

Translation**International Patent Application No. PCT/EP2012/063047****An overvoltage-protection device with a coil arrangement**

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The invention relates to a device for protecting a high-frequency terminal from overvoltage.

High-frequency terminals are protected from overvoltages, such
10 as can occur, for example, as a result of lightning, by
providing all inputs and outputs of an amplifier with
protection elements. In EP 1 333 454 A1, a coil comprising an
electrically conductive wire is used for this purpose. A
coarse protection is explained in conjunction with a fine
15 protection. This is achieved in that the coil provides a part
tapering in the direction towards an end of the coil connected
to the high-frequency terminal.

The disadvantage with the coil from EP 1 333 454 A1 is that it
20 must be manufactured using a complex method, because wire must
be wound onto a template. The template comprises a cylinder
and a pin, which is attached to a head end of the cylinder.
This is costly since only small or medium production runs can
generally be manufactured because an electrically conductive
25 wire must be wound onto the cylinder and the pin in a
complicated, special manufacturing process.

The object of the invention is therefore to provide an
overvoltage device which can be manufactured in a cost-
30 favourable manner and realised as far as possible with
standard components.

The object is achieved by the overvoltage device according to
the invention as specified in claim 1. Advantageous further

developments of the overvoltage-protection device according to the invention are specified in the dependent claims.

A coil arrangement according to the invention, which is made
5 up from two or more separate coils in the signal path from the high-frequency terminal to the ground potential with different, increasing inductances, is used in order to protect a circuit, for example, an amplifier, from overvoltages which could damage the components of the amplifier, for example,
10 during a lightning strike. The coils in the signal path are electrically connected in series.

The increasing inductances are preferably realised in that the cross-sections of the individual coils directly adjacent to
15 one another or directly contacted with one another in the signal path increase but remain constant within one coil, so that the cross-sectional areas of the coils with the relatively lower inductance is accordingly smaller than or equal to the cross-sectional areas of the directly contacted
20 or directly adjacent coils with a relatively larger inductance.

As a result of the different cross-sectional areas of the coils, the resonant frequency of the coil with the relatively
25 smaller cross-sectional area is increased because of the associated reduction of the parasitic capacitances of the coil. The operating range of the overvoltage-protection device provided in this manner is extended in the direction towards higher frequencies by comparison with a single coil with
30 constant inductance or cross-sectional area. As a result of the coil with a relatively larger inductance or respectively cross-sectional area, a sufficiently high inductance is secured even for low frequencies, and accordingly, the blind resistance of the coil is disposed significantly above the

rated impedance of the high-frequency terminal (generally 50 ohms). As a result of the high inductance of the coil achieved in this manner, the overall structural length of the coil can be kept small, so that installation within restricted spatial dimensions is also possible. Improved properties are achieved with regard to the individual resonant frequencies by comparison with the conical end disclosed in EP 1 333 454 A1.

Advantageous further developments of the overvoltage device according to the invention can be achieved with the measures specified in the dependent claims.

Exemplary embodiments of the overvoltage-protection device according to the invention are presented by way of example in the drawings and explained in greater detail with reference to the following description. The drawings show:

Figure 1 the prior art with one coil which tapers in a conical manner at one end;

Figure 2 a plan view of a first exemplary embodiment of an overvoltage-protection device according to the invention with a coil arrangement which is made from two separate coils;

Figure 3 a cross-section of the first exemplary embodiment according to the invention with a coil arrangement which is made from two coils;

Figure 4 a cross-section of a second exemplary embodiment according to the invention with a coil arrangement which comprises two coils which are connected to a solder pad; and

Figure 5 a plan view of a third exemplary embodiment according to the invention with a coil arrangement which is made from two separate coils which are largely magnetically decoupled;

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Figure 6 a manufacturing method for a fourth exemplary embodiment according to the invention made from a metal sheet;

10 Figure 7A a coil winding made from a metal sheet of the fourth exemplary embodiment with an arrangement of the metal strip in the longitudinal direction and

Figure 7B a coil winding made from a metal sheet of the
15 fourth exemplary embodiment with an arrangement of the metal strip in the radial direction.

Parts which correspond with one another are shown with the same reference numbers in all of the drawings. In particular,
20 the reference numbers in Figure 1, which relate to the prior art, are shown in agreement with the exemplary embodiments according to the invention.

