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TITLE OF INVENTION

REPLACED SHEETS	SG
✓ Description : paged ...1... to paged ...3...	
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RECEIPT	

Dies for extrusion moulding.

FIELD TO WHICH THE INVENTION BELONG

This invention relates to dies for an extrusion moulding, especially for dies for an extrusion moulding of a resin bound type magnet.

PRIOR ARTS

In general, a resin bound type magnet is produced by a process shown in Figure 6, ie:

A magnetic powder and an organic resin (thermosetting or thermoplastic resin) of suitable particle sizes are sufficiently mixed. If necessary, additives are added. The mixed raw materials are kneaded by a kneading machine such as a roller mill or an extrusion kneader, etc. with heating above a temperature at which the organic resin is molten. The kneaded raw material is roughly crushed into particles having

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particle sizes of around 1-10mm, and is charged into an extrusion moulding machine.

The charged magnet raw material is heated in the extrusion moulding machine to make it in a fluidized state, and is sent into a die equipped at a front end of a cylinder by screw or plunger.

The magnet raw material is moulded in a predetermined shape such as cylinder, thin plate, bar, etc. by passing through the said die. However, the moulding processes of an isotropic magnet and an anisotropic magnet are different.

Namely, in case of the anisotropic magnet, an axis of easy magnetization of the magnetic powder in the raw material is uniformed to the magnetic field direction ie the magnetic powder is orientated, by passing the magnetic raw material through a die to which the magnetic field is charged, and it is moulded. In the process, it is common to charge the magnetic field by a combination of an electromagnetic coil and a magnetic circuit comprising a magnetic material.

On the other hand, the isotropic magnet is moulded by the extrusion without charging the magnetic field. The moulded body is cooled near the outlet of the front end of the die, then it is picked up by a receiving machine located in front of the extrusion moulding machine, and it is cut into a suitable length by a cutter.

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Because the magnetism remains in the moulded body in case of the moulding with an orientation of the magnetic powder, it is subjected to a demagnetization to remove it. Further in case that the thermosetting resin is used as a binder, the moulded body is subjected to a curing process to cure the resin after its demagnetization, and the resin bound type magnet by an extrusion moulding is produced.

In these magnet productions, the die, which is used for an extrusion moulding in a magnetic field (ie it is used for a moulding of the anisotropic magnet), has a structure which is a combination of a magnetic material and a non-magnetic material, and they are disclosed in Japan Patent Laid-Open Sho 58-219705, Japan Patent Laid-Open Sho 60-100413, etc. as the prior arts.

For example, in the Japan Patent Laid-Open Sho 58-219705, a die structure shown in Figure 7 is disclosed.

In the die of Figure 7, a raw material injection outer die 201, a mandral 203, and a front end of the moulding section outer die 202 comprise magnetic materials and the rest of the moulding section outer die 202 comprises a non-magnetic material. It is constituted that an electromagnetic coil 204 is coiled around the moulding section outer die 202, and further a magnetic material bloc 205 is positioned around the electromagnetic coil 204.

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Toward to this die, the inventor of this application, etc disclosed a die structure as shown in Figure 8 by Japan Patent Laid-Open Sho 63-254713.

The die is constituted by a outer die comprising a raw material injection outer die 201 and moulding section outer dies 202a and 202b, and mandrels 203a and 203b. The raw material injection outer die 201 consists of a non-magnetic material, and the moulding section outer die 202a also consists of a non-magnetic material, but it is equipped with the moulding section outer die 202b made of a magnetic material to induce magnetic flux to the front end of the outer die.

The mandrel 203a also consists of a non-magnetic material, and at its front end of the mandrel, the mandrel 203b made of a magnetic material is equipped.

The electromagnetic coil 204 is installed at the outside of the die. When a current is passed through the electromagnetic coil 204, a radiated magnetic field is charged at a space (hereinafter called as an orientation section) between the front end of the mandrel 203b and the front end of the moulding section outer die 202b because the generated magnetic flux tends to pass through in a magnetic material with a high magnetic permeability.

A magnet raw material passes through the raw material injection section 206 and a raw material packing space 207 and it is moulded



in a cylindrical form by an extrusion with a progress of a radiatedly orientation of the magnet powder in the orientation section.

Today, (1) a press moulding, (2) an injection moulding and (3) an extrusion moulding are available for a resin bound type radial magnet.

Among them, the press moulding and the injection moulding are currently utilized for mass-production processes. On the contrary, though the extrusion moulding is widely applied for a moulding of a ferrite magnet, it is still in a stage not to be utilized in a mass-production of a high performance rare earth magnet, and the die for the extrusion moulding, especially a structure of the orientation section in the die has not be sufficiently considered.

OBJECTIVES OF THE INVENTION

It is important to have a sufficient consideration on the structure of the orientation section of a die for the extrusion moulding because it largely influences a magnetic performance of the moulded magnet.

In either the die or the machine of the extrusion moulding for a resin bound type magnet, coventionally used, no attention has not been paid on a material and a structure of the orientation section of the die, and it was generally made by a single body of a magnetic material. Therefore it has problems listed below.

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Namely, in case that a resin bound type magnet is moulded by an extrusion, a magnetic field is charged, when a mixture comprising a magnetic powder and a thermosetting or thermoplastic resin becomes a molten state by heating, to orientate the magnetic powder, and it is necessary to carry out a solidification by cooling after the moulding in the orientation section not to disorder the orientation and the moulded shape.

In order to achieve a sufficient orientation of the magnetic powder, it is preferable that a viscosity of the resin should be as low as possible as soon as it enters the orientation section, ie its temperature should be as high as possible. On the contrary, when the magnet orientated and moulded comes out from the die, it is preferable that its temperature is as low as possible to get a sufficient solidification by cooling in the orientation section not to disorder the orientation and the moulded shape.

Accordingly a temperature gradient is required in the orientation section. If the temperature gradient is not sufficiently taken in the orientation section for the solidification by cooling and the temperature of the whole orientation section drops, it results an insufficient orientation, and adversely if the temperature of the whole orientation section rises, the orientation and the moulded shape are disordered when the magnet comes out from the die.

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However, in case that the orientation section comprises a single body of a magnetic material, it is difficult to take the temperature gradient because of the property of the material and the structure of the orientation section, and in order to take the temperature gradient in the single metal body, it is necessary to equip a heater and a cooler with a high capacity resulting an extreme inefficiency.

Further, in case of a cylindrical magnet with anisotropy radiatedly toward its diameter direction (hereinafter called as a radial anisotropic magnet), the sufficiency of its radial anisotropic property depends on a shape and a size of the magnet. As an index to show the above, a radial factor f_R is given by the following equation.

$$f_R = 2 Dh/d^2$$

where D = Outer diameter of a ring shaped magnet moulded

h = Height of a ring shaped magnet moulded

and the radial factor can be classified into following categories.

$f_R < 1$	Sufficient radial achievable
$f_R = 1-2$	Insufficient
$f_R > 1$	Isotropic

The f_R is the first index to consider at designing of a die when a radial magnetic field moulding by a pressing or an injection is practiced.

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Namely, if the die structure satisfies $fR < 1$, a sufficient radial magnetic field can be charged at a cavity and thus it is possible to mould a magnet with a sufficient radial anisotropic property.

However when a die of $fR \geq 1$ is designed, it is not attainable to mould a magnet with a sufficient radial orientation.

Therefore there is an important index for the designing of a die for a radial magnetic field moulding by a pressing or an injection.

However in case of an extrusion moulding, since a shape of a moulded magnet and a die for the extrusion moulding do not coincide, and thus it is difficult to use fR as it is for designing of a die for the extrusion moulding.

As described above, when a resin bound type magnet is moulded by an extrusion, a mixture of a magnetic powder and a thermosetting or a thermoplastic resin is heated, a magnetic powder is orientated by charging a magnetic field as it becomes a molten state, and a solidification by cooling after the moulding should be performed in the orientation section not to disorder the orientation and the moulded shape.

In order to achieve a sufficient orientation of the magnetic powder, the temperature gradient in the orientation is required as described above. To get the temperature gradient in the orientation section, there are below-listed methods.

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- (1) Increasing the length of the orientation section,
- (2) Inserting a material with a low thermal conductivity into the orientation section and
- (3) Heating and cooling of both ends of the orientation section with extremely strong heater and cooler.

Among them, as to (1) the length of the orientation section, there is a limitation of the length of the orientation section because of an impossibility of a sufficient orientation magnetic field if it becomes too long, and as to (2), a material of low thermal conductivity is in general a non-magnetic material, and thus the magnetic field in the orientation is disordered unless the material inserted is thin.

Accordingly both of (1) and (2), though it may be possible to attain the temperature gradient with a reduction of the capacities of the heater and the cooler, still require a strong heater and cooler to get the temperature gradient as same to (3) in a certain degree.

However if a strong heater with an additional capacity is used, not only the orientation section, but also the whole of the die is heated resulting an temperature elevation of the whole of the die except for the front end of the die. Therefore a compound, which is heated to have a fluidity in the extrusion machine, is further heated in the die, in case that a resin in the compound is a thermosetting resin, it starts to cure in the die, and case of a thermoplastic resin, a thermal decomposition is initiated resulting



changes by time such as an increase of viscosity of the compound while it is in the extrusion moulding process, etc. They lead to a problem that a long time stable operation of the extrusion moulding is not achieved.

This invention aims to solve the problems of the die for an extrusion moulding of a resin bound type magnet as discussed above, and to provide a die for the extrusion moulding to mould a resin bound type magnet with a high performance and a superior shape accuracy.

Further, this invention provides a die for an extrusion moulding to produce a high performance resin bound type radial magnet and to produce a long size radial magnet which does not satisfy $FR < 1$.

Furthermore, this invention aims to provide a die for an extrusion moulding, by which a long time stable extrusion moulding can be operated by preventing the changes of a resin and a magnetic powder by time during the extrusion and by stabilizing the magnetic performance of a magnet to be moulded with a superior mass production capability as well.

EXPLANATION OF FIGURES

Figure 1-3 show outline drawings of dies for an extrusion moulding used in Examples of this invention.



Figure 4 shows a graph to exhibit a viscosity change of the compound by time.

Figure 5 (a) and (b) show graphs to exhibit a change of the magnetic performance when a die of Example 6 is used.

Figure 6 is a process outline of a magnet.

Figure 7 and 8 are outline drawings of dies for the conventional extrusion moulding.

SUMMARY OF THE INVENTION

This invention is a die for an extrusion moulding of a resin bound type magnet which is moulded by an orientation of a molten mixture of a magnetic powder and a resin and by a solidification with cooling, wherein an orientation section, which is from an orientating section of the said magnetic powder at the front end of the said die by charging a magnetic field to the die section, is formed by a layer structure comprising at least one or more of different materials.

It is a die for an extrusion moulding wherein at least one or more of the materials of the orientation section comprises magnetic material(s).

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Further, it is a die for an extrusion moulding wherein the layer structure is formed by inserting a low thermal conductivity material of which the thermal conductivity K (20°C) is

$$K \leq 0.01 \text{ [cal/cm}\cdot\text{sec}\cdot^{\circ}\text{C]}$$

into a partial section of the said orientation section.

Further, it is a die for an extrusion moulding wherein the material of the insertion into the orientation section of the said die for an extrusion moulding comprises a non-magnetic material and the thickness of the said non-magnetic material is $1/2$ or less of the contact section length of the molten mixture in the orientation section.

Furthermore the said die for an extrusion moulding is applied for a cylindrical resin bound type magnet.

Also this invention is a die for an extrusion moulding for a production of the aforementioned cylindrical resin bound type magnet, wherein the contact section length l of the orientation section with a molten mixture from a section from which the orientation of the aforementioned magnetic powder starts by charging a magnetic field at the front end of the said die to the outlet section of the die satisfies

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$$l < d^2 / 2D.$$

(d and D are inner and outer diameters of the molten mixture passage, respectively)

Further in case that a non-magnetic material is present in the orientation section of the aforementioned die for an extrusion moulding, it is a die for an extrusion moulding wherein a total length l' of the contact section length of the magnetic material with a mixture of a magnetic powder and a resin in a molten state satisfies

$$l' < d^2 / 2D.$$

Furthermore it is a die for an extrusion moulding wherein the aforementioned magnetic powder comprises a ferromagnetic material consisting of rare earth elements (including Y) and transition metals mainly constituting cobalt, or a ferromagnetic material consisting of rare earth element, transition metals mainly constituting iron and boron.

Further this invention is a die for an extrusion moulding of a resin bound type magnet which is moulded by an orientation of a molten mixture of a magnetic powder and a resin, and by a solidification with cooling wherein the structure of the said die is constituted in orders from a connection section of an extrusion machine to an outlet of the orientation section as

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(a) A converging section where a mixture of a magnetic powder and a resin which is in a molten state with a fluidity is pressed into the final shape.

(b) A heat-insulating section to hold a temperature difference between the whole of the die and a rear section

(c) A heating section by which the viscosity of the molten compound of the mixture in a molten state is further reduced.

(d) An orientating section in which a magnetic field is charged, the magnetic powder is orientated and it is solidified with cooling as its state.

This invention has effects to improve the performance of the moulded magnet and also to reform the dimensional accuracy as it is clear from the aftermentioned Examples as a result of formation of an temperature gradient in the orientation section, by forming a layer structure with at least one or more of different materials and by making at least one or more of materials of the said orientation section with magnetic materials, which is from the front end of the die at which the orientation of a magnetic powder starts to an outlet section of the die for an extrusion moulding of a resin bound type magnet which is moulded by orientating a molten mixture of a magnetic powder and a resin, and by a solidification with cooling.

Also in this invention, as one alternative case of the layer structure in the orientation section, when a material with a low thermal conductivity having the thermal conductivity K (20°C) of

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$K \leq 0.01$ [cal/cm·sec·°C] is inserted, the thermal conductivity at the insertion section drops approximately 1/10 or less because a material generally used for the die has the thermal conductivity of approximately 0.07-0.08 [cal/cm·sec·°C].

If a heat passing through the orientation section is constant, a temperature difference is able to be attained by the below listed equation by reducing the thermal conductivity.

$$Q = A \cdot K (T_1 - T_2) / l$$

Q : heat capacity, A: area, l: thickness

$T_1 - T_2 = \Delta T$: temperature difference

Further, in case that the insertion material in the orientation section comprises a non-magnetic material, the magnetic performance remarkably deteriorates if it is 1/2 or more of the length of the orientation section, in spite of a high temperature difference. This was due to an disorder of the magnetic field in the orientation section by insertion of a non-magnetic material in the orientation section. Although the temperature difference drops when a non-magnetic layer becomes thin, the magnetic performance is somewhat improved because of a reduction of the disorder of the magnetic field in the orientation section. Therefore it is preferable that the thickness of the non-magnetic layer is as thin as possible to take a sufficient temperature gradient, and when a

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non-magnetic material is inserted, it is preferable that its length is $1/2$ or less of the length of the orientation section.

Moreover by this invention, when the contact section length l of the orientation section of the die for an extrusion with the molten mixture is limited as $l < d^2 < 2D$, the magnetic performance is improved because of an availability of a sufficient orientation of the magnetic powder.

Further by arranging the composition of the die structure from the connecting section of an extrusion machine to the outlet of the orientation section in order of a converging section, a heat insulating section, a heating section and an orientating section, it is able to operate a stable extrusion moulding over a long time resulting effects such as a suitability for a mass production, etc.

According to this invention,

(1) It is able to take a temperature gradient in the orientation section by forming a layer structure for the orientation section, and therefore the degree of the orientation of a magnet is improved and the dimensional accuracy is also reformed.

(2) It is able to take a further high temperature gradient in the orientation section, by inserting a magnetic material of its thermal conductivity of 0.01 [cal/cm·sec·°C] or less or a non-magnetic material which has a thermal conductivity of 0.01 [cal/cm·sec·°C] or less having a length not more than $1/2$ of the length of the

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orientation section, into a partial section of the orientation section, and therefore it is able to mould a high performance anisotropic resin bound type magnet by an extrusion moulding.

(3) In case that a non-magnetic material is not present in the orientation section, by making the length l of the orientation section as

$$l < d^2 / (2D)$$

and in case that a non-magnetic material is present, by making the length l'

$$l' < d^2 / (2D)$$

it is able to mould a high performance resin bound type radial magnet with a sufficient radial orientation and to achieve prolongation of this magnet.

