

MATRIX DECODER

Cross-Reference to Related Applications

5 This application claims the benefit of priority of United States Provisional Application No. 61/010,896, filed January 11, 2008, hereby incorporated by reference.

Field of the Invention

 The invention relates to audio signal processing. More particularly, the
10 invention relates to an audio matrix decoder or decoding function or to a computer program stored on a computer-readable medium executing the decoding function. Although the decoder or decoding function is particularly useful for playback from a portable player using a headphone or loudspeaker virtualizer, a matrix decoder or decoding function according to aspects of the present invention is not limited to such
15 uses.

Summary of the Invention

 In accordance with an aspect of the present invention, an audio matrix decoding method receiving a stereo signal pair L_t , R_t , in which method the relative amplitudes and polarities of the pair determine the reproduced direction of decoded
20 signals, comprises panning L_t and R_t to outputs associated with front directions in response to a measure of the sum of L_t and R_t being greater than a measure of the difference between L_t and R_t , and panning L_t and R_t to outputs associated with rear directions in response to a measure of the sum of L_t and R_t being less than a measure of the difference between L_t and R_t , and modifying L_t and R_t to shift the direction of
25 reproduced signals.

 Modifying L_t and R_t to shift the direction of reproduced signals may shift signals panned to outputs associated with rear directions. Modifying L_t and R_t to shift the direction of reproduced signals shifts signals panned to outputs associated with rear directions may shift signals away from the rear-center direction. Such shifting
30 away from the rear-center direction may be in the direction in which such signals have the largest amplitude. Such shifting may progressively decrease for signals at directions increasingly away from the rear-center direction.

 Modifying L_t and R_t to shift the direction of reproduced signals may also shift signals panned to outputs associated with front directions. Such shifting of signals
35 panned to outputs associated with front directions may shift least signals at the front-

center direction and such shifting may progressively increase for signals at directions increasingly away from the front-center direction.

The degree of shifting, whether to the front or to the rear may be based on a measure of the difference between Lt and Rt .

5 The degree of shifting may change only when Lt and Rt are panned to outputs associated with rear directions.

According to a further aspect of the present invention, in an audio matrix decoding method receiving a stereo signal pair Lt , Rt , in which method the relative amplitudes and polarities of the pair determine the reproduced direction of decoded
10 signals, a method comprises shifting the direction of outputs associated with front and rear directions to the left or right, the direction of outputs associated with rear directions being shifted to a greater degree than the direction of outputs associated with front directions, wherein the shifting includes modifying the stereo signal pair Lt , Rt by forming a difference signal of Lt and Rt signals, scaling the difference signal by
15 a bias gain factor, and summing the scaled difference signal to both Lt and Rt signals to produce modified Lt and Rt signals such that the relative amplitudes and polarities of the modified Lt and Rt pair determine the reproduced direction of decoded signals.

According to a further aspect of the present invention, a method for modifying a stereo signal pair Lt , Rt before the signal pair is decoded by an audio matrix decoder
20 or decoding method, the relative amplitudes and polarities of the pair determining the reproduced direction of decoded signals comprises modifying the stereo signal pair Lt , Rt by forming a difference signal of Lt and Rt signals, scaling the difference signal by a bias gain factor, and summing the scaled difference signal to both Lt and Rt signals to produce modified Lt and Rt signals such that the relative amplitudes and polarities
25 of the modified Lt and Rt pair determine the reproduced direction of decoded signals.

Brief Description of the Drawings

FIG. 1 is a schematic functional block diagram showing an example of how Lt and Rt signals may be panned or steered to front and rear directions in accordance with aspects of the present invention.

30 FIG. 2 is a schematic functional block diagram showing an example of the details of the "Front-Back Steering Determination" of FIG. 1.

FIG. 3 is a schematic functional block diagram showing an example how Lt and Rt may be modified in accordance with aspects of the present invention.

