

Description

This invention relates generally to liquid crystal (LCD) displays of the type commonly used in calculators and computers and, more particularly, to multiplexed liquid crystal displays in which many display elements or pixels are driven by each row and column signal line. The intersection of each type of signal line generates one display element or pixel which can be controlled independently of the other display elements that comprise a matrix of such display elements. Each pixel responds to the RMS voltage difference between the row and column signals to that pixel. A higher RMS voltage difference applied to a pixel results in turning that pixel on harder, thereby making it appear darker to the user.

Typically, six different voltages are used to drive a 32-way or higher multiplexed liquid crystal display. Therefore, each pixel has some RMS voltage across it at all times. Two important parameters affect the appearance to the user of the display. First, the absolute value of the RMS voltage applied to an on pixel or to an off pixel basically determines the lightness or darkness of the display. In addition, an on/off ratio or bias level is defined as the ratio of the on and off waveform voltages applied to each pixel. It is desirable to maximize the on/off ratio in order to make an off pixel appear as much different as possible from an on pixel to the user. At the same time, it is important to guarantee that an off pixel does not appear dark or on to the user, but that an on pixel does appear dark to the user. The voltages required to obtain this condition are set by the manufacturer of the liquid crystal display. The state of the art in LCD manufacturing is such that in order to meet the LCD threshold voltage specification under ideal bias conditions (maximum on/off ratio) requires a high peak voltage across the pixel. The maximum peak voltage that can be safely applied to an LCD driver chip without destroying it is specified by the chip manufacturer. In many liquid crystal display systems, the peak voltage that may be permitted is limited such that the LCD threshold voltage specification and ideal bias level cannot both be maintained. This limitation on peak voltage can be one imposed by the chip manufacturer or by the user's LCD driver circuitry. It is therefore the principal object of the present invention to provide LCD compensation, operating within a peak voltage limitation, that maximizes the bias level while at the same time meeting the LCD threshold voltage specification.

One type of prior art LCD compensation technique maintains the ideal bias level (maximum on/off ratio) without controlling the threshold voltage level. In this case, the display becomes dim as

peak voltage limitations are imposed. Another type of prior art LCD compensation technique maintains the threshold voltage specification for the LCD without controlling the on/off ratio. See for example GB-A-2 097 971. In this second case, the display contrast suffers at all times, thus making making it difficult for the user to distinguish between pixels that are off and those that are on.

The LCD compensation technique of the present invention dynamically chooses between the options of threshold voltage level and bias level in order to optimize the appearance of the display at all times. It is intended to maintain the off voltage level constant even when peak voltage must be reduced below its optimum level. This is because a plot of on reflectance versus RMS voltage shows flat reflectance at each voltage extreme but rapidly changing reflectance over small central RMS voltage changes. In accordance with the illustrated embodiment of the present invention some function of the peak voltage is fed into generation of the other voltage levels employed in the waveforms applied to the LCD row and column signal lines. A peak voltage V_H and a step voltage V_B are the starting points for derivation of all other waveform voltage levels. A reference voltage V_A is the desired voltage to be applied to the LCD based upon temperature and user's contrast setting.

Figure 1 is a block diagram of an LCD compensation circuit in accordance with the present invention.

Figure 2 is a block diagram of circuitry employed to derive all waveform voltages necessary for driving an LCD display from the peak voltage and the step voltage produced by the circuit of Figure 1.

Figure 3 is a schematic diagram of a resistor summing amplifier that implements a portion of the LCD compensation circuit of Figure 1.

Figure 4 is a waveform diagram illustrating the various signals provided by the circuits of Figures 1 and 2 as they are applied to a typical 32-way multiplexed display.

Referring now to the block diagram of Figure 1, a reference voltage V_A that represents a desired voltage to be applied to an LCD, taking into account the temperature coefficient of the LCD and the user's contrast setting, and that may be derived externally from a summation of diode voltages, is applied to a conventional summer 10. The output of summer 10 represents a step voltage V_B . The output of summer 10 is also applied to a peak voltage function generator 20. Peak voltage function generator 20 may comprise, for example, a constant voltage source or a voltage multiplier whose output is simply a multiple of the applied input voltage. The output of peak voltage function generator 20 is defined as the peak voltage V_H .

Other functions for peak voltage function generator 20 could be chosen depending on desired characteristics of the relationship between the step voltage V_B and the peak voltage V_H and may include any constraints or limits that it is desired to impose on the peak voltage V_H . As stated above, V_H represents the peak voltage applied to the LCD, based on limitations imposed by the LCD driver chip itself or the LCD display system as a whole. The safety of the LCD driver chip could be in jeopardy if an excessive peak voltage is applied or the display system as a whole may simply not be capable of supplying a peak voltage higher than a certain level.