(4) By constituting a structure of the die, as shown in Figure 3, in order from a connecting section of an extrusion machine as a converging section, a heat insulating section, a heating section and an orientating section, it is able to operate an extrusion moulding with a stable magnetic performance for a long time, and a stable mass production is achievable.

This invention is hereafter explained by using Examples.



EXAMPLE 1

Figure 1 shows an outline drawing of a die for an extrusion moulding used in Example 1.

In Figure, 108 is the orientation section, 109 is a surface of the outlet of the orientation section, X and Y are temperature measurement points, and an explanation of other numbers is omitted because they are described in below.

A die for an extrusion moulding for a practice of this invention is constituted, as shown in Figure 1 by a outer die comprising a raw material injection outer die 101 and moulding section outer dies 102a and 102b, and mandrels 103a and 103b, the raw material injection outer die 101 and the moulding section outer die 102a are composed of non-magnetic materials, and the moulding section outer die 102b of a magnetic material is equipped at the front end of the outer die to induce a magnetic flux. Further the mandrel 103a comprises a non-magnetic material, and at its front end the mandrel 103b consisting of a magnetic material is equipped by a connection screw 105.

Further an electromagnetic coil 104 is installed at the outside of the die, and when a current passes through the electromagnetic coil, a radiated magnetic field is charged at the orientation section 108 between the front end of the mandrel 103b and the front end of the moulding section outer die 102b because the generated magnetic flux



tends to pass through a magnetic material with a high magnetic permeability.

Next, for a production of a magnet, a magnetic powder is mixed with an organic resin such as a thermosetting or a thermoplastic resin and when it is required with additives by a mixer.

The mixture of the magnetic powder and the resin is heated in an extrusion machine, and it becomes in a molten state. Then it, as in this state, is sent to the raw material injection section 106 of the die for an extrusion moulding.

The molten material of the magnetic powder and the resin poured is gradually converged while it is being passed through the raw materials packing space 107 in the die to mould the final shape. The magnetic powder is orientated in the orientation section 108, and it is moulded as its state by a solidification with cooling in the orientation section 108.

Next in Table 1, results of measurements of temperature difference between X and Y points in the orientation section 108 are shown when the orientation section 108 is formed by a layer structure with materials selecting from at least one or more of several materials, namely,

SKD 61 : JIS G 4404 specification, steel material

SKD 11 : JIS G 4404 specification, steel material

SiO₂ : oxide of silicon

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PES : polyethersulphone resin

for the structure of the orientation section of a die for an extrusion moulding.

The total length of the orientation section 108, by the way is, 6mm, and the temperature differences represent temperature differences between X and Y points which are 0.5mm from the both ends of the orientation section 108, respectively and are 3mm outside from the passage of a molten mixture of the magnetic powder and the resin. (In the measurement, the temperature at Y point was fixed at 50°C)

A heater with 800W capacity was used for heating, and a cooling plate by a water cooling was installed at the surface of the outlet of the orientation section 109 for cooling to cool the orientation section 108.

The structure column in Table 1 shows materials used for the front end structure, and among them, SKD 61 and SKD 11 are magnetic materials and the remainders SiO_2 and PES are non-magnetic materials.

Further the length of each layer is $6/A$ [mm]. (A means numbers of the layer.)

As shown in Table 1, in case of Comparative Test in which the orientation section was formed by a single metal, a temperature difference of only 20°C was obtained with the aforementioned system.

Although it was the same material, the temperature gradient was however able to get by forming the layer structure.

This was because that the contact surface resisted the heat transfer by forming the layer structure. This was also proved by Test 1 and Test 4.

Further as it was understood from Test 3, 5 and 6, a further high temperature gradient was attainable by using a material of the low thermal conductivity for a partial section of the orientation section.

However, in this case, since a magnetic material has, in general, high thermal conductivity, a non-magnetic material becomes suitable for the aforementioned material and it is unfavourable to get the magnetic field.

Next Table 1 also shows magnetic performance of magnets moulded by the dies having their structures as described above.

The magnets were produced by following process.

For the magnets produced here, a magnetic alloy of its coercive force at approximately 7 KOe having a basic magnetic powder composition of Sm (Co 0.672 Cu 0.08 Fe 0.22 Zr 0.028) 8.35 was crushed into particles of the average particle size of approximately 20 μm , and they were mixed with a resin. A ratio of the magnetic



powder and the resin was the magnetic powder 60 vol % and the resin 40 vol %.

A thermosetting resin mainly comprising an epoxy resin was used as the organic resin.

The aforementioned mixture was kneaded by a roller mill, a compound was prepared, then the compound was coarsely crushed, and it was charged in a screw type extrusion machine. The crushed compound was heated in the extrusion machine.

The thermosetting resin mainly comprising the epoxy resin had its thermoplastic region at approximately 100 - 150°C at which the viscosity remarkably dropped, the mixture of the magnetic powder and the resin made in a molten state in this temperature region, it was pushed into a die by the screw, and a magnet was extruded from the die by a solidification with cooling after orientating the magnetic powder in the orientation section at the front end of the die. The shape of the moulded magnet was a ring shaped with the outer diameter 32.8 mm and the inner diameter 31.8 mm.

In this Example, the magnetic performance was measured by using an uncured state magnet moulded in a molten state.

As it is clear from Table 1, the moulded magnet showed an improved performance in case a die structure by which the temperature

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gradient was secured, and it was also confirmed that the dimension accuracy was improved by having the temperature gradient as well.

Table 1

Code	Structure	Temp	Magnetic Property		Dimension
			difference	Br[KG] (BH) [MGOe] max	
Test 1	SKD61/SKD61	30°C	5.54	6.3	C
" 2	SKD61/SKD11	35°C	5.60	6.5	C
" 3	SKD61/SiO ₂	70°C	5.62	6.5	B
" 4	SKD61/SKD11/SKD61	40°C	5.95	7.0	C
" 5	SKD61/SiO ₂ /SKD61	100°C	6.15	8.0	A
" 6	SKD61/PES/SKD61	150°C	6.30	8.5	A
Comparative					
Test 1	SKD61	20°C	5.36	6.0	D

A... excellent

C... fair

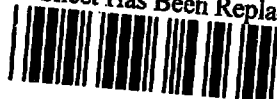
B... good

D... bad

EXAMPLE 2

Figure 2 shows an outline drawing of a die for an extrusion moulding used in Example 2.

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In Figure, 102c shows a moulding section outer die comprising a material of a low thermal conductivity, a distance between a-b shows a length of an orientation section 108, and an explanation of the other figures is omitted because they are same to Figure 1.

A die for an extrusion moulding for a practice of this invention is a die which possesses similar structure and effect as Figure 1 except that a different material is inserted in the centre of the orientation section 108, and the orientation section 108 at the inner part of the die has a structure divided into 3 layers ie A, B and C as shown in Figure 2. In this case, layer B was a material of the inserted layer, and a same material ie SKS2 was used for layer A and layer C. SKS2 is a steel material specified by JIS G 4404 standard.

A temperature difference in the orientation section 108 showed a temperature difference between X and Y points shown as temperature measuring points in Figure 2.

The temperature differences between X-Y, when several materials were used for the layer B material inserted, are shown in Table 2. The length of the orientation section [a distance between a-b in Figure 2] was 6mm, and all the lengths of every layer were 2mm.

As to Comparative Test 2, it was an example by using a die of which the orientation layer was not constituted by the layer structure as shown in Figure 8.



As same to Example 1, a heater with 800W capacity was used for heating, and as for cooling, a surface of the outlet of the die in layer C 109 was cooled by water and the temperature at Y point was kept at 60°C.

Next, cylindrical magnets of the outer diameter 30mm and the inner diameter 28mm were moulded in same basic composition and procedure as Example 1, by using the aforementioned die, and magnetic performance of their magnets was compared.

In Table 2, the temperature difference between X and Y in the orientation section 108 and the magnetic performance of the magnet prepared are shown when the orientation section 108 was formed by using a material as an inserting material selecting from,

PES : polyestersulphone resin

PEEK : polyetheretherketone resin

ZrO₂ : oxide of zirconium

YHD50 : steel material (a Hitachi Metal Product) and

SKD61 : steel material specified by JIS G 4404

which had different thermal conductivities,

Test 7-11 and Comparative Test 2 were cases when a resin mainly comprising an epoxy resin was used, and the extrusion condition was that the extrusion was made by keeping the temperature at Y point at 60°C as described above. The temperature was a temperature that the resin used was solidified, and the shape of the moulded magnet did not deform.

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On the other hand, for Test 8a-11a and Comparative Test 2a, a polyamide resin (Nylon 12) was used, and in this case, the extrusion was made by keeping the temperature at Y point at 160°C.

An example, which corresponds to Test 7 ie PES is used as a material to make the inserted layer, is not shown in Table 2, and this is due to an impossibility of the application because of a poor heat resistance of PES.

As shown in Table 2, the cases, in which materials of low thermal conductivity were inserted, uniformly exhibited better magnetic performance than Comparative Test 2 and 2a in which the orientation section was formed by only a single metal SKD61. However when the material inserted has the thermal conductivity (at 20°C) above 0.01 [cal/cm·sec·°C], the improvement on the magnetic performance is slight, and it is preferable to insert a material having the thermal conductivity of 0.01 [cal/cm·sec·°C] or less.

Table 2

Code	Material Inserted	Thermal Conductivity [cal/cm·sec·°C]	Temp Difference [°C]	Magnetic Performance	
				Br[KG] (BH) max	[MGOe]
Test 7	PES	4.54×10^4	105	6.30	8.5
-	-	-	-	-	-
8	PEEK	5.97×10^4	100	6.28	8.4

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" 8a	"	"		6.27	8.4
" 9	ZrO ₂	0.007	80	6.18	8.1
" 9a	"	"		6.15	8.0
" 10	YHD50	0.038	40	5.65	6.6
" 10a	"	"		5.57	6.4
" 11	SKD61	0.073	30	5.60	6.4
" 11a	"	"		5.50	6.3
Comparative					
Test 2	-	0.073	25	5.36	6.0
" 2a	-	"		5.34	6.0

EXAMPLE 3

Next, an effect to a magnet, when a thickness of a non-magnetic material to be inserted in the orientation section in Figure 1 was varied, was investigated.

PEEK was used as the material to be inserted, the length of the orientation section including the thickness of PEEK was always kept at 6mm, layer A and layer C were made as the same length, and a cooling capacity was adjusted to make the temperature at Y point always at 160°C. Further as for a resin to be mixed with a magnetic powder, polyamide resin (Nylon 12) was used, and a moulding process and a shape of the moulded magnet were same as the aforementioned Example 2.

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In Table 3, temperature difference between X-Y and magnetic performance are shown when the thickness of layer B was varied from 0.5 to 3.5mm. (Test 12-16).

As it is clear from Table 3, the temperature difference is saturated at the PEEK thickness of 2mm with the heater capacity used. Since the thermal conductivity of PEEK is extremely low, a temperature difference of around 80°C is attained even at the PEEK thickness of 0.5mm.

Further as understood from Table 3, when the PEEK thickness becomes 3mm (1/2 of the length of the orientation section) or more, the magnetic property drops remarkably, though the temperature difference between X - Y is large. This is due to a disorder of a magnetic field in the orientation section by entering a non-magnetic material into the orientation section. Similarly even when the PEEK thickness is 1mm or less, it is seen that the magnetic performance is somewhat improved in spite of a reduced temperature difference.

Although the temperature difference drops if the thickness of a non-magnetic layer becomes thin, it is observed that the magnetic performance is somewhat improved because of a decrease of the disorder of the magnetic field in the orientation section.

Basing on these observations, it is preferable that the non-magnetic layer should be as thin as possible if it is able to secure a sufficient temperature difference, and from the results of Table 3,

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it is preferable that it is $1/2$ or less of the length of the orientation length when a non-magnetic material is inserted.

Table 3

	Thickness of Layer B [mm]	Temperature Difference [°C]	Magnetic Property Br [KG] (BH) [MGoe] max	
Test 12	3.5	105	5.54	6.3
" 13	3.0	102	5.95	7.0
" 14	2.0	100	6.28	8.4
" 15	1.0	92	6.32	8.5
" 16	0.5	85	6.30	8.5

EXAMPLE 4

Next, in a die for an extrusion shown in Figure 1, the length of the orientation section 108 of the die was varied, and magnets were produced by an extrusion moulding as similar to Example 1.

In this example, the magnetic powder and the polyamide resin were however mixed to make a volume ratio of the magnetic powder and the resin as 3:2. The magnetic field was made by charging a 200A current to a 123 turn coil, and the shape of the moulded magnet by an extrusion was a cylindrical with the outer diameter 30mm and the inner diameter 28mm.

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The magnetic fields for the orientation at the orientation section when the length of the orientation section 108 was varied, are shown in Table 4 together with the magnetic property of the magnets extruded.

In this example, as to the temperature of the orientation section X and Y points, a heating and cooling was applied from both ends of the orientation section to make Y point always at 160°C and X always at 250°C. However in case of the length at 5mm, the temperature at X point was 240°C, and it was not able to get 250°C. The shape of the magnet moulded had a $d^2/2D$ value at approximately 13mm.

Table 4

	Length [mm]	Magnetic Field [Koe]	Magnetic Performance	
			Br [KG]	(BH) max
Test 17	25	5.0	3.70	2.7
18	15	9.3	4.93	5.5
19	13	11.1	5.95	7.5
20	10	13.3	6.15	8.0
21	5	15.0	6.12	7.9

From Table 4, the magnetic performance of the magnet drops extremely when the length of the orientation exceeds in 13mm. This is because of an impossibility of an sufficient orientation of the magnetic

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powder by an increase of the length of the orientation section resulting a low magnetic field at the orientation section.

$$1 < d^2 / 2D \quad \dots(1)$$

The above equation is an modified equation of the condition in which the orientation of the radial factor is sufficient ie

$$fR = 2Dh / d^2 < 1,$$

by replacing h with l, and the results obtained almost have an agreement with the equation of (1). In case of a radial magnetic field moulding by a press and an injection, there is a limitation on the height at around 13mm for the magnet moulded, but there is no such limitation on the magnet height in case of the extrusion moulding, and it was able to produce a magnet with a sufficient radial orientation even if its height was several ten mm.

EXAMPLE 5

Next the similar test to Example 4 was carried out by using the die shown in Figure 2.

As to the die shown in Figure 2, as similar to Example 2, the orientation section 108 of the die is divided into 3 layers of layer A 102b, layer B 102c and layer C 102b, 102c of layer B is a non-magnetic material PEEK of 0.5 mm thickness, and it has a

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structure that 102c of layer B comprising a different material is inserted in the centre of the orientation section 108. 102b of layer A and layer C is a magnetic material, and a sum of these length is 1'. Layer A and layer C were made as always the same thickness.

The magnetic field for the orientation and the change of the magnet performance when the magnets were moulded by varying the length 1' were examined, and the results were shown in Table 5.

The magnetic field for the orientation was a result observed at a passage which contacted with layer A 102b, and the shape of the moulded magnet was a ring of the outer diameter 25mm and the inner diameter 23mm.

Table 5

	1'	Magnetic Field	Magnetic Performance	
			Br [KG]	(BH) max
	[mm]	[KOe]		
Test 22	18	3.0	3.68	2.7
23	15	5.0	3.73	2.7
24	11	9.2	4.90	5.5
25	10	10.5	6.02	7.8
26	8	13.0	6.28	8.5
27	5	15.0	6.30	8.5
28	3	15.2	6.22	8.3

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The temperatures at X and Y points were 160°C and 280°C respectively. The temperature at Y point raised when compared with Example 4, and this was due to a heat insulation effect between layer A - C by the insertion of PEEK in layer B resulting a security of the temperature difference.

There magnets produced herewith had

$$d^2 / 2D = 10.6 \text{ [mm]}.$$

Even on the results of Table 5 when l' becomes 10.6 mm or more, the magnetic performance of the magnet produced drops remarkably as similar to Example 4. When it becomes 10.6 mm or less, it shows a value which is considered that the radial orientation is almost sufficient. The magnetic property is more improved than Example 4, and this is due to a further decrease of the resin viscosity at X point when compared with Example 4 because of a security of the temperature gradient between X - Y by a heat insulation effect of layer B. When the length of a magnetic material in the orientation section, ie the length of l' in which a magnetic field is charged to a magnetic powder, satisfies

$$l' < d^2 / 2D,$$

a magnet with a sufficient radial orientation can be formed.