FIG. 4 is a conceptual diagram useful in understanding an effect of modifying the Lt and Rt signals in accordance with aspects of the present invention.

FIG. 5 is a schematic functional block diagram showing an example of how the LR_bias control signal of FIG. 3 may be derived.

5 FIG. 6 is a schematic functional block diagram showing the overall arrangement of the arrangements of FIGS. 1, 2, 3, and 5.

Description of the Invention

Front-back panning

The matrix decoder according to aspects of the present invention treats the Lt and Rt signals applied to its inputs as a stereo signal pair, and it pans those signals to the front (left, L and right, R) or to the back (left surround, Ls, and right surround, Rs). Lt and Rt are panned to outputs associated with front directions in response to a measure of the sum of Lt and Rt being greater than a measure of the difference between Lt and Rt . Lt and Rt are panned to outputs associated with rear directions in response to a measure of the sum of Lt and Rt being less than a measure of the difference between Lt and Rt . The Front-Back panning may be achieved, for example, as shown in FIG. 1. In this block diagram, the $panF$ and $panB$ signals are slow-changing gain signals (not full bandwidth audio signals) that may vary, for example, between 0 to 1. The $panF$ and $panB$ signals operate together (they are complementary to each other) to effect a smooth crossfade between the L and R front signals and the Ls and Rs back signals.

Referring to FIG. 1, the Lt input signal is applied to the L output via a multiplier or multiplier function 2 and to the Ls output via a multiplier or multiplier function 4. The Rt input signal is applied to the R output via a multiplier or multiplier function 6 and to the Rs output via a multiplier or multiplier function 8. The gain of each of the multipliers 2 and 6 are controlled by the $panF$ gain signal; the gain of each of the multipliers 4 and 8 are controlled by the $panB$ gain signal. The Lt and Rt input signals are also applied to a circuit or function ("Front-Back Steering Determination") 10 that generates the $panF$ and $panB$ signals. Details of the Front-Back Steering Determination are shown in FIG. 2.

Subject to time smoothing, as described below, when the "Front-Back Steering Determination" 10 detects out-of-phase audio but no in-phase audio in the Lt and Rt input signals for a sufficient period of time, it sets $panB=1.0$ and $panF=0.0$, thereby directing, panning, or "steering" the Lt and Rt input signals only to the Ls and Rs

surround output channels (hard rear steering). Likewise, when there is in-phase audio but no out-of-phase audio present in the input signal for a sufficient period of time, the “Front-Back Steering Determination” 10 sets $panB=0.0$ and $panF=1.0$, thereby steering the Lt and Rt input signals only to the front output channels, L and R (hard front steering).

The arrangement in FIG. 2 generates, on an instantaneous basis, the difference between the magnitudes of the sum and the difference of the input signals Lt and Rt (a rapidly-varying waveform swinging both positively and negatively) and compares it with a small threshold ϵ (epsilon). This is accomplished by adder or adding function 12 that receives Lt and Rt to produce $Lt + Rt$ at its output, adder or adding function 14 that subtracts Rt from Lt to produce $Lt - Rt$ at its output, scalers or scaling functions 16 and 18 that scale the amplitudes of $Lt + Rt$ and $Lt - Rt$ to produce “Front” and “Back” signals F and B,

$$\begin{aligned} F &= \frac{Lt + Rt}{2} \\ B &= \frac{Lt - Rt}{2}, \end{aligned} \quad (1)$$

which signals F and B have their absolute values taken, shown at absolute value devices or functions 20 and 22, and an adder or adding function 24 that subtracts the absolute value of B from the absolute value of F and adds a small value epsilon. Elements 12, 14, 16, 18, 20, 22 and 24 may be considered collectively as a “Difference of Measures of Sum and Difference” device or function as shown in the overall arrangement of FIG. 6.

