

A Noise Reduction Circuit With Monitoring Functionality

Background and Field of the Invention

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This invention relates to a noise reduction circuit with monitoring functionality, particularly but not exclusively for a headphone.

Headphones with passive noise reduction are usually equipped with ear
10 cushions that completely enclose the ears (i.e. circumaural) and the cushions provide passive reduction or isolation from ambient noise. The extent of reduction is largely dependent on the nature of the ambient noise and the acoustics characteristics of ear cushions of the headphone. Due to the characteristics of the ear cushions, most passive noise reduction headphones
15 attenuate the higher frequency components (approximately from 200 Hz and above) of the ambient noise, and the lower frequency components would still be heard by a user of the headphone. As a result, such passive headphones may not provide sufficient or effective noise reduction in certain noisy environments.

20 To address the above problem, active noise reduction circuits have been provided in headphones and such circuits are configured to eliminate or attenuate lower frequency components of the ambient noise to result in more effective noise attenuation. Ideally, ambient noise waveform is detected and an identical anti-noise waveform, which is equal in magnitude, but of opposite

polarity is produced. Interaction of the noise waveform with the anti-noise waveform results in cancellation of the noise waveform.

It is an object of the present invention to provide a noise reduction circuit with
5 monitoring function which provides a useful alternative to similar known circuits.

Summary of the Invention

In a first aspect of the invention, there is provided a noise reduction circuit with
10 monitoring functionality for a headphone having at least one speaker driver, the circuit comprising:

- a microphone configured to convert ambient sound into a corresponding electrical ambient signal, the microphone being disposed adjacent to the speaker driver's diaphragm;
- 15 an active noise reduction path configured to provide active noise reduction of the ambient sound based on the corresponding electrical ambient signal;
- a vocal signal compensation path configured to restore attenuated signals within the vocal range of the corresponding electrical ambient signal to increase audibility of vocal signals of the ambient sound; and
- 20 a switching device arranged to selectively deliver the corresponding electrical ambient signal to the active noise reduction path or to the vocal signal compensation path.

Preferably, the vocal signal compensation path comprises a vocal clarity
25 compensator configured to enhance the frequency response of the attenuated

signal within the vocal range. The vocal clarity compensator may include a band pass filter and a signal amplifier coupled to the band pass filter's output. In an alternative, the vocal clarity compensator may include more than one band pass filter cascaded in parallel. In a further alternative, the vocal clarity compensator
5 may include a high pass filter.

The frequency response may be dependent on both construction and design of earcups of the headphone, the frequency response being between 200 Hz and 1 KHz of the vocal range.

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Preferably, the noise reduction circuit further comprises a microphone amplifier arranged to amplify the corresponding electrical ambient signal, and wherein the switching device is arranged to receive the amplified corresponding electrical ambient signal.

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Advantageously, the active noise reduction path includes an active-noise cancellation filter. The microphone may be arranged to face the user. In addition, or as an alternative, the microphone may be arranged at the front of the speaker driver's diaphragm.

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It is envisaged that the noise reduction circuit described above may be incorporated in a headphone, and this forms a second aspect of the invention.

Brief Description of the Drawings

An embodiment of the invention will now be described, by way of example, with reference to the accompanying drawings in which,

5 Figure 1 is a schematic diagram of a headphone 100 including an active noise reduction circuit of the present invention;

 Figure 2 is a block diagram showing the active noise reduction circuit of Figure 1 which includes a vocal clarity compensator;

 Figure 3 shows a generic passive isolation frequency response provided
10 by the headphone 100 of Figure 1;

 Figure 4 is a schematic diagram of the vocal clarity compensator of Figure 2;

 Figure 5 is a graph showing the effects of the vocal clarity compensator of Figure 2; and

15 Figure 6 is a schematic diagram of a variation of the vocal clarity compensator of Figure 4.

Detailed Description of the Preferred Embodiment

20 Figure 1 is a schematic diagram showing a headphone 100 including a pair of earcups 102a, 102b connected by a headband 104. Each earcup 102a, 102b includes an ear cushion 106a, 106b of circumaural type and is arranged to be fit around an ear. Each of the earcups 102a, 102b includes a speaker driver 108 (only one is shown in Figure 1 to prevent clutter in the figure) having a
25 diaphragm 110. The headphone 100 also includes an active noise reduction

circuit 200 with monitoring functionality (not shown in Figure 1) which includes a microphone 112. The microphone 112 is disposed adjacent the front of the diaphragm 110 and arranged to face the ear of a user. The microphone 112 is positioned to face the ear of the user so as to detect ambient noise which is audible to the ear of the user. Audio output emanating from the speaker driver 108 may be cancelled using phase inversion by the active noise cancellation circuit 200, the active noise cancellation circuit 200 being described in greater detail at a subsequent section of the description.