EXAMPLE 6

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A magnetic powder having a same basic composition to Example 4 was mixed with a resin mainly comprising an epoxy resin to make a volume ratio of the magnetic powder and the resin as 3:2, a magnet was moulded by an extrusion from a die, and then the moulded magnet was heated in an oven to cure it.

A die used in this example is shown in Figure 3. Namely in this example it is constituted by devided sections in following order as an converging section 111, a heat insulating section 112, a heating section 113 and an orientating section 110 from a connecting section of the extrusion machine to an outlet of the orientation section. X, Y and Z are measuring points of temperature.

A compound extruded from an extrusion machine is converged at the converging section 111. The compound is further heated in the heating section 113 after passing through the heat insulating section 112, the magnetic powder is orientated in the orientating section 110 and a magnet is moulded as its state by a solidification with cooling.

Next as -for a die used in Comparative Example, there is no heat insulating section 112, and no distinction between the converging section 111 and the heating section 113, but the remainder is the same to the die of Figure 3.

A change of the compound viscoisty, when these dies are applied, is shown in Figure 4.

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The viscosity herewith measured is a value at 120°C of a crushed material of an uncured magnet extruded through the die after charging in an extrusion machine.

The time of the axis of abscissa is time setting 0 minute when the charged compound first comes out from the die and magnets are sampled after it, and their viscosities are measured.

The temperature of the die at X, Y and Z points were 60°C, 150°C and 120° respectively, the temperature of the die of Comparative Example at X, Y and Z points were 60°C, 150°C and 160°C, and the extrusion speed of the magnet was 1 mm/sec.

As it is shown in Figure 4, the compound viscosity increases largely by passing time in case that the die of comparative Example is used. It is considered that it was due to an initiation of cure of a part of the resin because of heating of the compound extruded from the extrusion machine even at 160°C. When the operation time exceeded over 4 hours, the extrusion moulding was not able to continue. On the contrary in case of the die of Example, a section where it was heated at 150°C was small resulting slight change of the viscosity by time.

A change of the magnetic performance when these dies were used, are shown in Figure 5 (a) and (b). The time of the axis of abscissa is the same as Figure 4.

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As it is clear from Table 5, the magnetic performance suddenly drops by passing the time in case of Comparative Example. This was due to a decrease of degree of the orientation since the magnetic powder in the compound became difficult to orientate in progress of the elevation of the compound viscosity by time resulting a drop of the magnetic performance.

On the other hand, in case of Example, it is not almost observed the change of the magnetic performance by time, and a high magnetic performance is attained stably.

CLAIMS

(1) A die for an extrusion moulding of a resin bound type magnetic which is moulded by orientating a magnetic powder in a molten mixture of the magnetic powder and a resin and by a solidification with cooling wherein an orientation section located from a section at the front end of the said die where a magnetic field is charged and the aforementioned magnetic powder is orientated to the die section comprises a layer structure with at least one or more of different materials.

(2) a die for an extrusion moulding as claimed in Claim 1 wherein at least one or more of materials of the aforementioned orientation section comprises a magnetic material.

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As it is clear from Table 5, the magnetic performance suddenly drops by passing the time in case of Comparative Example. This was due to a decrease of degree of the orientation since the magnetic powder in the compound became difficult to orientate in progress of the elevation of the compound viscosity by time resulting a drop of the magnetic performance.

On the other hand, in case of Example, it is not almost observed the change of the magnetic performance by time, and a high magnetic performance is attained stably.

CLAIMS

(1) A die for an extrusion moulding of a resin bound type magnetic which is moulded by orientating a magnetic powder in a molten mixture of the magnetic powder and a resin and by a solidification with cooling wherein an orientation section located from a section at the front end of the said die where a magnetic field is charged and the aforementioned magnetic powder is orientated to the die section comprises a layer structure with at least one or more of different materials.

(2) a die for an extrusion moulding as claimed in Claim 1 wherein at least one or more of materials of the aforementioned orientation section comprises a magnetic material.

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(3) A die for an extrusion moulding as claimed in Claim 1 wherein a layer structure is formed by inserting a low thermal conductive material having the thermal conductivity K (at 20°C) of

$$K \leq 0.01 \text{ [cal/cm} \cdot \text{sec} \cdot \text{°C]}$$

in a part of the aforementioned orientation section.

(4) A die for an extrusion moulding as claimed in Claim 1 wherein the insertion material in the aforementioned orientation section comprises a non-magnetic material, and a thickness of the said non-magnetic material is 1/2 or less of a contacting length with the molten mixture of the aforementioned orientation section.

(5) A die for an extrusion moulding as claimed any of Claim 1 to Claim 4 wherein the aforementioned die for an extrusion moulding is used for production of a cylindrical resin bound type magnet.

(6) A die for an extrusion moulding as claimed in Claim 5 wherein a length of the orientation section located from a section at the front end of the said die where a magnetic field is charged and the aforementioned magnetic powder is orientated to an outlet section of the die satisfies

$$l < d^2 / 2D.$$

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(d and D are the inner diameter and the outer diameter of the molten mixture passage)

(7) A die for an extrusion moulding as claimed in Claim 5 wherein in case a presence of a non-magnetic material in the aforementioned orientation section, a length l' of a contacting section of the magnetic material with a mixture of the magnetic powder and the resin in a molten state satisfies

$$l' < d^2 / (2D).$$

(8) A die for an extrusion moulding as claimed in any of Claim 1 to Claim 7 wherein the aforementioned magnetic powder comprises a ferromagnetic material consisting of rare earth elements (including Y) and transition metals mainly constituting cobalt or a ferromagnetic material consisting of rare earth elements, transition metals mainly constituting iron and boron.

(9) A die for an extrusion moulding of a resin bound type magnet which is moulded by orientating a molten mixture of a magnetic powder and a resin and by solidification with cooling wherein the structure of the said die comprises in orders from a connecting section to an outlet of the orientation section as

(a) Converging section in which a mixture of a magnetic powder and a resin which becomes in a molten state and has fluidity is converged.

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(b) Heat insulating section to hold a temperature difference between the whole of the die and the rear section.

(c) Heating section in which the viscosity of the molten compound of the mixture in the molten state further drops, and

(d) Orientation section in which a magnetic field is charged, the magnetic powder is orientated and it is solidified with cooling as its state.

ABSTRACT

A die for an extrusion moulding of a resin bound type magnet which is moulded by orientating a magnetic powder in a molten mixture of a magnetic powder and a resin and by solidification with cooling wherein

the orientation section, located from a section from which the orientation of the aforementioned magnetic powder commences by application of a magnetic field at the front end of the said die to a section of the die outlet, comprises a layer structure with at least one or more of different material, and at least one or more of the material of the said orientation section is a magnetic material, or the layer structure is comprised by an insertion of a low thermal conductive material having the thermal conductivity of

$$K < 0.01 \text{ [cal/cm} \cdot \text{sec} \cdot ^\circ\text{C]}$$

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(b) Heat insulating section to hold a temperature difference between the whole of the die and the rear section.

(c) Heating section in which the viscosity of the molten compound of the mixture in the molten state further drops, and

(d) Orientation section in which a magnetic field is charged, the magnetic powder is orientated and it is solidified with cooling as its state.

ABSTRACT

A die for an extrusion moulding of a resin bound type magnet which is moulded by orientating a magnetic powder in a molten mixture of a magnetic powder and a resin and by solidification with cooling wherein

the orientation section, located from a section from which the orientation of the aforementioned magnetic powder commences by application of a magnetic field at the front end of the said die to a section of the die outlet, comprises a layer structure with at least one or more of different material, and at least one or more of the material of the said orientation section is a magnetic material, or the layer structure is comprised by an insertion of a low thermal conductive material having the thermal conductivity of

$$K < 0.01 \text{ [cal/cm} \cdot \text{sec} \cdot ^\circ\text{C]}$$

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, the insertion material comprises a non-magnetic material and the thickness of the non-magnetic material is $1/2$ or less of a contacting length of the orientation section with the molten mixture,

or the length l of the orientation section located from a section where a magnetic powder is orientated by an application of a magnetic field at the front end of the die to the die section satisfies

$$l < d^2 / 2D$$

(d and D are the inner diameter and the outer diameter of the molten mixture passage)

and in case a non-magnetic material is present in the orientation section, the total length l' of the contacting section of the magnetic material with a mixture of a magnetic powder and a resin in a molten state satisfies

$$l' < d^2 / (2D).$$

A die for an extrusion moulding wherein a structure of the die comprises in order from a connecting section of an extrusion machine to an outlet of the orientation section as a converging section, a heat insulating section, a heating section and an orientation

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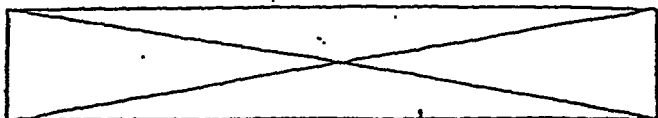


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section, and the die which is suitable for production of a cylindrical resin bound type magnet.

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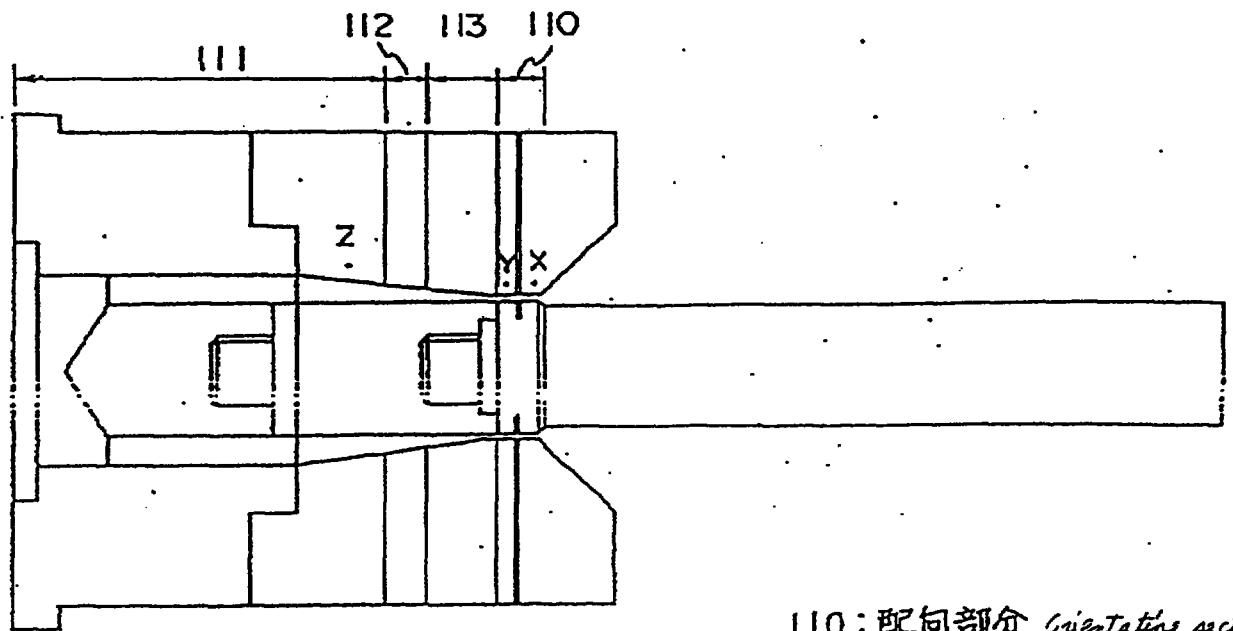
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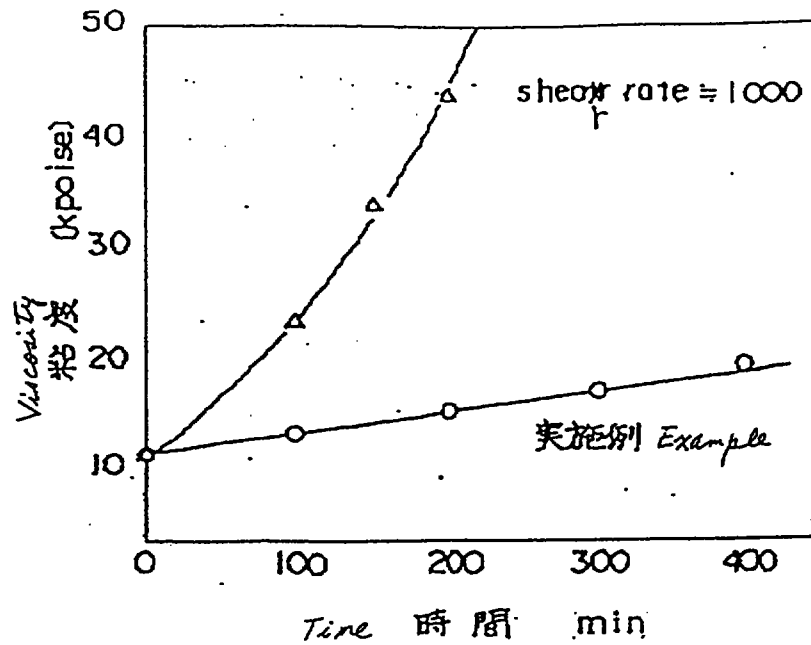
- 110: 配向部分 Orientating section
 111: 収束部 Convergence section
 112: 断熱部 Heat insulating section
 113: 加熱部 Heating section
 Z: 温度測定点 Temperature measurement point

