, 78) einer zugehörigen Hauptschneidkante (72, 74) anschließt und dazwischen gekrümmt ist, wobei die gerundete Fläche einen Krümmungsradius aufweist, der abnimmt, wenn sich die Kehle (92, 100) von der vorderen Kante (90, 98) zur nachfolgenden Ecke (102, 104) erstreckt.
13. Bohrwerkzeug nach einem der vorhergehenden Ansprüche, **dadurch gekennzeichnet**, daß die radial verlaufende, äußere Fläche (58, 60) des zweiten Abschnitts (34) im wesentlichen geglättet ist.

Revendications

1. Foret de coupe de trous de forme ronde précise dans du bois et du métal, ayant une configuration de forage échelonnée et comprenant un corps allongé de foret (22) ayant une extrémité de queue (24), une partie intermédiaire (28) et une extrémité de travail (26) ; l'extrémité de queue (24), la partie intermédiaire (28) et l'extrémité de travail (26) étant toutes formées en une pièce dans le corps de foret (22) ; des cannelures (36) réalisées dans le corps de foret (22), chaque et toute cannelure (36) comportant une surface continue ininterrompue allant d'une jonction de l'extrémité de queue (24) et de la partie intermédiaire (28) à un bout libre d'extrémité (38) du corps de foret (22) à l'extrémité de travail (26) ; l'extrémité de travail (26) du corps de foret comprenant une première partie (32) de grand diamètre prescrit de forage (D) et comportant des grandes lèvres de coupe (72, 74) pour couper un trou primaire (114) dans une pièce (110) ; l'extrémité de travail (26) du corps de foret (22) comprenant une seconde partie (34) qui est réalisée en une pièce avec et qui part de la première partie (32) dans