The output of peak voltage function generator 20 is applied to a V_H feedback function generator 30, whose output may be a predefined function, such as a fractional or square root function, for example, of its input. It has been found that the fractional function 0.28 for peak voltage function generator 20 maintains the LCD off voltage relatively constant over an expected range of limitation on peak voltage V_H . Other functions may be implemented by the feedback function generator 30 based upon design parameters such as the LCD multiplexing level, the function implemented by peak voltage function generator 20, and the expected limitations on peak voltage V_H . The output of V_H feedback function generator 30 is subtracted from the reference voltage V_A in summer 10 to produce a continuously updated value of step voltage V_B .

Referring now to Figure 2, there are shown conventional summer and multiplier circuit blocks employed to combine the peak voltage V_H and the step voltage V_B supplied by the circuitry of Figure 1 to provide a number of different voltages to be switched onto the LCD row and column signal lines.

Referring now to Figure 3, there is shown a schematic diagram of a resistor summing amplifier circuit that implements the preferred functions of summer 10 and V_H feedback function generator 30 of Figure 1. In this resistor summing amplifier circuit, the step voltage $V_B = V_A(1 + RF/RH)(R2/(R1 + R2)) - V_H(RF/RH) = V_A - 0.28 V_H$.

Referring now to Figure 4, there are illustrated the various waveforms derived from the voltages supplied by the circuits of Figures 1 and 2 as they are applied to a typical 32-way multiplexed LCD display. At any point in time four voltages are employed to drive the LCD display. All rows except the selected row are driven with the row non-select voltage, while the selected row is driven by the row select voltage. Any column which has an on pixel in the current row is driven to the column select voltage level, while off columns in the current row are driven to the column non-select voltage. The

voltage seen by each pixel is the difference of its column and row voltages. As stated above, pixels respond to the RMS voltage across them. By setting the row non-select voltage halfway between the column select voltage level and the column non-select voltage level, each pixel can only see a change in its RMS voltage when its row is selected. Since pixels are turned on by higher RMS voltage, the row select and column select voltages are set at the opposite extremes of the available voltage. The voltage difference between the column select and column non-select voltage levels is what has been referred to in the description above as the step voltage V_B . One-half the ratio of the step voltage V_B to the peak voltage V_H is referred to as the LCD bias. Thus, $\text{bias} = V_B/(2 * V_H)$. For maximum on to off voltage ratio, the ideal bias for 32 rows is about 1/6.66. In effect, step voltage V_B is approximately equal to 0.3 times the peak voltage V_H .

Claims

1. A liquid crystal display compensation circuit, the circuit comprising:
reference voltage source means for supplying a desired reference voltage (V_A) to be applied to the liquid crystal display;
summer means (10) having a first summing input for receiving the reference voltage (V_A), having a second summing input, and having an output providing a step voltage (V_B);
peak voltage function generator means (20) having an input for receiving the step voltage (V_B) and having an output that provides a source of peak voltage (V_H); and
feedback function generator means (30) having an input for receiving the peak voltage (V_H) and having an output connected to the second summing input of the summer means (10), the summer means (10) being thereby operative for subtracting the output of the feedback function generator means (30) from the reference voltage (V_A) to produce a continuously updated value of step voltage (V_B).
2. A liquid crystal display compensation circuit as in claim 1 wherein the peak voltage function generator means (20) comprises a constant voltage source.
3. A liquid crystal display compensation circuit as in claim 1 wherein the peak voltage function generator means (20) comprises a voltage multiplier.
4. A liquid crystal display compensation circuit as in claim 1 wherein the output of the feedback



Other functions for peak voltage function generator 20 could be chosen depending on desired characteristics of the relationship between the step voltage V_B and the peak voltage V_H and may include any constraints or limits that it is desired to impose on the peak voltage V_H . As stated above, V_H represents the peak voltage applied to the LCD, based on limitations imposed by the LCD driver chip itself or the LCD display system as a whole. The safety of the LCD driver chip could be in jeopardy if an excessive peak voltage is applied or the display system as a whole may simply not be capable of supplying a peak voltage higher than a certain level.

The output of peak voltage function generator 20 is applied to a V_H feedback function generator 30, whose output may be a predefined function, such as a fractional or square root function, for example, of its input. It has been found that the fractional function 0.28 for peak voltage function generator 20 maintains the LCD off voltage relatively constant over an expected range of limitation on peak voltage V_H . Other functions may be implemented by the feedback function generator 30 based upon design parameters such as the LCD multiplexing level, the function implemented by peak voltage function generator 20, and the expected limitations on peak voltage V_H . The output of V_H feedback function generator 30 is subtracted from the reference voltage V_A in summer 10 to produce a continuously updated value of step voltage V_B .