第 3 図 Figure 3

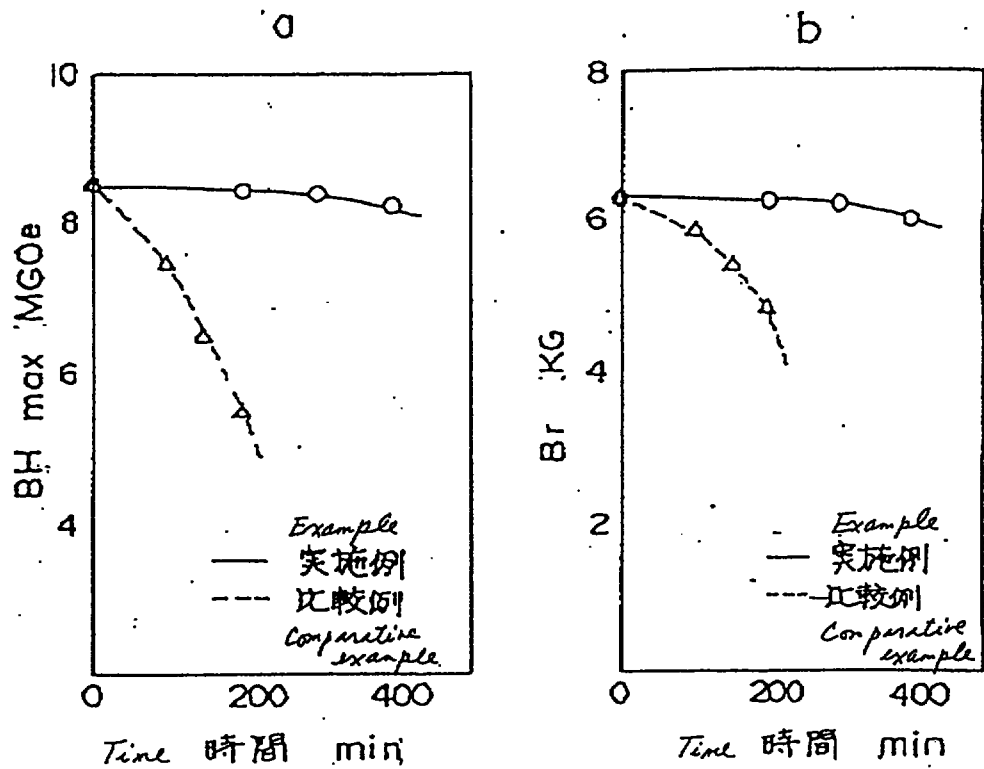
代理人 井上 隆夫 氏

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第 4 図 Figure 4

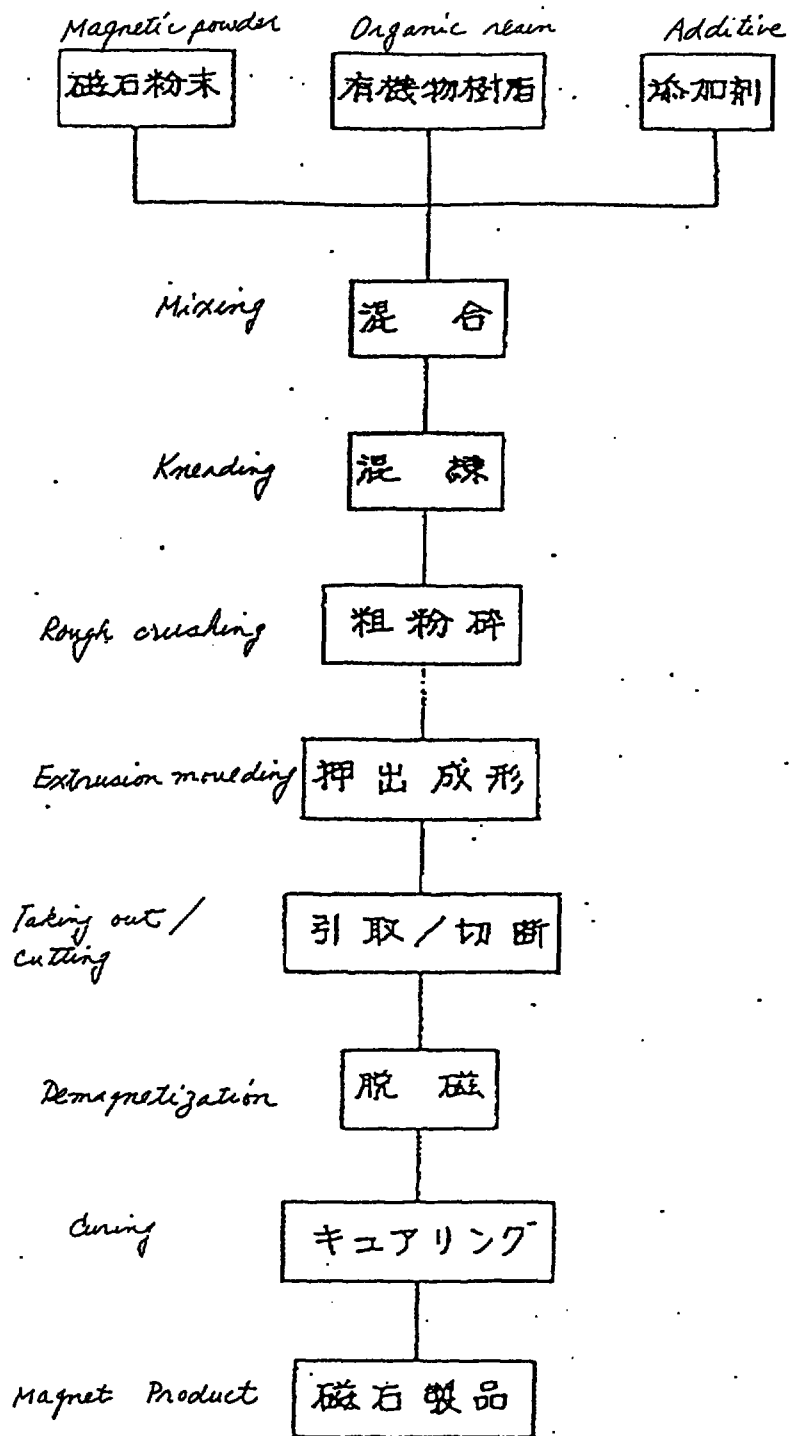


第 5 図 Figure 5

代理人 井坂士 益々木宗光

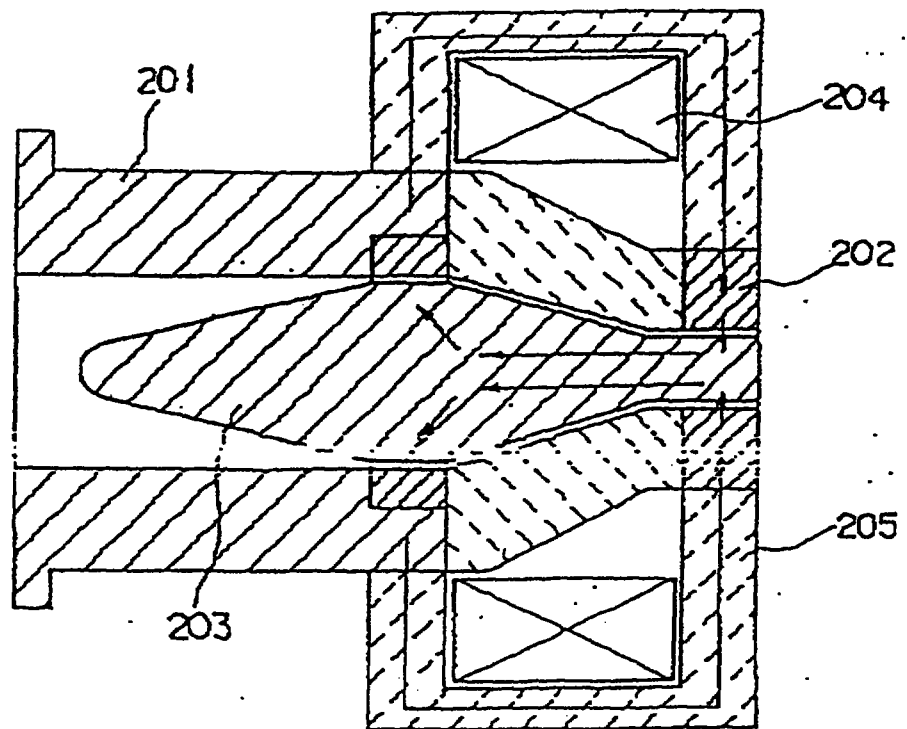
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第 6 図 Figure 6



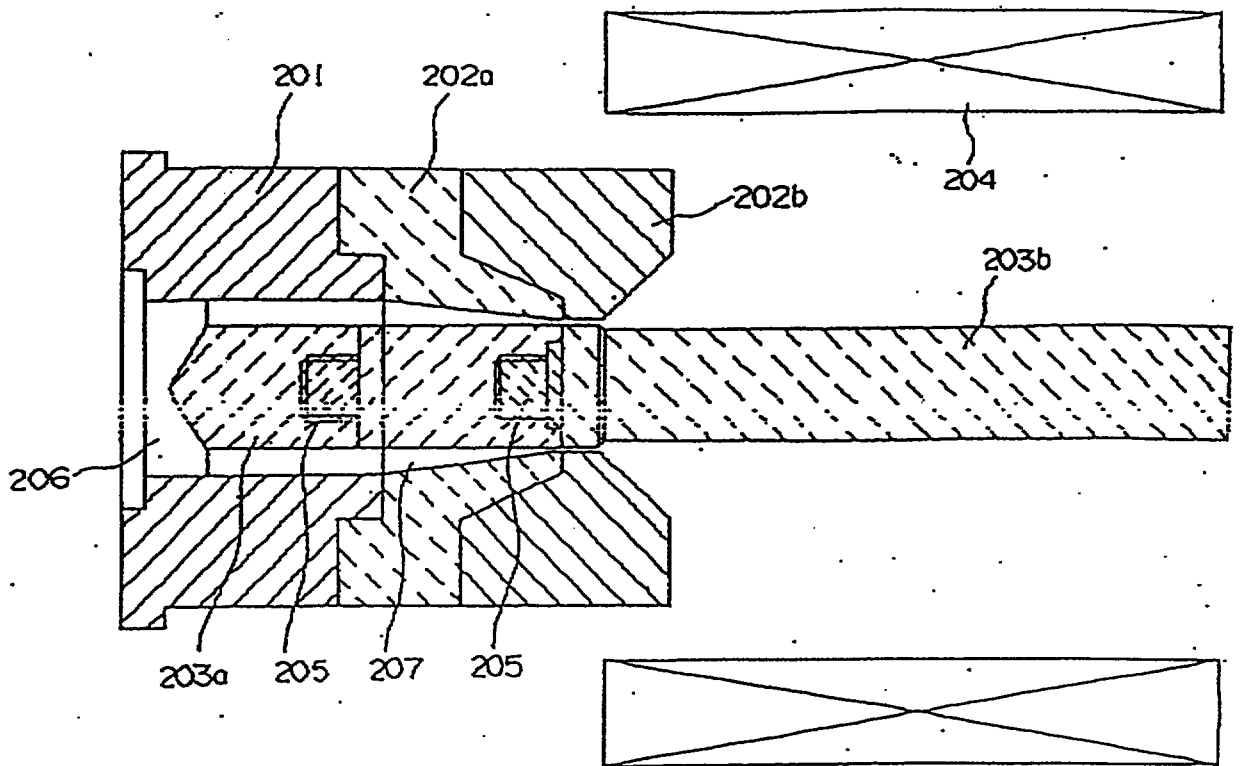


- 201 : 材料注入部外ダイ Raw material injection outer die
 202 : 成形部外ダイ Moulding section outer die
 203 : マンドレル Mandrel
 204 : 電磁コイル Electromagnetic coil
 205 : 磁性体アロツ Magnetic material floc

第 7 図 Figure 7

代理人 弁護士 佐々木 宗治





201: 材料注入部外ダイ Raw material injection outer die

202a, 202b: 成形部外ダイ Moulding section outer die

203a, 203b: マンドレル Mandrel

204: 電磁コイル Electromagnetic coil

205: 接合ネジ Connection screw

206: 材料注入部 Raw material injection section

207: 材料充填空間部 Raw material packing space

第 8 図 Figure 8

代理人 弁護士 佐々木宗浩

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✓	35	36	37
✓	38	39	40

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4	5	6
7	8	9
10	11	12

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TITLE OF INVENTION

Dies for extrusion moulding.

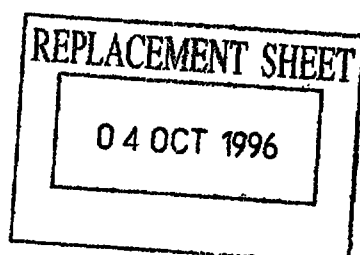
FIELD TO WHICH THE INVENTION BELONG

This invention relates to dies for an extrusion moulding, especially for dies for an extrusion moulding of a resin bound type magnet.

PRIOR ARTS

In general, a resin bound type magnet is produced by a process shown in Figure 6, ie:

A magnetic powder and an organic resin (thermosetting or thermoplastic resin) of suitable particle sizes are sufficiently mixed. If necessary, additives are added. The mixed raw materials are kneaded by a kneading machine such as a roller mill or an extrusion kneader, etc. with heating above a temperature at which the organic resin is molten. The kneaded raw material is roughly crushed into particles having



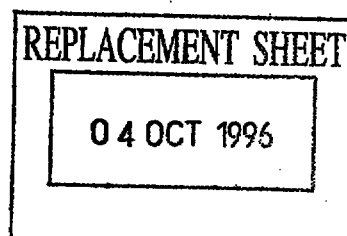
particle sizes of around 1-10mm, and is charged into an extrusion moulding machine.

The charged magnet raw material is heated in the extrusion moulding machine to make it in a fluidized state, and is sent into a die equipped at a front end of a cylinder by screw or plunger.

The magnet raw material is moulded in a predetermined shape such as cylinder, thin plate, bar, etc. by passing through the said die. However, the moulding processes of an isotropic magnet and an anisotropic magnet are different.

Namely, in case of the anisotropic magnet, an axis of easy magnetization of the magnetic powder in the raw material is uniformed to the magnetic field direction i.e. the magnetic powder is orientated, by passing the magnetic raw material through a die to which the magnetic field is charged, and it is moulded. In the process, it is common to charge the magnetic field by a combination of an electromagnetic coil and a magnetic circuit comprising a magnetic material.

On the other hand, the isotropic magnet is moulded by the extrusion without charging the magnetic field. The moulded body is cooled near the outlet of the front end of the die, then it is picked up by a receiving machine located in front of the extrusion moulding machine, and it is cut into a suitable length by a cutter.

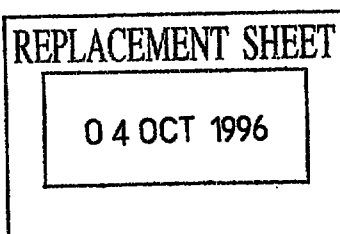


Because the magnetism remains in the moulded body in case of the moulding with an orientation of the magnetic powder, it is subjected to a demagnetization to remove it. Further in case that the thermosetting resin is used as a binder, the moulded body is subjected to a curing process to cure the resin after its demagnetization, and the resin bound type magnet by an extrusion moulding is produced.

In these magnet productions, the die, which is used for an extrusion moulding in a magnetic field (ie it is used for a moulding of the anisotropic magnet), has a structure which is a combination of a magnetic material and a non-magnetic material, and they are disclosed in Japan Patent Laid-Open Sho 58-219705, Japan Patent Laid-Open Sho 60-100413, etc. as the prior arts.

For example, in the Japan Patent Laid-Open Sho 58-219705, a die structure shown in Figure 7 is disclosed.

In the die of Figure 7, a raw material injection outer die 201, a mandral 203 and a front end of the moulding section outer die 202 comprise magnetic materials and the rest of the moulding section outer die 202 comprises a non-magnetic material. It is constituted that an electromagnetic coil 204 is coiled around the moulding section outer die 202, and further a magnetic material bloc 205 is positioned around the electromagnetic coil 204.



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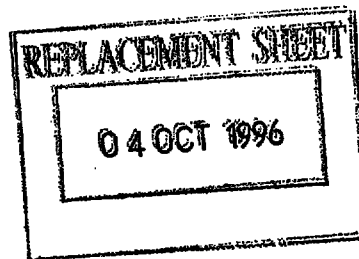
Toward to this die, the inventor of this application, etc disclosed a die structure as shown in Figure 8 by Japan Patent Laid-Open Sho 63-254713.

The die is constituted by a outer die comprising a raw material injection outer die 201 and moulding section outer dies 202a and 202b, and mandrels 203a and 203b. The raw material injection outer die 201 consists of a non-magnetic material, and the moulding section outer die 202a also consists of a non-magnetic material, but it is equipped with the moulding section outer die 202b made of a magnetic material to induce magnetic flux to the front end of the outer die.

The mandrel 203a also consists of a non-magnetic material, and at its front end of the mandrel, the mandrel 203b made of a magnetic material is equipped.

The electromagnetic coil 204 is installed at the outside of the die. When a current is passed through the electromagnetic coil 204, a radiated magnetic field is charged at a space (hereinafter called as an orientation section) between the front end of the mandrel 203b and the front end of the moulding section outer die 202b because the generated magnetic flux tends to pass through in a magnetic material with a high magnetic permeability.

A magnet raw material passes through the raw material injection section 206 and a raw material packing space 207 and it is moulded



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in a cylindrical form by an extrusion with a progress of a radiatedly orientation of the magnet powder in the orientation section.

Today, (1) a press moulding, (2) an injection moulding and (3) an extrusion moulding are available for a resin bound type radial magnet.

Among them, the press moulding and the injection moulding are currently utilized for mass-production processes. On the contrary, though the extrusion moulding is widely applied for a moulding of a ferrite magnet, it is still in a stage not to be utilized in a mass-production of a high performance rare earth magnet, and the die for the extrusion moulding, especially a structure of the orientation section in the die has not be sufficiently considered.

OBJECTIVES OF THE INVENTION

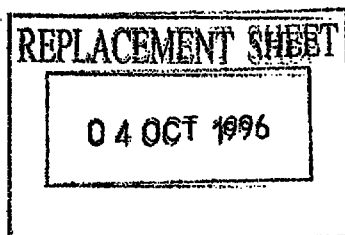
It is important to have a sufficient consideration on the structure of the orientation section of a die for the extrusion moulding because it largely influences a magnetic performance of the moulded magnet.

In either the die or the machine of the extrusion moulding for a resin bound type magnet, coventionally used, no attention has not been paid on a material and a structure of the orientation section of the die, and it was generally made by a single body of a magnetic material. Therefore it has problems listed below.

Namely, in case that a resin bound type magnet is moulded by an extrusion, a magnetic field is charged, when a mixture comprising a magnetic powder and a thermosetting or thermoplastic resin becomes a molten state by heating, to orientate the magnetic powder, and it is necessary to carry out a solidification by cooling after the moulding in the orientation section not to disorder the orientation and the moulded shape.