The polarity of the result $|F| - |B| + \epsilon$ is determined by a “Detect Polarity” device or function 26. If negative, the answer is one value, for example minus 1, if positive, another value, such as zero. Clearly, values other than minus 1 and zero may be employed. The result is a two-valued waveform alternating between two levels, minus 1 and 0, in this example. A low-pass filter or filtering function (“Low-pass Filter”) (“LPF”) 28 is applied, resulting in a more slowly varying waveform FB that may have any value in the range between or including the values of the two levels, depending on the proportion of time that the square wave spends at each of the levels. In response to real audio signals, the smoothed waveform produced by LPF 28 tends to remain near one or the other of the extremes. In effect, LPF 28 delivers a short-term average of its input, having a time constant, for example, in the range of 5

to 100 milliseconds. Although a 40 millisecond time constant has been found to be suitable, the value is not critical. LPF 28 may be implemented as a single-pole filter.

Still referring to the example of FIG. 2, having determined the intermediate control signal FB, two complementary panning coefficients $panF$ and $panB$ may then be obtained in any of a number of ways by a "Determine Panning Functions" device or function 30. In principle, any of various commonly-used crossfade functions may be employed, such as a linear ramp, log, Hanning, Hamming and sine functions. It will be appreciated that the actual formulae will vary depending on the output values chosen for Detect Polarity 26.

If constant power panning is desired, the following formulae may be employed:

$$panF = \sin(\pi/2 * (1 + FB)) \quad (3)$$

$$panB = \cos(\pi/2 * (1 + FB)) \quad (4)$$

Alternatively, if constant sound pressure is deemed preferable, or at least acceptable, the following formulae may be employed:

$$panF = 1 + FB \quad (5)$$

$$panB = -FB \quad (6)$$

Although equations 3 and 4 above provide constant power (the sum of the squares of the $panF$ and $panB$ coefficients is one), constant power can be approximated by employing the following formulae:

$$panF = 1 - FB^2 \quad (7)$$

$$panB = 1 - (FB + 1)^2 \quad (8)$$

The values of each of $panF$ and $panB$ in the example of equations 7 and 8 can lie anywhere between 0 and 1 and are complementary to each other, each tracing the path of a parabola. The result is two coefficients or control signals with ranges between 0 and 1, whose squares add approximately to 1.

If $panF$ were consistently greater say than $panB$ in any of the above sets of formulae, which is the result, for example, when Lt and Rt are equal with the same polarity, so that the input to the LPF 28 is 0 over a long time, the panning would steer hard front ($panF=1$ and $panB=0$). If $panF$ were consistently smaller than $panB$, which is the result, for example, when Lt and Rt are equal but out of phase, so that the input to the LPF would be -1 over a long time, the panning would steer hard back ($panF=0$ and $panB=1$). On real signals, as with the intermediate signal FB, panning tends to remain either hard front or hard back. Thus, Lt and Rt are panned to outputs

associated with front directions in response to a measure of the sum of L_t and R_t being greater than a measure of the difference between L_t and R_t , and L_t and R_t are panned to outputs associated with rear directions in response to a measure of the sum of L_t and R_t being less than a measure of the difference between L_t and R_t . When a
5 measure of the sum of L_t and R_t is the same as a measure of the difference between L_t and R_t , L_t and R_t may be panned to outputs associated with front directions, although this is not critical.

FIG. 2 provides an example of generating suitable $panF$ and $panB$ control signals. Modifications of FIG. 2, for example as suggested above, may be employed.
10 Alternatively, other arrangements that provide smooth panning signals in response to measures of the sum and difference of L_t and R_t may be employed.

Left-Right panning

Ideally, left-right panning is as follows:

When L_t , R_t is panned to the front (L , R), use less left-right
15 steering than is applied when L_t , R_t is panned to the rear, because the L_t , R_t signal likely contains complete L , C , R signal components already mixed into a stereo pair in a manner that is likely to provide a good left-right soundfield when reproduced, including a phantom center image.