Referring now to Figure 2, there are shown conventional summer and multiplier circuit blocks employed to combine the peak voltage V_H and the step voltage V_B supplied by the circuitry of Figure 1 to provide a number of different voltages to be switched onto the LCD row and column signal lines.

Referring now to Figure 3, there is shown a schematic diagram of a resistor summing amplifier circuit that implements the preferred functions of summer 10 and V_H feedback function generator 30 of Figure 1. In this resistor summing amplifier circuit, the step voltage $V_B = V_A(1 + R_F/R_H)(R_2/(R_1 + R_2)) - V_H(R_F/R_H) = V_A - 0.28 V_H$.

Referring now to Figure 4, there are illustrated the various waveforms derived from the voltages supplied by the circuits of Figures 1 and 2 as they are applied to a typical 32-way multiplexed LCD display. At any point in time four voltages are employed to drive the LCD display. All rows except the selected row are driven with the row non-select voltage, while the selected row is driven by the row select voltage. Any column which has an on pixel in the current row is driven to the column select voltage level, while off columns in the current row are driven to the column non-select voltage. The

voltage seen by each pixel is the difference of its column and row voltages. As stated above, pixels respond to the RMS voltage across them. By setting the row non-select voltage halfway between the column select voltage level and the column non-select voltage level, each pixel can only see a change in its RMS voltage when its row is selected. Since pixels are turned on by higher RMS voltage, the row select and column select voltages are set at the opposite extremes of the available voltage. The voltage difference between the column select and column non-select voltage levels is what has been referred to in the description above as the step voltage V_B . One-half the ratio of the step voltage V_B to the peak voltage V_H is referred to as the LCD bias. Thus, $\text{bias} = V_B/(2 \cdot V_H)$. For maximum on to off voltage ratio, the ideal bias for 32 rows is about 1/6.66. In effect, step voltage V_B is approximately equal to 0.3 times the peak voltage V_H .

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reference voltage source means for supplying a desired reference voltage (V_A) to be applied to the liquid crystal display;

summer means (10) having a first summing input for receiving the reference voltage (V_A), having a second summing input, and having an output providing a step voltage (V_B);

peak voltage function generator means (20) having an input for receiving the step voltage (V_B) and having an output that provides a source of peak voltage (V_H); and

feedback function generator means (30) having an input for receiving the peak voltage (V_H) and having an output connected to the second summing input of the summer means (10), the summer means (10) being thereby operative for subtracting the output of the feedback function generator means (30) from the reference voltage (V_A) to produce a continuously updated value of step voltage (V_B).

2. A liquid crystal display compensation circuit as in claim 1 wherein the peak voltage function generator means (20) comprises a constant voltage source.

3. A liquid crystal display compensation circuit as in claim 1 wherein the peak voltage function generator means (20) comprises a voltage multiplier.

4. A liquid crystal display compensation circuit as in claim 1 wherein the output of the feedback



function generator means (30) is a defined fractional function of its input.

A liquid crystal display compensation circuit as in claim 4 wherein the defined fractional function is equal to 0.28.

6. A liquid crystal display compensation circuit as in claim 1 wherein the output of the feedback function generator means (30) is a defined square root function of its input.

7. A liquid crystal display compensation circuit as in claim 1 wherein the output of the feedback function generator means (30) is related to its input by a multiple of 0.28.

8. A liquid crystal display compensation circuit as in claim 1 wherein the summer means (10) and the feedback function generator means (30) comprise a resistor summing amplifier.

Patentansprüche

1. Flüssigkristallanzeigekompensationsschaltkreis, wobei der Schaltkreis umfaßt:
 - eine Referenzspannungsquelle zum Liefern einer gewünschten Referenzspannung (V_A) zum Anlegen an die Flüssigkristallanzeige,
 - eine Summationseinrichtung (10) mit einem ersten Summiereingang zur Aufnahme der Referenzspannung (V_A), mit einem zweiten Summiereingang und mit einem Ausgang, der eine Stufenspannung (V_B) liefert,
 - eine Spitzenspannungsfunktionserzeugungseinrichtung (20) mit einem Eingang zur Aufnahme der Stufenspannung (V_B) und mit einem Ausgang, der eine Quelle von Spitzenspannung (V_H) bildet und
 - eine Feedbackfunktionserzeugungseinrichtung (30) mit einem Eingang zur Aufnahme der Spitzenspannung (V_H) und mit einem Ausgang, der mit dem zweiten Summiereingang der Summationseinrichtung (10) verbunden ist, wobei die Summationseinrichtung (10) dadurch so wirkt, daß der Ausgang der Feedbackfunktionserzeugungseinrichtung (30) von der Referenzspannung (V_A) abgezogen wird, um einen kontinuierlich aktualisierten Wert der Stufenspannung (V_B) zu erzeugen.
2. Flüssigkristallanzeigekompensationsschaltkreis nach Anspruch 1,