In order to achieve a sufficient orientation of the magnetic powder, it is preferable that a viscosity of the resin should be as low as possible as soon as it enters the orientation section, ie its temperature should be as high as possible. On the contrary, when the magnet orientated and moulded comes out from the die, it is preferable that its temperature is as low as possible to get a sufficient solidification by cooling in the orientation section not to disorder the orientation and the moulded shape.

Accordingly a temperature gradient is required in the orientation section. If the temperature gradient is not sufficiently taken in the orientation section for the solidification by cooling and the temperature of the whole orientation section drops, it results an insufficient orientation, and adversely if the temperature of the whole orientation section rises, the orientation and the moulded shape are disordered when the magnet comes out from the die.



However, in case that the orientation section comprises a single body of a magnetic material, it is difficult to take the temperature gradient because of the property of the material and the structure of the orientation section, and in order to take the temperature gradient in the single metal body, it is necessary to equip a heater and a cooler with a high capacity resulting an extreme inefficiency.

Further, in case of a cylindrical magnet with anisotropy radiatedly toward its diameter direction (hereinafter called as a radial anisotropic magnet), the sufficiency of its radial anisotropic property depends on a shape and a size of the magnet. As an index to show the above, a radial factor f_R is given by the following equation.

$$f_R = 2 Dh/d^2$$

where D = Outer diameter of a ring shaped magnet moulded

h = Height of a ring shaped magnet moulded

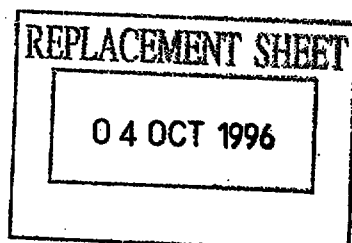
and the radial factor can be classified into following categories.

$f_R < 1$ Sufficient radial achievable

$f_R = 1-2$ Insufficient

$f_R > 1$ Isotropic

The f_R is the first index to consider at designing of a die when a radial magnetic field moulding by a pressing or an injection is practiced.



Namely, if the die structure satisfies $fR < 1$, a sufficient radial magnetic field can be charged at a cavity and thus it is possible to mould a magnet with a sufficient radial anisotropic property.

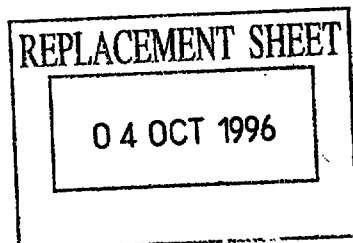
However when a die of $fR \geq 1$ is designed, it is not attainable to mould a magnet with a sufficient radial orientation.

Therefore there is an important index for the designing of a die for a radial magnetic field moulding by a pressing or an injection.

However in case of an extrusion moulding, since a shape of a moulded magnet and a die for the extrusion moulding do not coincide, and thus it is difficult to use fR as it is for designing of a die for the extrusion moulding.

As described above, when a resin bound type magnet is moulded by an extrusion, a mixture of a magnetic powder and a thermosetting or a thermoplastic resin is heated, a magnetic powder is orientated by charging a magnetic field as it becomes a molten state, and a solidification by cooling after the moulding should be performed in the orientation section not to disorder the orientation and the moulded shape.

In order to achieve a sufficient orientation of the magnetic powder, the temperature gradient in the orientation is required as described above. To get the temperature gradient in the orientation section, there are below-listed methods.



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- (1) Increasing the length of the orientation section,
- (2) Inserting a material with a low thermal conductivity into the orientation section and
- (3) Heating and cooling of both ends of the orientation section with extremely strong heater and cooler.

Among them, as to (1) the length of the orientation section, there is a limitation of the length of the orientation section because of an impossibility of a sufficient orientation magnetic field if it becomes too long, and as to (2), a material of low thermal conductivity is in general a non-magnetic material, and thus the magnetic field in the orientation is disordered unless the material inserted is thin.

Accordingly both of (1) and (2), though it may be possible to attain the temperature gradient with a reduction of the capacities of the heater and the cooler, still require a strong heater and cooler to get the temperature gradient as same to (3) in a certain degree.

However if a strong heater with an additional capacity is used, not only the orientation section, but also the whole of the die is heated resulting an temperature elevation of the whole of the die except for the front end of the die. Therefore a compound, which is heated to have a fluidity in the extrusion machine, is further heated in the die, in case that a resin in the compound is a thermosetting resin, it starts to cure in the die, and case of a thermoplastic resin, a thermal decomposition is initiated resulting

changes by time such as an increase of viscosity of the compound while it is in the extrusion moulding process, etc. They lead to a problem that a long time stable operation of the extrusion moulding is not achieved.

This invention aims to solve the problems of the die for an extrusion moulding of a resin bound type magnet as discussed above, and to provide a die for the extrusion moulding to mould a resin bound type magnet with a high performance and a superior shape accuracy.

Further, this invention provides a die for an extrusion moulding to produce a high performance resin bound type radial magnet and to produce a long size radial magnet which does not satisfy $FR < 1$.

Furthermore, this invention aims to provide a die for an extrusion moulding, by which a long time stable extrusion moulding can be operated by preventing the changes of a resin and a magnetic powder by time during the extrusion and by stabilizing the magnetic performance of a magnet to be moulded with a superior mass production capability as well.

EXPLANATION OF FIGURES

Figure 1-3 show outline drawings of dies for an extrusion moulding used in Examples of this invention.

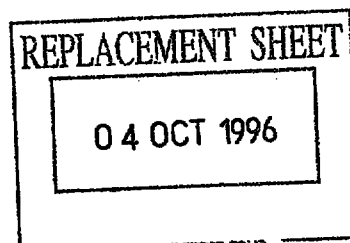


Figure 4 shows a graph to exhibit a viscosity change of the compound by time.

Figure 5 (a) and (b) show graphs to exhibit a change of the magnetic performance when a die of Example 6 is used.

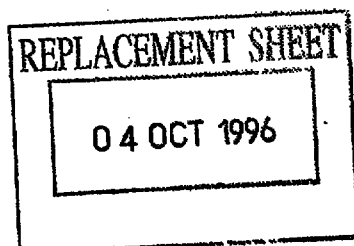
Figure 6 is a process outline of a magnet.

Figure 7 and 8 are outline drawings of dies for the conventional extrusion moulding.

SUMMARY OF THE INVENTION

This invention is a die for an extrusion moulding of a resin bound type magnet which is moulded by an orientation of a molten mixture of a magnetic powder and a resin and by a solidification with cooling, wherein an orientation section, which is from an orientating section of the said magnetic powder at the front end of the said die by charging a magnetic field to the die section, is formed by a layer structure comprising at least one or more of different materials.

It is a die for an extrusion moulding wherein at least one or more of the materials of the orientation section comprises magnetic material(s).



Further, it is a die for an extrusion moulding wherein the layer structure is formed by inserting a low thermal conductivity material of which the thermal conductivity K (20°C) is

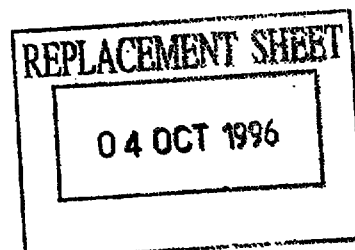
$$K \leq 0.01 \text{ [cal/cm}\cdot\text{sec}\cdot^{\circ}\text{C]}$$

into a partial section of the said orientation section.

Further, it is a die for an extrusion moulding wherein the material of the insertion into the orientation section of the said die for an extrusion moulding comprises a non-magnetic material and the thickness of the said non-magnetic material is $1/2$ or less of the contact section length of the molten mixture in the orientation section.

Furthermore the said die for an extrusion moulding is applied for a cylindrical resin bound type magnet.

Also this invention is a die for an extrusion moulding for a production of the aforementioned cylindrical resin bound type magnet, wherein the contact section length l of the orientation section with a molten mixture from a section from which the orientation of the aforementioned magnetic powder starts by charging a magnetic field at the front end of the said die to the outlet section of the die satisfies



$$l < d^2 / 2D.$$

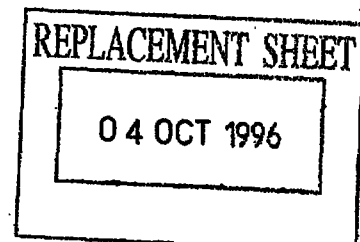
(d and D are inner and outer diameters of the molten mixture passage, respectively)

Further in case that a non-magnetic material is present in the orientation section of the aforementioned die for an extrusion moulding, it is a die for an extrusion moulding wherein a total length l' of the contact section length of the magnetic material with a mixture of a magnetic powder and a resin in a molten state satisfies

$$l' < d^2 / 2D.$$

Furthermore it is a die for an extrusion moulding wherein the aforementioned magnetic powder comprises a ferromagnetic material consisting of rare earth elements (including Y) and transition metals mainly constituting cobalt, or a ferromagnetic material consisting of rare earth element, transition metals mainly constituting iron and boron.

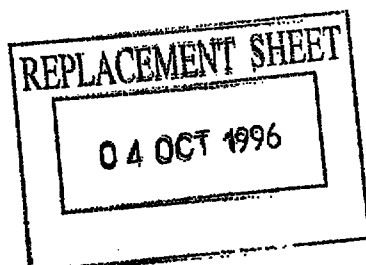
Further this invention is a die for an extrusion moulding of a resin bound type magnet which is moulded by an orientation of a molten mixture of a magnetic powder and a resin, and by a solidification with cooling wherein the structure of the said die is constituted in orders from a connection section of an extrusion machine to an outlet of the orientation section as

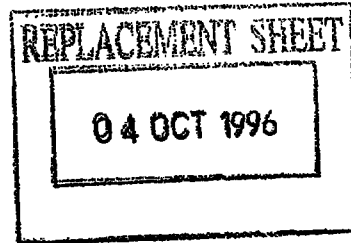


- (a) A converging section where a mixture of a magnetic powder and a resin which is in a molten state with a fluidity is pressed into the final shape.
- (b) A heat-insulating section to hold a temperature difference between the whole of the die and a rear section
- (c) A heating section by which the viscosity of the molten compound of the mixture in a molten state is further reduced.
- (d) An orientating section in which a magnetic field is charged, the magnetic powder is orientated and it is solidified with cooling as its state.

This invention has effects to improve the performance of the moulded magnet and also to reform the dimensional accuracy as it is clear from the aftermentioned Examples as a result of formation of an temperature gradient in the orientation section, by forming a layer structure with at least one or more of different materials and by making at least one or more of materials of the said orientation section with magnetic materials, which is from the front end of the die at which the orientation of a magnetic powder starts to an outlet section of the die for an extrusion moulding of a resin bound type magnet which is moulded by orientating a molten mixture of a magnetic powder and a resin, and by a solidification with cooling.

Also in this invention, as one alternative case of the layer structure in the orientation section, when a material with a low thermal conductivity having the thermal conductivity K (20°C) of





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$K \leq 0.01$ [cal/cm·sec·°C] is inserted, the thermal conductivity at the insertion section drops approximately 1/10 or less because a material generally used for the die has the thermal conductivity of approximately 0.07-0.08 [cal/cm·sec·°C].

If a heat passing through the orientation section is constant, a temperature difference is able to be attained by the below listed equation by reducing the thermal conductivity.

$$Q = A \cdot K (T_1 - T_2) / l$$

Q : heat capacity, A: area, l: thickness

$T_1 - T_2 = \Delta T$: temperature difference

Further, in case that the insertion material in the orientation section comprises a non-magnetic material, the magnetic performance remarkably deteriorates if it is 1/2 or more of the length of the orientation section, in spite of a high temperature difference. This was due to an disorder of the magnetic field in the orientation section by insertion of a non-magnetic material in the orientation section. Although the temperature difference drops when a non-magnetic layer becomes thin, the magnetic performance is somewhat improved because of a reduction of the disorder of the magnetic field in the orientation section. Therefore it is preferable that the thickness of the non-magnetic layer is as thin as possible to take a sufficient temperature gradient, and when a

non-magnetic material is inserted, it is preferable that its length is $1/2$ or less of the length of the orientation section.

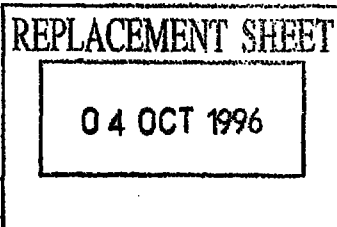
Moreover by this invention, when the contact section length l of the orientation section of the die for an extrusion with the molten mixture is limited as $l < d^2 < 2D$, the magnetic performance is improved because of an availability of a sufficient orientation of the magnetic powder.

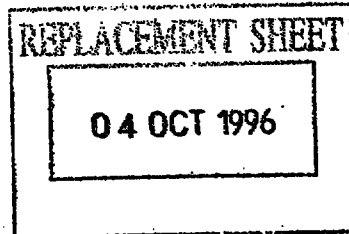
Further by arranging the composition of the die structure from the connecting section of an extrusion machine to the outlet of the orientation section in order of a converging section, a heat insulating section, a heating section and an orientating section, it is able to operate a stable extrusion moulding over a long time resulting effects such as a suitability for a mass production, etc.

According to this invention,

(1) It is able to take a temperature gradient in the orientation section by forming a layer structure for the orientation section, and therefore the degree of the orientation of a magnet is improved and the dimensional accuracy is also reformed.

(2) It is able to take a further high temperature gradient in the orientation section, by inserting a magnetic material of its thermal conductivity of 0.01 [cal/cm·sec·°C] or less or a non-magnetic material which has a thermal conductivity of 0.01 [cal/cm·sec·°C] or less having a length not more than $1/2$ of the length of the





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orientation section, into a partial section of the orientation section, and therefore it is able to mould a high performance anisotropic resin bound type magnet by an extrusion moulding.

(3) In case that a non-magnetic material is not present in the orientation section, by making the length l of the orientation section as

$$l < d^2 / (2D)$$

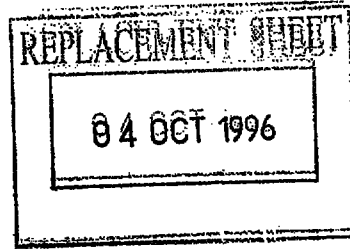
and in case that a non-magnetic material is present, by making the length l'

$$l' < d^2 / (2D)$$

it is able to mould a high performance resin bound type radial magnet with a sufficient radial orientation and to achieve prolongation of this magnet.

(4) By constituting a structure of the die, as shown in Figure 3, in order from a connecting section of an extrusion machine as a converging section, a heat insulating section, a heating section and an orientating section, it is able to operate an extrusion moulding with a stable magnetic performance for a long time, and a stable mass production is achievable.

This invention is hereafter explained by using Examples.



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EXAMPLE 1

Figure 1 shows an outline drawing of a die for an extrusion moulding used in Example 1.

In Figure, 108 is the orientation section, 109 is a surface of the outlet of the orientation section, X and Y are temperature measurement points, and an explanation of other numbers is omitted because they are described in below.

A die for an extrusion moulding for a practice of this invention is constituted, as shown in Figure 1 by a outer die comprising a raw material injection outer die 101 and moulding section outer dies 102a and 102b, and mandrels 103a and 103b, the raw material injection outer die 101 and the moulding section outer die 102a are composed of non-magnetic materials, and the moulding section outer die 102b of a magnetic material is equipped at the front end of the outer die to induce a magnetic flux. Further the mandrel 103a comprises a non-magnetic material, and at its front end the mandrel 103b consisting of a magnetic material is equipped by a connection screw 105.

Further an electromagnetic coil 104 is installed at the outside of the die, and when a current passes through the electromagnetic coil, a radiated magnetic field is charged at the orientation section 108 between the front end of the mandrel 103b and the front end of the moulding section outer die 102b because the generated magnetic flux

tends to pass through a magnetic material with a high magnetic permeability.

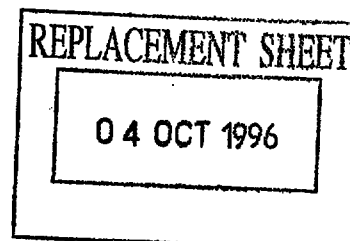
Next, for a production of a magnet, a magnetic powder is mixed with an organic resin such as a thermosetting or a thermoplastic resin and when it is required with additives by a mixer.