When L_t , R_t is panned to the back (L_s , R_s), determine which
20 channel (L_s or R_s) has the greater amplitude, and then modify the L_t , R_t signals so that rear signals are shifted to the side in which such signals have the largest amplitude. As explained further below, in an implementation of the invention, such shifting may also have an effect,
25 albeit a lesser one, when L_t , R_t is panned to the front (L , R).

A common problem in many matrix decoders is the inability to work well for the case where input signals are panned to the rear-center position. This is particularly a problem when playback employs a headphone virtualizer or a loudspeaker virtualizer. The rear-center position, for example, is encoded with L_t and
30 R_t out-of-phase with each other. Hence, when the L_t , R_t signals are panned to L_s , R_s , rear-center signals appear in the L_s , R_s signals out-of-phase. A rear phantom image is not formed well by such out-of-phase signals.

An aspect of the present invention is to shift L_s , R_s signals to the left or right, thereby avoiding the rear-center phantom position that causes difficulty in imaging.

This may be achieved by performing a “shift” operation on the Lt , Rt signals, as shown in FIG. 3 and as described below. The greatest shift may be applied to rear-center signals and less shift for positions progressively away from rear center. The least shift (or no shift) may be applied to front-center signals with a progressively increasing shift for positions away from front-center. In other words shifting should alter the rear-center the most and the front-center the least. By avoiding or minimizing shift at the front-center position under all conditions, image location shifts of voices (dialog), which are usually at the front-center, are avoided or minimized. In principle, a shifting device or function in the manner of the example of FIG. 3 may be employed so as to modify the Lt , Rt input to any two input matrix decoder or decoding function in which the decoder or decoding function operation responds to the relative amplitudes and polarities of Lt and Rt .

One suitable “shift” operation is shown in FIG. 3 in which an Lt - Rt difference signal is generated. Then, a weighted amount of this difference signal is mixed back into both Lt and Rt to produce Lt_{biased} and Rt_{biased} . The control input (LR_Bias) may take on a value of $+\alpha$ or $-\alpha$, depending on whether the “shift” is intended to shift the rear channels to the left or the right. LR_bias may be determined, for example, as shown in the example of FIG. 5. Alpha may have a value, for example, in the range of 0.05 to 0.2. A value of 0.1 has been found to provide useful results.

Referring to the details of FIG. 3, Rt is subtracted from Lt in an adder or adding device 32 to obtain $Lt-Rt$ which is then scaled by LR_bias in a multiplier or multiplying function 34. The scaled version of $Lt-Rt$ is then summed with each of Lt and Rt in respective adders or adding functions 36 and 38 to obtain Lt_{biased} and Rt_{biased} .

Consider several examples of the operation of the shifting arrangement of FIG. 3 as follows.

For example, when $LR_Bias = +0.1$ (indicating that the shift should be to the left), one gets:

$$\begin{aligned}
 Lt_{biased} &= Lt + [0.1 \times (Lt - Rt)] \\
 &= 1.1 \times Lt - 0.1 \times Rt \\
 Rt_{biased} &= Rt + [0.1 \times (Lt - Rt)] \\
 &= 0.9 \times Rt + 0.1 \times Lt
 \end{aligned} \tag{9}$$

Continuing with this example ($LR_Bias = +0.1$), consider the case where the Lt , Rt input signal is composed of a center-panned signal: $Lt = Rt = C$. In this case, one has:

$$\begin{aligned}
Lt &= Rt = C \\
Lt_{biased} &= Lt + [0.1 \times (Lt - Rt)] \\
&= 1.1 \times Lt - 0.1 \times Rt \\
&= 1.1 \times C - 0.1 \times C \\
&= C \\
Rt_{biased} &= Rt + [0.1 \times (Lt - Rt)] \\
&= 0.9 \times Rt + 0.1 \times Lt \\
&= 0.9 \times C + 0.1 \times C \\
&= C
\end{aligned}$$

(10)

In this case, the Lt_{biased} and Rt_{biased} signals are the same as Lt , Rt . In other words, the shift circuit does not modify the Lt , Rt signals when the input contains only front-center panned audio.