Figure 1 shows, as the prior art, an overvoltage-protection
25 device for protecting a high-frequency terminal 22 from overvoltage. The high-frequency terminal 22 comprises a through-connected contact 23 and an electromagnetic shield 24. The actual conduction of the signal takes place through the contact 23, which is connected through the interior of the
30 housing 21 and is referred to there as the through-connected contact 23'. The coil 1a is wound from an electric wire. The second connecting element 5 of the coil 1a is contacted to a ground potential 28. In the direction of a coil axis, the coil 1a provides a part 3 tapering in the direction towards an end

of the coil connected to the through-connected contact 23' of the high-frequency terminal 22. The tapering ends at the first connecting element 4, which is connected to the through-connected contact 23' of the high-frequency terminal 22 of a circuit 20 via a soldered connection 30. The components 26 of the circuit 20 are contacted via a high-frequency conductor 27. The overvoltage-protection device is electromagnetically insulated via a metallic housing 21 and a dividing wall 21.1.

By contrast, in the exemplary embodiment shown in Figure 2, the overvoltage-protection device according to the invention for protecting a high-frequency terminal 22 from overvoltage provides a coil arrangement 1 which comprises two or more cylindrical coils in series with n different, cross-sectional areas $A_1, A_2, \dots, A_n$ increasing in size, or respectively, in the case of circular cross-sections, with increasing diameters $d_1, d_2, \dots, d_n$. In this context, n denotes the number of coils. The coil end with the smallest cross-sectional area A_1 is connected to the high-frequency terminal 22 shown in Figure 3 via a first connecting element 4. A second connecting element 5 for the coil end with the largest cross-sectional area A_n is connected either directly or via a current source or voltage source 11 to a ground potential 28. In general, this is a direct voltage (DC) source.

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Figure 2 shows the plan view of the first exemplary embodiment of a device according to the invention for protecting the circuit 20. The structure according to the invention is surrounded by a metallic housing 21. This provides electromagnetic shielding. The coil arrangement 1 guides the through-connected contact 23' of the high-frequency terminal 22 to the current or voltage supply 11. The circuit 20 to be protected or the components 26 to be protected are contacted both to the high-frequency terminal 22 and also to ground

potential 28. The printed-circuit board 25 is metallised over its full area. Only a rectangular cut-out 10 in the metallisation 16 is provided under the coil arrangement 1 or respectively under each of the coils L_1 , L_2 , ..., L_n .

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Figure 3 illustrates a cross-section through the exemplary embodiment of the overvoltage-protection device already explained in Figure 2. The high-frequency terminal 22 is additionally shown. This is guided to the circuit 20 from above. The circuit 20, the coil arrangement 1 and the current or voltage source 11 are disposed on the printed-circuit board 25, which is attached to the housing 21 with support elements 15. A cut-out 12 in the metallic housing 21, which can be manufactured, for example, by milling or with an appropriately shaped die, is disposed directly under the coil arrangement 1. The additional hollow cavity or spacing of the cut-out 12 saves weight and achieves a considerable reduction of parasitic capacitances. The two coils L_1 , L_2 , which form the coil arrangement 1 are electromechanically connected to one another by a length of wire 14.

The coil arrangement 1 is advantageously made up from a first coil L_1 and a second coil L_2 , comprising separate coils, which are electromechanically connected to one another, especially by a soldered connection. The ends of the individual coils L_1 , L_2 are preferably embodied as contact points and can be connected to one another. However, other connections, such as plug connections, welding, twisting or biscuit connectors are also conceivable. The same applies for the further coils L_1 , L_2 , ..., L_n electromechanically contacted or directly connected to one another. In this manner, standard components can be used for the manufacture of the coils 1, so that the costly process of winding a wire onto a template can be dispensed with according to the invention.

The exemplary embodiment illustrated in Figure 4 differs from Figure 3 in that the connection of the two coils L_1 , L_2 is not provided through a connection with a simple length of wire,
 5 but the projecting legs 19 of the coils L_1 , L_2 are attached to a solder pad 18 preferably by reflow soldering, that is, the electromechanical connection of the separate coils L_1 , L_2 , ..., L_n is achieved with solder pads 18 which are contacted with legs 19 of the coils L_1 , L_2 , ..., L_n . On its rear side, the
 10 solder pad 18 also provides a metallisation 17 which is contacted to the ground potential 28.

The ends of the individual coils L_1 , L_2 are preferably embodied as contact points and can therefore simply be
 15 electromechanically connected to a solder pad 18 or a printed circuit board 25. The legs 19 can be optimised for reflow soldering. For example, the shape of the legs 20 can be adapted by means of pressing tools. Accordingly, the coil 1 according to the invention can be manufactured simply, rapidly
 20 and in a cost favourable manner in medium to large production runs.