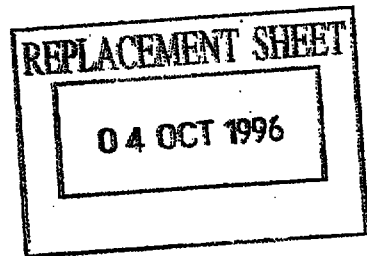
The mixture of the magnetic powder and the resin is heated in an extrusion machine, and it becomes in a molten state. Then it, as in this state, is sent to the raw material injection section 106 of the die for an extrusion moulding.

The molten material of the magnetic powder and the resin poured is gradually converged while it is being passed through the raw materials packing space 107 in the die to mould the final shape. The magnetic powder is orientated in the orientation section 108, and it is moulded as its state by a solidification with cooling in the orientation section 108.

Next in Table 1, results of measurements of temperature difference between X and Y points in the orientation section 108 are shown when the orientation section 108 is formed by a layer structure with materials selecting from at least one or more of several materials, namely,

SKD 61 : JIS G 4404 specification, steel material
SKD 11 : JIS G 4404 specification, steel material
SiO₂ : oxide of silicon





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PES : polyethersulphone resin

for the structure of the orientation section of a die for an extrusion moulding.

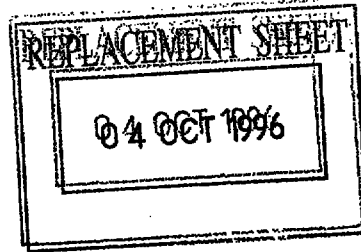
The total length of the orientation section 108, by the way is, 6mm, and the temperature differences represent temperature differences between X and Y points which are 0.5mm from the both ends of the orientation section 108, respectively and are 3mm outside from the passage of a molten mixture of the magnetic powder and the resin. (In the measurement, the temperature at Y point was fixed at 50°C)

A heater with 800W capacity was used for heating, and a cooling plate by a water cooling was installed at the surface of the outlet of the orientation section 109 for cooling to cool the orientation section 108.

The structure column in Table 1 shows materials used for the front end structure, and among them, SKD 61 and SKD 11 are magnetic materials and the remainders SiO_2 and PES are non-magnetic materials.

Further the length of each layer is $6/A$ [mm]. (A means numbers of the layer.)

As shown in Table 1, in case of Comparative Test in which the orientation section was formed by a single metal, a temperature difference of only 20°C was obtained with the aforementioned system.



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Although it was the same material, the temperature gradient was however able to get by forming the layer structure.

This was because that the contact surface resisted the heat transfer by forming the layer structure. This was also proved by Test 1 and Test 4.

Further as it was understood from Test 3, 5 and 6, a further high temperature gradient was attainable by using a material of the low thermal conductivity for a partial section of the orientation section.

However, in this case, since a magnetic material has, in general, high thermal conductivity, a non-magnetic material becomes suitable for the aforementioned material and it is unfavourable to get the magnetic field.

Next Table 1 also shows magnetic performance of magnets moulded by the dies having their structures as described above.

The magnets were produced by following process.

For the magnets produced here, a magnetic alloy of its coercive force at approximately 7 KOe having a basic magnetic powder composition of Sm (Co 0.672 Cu 0.08 Fe 0.22 Zr 0.028) 8.35 was crushed into particles of the average particle size of approximately 20 μm , and they were mixed with a resin. A ratio of the magnetic

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powder and the resin was the magnetic powder 60 vol % and the resin 40 vol %.

A thermosetting resin mainly comprising an epoxy resin was used as the organic resin.

The aforementioned mixture was kneaded by a roller mill, a compound was prepared, then the compound was coarsely crushed, and it was charged in a screw type extrusion machine. The crushed compound was heated in the extrusion machine.

The thermosetting resin mainly comprising the epoxy resin had its thermoplastic region at approximately 100 - 150°C at which the viscosity remarkably dropped, the mixture of the magnetic powder and the resin made in a molten state in this temperature region, it was pushed into a die by the screw, and a magnet was extruded from the die by a solidification with cooling after orientating the magnetic powder in the orientation section at the front end of the die. The shape of the moulded magnet was a ring shaped with the outer diameter 32.8 mm and the inner diameter 31.8 mm.

In this Example, the magnetic performance was measured by using an uncured state magnet moulded in a molten state.

As it is clear from Table 1, the moulded magnet showed an improved performance in case a die structure by which the temperature

gradient was secured, and it was also confirmed that the dimension accuracy was improved by having the temperature gradient as well.

Table 1

code	Structure	Temp	Magnetic Property		Dimension
			difference	Br[KG] (BH) [MGoe]	Accuracy
				max	
Test 1	SKD61/SKD61	30°C	5.54	6.3	C
" 2	SKD61/SKD11	35°C	5.60	6.5	C
" 3	SKD61/SiO ₂	70°C	5.62	6.5	B
" 4	SKD61/SKD11/SKD61	40°C	5.95	7.0	C
" 5	SKD61/SiO ₂ /SKD61	100°C	6.15	8.0	A
" 6	SKD61/PES/SKD61	150°C	6.30	8.5	A
Comparative					
Test 1	SKD61	20°C	5.36	6.0	D

A... excellent

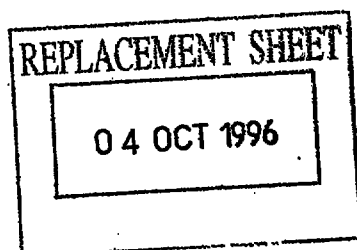
C... fair

B... good

D... bad

EXAMPLE 2

Figure 2 shows an outline drawing of a die for an extrusion moulding used in Example 2.



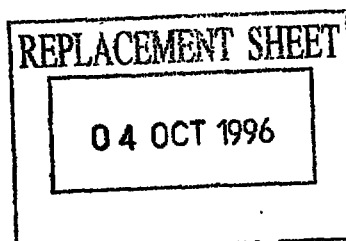
In Figure, 102c shows a moulding section outer die comprising a material of a low thermal conductivity, a distance between a-b shows a length of an orientation section 108, and an explanation of the other figures is omitted because they are same to Figure 1.

A die for an extrusion moulding for a practice of this invention is a die which possesses similar structure and effect as Figure 1 except that a different material is inserted in the centre of the orientation section 108, and the orientation section 108 at the inner part of the die has a structure divided into 3 layers ie A, B and C as shown in Figure 2. In this case, layer B was a material of the inserted layer, and a same material ie SKS2 was used for layer A and layer C. SKS2 is a steel material specified by JIS G 4404 standard.

A temperature difference in the orientation section 108 showed a temperature difference between X and Y points shown as temperature measuring points in Figure 2.

The temperature differences between X-Y, when several materials were used for the layer B material inserted, are shown in Table 2. The length of the orientation section [a distance between a-b in Figure 2] was 6mm, and all the lengths of every layer were 2mm.

As to Comparative Test 2, it was an example by using a die of which the orientation layer was not constituted by the layer structure as shown in Figure 8.



As same to Example 1, a heater with 800W capacity was used for heating, and as for cooling, a surface of the outlet of the die in layer C 109 was cooled by water and the temperature at Y point was kept at 60°C.

Next, cylindrical magnets of the outer diameter 30mm and the inner diameter 28mm were moulded in same basic composition and procedure as Example 1, by using the aforementioned die, and magnetic performance of their magnets was compared.

In Table 2, the temperature difference between X and Y in the orientation section 108 and the magnetic performance of the magnet prepared are shown when the orientation section 108 was formed by using a material as an inserting material selecting from,

PES : polyestersulphone resin

PEEK : polyetheretherketone resin

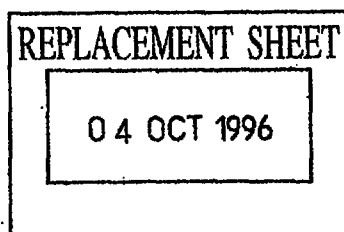
ZrO₂ : oxide of zirconium

YHD50 : steel material (a Hitachi Metal Product) and

SKD61 : steel material specified by JIS G 4404

which had different thermal conductivities,

Test 7-11 and Comparative Test 2 were cases when a resin mainly comprising an epoxy resin was used, and the extrusion condition was that the extrusion was made by keeping the temperature at Y point at 60°C as described above. The temperature was a temperature that the resin used was solidified, and the shape of the moulded magnet did not deform.



On the other hand, for Test 8a-11a and Comparative Test 2a, a polyamide resin (Nylon 12) was used, and in this case, the extrusion was made by keeping the temperature at Y point at 160°C.

An example, which corresponds to Test 7 ie PES is used as a material to make the inserted layer, is not shown in Table 2, and this is due to an impossibility of the application because of a poor heat resistance of PES.

As shown in Table 2, the cases, in which materials of low thermal conductivity were inserted, uniformly exhibited better magnetic performance than Comparative Test 2 and 2a in which the orientation section was formed by only a single metal SKD61. However when the material inserted has the thermal conductivity (at 20°C) above 0.01 [cal/cm·sec·°C], the improvement on the magnetic performance is slight, and it is preferable to insert a material having the thermal conductivity of 0.01 [cal/cm·sec·°C] or less.

Table 2

Code	Material Inserted	Thermal Conductivity [cal/cm·sec·°C]	Temp Difference [°C]	Magnetic Performance	
				Br[KG] (BH)	[MGOe] max
Test 7	PES	4.54×10^4	105	6.30	8.5
-	-	-	-	-	-
8	PEEK	5.97×10^4	100	6.28	8.4

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" 8a	"	"		6.27	8.4
" 9	ZrO ₂	0.007	80	6.18	8.1
" 9a	"	"		6.15	8.0
" 10	YHD50	0.038	40	5.65	6.6
" 10a	"	"		5.57	6.4
" 11	SKD61	0.073	30	5.60	6.4
" 11a	"	"		5.50	6.3
Comparative					
Test 2	-	0.073	25	5.36	6.0
" 2a	-	"		5.34	6.0

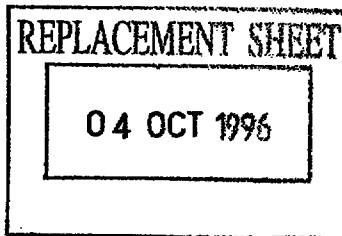
EXAMPLE 3

Next, an effect to a magnet, when a thickness of a non-magnetic material to be inserted in the orientation section in Figure 1 was varied, was investigated.

PEEK was used as the material to be inserted, the length of the orientation section including the thickness of PEEK was always kept at 6mm, layer A and layer C were made as the same length, and a cooling capacity was adjusted to make the temperature at Y point always at 160°C. Further as for a resin to be mixed with a magnetic powder, polyamide resin (Nylon 12) was used, and a moulding process and a shape of the moulded magnet were same as the aforementioned Example 2.

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In Table 3, temperature difference between X-Y and magnetic performance are shown when the thickness of layer B was varied from 0.5 to 3.5mm. (Test 12-16).

As it is clear from Table 3, the temperature difference is saturated at the PEEK thickness of 2mm with the heater capacity used. Since the thermal conductivity of PEEK is extremely low, a temperature difference of around 80°C is attained even at the PEEK thickness of 0.5mm.

Further as understood from Table 3, when the PEEK thickness becomes 3mm (1/2 of the length of the orientation section) or more, the magnetic property drops remarkably, though the temperature difference between X - Y is large. This is due to a disorder of a magnetic field in the orientation section by entering a non-magnetic material into the orientation section. Similarly even when the PEEK thickness is 1mm or less, it is seen that the magnetic performance is somewhat improved in spite of a reduced temperature difference.

Although the temperature difference drops if the thickness of a non-magnetic layer becomes thin, it is observed that the magnetic performance is somewhat improved because of a decrease of the disorder of the magnetic field in the orientation section.

Basing on these observations, it is preferable that the non-magnetic layer should be as thin as possible if it is able to secure a sufficient temperature difference, and from the results of Table 3,

it is preferable that it is $1/2$ or less of the length of the orientation length when a non-magnetic material is inserted.

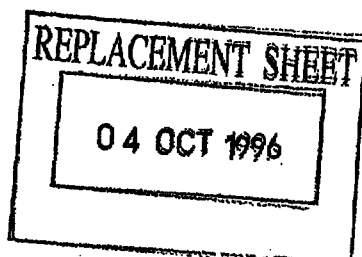
Table 3

	Thickness of Layer B [mm]	Temperature Difference [°C]	Magnetic Property	
			Br [KG]	(BH) [MGoe] max
Test 12	3.5	105	5.54	6.3
" 13	3.0	102	5.95	7.0
" 14	2.0	100	6.28	8.4
" 15	1.0	92	6.32	8.5
" 16	0.5	85	6.30	8.5

EXAMPLE 4

Next, in a die for an extrusion shown in Figure 1, the length of the orientation section 108 of the die was varied, and magnets were produced by an extrusion moulding as similar to Example 1.

In this example, the magnetic powder and the polyamide resin were however mixed to make a volume ratio of the magnetic powder and the resin as 3:2. The magnetic field was made by charging a 200A current to a 123 turn coil, and the shape of the moulded magnet by an extrusion was a cylindrical with the outer diameter 30mm and the inner diameter 28mm.



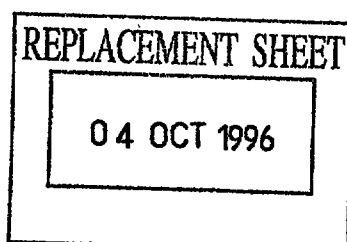
The magnetic fields for the orientation at the orientation section when the length of the orientation section 108 was varied, are shown in Table 4 together with the magnetic property of the magnets extruded.

In this example, as to the temperature of the orientation section X and Y points, a heating and cooling was applied from both ends of the orientation section to make Y point always at 160°C and X always at 250°C. However in case of the length at 5mm, the temperature at X point was 240°C, and it was not able to get 250°C. The shape of the magnet moulded had a $d^2/2D$ value at approximately 13mm.

Table 4

	Length [mm]	Magnetic Field [Koe]	Magnetic Performance	
			Br [KG]	(BH) max
Test 17	25	5.0	3.70	2.7
18	15	9.3	4.93	5.5
19	13	11.1	5.95	7.5
20	10	13.3	6.15	8.0
21	5	15.0	6.12	7.9

From Table 4, the magnetic performance of the magnet drops extremely when the length of the orientation exceeds in 13mm. This is because of an impossibility of an sufficient orientation of the magnetic



powder by an increase of the length of the orientation section resulting a low magnetic field at the orientation section.

$$1 < d^2 / 2D \quad \dots(1)$$

The above equation is an modified equation of the condition in which the orientation of the radial factor is sufficient ie

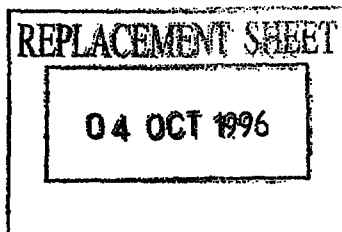
$$fR = 2Dh / d^2 < 1,$$

by replacing h with 1, and the results obtained almost have an agreement with the equation of (1). In case of a radial magnetic field moulding by a press and an injection, there is a limitation on the height at around 13mm for the magnet moulded, but there is no such limitation on the magnet height in case of the extrusion moulding, and it was able to produce a magnet with a sufficient radial orientation even if its height was several ten mm.

EXAMPLE 5

Next the similar test to Example 4 was carried out by using the die shown in Figure 2.

As to the die shown in Figure 2, as similar to Example 2, the orientation section 108 of the die is divided into 3 layers of layer A 102b, layer B 102c and layer C 102b, 102c of layer B is a non-magnetic material PEEK of 0.5 mm thickness, and it has a



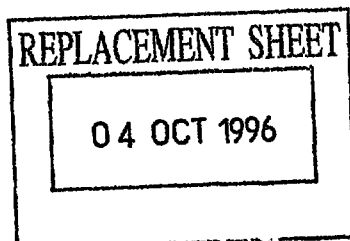
structure that 102c of layer B comprising a different material is inserted in the centre of the orientation section 108. 102b of layer A and layer C is a magnetic material, and a sum of these length is 1'. Layer A and layer C were made as always the same thickness.

The magnetic field for the orientation and the change of the magnet performance when the magnets were moulded by varying the length 1' were examined, and the results were shown in Table 5.