In contrast, consider the case where the Lt , Rt input signal is composed of a rear-center panned signal, S : $Lt = S$, $Rt = -S$. In this case, one gets:

$$\begin{aligned}
Lt &= S, Rt = -S \\
Lt_{biased} &= Lt + [0.1 \times (Lt - Rt)] \\
&= 1.1 \times Lt - 0.1 \times Rt \\
&= 1.1 \times S - 0.1 \times (-S) \\
&= 1.2 \times S \\
Rt_{biased} &= Rt + [0.1 \times (Lt - Rt)] \\
&= 0.9 \times Rt + 0.1 \times Lt \\
&= 0.9 \times (-S) + 0.1 \times S \\
&= -0.8 \times S
\end{aligned}$$

(11)

In this case, the Lt_{biased} and Rt_{biased} signals are modified by the shift circuit or process, such that Lt_{biased} has been boosted in amplitude, and Rt_{biased} has been reduced in amplitude. Note that, if LR_Bias were set to -0.1 instead of +0.1, the amplitude shifts would be reversed, with Rt_{biased} being boosted in level while Lt_{biased} is reduced.

Ideally, the shifting circuit or process operates so that the surround channels are shifted to the left or right, and the front channels are similarly shifted but to a lesser degree. An example of shifting to the left is shown in FIG. 4 in which the solid line circle represents a matrix encoding circle, in which traditional L (left), C (center), R (right), Ls (left surround), S (surround or rear surround), and Rs (right surround) channel positions are shown. This circle has unity radius, reflecting the fact that each channel has unity power. The dashed line circle shows the effect on the unit circle of

the shift operation. The shift away from the unit circle indicates that the power of some signal directions has been boosted or attenuated. In particular, note that the rear-center position S is shifted by the greatest amount with progressively less shifting for directions farther and farther away from S with no shifting occurring at the front-

5 center position C.

An example of a way to determine a suitable LR_bias signal is shown in FIG. 5. The *LR_bias* signal is based principally on *LR*, a short-term-averaged amplitude difference between the *Lt_{biased}* and *Rt_{biased}* signals. In other words, *LR* is an estimate of *Lt_{biased}* versus *Rt_{biased}*. *LR_Bias* is calculated in "Determine Shifting" device or function 40 in response to whether each of *LR*, *FB* (FIG. 2) is less than or greater than a threshold, and in response to *Lt - Rt*. Such a calculation may be expressed in programming pseudocode:

```

15      If ( zero_crossing (Lt-Rt) &&
          (FB < 0.1) ) {
          if (LR<-0.1) {
              Bias == -0.1;
          }
          if (LR>0.1) {
              Bias = 0.1;
20      }
      }
  
```

Alternatively, *FB* and *LR* may be multiplied and the bias determined by whether the result is greater than a threshold. Such calculation may be expressed in programming pseudocode:

```

25      If ( zero_crossing (Lt-Rt) &&
          if (LR*FB<-0.01) {
              Bias == + 0.1;
          }
          If ( zero_crossing (Lt-Rt) &&
              if (LR*FB>0.01) {
30          Bias = -0.1;
              }
          }
  
```

The *LR_bias* signal may be determined as follows. First measure the relative amplitude of the *Lt_{biased}* and *Rt_{biased}* signals. Intermediate signal, *LR*, an estimate of

Lt_{biased} versus Rt_{biased} , a short-term-averaged amplitude difference between the Lt_{biased} and Rt_{biased} signals, may be determined as follows:

$$LR = \frac{\text{avg}(|Lt_{biased}| - |Rt_{biased}|)}{\text{avg}(|Lt_{biased}| + |Rt_{biased}| + \varepsilon)} \quad (12)$$