In a further embodiment, the leads h between the individual coil portions differ, so that both the inductance and also the
 25 capacitance of the individual coil portions vary. In particular, the inductance L is varied in that, in equation 1, the number of windings N progresses in a quadratic manner, while the lead h between the individual windings in equation 2, determines the capacitance C in a reciprocal manner. A is
 30 the cross-sectional area, μ is the permeability and ϵ is the dielectric constant

$$L = \mu * N^2 / l * A \quad (1)$$

$$C = \varepsilon * A / h \quad (2)$$

The frequency range which can be covered by the coil arrangement 1 can be further increased in that the wire diameter of the second coil L_2 is larger than the wire diameter of the first coil L_1 , or respectively, in that the wire diameter increases or at least remains constant with an increasing cross-sectional area $A_1, A_2, \dots, A_n$ or inductance of the individual coils $L_1, L_2, \dots, L_n$, so that the wire diameter of the coils $L_1, L_2, \dots, L_n$ with relatively lower inductance is smaller than or equal to the wire diameter of the coil with the relatively larger inductance $L_1, L_2, \dots, L_n$ directly electrically contacted or directly adjacent to the named coil $L_1, L_2, \dots, L_n$.

This has the advantage that the capacitance between the individual windings in the signal path from the high-frequency terminal 22 to the ground potential 28 of the observed coil L_k is smaller than the capacitance between the windings of the directly following coil L_{k+1} in each case. In this context, k is a natural number with values from 1 to $n-1$. As a result of the associated, relatively lower parasitic capacitance of the observed front coil L_k , the resonant frequency is increased, so that the operating range of the overvoltage-protection device is accordingly additionally extended towards relatively higher frequencies. This effect cannot be achieved in technical production with a single conical coil, because this would then necessitate different wire thicknesses along its length, so that it could be wound onto a template.

The electrically conductive wire preferably comprises lacquered copper wire with a cross-sectional area of $0.1 - 1 \text{ mm}^2$. The cross-sectional area of the wire determines the maximum current, which can be drained, for example, in the

event of a lightning strike. In one advantageous embodiment, the individual windings of the coil arrangement 1 are wound tightly together.

5 In a further embodiment of the invention, as shown in Figure 6, coils can be manufactured by separating extremely elongated rectangles 6 of length l , width b and thickness h from a thin sheet 7 preferably made of metal, for example, by cutting, especially with a laser, or by punching.

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In an embodiment illustrated in Figure 7A, coils $L_1, L_2, \dots, L_n$ of low capacitance, that is, with a high resonant frequency, are wound in such a manner that the thickness d determines the capacitance between the individual windings of the coils $L_1,$
15 $L_2, \dots, L_n$. By preference, the coils $L_1, L_2, \dots, L_n$ of this design of the perpendicular type 31, as illustrated in Figure 7A, also provide a small cross-sectional area $A_1, A_2, \dots, A_n$. With this design, the relatively narrower surfaces, which correspond to the thickness of the metal sheet and are not
20 illustrated in Figure 7A and Figure 7B, are disposed opposite to one another.

In a further design illustrated in Figure 7B of the flat type 32, coils $L_1, L_2, \dots, L_n$ with a high capacitance with an
25 approximately identical inductance by comparison with Figure 7A, that is, of low resonant frequency, are wound in such a manner that the width b determines the capacitance between the individual windings of the coils $L_1, L_2, \dots, L_n$. With the shape of the coil of the flat type 32, the relatively larger
30 surfaces are disposed opposite to one another. In this manner, the maximum possible current in all coils $L_1, L_2, \dots, L_n$ of the coil arrangement 1 can be of the same magnitude, but a further degree of freedom is obtained for adjusting the inductance or respectively the capacitance of the individual

coils $L_1, L_2, \dots, L_n$. In particular, the resonant frequency can be reduced, if the capacitance between the windings of a coil $L_1, L_2, \dots, L_n$ is increased by positioning the flat sides of the windings with a small spacing distance from one
 5 another.

If the flat sides are positioned facing radially outwards, that is, so that the normal of the flat side faces radially outwards, ideally with a large spacing distance from the coil
 10 windings, a very high resonant frequency is obtained, because the coils $L_1, L_2, \dots, L_n$ provides a low capacitance and inductance.

Figure 6 and Figures 7A and 7B are not shown to scale for
 15 reasons of improved visual orientation. However, the ratio $1 \gg b > 3h$ applies, and the cross-sectional area of the current-conducting, metallic strip 6 wound into a coil $L_1, L_2, \dots, L_n$ should be constant in the case of coils $L_1, L_2, \dots, L_n$ in a coil arrangement 1.