The magnetic field for the orientation was a result observed at a passage which contacted with layer A 102b, and the shape of the moulded magnet was a ring of the outer diameter 25mm and the inner diameter 23mm.

Table 5

	1'	Magnetic Field	Magnetic Performance	
			Br [KG]	(BH) max
	[mm]	[KOe]		
Test 22	18	3.0	3.68	2.7
23	15	5.0	3.73	2.7
24	11	9.2	4.90	5.5
25	10	10.5	6.02	7.8
26	8	13.0	6.28	8.5
27	5	15.0	6.30	8.5
28	3	15.2	6.22	8.3



The temperatures at X and Y points were 160°C and 280°C respectively. The temperature at Y point raised when compared with Example 4, and this was due to a heat insulation effect between layer A - C by the insertion of PEEK in layer B resulting a security of the temperature difference.

There magnets produced herewith had

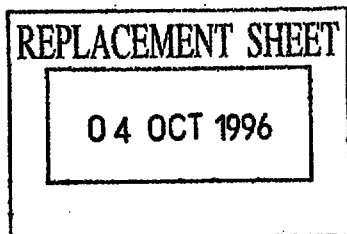
$$d^2 / 2D = 10.6 \text{ [mm]}.$$

Even on the results of Table 5 when l' becomes 10.6 mm or more, the magnetic performance of the magnet produced drops remarkably as similar to Example 4. When it becomes 10.6 mm or less, it shows a value which is considered that the radial orientation is almost sufficient. The magnetic property is more improved than Example 4, and this is due to a further decrease of the resin viscosity at X point when compared with Example 4 because of a security of the temperature gradient between X - Y by a heat insulation effect of layer B. When the length of a magnetic material in the orientation section, ie the length of l' in which a magnetic field is charged to a magnetic powder, satisfies

$$l' < d^2 / 2D,$$

a magnet with a sufficient radial orientation can be formed.

EXAMPLE 6



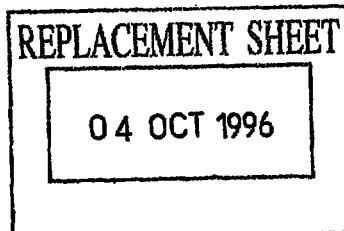
A magnetic powder having a same basic composition to Example 4 was mixed with a resin mainly comprising an epoxy resin to make a volume ratio of the magnetic powder and the resin as 3:2, a magnet was moulded by an extrusion from a die, and then the moulded magnet was heated in an oven to cure it.

A die used in this example is shown in Figure 3. Namely in this example it is constituted by devided sections in following order as an converging section 111, a heat insulating section 112, a heating section 113 and an orientating section 110 from a connecting section of the extrusion machine to an outlet of the orientation section. X, Y and Z are measuring points of temperature.

A compound extruded from an extrusion machine is converged at the converging section 111. The compound is further heated in the heating section 113 after passing through the heat insulating section 112, the magnetic powder is orientated in the orientating section 110 and a magnet is moulded as its state by a solidification with cooling.

Next as-for a die used in Comparative Example, there is no heat insulating section 112, and no distinction between the converging section 111 and the heating section 113, but the remainder is the same to the die of Figure 3.

A change of the compound viscoisty, when these dies are applied, is shown in Figure 4.



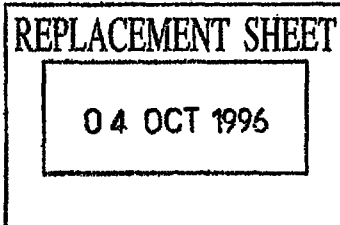
The viscosity herewith measured is a value at 120°C of a crushed material of an uncured magnet extruded through the die after charging in an extrusion machine.

The time of the axis of abscissa is time setting 0 minute when the charged compound first comes out from the die and magnets are sampled after it, and their viscosities are measured.

The temperature of the die at X, Y and Z points were 60°C, 150°C and 120° respectively, the temperature of the die of Comparative Example at X, Y and Z points were 60°C, 150°C and 160°C, and the extrusion speed of the magnet was 1 mm/sec.

As it is shown in Figure 4, the compound viscosity increases largely by passing time in case that the die of comparative Example is used. It is considered that it was due to an initiation of cure of a part of the resin because of heating of the compound extruded from the extrusion machine even at 160°C. When the operation time exceeded over 4 hours, the extrusion moulding was not able to continue. On the contrary in case of the die of Example, a section where it was heated at 150°C was small resulting slight change of the viscosity by time.

A change of the magnetic performance when these dies were used, are shown in Figure 5 (a) and (b). The time of the axis of abscissa is the same as Figure 4.



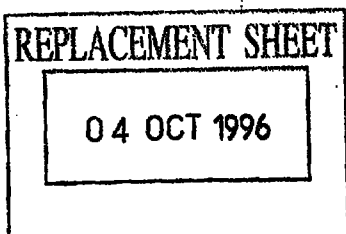
As it is clear from Table 5, the magnetic performance suddenly drops by passing the time in case of Comparative Example. This was due to a decrease of degree of the orientation since the magnetic powder in the compound became difficult to orientate in progress of the elevation of the compound viscosity by time resulting a drop of the magnetic performance.

On the other hand, in case of Example, it is not almost observed the change of the magnetic performance by time, and a high magnetic performance is attained stably.

CLAIMS

(1) A die for an extrusion moulding of a resin bound type magnetic which is moulded by orientating a magnetic powder in a molten mixture of the magnetic powder and a resin and by a solidification with cooling wherein an orientation section located from a section at the front end of the said die where a magnetic field is charged and the aforementioned magnetic powder is orientated to the die section comprises a layer structure with at least one or more of different materials.

(2) a die for an extrusion moulding as claimed in Claim 1 wherein at least one or more of materials of the aforementioned orientation section comprises a magnetic material.



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As it is clear from Table 5, the magnetic performance suddenly drops by passing the time in case of Comparative Example. This was due to a decrease of degree of the orientation since the magnetic powder in the compound became difficult to orientate in progress of the elevation of the compound viscosity by time resulting a drop of the magnetic performance.

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CLAIMS

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(2) a die for an extrusion moulding as claimed in Claim 1 wherein at least one or more of materials of the aforementioned orientation section comprises a magnetic material.

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(3) A die for an extrusion moulding as claimed in Claim 1 wherein a layer structure is formed by inserting a low thermal conductive material having the thermal conductivity K (at 20°C) of

$$K \leq 0.01 \text{ [cal/cm} \cdot \text{sec} \cdot \text{°C]}$$

in a part of the aforementioned orientation section.

(4) A die for an extrusion moulding as claimed in Claim 1 wherein the insertion material in the aforementioned orientation section comprises a non-magnetic material, and a thickness of the said non-magnetic material is 1/2 or less of a contacting length with the molten mixture of the aforementioned orientation section.

(5) A die for an extrusion moulding as claimed any of Claim 1 to Claim 4 wherein the aforementioned die for an extrusion moulding is used for production of a cylindrical resin bound type magnet.

(6) A die for an extrusion moulding as claimed in Claim 5 wherein a length of the orientation section located from a section at the front end of the said die where a magnetic field is charged and the aforementioned magnetic powder is orientated to an outlet section of the die satisfies

$$1 < d^2 / 2D.$$

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(d and D are the inner diameter and the outer diameter of the molten mixture passage)

(7) A die for an extrusion moulding as claimed in Claim 5 wherein in case a presence of a non-magnetic material in the aforementioned orientation section, a length l' of a contacting section of the magnetic material with a mixture of the magnetic powder and the resin in a molten state satisfies

$$l' < d^2 / (2D).$$

(8) A die for an extrusion moulding as claimed in any of Claim 1 to Claim 7 wherein the aforementioned magnetic powder comprises a ferromagnetic material consisting of rare earth elements (including Y) and transition metals mainly constituting cobalt or a ferromagnetic material consisting of rare earth elements, transition metals mainly constituting iron and boron.

(9) A die for an extrusion moulding of a resin bound type magnet which is moulded by orientating a molten mixture of a magnetic powder and a resin and by solidification with cooling wherein the structure of the said die comprises in orders from a connecting section to an outlet of the orientation section as

(a) Converging section in which a mixture of a magnetic powder and a resin which becomes in a molten state and has fluidity is converged.

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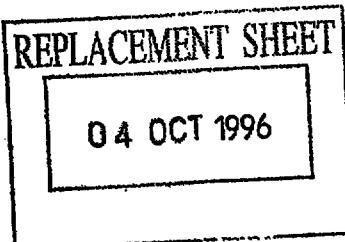
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(b) Heat insulating section to hold a temperature difference between the whole of the die and the rear section.

(c) Heating section in which the viscosity of the molten compound of the mixture in the molten state further drops, and

(d) Orientation section in which a magnetic field is charged, the magnetic powder is orientated and it is solidified with cooling as its state.

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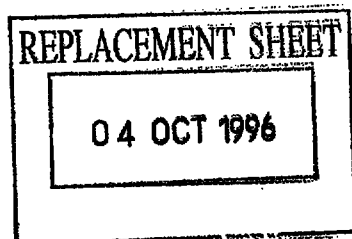


Abstract

Dies For Extrusion Moulding

An extrusion moulding die capable of mass producing cylindrical resin bound type magnets with high performance and superior shape accuracy. The die comprises of the orientation, converging, heat insulating and heating sections. The orientation section consists of different layers of one or more materials having different magnetic and thermal conductivity characteristics. The orientation section applies the magnetic field to the molten mixture; in the converging section, the mixture is pressed into shape; the heat insulating section holds the temperature difference between the rear section of the die and the rest of it; the heating section, lowers the viscosity of the molten mixture. The magnet is moulded from a molten mixture of magnetic powder, thermoplastic organic resin and additives resulting in a mixture with low viscosity and high temperature. The molten mixture is then allowed to cool and solidify in the orientation section.

(Figure 3)



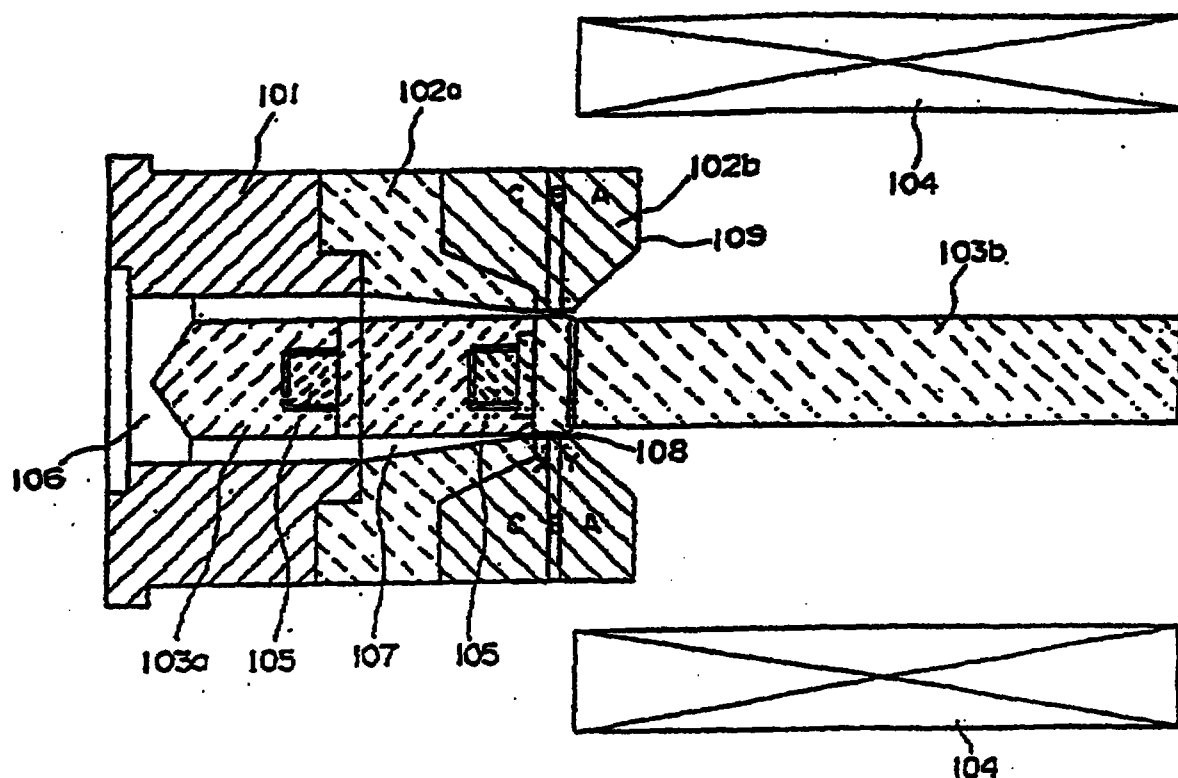


FIGURE 1

- 101 Raw material injection outer die
102a, 102b Moulding section outer die
103a, 103b Mandrel
104 Electromagnetic coil
105 Connection screw
106 Raw material injection section
107 Raw material packing space
108 Orientation section
109 Surface of the outlet of the orientation section
X,Y Temperature measurement point

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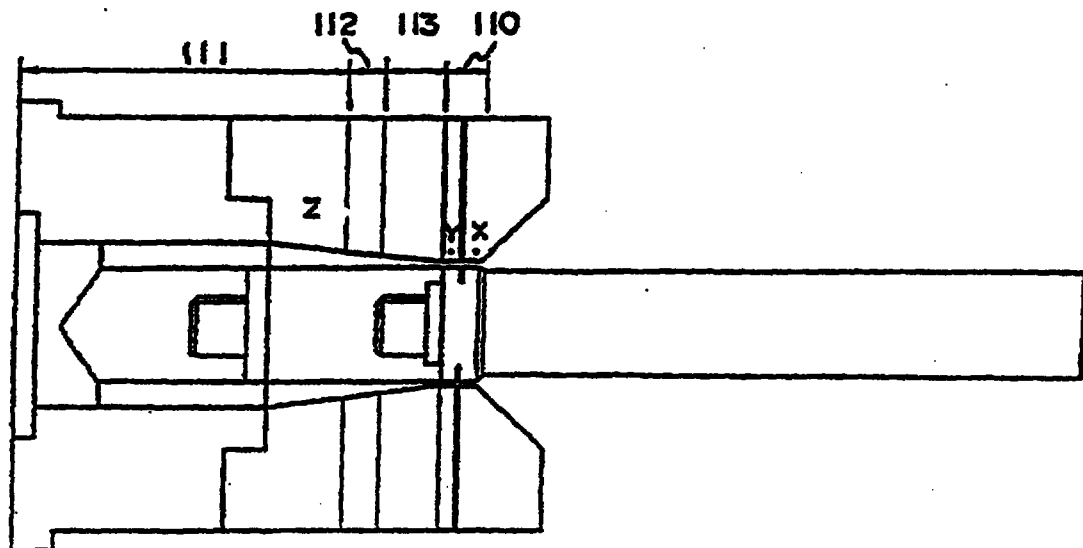
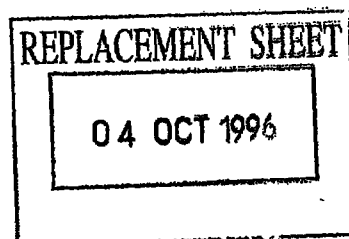


FIGURE 3

- 110. Orientating section
- 111. Converging section
- 112. Heat insulating section
- 113. Heating section
- Z. Temperature measurement point