- 5 Note that a small positive offset, ε (epsilon), is added to the denominator of the fraction in equation 7, to ensure that no error occurs when Lt and Rt are both zero. In order to estimate LR , one notes that the correct value of LR should result in $Error_{LR}$ being equal to zero:

$$Error_{LR} = \text{avg}(|Lt_{biased}| - |Rt_{biased}|) - LR \times \{\text{avg}(|Lt_{biased}| + |Rt_{biased}| + \varepsilon)\} = 0 \quad (13)$$

One way to create the short-term smoothed value of LR is to increment or decrement the instantaneous value of the amplitude difference between the Lt_{biased} and Rt_{biased} signals (by a small increment, such as 2^{-10}), based on the value of $Error_{LR}$, as follows:

$$LR' = \begin{cases} LR + \frac{1}{1024} & (Error_{LR} \geq 0) \\ LR - \frac{1}{1024} & (Error_{LR} < 0) \end{cases} \quad (14)$$

In this way, the next value of LR (referred to as LR' in the equation above), will move towards the correct value in a stair step manner.

- The short-term smoothing or averaging (reflected in equations 1.5 and 1.6 as “avg”) is a result of the smoothing that results from the incremental steps that attempt to reduce the LR error. The smoothing may have a time constant between about 5 and 100 milliseconds. Values of 20 and 40 milliseconds have been found to be useful. In the implementation described, LR can take on values from -1 (indicating a hard left pan) to +1 (indicating a hard right pan). LR may have an initial value of zero, thus requiring 1024 increments for it to reach +1 or -1. Obviously, 2048 increments are required for LR to go from hard left to hard right.

- If implemented in a digital system, the increments and decrements may be done at the audio bit rate (48 kHz, for example, when increments of 2^{-10} are employed). In principle, the present invention may be implemented wholly or partly in the analog domain.

Referring again to FIG. 5, Lt_{biased} and Rt_{biased} have their absolute values taken, shown at absolute value devices or functions 42 and 44. An adder or adding function 46 adds the absolute value of Lt_{biased} and the absolute value Rt_{biased} to the small value epsilon and applies the result to a multiplier or multiplier function 48 that also
 5 receives a one-sample-delayed version of LR to produce the product of LR and the sum of the absolute value of Lt_{biased} , the absolute value Rt_{biased} , and epsilon. An adder or adding function 50 subtracts the absolute value of Rt_{biased} from the absolute value of Lt_{biased} . The error signal (equation 8) is then obtained from the output of adder or
 10 adding function 52. The error signal is applied to *signum()* device or function 54 that produces +1 if the input is greater than zero, -1 if the input is less than zero, and 0 if the input is zero (although some DSP implementations of such a function are simplified, so that *signum()* may be +1 for an input that is greater than or equal to zero, and -1 for negative input). The signum device or function 54 output is multiplied by the 2^{-10} scaling factor in multiplier or multiplying function 56 and
 15 summed with the one-sample-delayed version of LR (provided by delay device or function 60) in adder or adding function 58. Elements 42, 44, 46, 48, 50, 52, 54, 56, 59 and 60 may be considered collectively as a "Determine Short-Term Averaged Difference" device or function as shown in the overall arrangement of FIG. 6.

Once the value of LR has been determined, the LR_Bias signal value is
 20 updated in Determine Shifting 40 according to the pseudocode shown first above and the following logical rules:

1. LR_Bias will always be equal to $+\alpha$ or $-\alpha$, where α is in the range of, for example, 0.05 to 0.2. In practice, a value of 0.1 has been found to provide useful results.
- 25 2. The LR_Bias signal only flips between its two allowable values when there is a zero-crossing in the $Lt-Rt$ signal. This minimizes the possibility that a change in LR_Bias will result in an audible click in the output.
3. When the LR signal indicates that Lt_{biased} is greater in amplitude than
 30 Rt_{biased} (when $LR > 0$), and when the FB signal indicates that the Lt , Rt signals should be panned towards the back by more than an appropriate threshold (for example, when $FB < -0.1$), then set LR_Bias to $+0.1$ (when there is a zero-crossing in the $Lt-Rt$ difference signal). In other words, the value of LR_Bias

is allowed to change when the Lt , Rt signals are panned to the back by more than a threshold. However, the latest value of LR_Bias remains effective whether or not the Lt , Rt signals are panned to the back or panned to the front.