20 It is advantageous that the ratio of the inductances of the first coil L_1 relative to the second coil L_2 or respectively two coils L_1, L_2 directly electrically contacted or directly adjacent to one another is disposed between 4 to 1 and 16 to
 25 1, preferably at approximately 8 to 1. The diameters of the second and the first coil L_2, L_1 provide a ratio between 1.5 to 1 and 3 to 1, particularly advantageously a ratio from 2 to 1. Typical diameters of the first round coil L_1 are disposed between 1 mm and 4 mm, especially 2 mm. Typical diameters of
 30 the second round coil L_2 are disposed between 1 mm and 4 mm, especially 2 mm. The diameter of the first coil L_1 should advantageously be smaller than the diameter of the second coil L_2 .

Further possible embodiments are formed by coils with rectangular or oval cross-section instead of circular.

The corresponding cross-sectional areas A_1 , A_2 for round coils
 5 can be determined with reference to equation 3, in which A denotes the cross-sectional area and d denotes the diameter.

$$A = \pi \cdot (d/2)^2 \quad (3)$$

10 Accordingly, a corresponding cross-sectional area A_1 of the first coil L_1 between 0.78 mm^2 and 12.57 mm^2 , especially 3.14 mm^2 is obtained. The corresponding cross-sectional area A_2 of the second coil L_2 is between 3.14 mm^2 and 28.27 mm^2 , especially 12.56 mm^2 . In general, the lengths of the
 15 individual coils with different diameter or respectively different cross-sectional area are approximately identical.

The overvoltage device is conventionally disposed on a printed circuit board 25 metallised over its entire surface, which is
 20 contacted to ground potential 28. Parasitic capacitances between the coils L_1 , L_2 , ..., L_n and the printed-circuit board 25 can be significantly reduced through cut-outs 10 in the metallisation 16 of the printed circuit board 25, especially rectangular cut-outs under the coils L_1 , L_2 , ..., L_n .

25 According to the invention, the coil arrangement 1 is preferably implemented as an air coil. An air coil provides the advantage of a low mass. However, especially in the case of different leads h , it is advantageous to provide coil
 30 portions with a soft-magnetic core, so that each coil portion L_1 , L_2 , ..., L_n can be optimised individually, without influencing the other coil portions L_1 , L_2 , ..., L_n via stray fields or influencing the coil portion L_1 , L_2 , ..., L_n . It may

also be advantageous to provide only certain coil portions L_1 , L_2 , ..., L_n with a magnetic core.

As an alternative, in a further embodiment, a decoupling of
5 the individual coil portions L_1 , L_2 , ..., L_n can be largely
achieved, as shown in Figure 5, in that the directly,
electromechanically contacted or adjacent coil portions are
orientated in different directions relative to one another,
preferably orthogonally. Accordingly, the magnetic fields of
10 the individual coil portions L_1 , L_2 , ..., L_n hardly influence
one another. However, coil portions L_1 , L_2 , ..., L_n not
directly adjacent or not directly contacted can also be
arranged with a parallel orientation, provided the coil
portions L_1 , L_2 , ..., L_n are disposed with an adequate
15 geometric spacing distance from one another, for example,
approximately 5 mm. The cut-outs 10 in the metallisation 16
under the individual coils L_1 , L_2 , ..., L_n are advantageously
rectangular and can overlap as illustrated in Figure 5.

20 A further alternative for the electromagnetic decoupling of
the coils L_1 , L_2 , ..., L_n is to attach, in each case between
the individual, especially the directly electrically contacted
or mutually, directly adjacent coils L_1 , L_2 , ..., L_n , a
metallic, ideally non-magnetisable, electrically conductive
25 plate 9, which is electrically connected to ground potential
28, as illustrated in Figure 2. The plate 9 can be attached
with support elements 15 to the printed circuit board 25 or to
the housing 21.

30 It is also advantageous, if the outer regions of the coil
arrangement 1 are distanced, for example, by at least 3 mm
from the housing 21 and/or from electrically conductive parts.
This significantly reduces the influence of parasitic
capacitances. The housing 21 is generally also connected to

ground potential 28. However, in order to occupy as little volume as possible, the spacing distance should not be greater than 10 mm. A spacing distance of, for example, approximately 5 mm is therefore selected by preference.

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According to the invention, all of the devices described can also be realised with more than two coils and combined with one another. All of the features described or illustrated can be combined with one another as required within the scope of

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the invention.