wobei die Spitzenspannungsfunktionserzeugungseinrichtung (20) eine Konstantspannungsquelle umfaßt.

3. Flüssigkristallanzeigekompensationsschaltkreis nach Anspruch 1, wobei die Spitzenspannungsfunktionserzeugungseinrichtung (20) einen Spannungsvervielfacher umfaßt.
4. Flüssigkristallanzeigekompensationsschaltkreis nach Anspruch 1, wobei der Ausgang der Feedbackfunktionserzeugungseinrichtung (30) ein Bruchteil ihres Eingangs ist.
5. Flüssigkristallanzeigekompensationsschaltkreis nach Anspruch 4, wobei der Bruchteil gleich 0,28 ist.
6. Flüssigkristallanzeigekompensationsschaltkreis nach Anspruch 1, wobei der Ausgang der Feedbackfunktionserzeugungseinrichtung (30) eine festgelegte Quadratwurzelfunktion ihres Eingangs ist.
7. Flüssigkristallanzeigekompensationsschaltkreis nach Anspruch 1, wobei der Ausgang der Feedbackfunktionserzeugungseinrichtung (30) über ein Vielfaches von 0,28 mit seinem Eingang in Relation steht.
8. Flüssigkristallanzeigekompensationsschaltkreis nach Anspruch 1, wobei die Summationseinrichtung (10) und die Feedbackfunktionserzeugungseinrichtung (30) einen Widerstands-Summierversärker umfassen.

Revendications

1. Un circuit de compensation pour affichage à cristaux liquides, le circuit comprenant :
 - un moyen formant source de tension de référence pour produire une tension de référence désirée (V_A) à appliquer à l'affichage à cristaux liquides ;
 - un moyen formant sommateur (10) comportant une première entrée de sommation pour recevoir la tension de référence (V_A), comportant une seconde entrée de sommation et comportant une sortie produisant une tension différentielle (V_B) ;
 - un moyen formant générateur de fonction de tension de crête (20) comportant une entrée pour recevoir la tension différentielle (V_B) et comportant une sortie qui constitue une source de tension de crête



(V_H) ; et

- un moyen formant générateur de fonction de réaction (30) comportant une entrée pour recevoir la tension de crête (V_H) et comportant une sortie reliée à la seconde entrée de sommation du moyen de sommation (10), le moyen de sommation (10) opérant alors pour soustraire la tension de sortie du moyen formant générateur de fonction de réaction (30) de la tension de référence (V_A) afin de produire une valeur, mise à jour en continu, de la tension différentielle (V_B).
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- 2. Un circuit de compensation pour affichage à cristaux liquides selon la revendication 1, dans lequel le moyen formant générateur de fonction de tension de crête (20) comprend une source de tension constante.
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- 3. Un circuit de compensation pour affichage à cristaux liquides selon la revendication 1, dans lequel le moyen formant générateur de fonction de tension de crête (20) comprend un multiplicateur de tension.
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- 4. Un circuit de compensation pour affichage à cristaux liquides selon la revendication 1, dans lequel le signal de sortie du moyen formant générateur de fonction de réaction (30) est une fonction fractionnaire définie de son signal d'entrée.
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- 5. Un circuit de compensation pour affichage à cristaux liquides selon la revendication 4, dans lequel la fonction fractionnaire définie est égale à 0,28.
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- 6. Un circuit de compensation pour affichage à cristaux liquides selon la revendication 1, dans lequel le signal de sortie du moyen formant générateur de fonction de réaction (30) est une fonction de racine carrée définie de son signal d'entrée.
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- 7. Un circuit de compensation pour affichage à cristaux liquides selon la revendication 1, dans lequel le signal de sortie du moyen formant générateur de fonction de réaction (30) est lié à son signal d'entrée par un multiple de 0,28.
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- 8. Un circuit de compensation pour affichage à cristaux liquides selon la revendication 1, dans lequel le moyen de sommation (10) et le moyen formant générateur de fonction de réaction (30) comprennent un amplification de sommation à résistances.
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