4. When the LR signal indicates that Rt_{biased} is greater in amplitude than Lt_{biased} (when $LR < 0$), and when the FB signal indicates that the Lt , Rt signals should be panned towards the back by more than a threshold (for example, when $FB < -0.1$ as mentioned above), then set LR_Bias to -0.1 (when there is a zero-crossing in the $Lt-Rt$ difference signal). The manner in which $LR = 0$ is handled is not critical. One possibility is that when $LR = 0$ do nothing (leave LR_bias unchanged) or, alternatively, act as when $LR > 0$ as described just above in paragraph 3.

Note that the LR_Bias signal is determined from the amplitudes of the Lt_{biased} and Rt_{biased} signals, and the Lt_{biased} and Rt_{biased} signal are modified by the LR_Bias signal, thus forming a feedback loop in the overall algorithm. This is a positive feedback loop that makes the overall behavior bi-stable in nature. As a result, the arrangement exhibits hysteresis. For example, when $LR_Bias = +0.1$, this causes the shifting circuit to exaggerate the Lt_{biased} signal, boosting it proportionally in comparison to the Rt_{biased} signal which will, in turn, increase the LR signal (pushing it upwards in a positive direction). As a result, a much larger Rt signal (relative to Lt) is required to flip LR_Bias back to -0.1 . Such hysteresis ensures that the system is less likely to exhibit rapid flipping back and forth in the LR_Bias signal, which might otherwise be undesirable by causing audible artifacts such as image shifting.

Image shifting is also minimized by allowing LR_bias to change only when the pan is to the rear. Image shifts are more noticeable when at the front. Also, retaining the same shift when panning from rear to front and from front to rear avoids image shifts when such pans occur. However, changes in LR_bias typically will occur when a change in audio content occurs. Thus, a shift in image location is often required at such a change and is desirable.

It will be noted that both the front-back panning and left-right panning employ time constants. Although suggested values for such time constants has been given, it will be understood that smoothing values are to a degree a matter of the designer's taste and may be chosen by trial and error. In addition, desirable smoothing values may vary depending on the audio content.

FIG. 6 shows the manner in which the above-described FIGS. 1, 2, 3 and 5 fit together.

Implementation

Although in principle the invention may be practiced either in the analog or digital domain (or some combination of the two), in practical embodiments of the invention, audio signals are represented by samples in blocks of data and processing is done in the digital domain.

The invention may be implemented in hardware or software, or a combination of both (*e.g.*, programmable logic arrays). Unless otherwise specified, algorithms and processes included as part of the invention are not inherently related to any particular computer or other apparatus. In particular, various general-purpose machines may be used with programs written in accordance with the teachings herein, or it may be more convenient to construct more specialized apparatus (*e.g.*, integrated circuits) to perform the required method steps. Thus, the invention may be implemented in one or more computer programs executing on one or more programmable computer systems each comprising at least one processor, at least one data storage system (including volatile and non-volatile memory and/or storage elements), at least one input device or port, and at least one output device or port. Program code is applied to input data to perform the functions described herein and generate output information. The output information is applied to one or more output devices, in known fashion.

Each such program may be implemented in any desired computer language (including machine, assembly, or high level procedural, logical, or object oriented programming languages) to communicate with a computer system. In any case, the language may be a compiled or interpreted language.

Each such computer program is preferably stored on or downloaded to a storage media or device (*e.g.*, solid state memory or media, or magnetic or optical media) readable by a general or special purpose programmable computer, for configuring and operating the computer when the storage media or device is read by the computer system to perform the procedures described herein. The inventive system may also be considered to be implemented as a computer-readable storage medium, configured with a computer program, where the storage medium so configured causes a computer system to operate in a specific and predefined manner to perform the functions described herein.