Claims

- 5 1. An overvoltage-protection device for protecting a high-frequency terminal (22) from overvoltage, which provides a coil arrangement (1),
characterised in that
the coil arrangement (1) comprises several separate coils
10 ($L_1, L_2, \dots, L_n$), which are electrically connected in series with different, increasing inductances.
2. The overvoltage-protection device according to claim 1,
characterised in that
15 the coil (L_1) with the lowest inductance is connected electromechanically via a first connecting element (4) to the high-frequency terminal (12), and the coil (L_n) with the highest inductance is connected either directly via a second connecting element (5) or via a current source or
20 voltage source (11) to a ground potential (28).
3. The overvoltage-protection device according to any one of the preceding claims,
characterised in that
25 the cross-sectional areas ($A_1, A_2, \dots, A_{n-1}$) of the coils with the relatively lower inductance ($L_1, L_2, \dots, L_{n-1}$) is smaller than or equal to the cross-sectional areas ($A_2, \dots, A_n$) of the directly adjacent or directly contacted coils with the relatively larger inductance ($L_2, \dots, L_n$).
30
4. The overvoltage-protection device according to any one of the preceding claims,
characterised in that

the coil arrangement (1) comprises several separate coils ($L_1, L_2, \dots, L_n$), which are connected electromechanically to one another in each case via a soldered connection.

- 5 5. The overvoltage-protection device according to claim 4,
characterised in that
the electromechanical connection of the separate coils ($L_1, L_2, \dots, L_n$) is embodied through solder pads (18), which are contacted with legs (19) of the coils ($L_1, L_2, \dots, L_n$).
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6. The overvoltage-protection device according to any one of the preceding claims,
characterised in that
15 the wire diameter of the coils ($L_1, L_2, \dots, L_{n-1}$) with the relatively lower inductance is smaller than or equal to the wire diameter of the coil with the relatively larger inductance ($L_2, L_3, \dots, L_n$) directly electrically contacted with or adjacent to this coil ($L_1, L_2, \dots, L_{n-1}$).
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7. The overvoltage-protection device according to any one of the preceding claims,
characterised in that
the ratio of the inductances of two coils (L_k, L_{k+1})
25 directly electrically contacted with or directly adjacent to one another is disposed between 4 to 1 and 16 to 1, preferably at approximately 8 to 1.
8. The overvoltage-protection device according to any one of
30 the preceding claims,
characterised in that
the overvoltage-protection device is disposed on a metallised printed circuit board (25).

9. The overvoltage-protection device according to claim 8,
characterised in that
a cut-out (10) in the metallisation (16) of the printed
circuit board (25) is disposed under the coils (L_1 , L_2 ,
5 ..., L_n).
10. The overvoltage-protection device according to any one of
the preceding claims,
characterised in that
10 the external dimensions of the coil arrangement (1) are
disposed between 3 mm and 10 mm, preferably 5 mm, away
from a housing (21) and/or from electrically conductive
parts.
- 15 11. The overvoltage-protection device according to any one of
the preceding claims,
characterised in that
the coils (L_1 , L_2 , ..., L_n) directly electromechanically
connected or directly adjacent to one another are arranged
20 orthogonally relative to one another.
12. The overvoltage-protection device according to any one of
the preceding claims,
characterised in that,
25 metallic and/or non-magnetisable but electrically
conductive plates (9) which are electrically connected to
the ground potential (28) are arranged between the coils
(L_1 , L_2 , ..., L_n) directly electromechanically connected or
directly adjacent to one another.
- 30 13. The overvoltage-protection device according to any one of
the preceding claims,
characterised in that

the cross-sectional area ($A_1, A_2, \dots, A_n$) of the coils ($L_1, L_2, \dots, L_n$) has the shape of a circle, a rectangle or an oval.

- 5 14. The overvoltage-protection device according to any one of the preceding claims,
characterised in that
the cross-sectional area of the coil wire is rectangular
and/or that the coils ($L_1, L_2, \dots, L_n$) are manufactured by
10 separating a long rectangle from a metal sheet.
15. The overvoltage-protection device according to any one of the preceding claims,
characterised in that
15 the coils ($L_1, L_2, \dots, L_n$) with low inductance are wound in such a manner that the thickness of the coil wire determines the capacitance between the individual windings of the coils ($L_1, L_2, \dots, L_n$), in that the relatively smaller surfaces of the coil wire face towards one
20 another, and/or that coils ($L_1, L_2, \dots, L_n$) with high inductance are wound in such a manner that the width (b) of the coil wire determines the capacitance between the individual windings of the coils ($L_1, L_2, \dots, L_n$), in that the relatively larger surfaces of the coil wire face
25 towards one another.