- le sens opposé à celui de l'extrémité de queue (24) du corps de foret, ladite seconde partie (34) ayant une surface extérieure (60, 58) comportant des arêtes (62, 66) partant en continu des extrémités intérieures des grandes lèvres de coupe (72, 74) ; la seconde partie (34) du corps de foret ayant un petit diamètre de forage (d) qui est plus petit que le grand diamètre prescrit de forage (D) ; caractérisé en ce que la seconde partie (34) du corps de foret comporte un point d'entame ayant des petites lèvres de coupe (46, 48) afin de couper dans la pièce (110) un trou secondaire précédant la coupe du trou primaire (114) et en ce que les grandes lèvres de coupe (72, 74) sont réalisées sous une forme de "queue de poisson".
- 10 2. Foret selon la revendication 1, caractérisé en ce que ledit point d'entame comporte deux arêtes de coupe (40, 42) qui, en service, pénètrent dans la pièce (110) avant que lesdites petites lèvres de coupe (46, 48) pénètrent dans la pièce (110) afin d'attaquer le forage par le foret (20) et lesdites arêtes de coupe (40, 42) sont placées à distance l'une de l'autre et se raccordent au bout extrême de la pointe de coupe (38) du point d'entame par une légère arête de ciseau (44).
 - 15 3. Foret selon la revendication 1 ou 2, caractérisé en ce qu'un congé (92, 100) est formé à une jonction entre ladite surface extérieure (60, 58) et ladite première partie (32), ledit congé (92, 100) présentant une inclinaison radialement vers l'intérieur pour former un jeu de dégagement.
 - 20 4. Foret selon la revendication 3, caractérisé en ce qu'un bord antérieur (90 ; 98) dudit congé (92 ; 100) est contigu avec une, correspondante, desdites grandes lèvres de coupe (74 ; 72) et ledit congé (92 ; 100) a un rayon qui diminue avec l'éloignement par rapport audit congé (92 ; 100) dudit bord antérieur du congé (90 ; 98).
 - 25 5. Foret selon la revendication 3 ou 4, caractérisé en ce que ladite seconde partie (34) comporte deux surfaces extérieures arrondies (60, 58) qui sont diamétralement opposées et qui sont inclinées radialement vers l'intérieur l'une vers l'autre en direction axiale vers leurs congés respectifs (92 ; 100) pour former une inclinaison arrière vers l'intérieur (BT) de ladite seconde partie (34).
 - 30 6. Foret selon l'une quelconque des revendications précédentes, caractérisé en ce que lesdites cannelures (36) comprennent deux cannelures hélicoïdales diamétralement opposées (36) avec un élément de surface pleine (116) entre elles, ledit élément de surface pleine (116) ayant une inclinaison radialement vers l'extérieur qui débute à l'extrémité libre dudit bout (38) et qui est orientée vers ladite extrémité de queue (24).
 - 35 7. Foret selon l'une quelconque des revendications précédentes, caractérisé en ce que l'extérieur en longueur dudit corps de foret (22) comporte une inclinaison arrière radialement vers l'intérieur, allant desdites grandes lèvres de coupe (72, 74) vers ladite extrémité de queue (24).
 - 40 8. Foret selon l'une quelconque des revendications précédentes, caractérisé en ce que ledit corps de foret (22) comporte des surfaces peu profondes de dégagement de lèvre (76, 78) qui sont à l'arrière des grandes lèvres de coupe (72, 74).
 - 45 9. Foret selon la revendication 8, caractérisé en ce que ledit corps de foret (22) comporte des surfaces raides de dégagement de lèvre (80, 82) à l'arrière desdites surfaces peu profondes de dégagement de lèvre (76, 78).
 - 50 10. Foret à auto-centrage selon l'une quelconque des revendications précédentes, caractérisé en ce que lesdites cannelures (36) sont réalisées en hélice dans ledit corps de foret (22) suivant un angle d'hélice de 22,5 degrés ; lesdites grandes lèvres de coupe (72, 74) sont formées avec un angle de pointe de 190 degrés ; ledit petit diamètre de forage (d) représente trente-sept pour cent dudit grand diamètre prescrit de forage (D) ; ladite seconde partie (38) part de ladite première partie (32) dans le sens opposé à celui de l'extrémité de queue (24) sur une longueur prescrite qui représente soixante dix pour cent du petit diamètre de forage (d) ; ledit point d'entame comporte deux petites lèvres de coupe (46, 48) inscrivant un angle d'entame de 135 degrés, ladite seconde partie (34) comporte des surfaces latérales extérieures arrondies (58, 60) qui sont inclinées vers la première partie (32) sous un angle d'inclinaison arrière (BT) de un degré et demi ; et lesdites surfaces latérales extérieures (58, 60) sont inclinées radialement vers l'intérieur à partir de leur bord intérieur (62, 66) afin de former un second jeu
 - 55



de dégagement (RR).

11. Foret à auto-centrage selon l'une quelconque des revendications précédentes, caractérisé en ce que ladite une surface extérieure (58, 60) est reliée de manière continue à la première partie (32); et un congé (92, 100) est réalisé à une jonction de ladite surface extérieure (58, 60) et de ladite première partie (32), ledit congé (92, 100) s'inclinant radialement vers l'intérieur au fur et à mesure que ledit congé (92, 100) s'éloigne d'un bord antérieur (62, 66) de ladite surface extérieure (58, 60) afin de former un jeu radial de dégagement (RR) sur le congé (92, 100).

12. Foret selon la revendication 11, caractérisé en ce que ledit congé (92, 100) comporte une surface courbe entre un bord antérieur (90, 98) et son angle arrière (102, 104) qui est contigu à et s'incurve entre ladite surface latérale extérieure (58, 60) et une surface de dégagement (76, 78) de l'une respective desdites grandes lèvres de coupe (72, 74), ladite surface courbe ayant un rayon de courbure qui diminue au fur et à mesure que le congé (92, 100) s'éloigne dudit bord antérieur (90, 98) et se rapproche dudit angle arrière (102, 104).

13. Foret selon l'une quelconque des revendications précédentes, caractérisé en ce que la surface radialement extérieure (58, 60) de ladite seconde partie (34) est sensiblement lisse.