A number of embodiments of the invention have been described. Nevertheless, it will be understood that various modifications may be made without departing from the spirit and scope of the invention. For example, some of the steps described herein may be order independent, and thus can be performed in an order different from that described.

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We claim:

1. An audio matrix decoding method receiving a stereo signal pair L_t , R_t , in which method the relative amplitudes and polarities of the pair determine the reproduced direction of decoded signals, comprising
5 panning L_t and R_t to outputs associated with front directions in response to a measure of the sum of L_t and R_t being greater than a measure of the difference between L_t and R_t , and panning L_t and R_t to outputs associated with rear directions in response to a measure of the sum of L_t and R_t being less than a measure of the
10 difference between L_t and R_t , and
modifying L_t and R_t to shift the direction of reproduced signals.
2. A method according to claim 1 wherein modifying L_t and R_t to shift the direction of reproduced signals shifts signals panned to outputs associated with rear
15 directions.
3. A method according to claim 2 wherein modifying L_t and R_t to shift the direction of reproduced signals shifts signals panned to outputs associated with rear directions so as to shift signals away from the rear-center direction.
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4. A method according to claim 3 wherein signals panned to outputs associated with rear directions are shifted away from the rear-center direction in the direction in which such signals have the largest amplitude.
- 25 5. A method according to claim 3 or claim 4 wherein the degree of shifting is greatest for signals at the rear-center position, the shifting progressively decreasing for signals at directions increasingly away from the rear-center direction.
6. A method according to any one of claims 2-5 wherein modifying L_t and R_t
30 to shift the direction of reproduced signals also shifts signals panned to outputs associated with front directions.

7. A method according to claim 6 wherein modifying Lt and Rt to shift the direction of reproduced signals shifts signals panned to outputs associated with front directions so as to shift least signals at the front-center direction.

5 8. A method according to claim 7 wherein the degree of shifting is least for signals at the front-center position, the shifting progressively increasing for signals at directions increasingly away from the front-center direction.

9. A method according to any one of claims 1-8 wherein the degree of shifting
10 is based on a measure of the difference between Lt and Rt .

10. A method according to any one of claims 1-9 wherein the degree of shifting changes only when Lt and Rt are panned to outputs associated with rear directions.

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11. In an audio matrix decoding method receiving a stereo signal pair Lt, Rt , in which method the relative amplitudes and polarities of the pair determine the reproduced direction of decoded signals, a method comprising

shifting the direction of outputs associated with front and rear directions to the
20 left or right, the direction of outputs associated with rear directions being shifted to a greater degree than the direction of outputs associated with front directions, wherein said shifting includes modifying the stereo signal pair Lt, Rt by forming a difference signal of Lt and Rt signals, scaling said difference signal by a bias gain factor, and summing said scaled difference signal to both Lt and Rt signals to produce modified
25 Lt and Rt signals such that the relative amplitudes and polarities of the modified Lt and Rt pair determine the reproduced direction of decoded signals.

12. A method for modifying a stereo signal pair Lt, Rt before the signal pair is decoded by an audio matrix decoder or decoding method, the relative amplitudes and
30 polarities of the pair determining the reproduced direction of decoded signals, comprising

modifying the stereo signal pair Lt, Rt by forming a difference signal of Lt and Rt signals, scaling said difference signal by a bias gain factor, and summing said scaled difference signal to both Lt and Rt signals to produce modified Lt and Rt

signals such that the relative amplitudes and polarities of the modified L_t and R_t pair determine the reproduced direction of decoded signals.

13. Apparatus adapted to perform the methods of any one of claims 1 through
5 12.

14. A computer program, stored on a computer-readable medium for causing a computer to perform the methods of any one of claims 1 through 12.