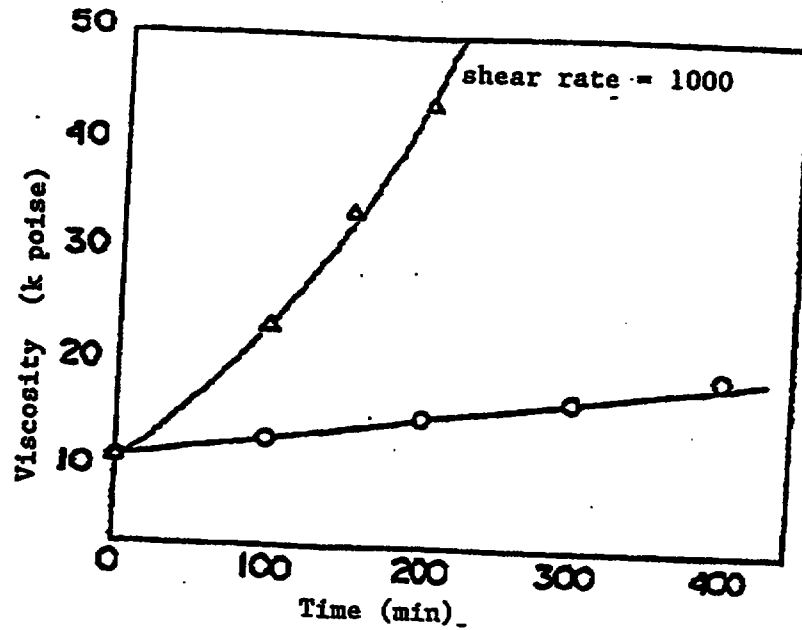


FIGURE 4

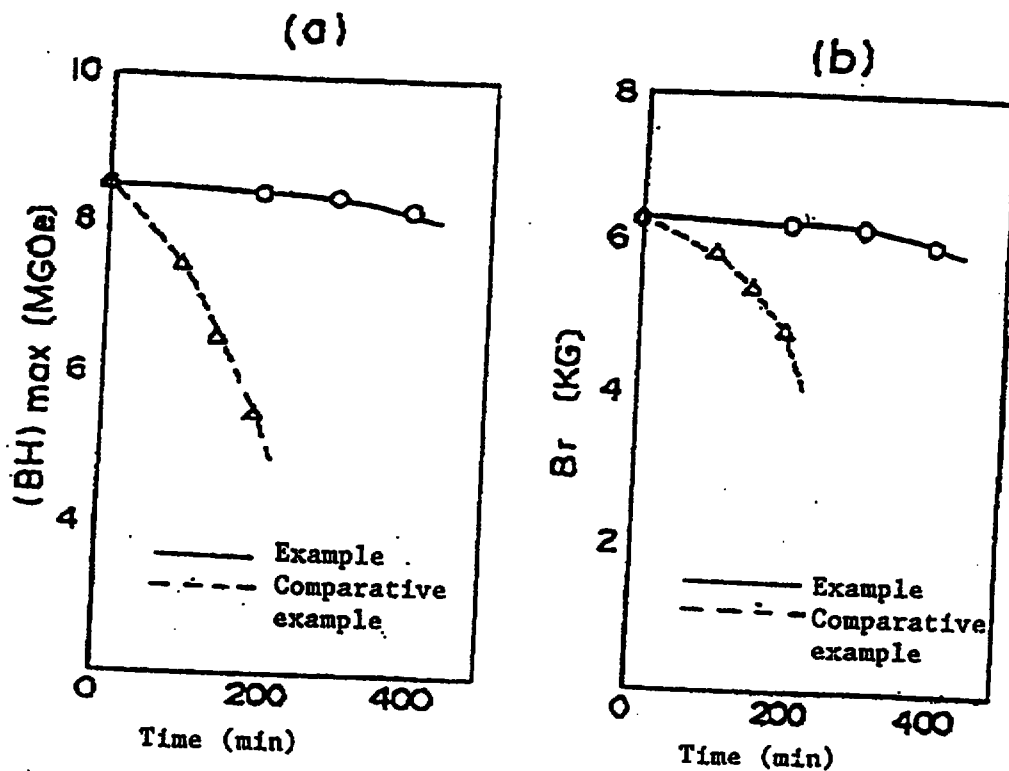


FIGURE 5

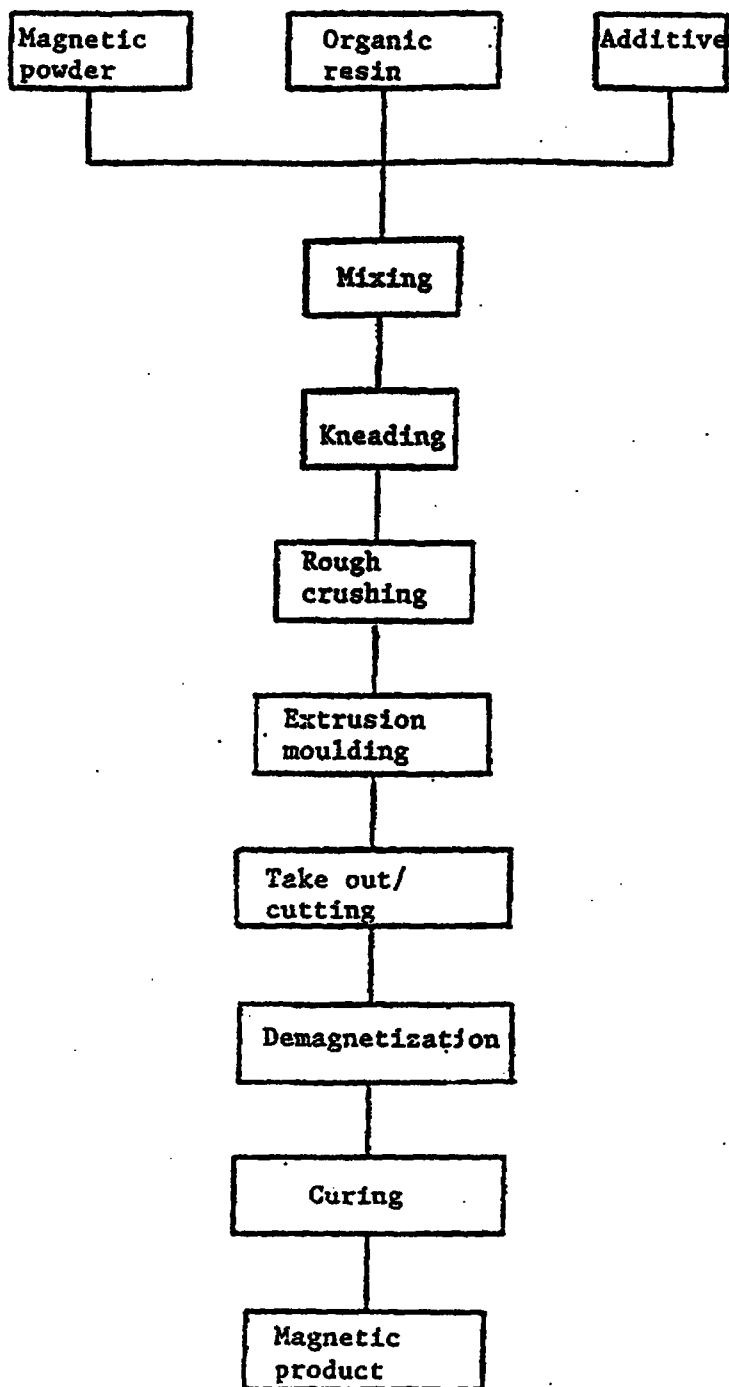
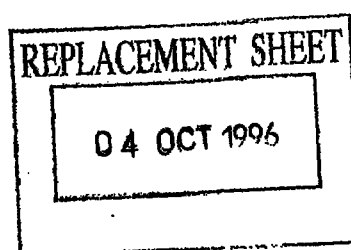


FIGURE 6



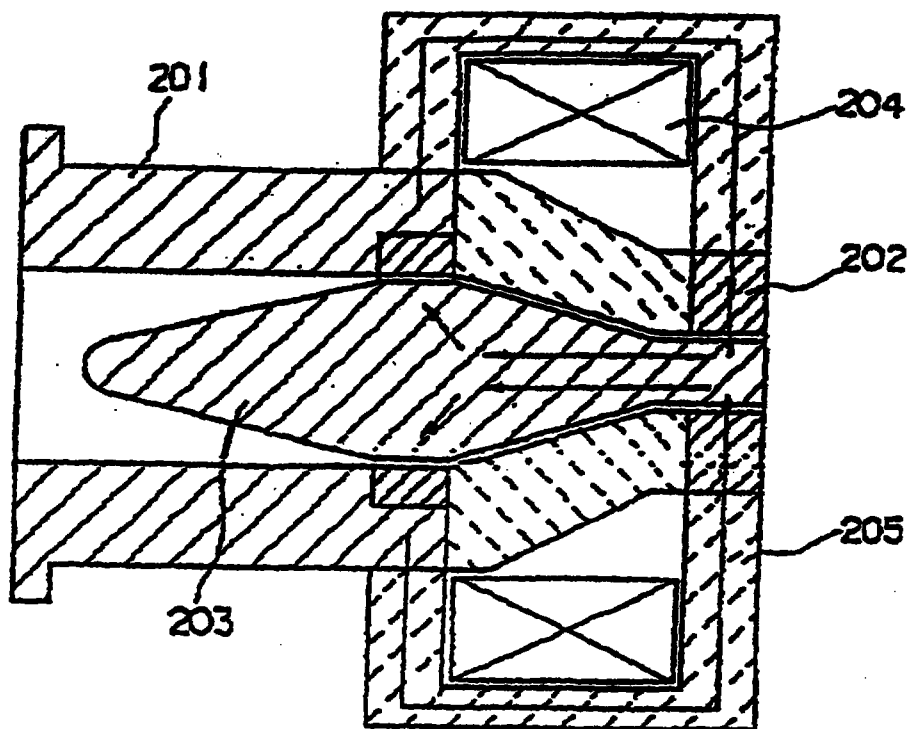


FIGURE 7

- 201 Raw material injection outer die
- 202 Moulding section outer die
- 203 Mandrel
- 204 Electromagnetic coil
- 205 Magnetic material block

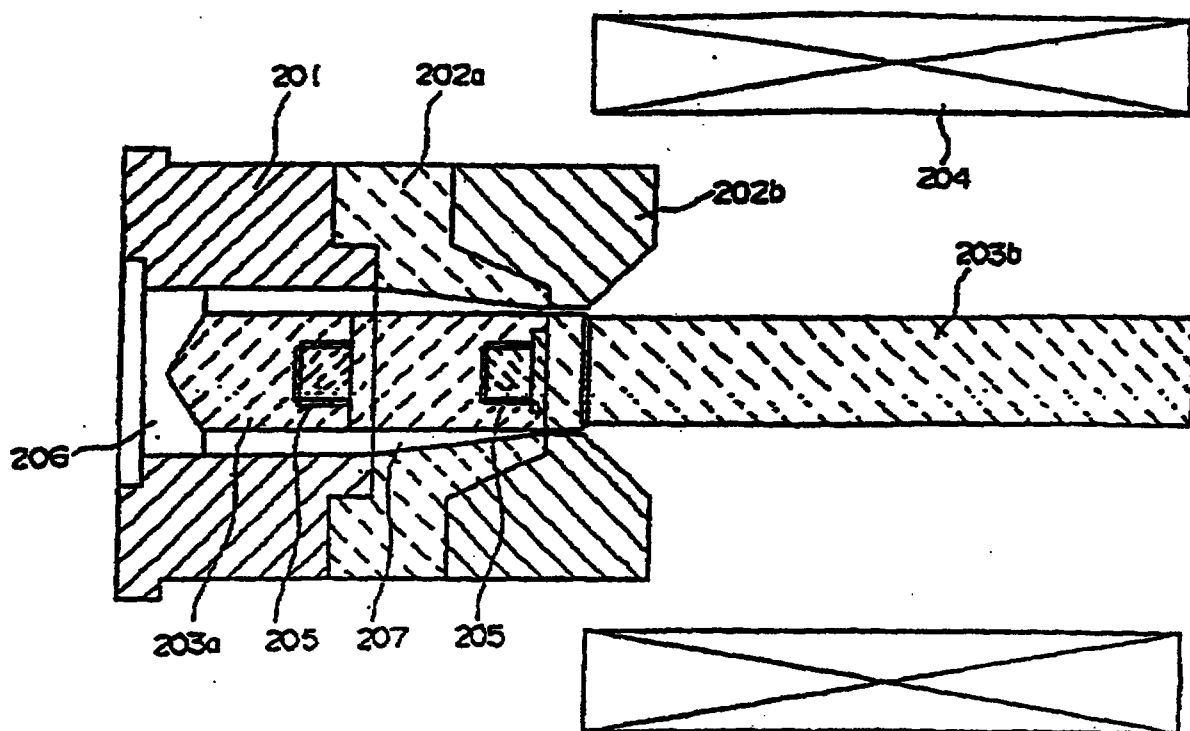


FIGURE 8

- 201 Raw material injection outer die
- 202a, 202b Moulding section outer die
- 203a, 203b Mandrel
- 204 Electromagnetic coil
- 205 Connection screw
- 206 Raw material injection section
- 207 Raw material packing space

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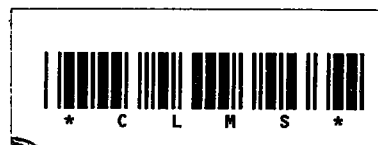
As it is clear from Table 5, the magnetic performance suddenly drops by passing the time in case of Comparative Example. This was due to a decrease of degree of the orientation since the magnetic powder in the compound became difficult to orientate in progress of the elevation of the compound viscosity by time resulting a drop of the magnetic performance.

On the other hand, in case of Example, it is not almost observed the change of the magnetic performance by time, and a high magnetic performance is attained stably.

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☐ Item 4: replaced 24 to page 25	
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(1) A die for an extrusion moulding of a resin bound type magnetic which is moulded by orientating a magnetic powder in a molten mixture of the magnetic powder and a resin and by a solidification with cooling wherein an orientation section located from a section at the front end of the said die where a magnetic field is charged and the aforementioned magnetic powder is orientated to the die section comprises a layer structure with at least one or more of different materials.

(2) A die for an extrusion moulding as claimed in Claim 1 wherein at least one or more of materials of the aforementioned orientation section comprises a magnetic material.

(3) A die for an extrusion moulding as claimed in Claim 1 wherein a layer structure is formed by inserting a low thermal conductive material having the thermal conductivity K (at 20°C) of

$$K < 0.01 \text{ [cal/cm}\cdot\text{sec}\cdot^{\circ}\text{C]}$$

in a part of the aforementioned orientation section.

(4) A die for an extrusion moulding as claimed in Claim 1 wherein the insertion material in the aforementioned orientation section comprises a non-magnetic material, and a thickness of the said non-magnetic material is 1/2 or less of a contacting length with the molten mixture of the aforementioned orientation section.

(5) A die for an extrusion moulding as claimed any of Claim 1 to Claim 4 wherein the aforementioned die for an extrusion moulding is used for production of a cylindrical resin bound type magnet.

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(6) A die for an extrusion moulding as claimed in Claim 5 wherein a length of the orientation section located from a section at the front end of the said die where a magnetic field is charged and the aforementioned magnetic powder is orientated to an outlet section of the die satisfies

$$1 < d^2 / 2D$$

(d and D are the inner diameter and the outer diameter of the molten mixture passage)

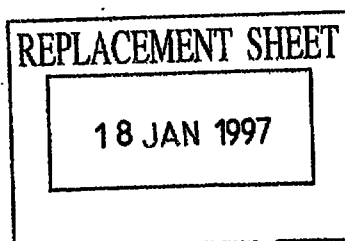
(7) A die for an extrusion moulding as claimed in Claim 5 wherein in case a presence of a non-magnetic material in the aforementioned orientation section, a length 1' of a contacting section of the magnetic material with a mixture of the magnetic powder and the resin in a molten state satisfies

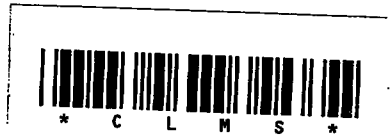
$$1' < d^2 / (2D)$$

(8) A die for an extrusion moulding as claimed in any of Claim 1 to Claim 7 wherein the aforementioned magnetic powder comprises a ferromagnetic material consisting of rare earth elements (including Y) and transition metals mainly constituting cobalt or a ferromagnetic material consisting of rare earth elements, transition metals mainly constituting iron and boron.

(9) A die for an extrusion moulding of a resin bound type magnet which is moulded by orientating a molten mixture of a magnetic powder and a resin and by solidification with cooling wherein the structure of the said die comprises in orders from a connecting section to an outlet of the orientation section as

- (a) Converging section in which a mixture of a magnetic powder and a resin which becomes in a molten state and has fluidity is converged.





- (b) Heat insulating section to hold a temperature difference between the whole of the die and the rear section.
- (c) Heating section in which the viscosity of the molten compound of the mixture in the molten state further drops, and
- (d) Orientation section in which a magnetic field is charged, the magnetic powder is orientated and it is solidified with cooling as its state.