10 The microphone 112 is arranged in front of and in close proximity to the speaker driver's diaphragm 110 and arranged to face the ear so as to more accurately pick up the undesired ambient noise which would be picked up by the ear. During monitoring mode, the microphone 112 is also used to pick up desired ambient sound such as speech or voice communication. The preferred
15 embodiment of the present invention will be described in greater detail such that the undesired ambient noise is accurately picked up and yet desired ambient sound is still satisfactorily compensated through the use of the microphone 112.

Figure 2 is a block diagram of the active noise reduction circuit 200 incorporated
20 within one of the earcups 102b of the headphone 100. The active noise reduction circuit 200 is housed within a casing of the earcup 102b and includes a microphone preamplifier 202, a first switching device 204, an Anti-Noise Cancellation (ANC) filter 206, a vocal clarity compensator 208, a second switching device 210, an adder 212 and a headphone amplifier 214.

As mentioned earlier, the microphone 112 is arranged to receive both undesired and desired sound waves. The microphone 112 converts this to electrical energy and provides this as a feedback signal to the microphone preamplifier 202 that boosts the gain of the feedback signal before passing the signal to the first switching device 204. The first switching device 204 includes a switch 204a and two connectors 204b, 204c. When the switch 204a makes contact with the first connector 204b, this creates an active noise reduction path for the boosted feedback signal to travel to the ANC filter 206. When the switch 204a makes contact with the second connector 204c, this creates a vocal signal compensation path for the boosted feedback signal to be directed to the vocal clarity compensator 208.

The ANC filter 206 is configured to compensate for inadequacies of the passive ear cushion 106b in cancelling low frequency components of the ambient noise. In this regard, the ANC filter 206 is arranged to filter and amplify the boosted feedback signal to allow the low frequency components of the undesired ambient sound (i.e. noise) to pass to the second switching device 210. The second switching device 210 may have a same configuration as the first switching device 204 and it comprises a switch 210a with two connectors 210b, 210c. When the switch 210a makes contact with the first connector 210b, this delivers the filtered feedback signal from the ANC filter 206 to the adder 212.

The adder 212 has two inputs 212a, 212b and an output 212c with the first input 212a configured as a positive polarity whereas the second input 212b is configured as a negative input. The first input 212a is connected to an audio

compensator 216 which in turn is connected to an audio source 218, which delivers or streams audio signals, such as music or a sound track of a video, to the earcups 102a, 102b. As part of the audio source 218 may be distorted or lost (adversely affected in relation to quality) with the implementation of the active noise cancellation, the audio compensator 216 restores the audio input to its original waveform and provides this as an audio input to the first input 212a of the adder 212.

The second input 212b is connected to the second switching device 210 and in view of its negative polarity, this inverts the polarity of the filtered feedback signal from the ANC filter 206 to create an anti-noise signal. The output of the adder 212 is a combined signal comprising the audio input and the anti-noise signal which is then passed to the headphone amplifier 214. The headphone amplifier 214 is arranged to boost the gain of the combined signal for processing by the headphone driver 108. On receipt of the combined signal, the headphone driver 108 converts the combined signal into sound waves of the audio input and the anti-noise signal. The anti-noise signal is intended to cancel out the low frequency noise components picked up by the ear and which are not attenuated by the ear cushions 106a, 106b. In this way, active noise reduction or cancellation is achieved.

It is advantageous for the user of the headphone 100 to be able to listen to the ambient sound when required for example, when the user is engaged in a conversation with another person while using the headphone 100. This improves the ease of use and speech (conversational) audibility of the

headphone 100. The first and second switching devices 204, 210 are used as a toggle to allow the user of the headphone 100 to select whether the feedback signal is to be delivered to either the active noise reduction path in which the ambient sound is blocked/reduced, or to the vocal signal compensation path in which the ambient sound, such as speech, is enhanced to increase the audibility to the user. Because of the location of the microphone 112, this creates difficulty for the microphone 112 to pick up desired ambient sound which is external to the headphone 100. However, this is addressed by the vocal clarity compensator 208.

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The vocal clarity compensator 208 has an input connected to the second connector 204c of the first switching element 204 and an output connected to the second connector 210c of the second switching element 210. To activate the vocal clarity compensator 208, the user activates a monitor mode by selecting the switch 204a of the first switching device 204 and the switch 210a of the second switching device 210 to make contact with the second connectors 204c and 210c respectively. It should be appreciated that signals passing through the vocal clarity compensator 208 are out of phase, and thus the second switching element 210 is required such that signals passing through the audio compensator 216 and the signals passing through the vocal clarity compensator 208 are in phase.

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Configuration of the vocal clarity compensator 208 is based on a study of the passive isolation frequency response of the active noise reduction headphone 100 of Figure 1. A generic passive isolation frequency response is shown in

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Figure 3. The low frequency components of the ambient noise which are below f_0 , are not blocked by the passive isolation (provided by the ear cushions 106a, 106b) of the earcups 102a, 102b. Higher frequency components above f_0 of the ambient noise are reduced tremendously by the passive isolation. At frequency f_1 , the reduction in audio level may be -20 dB lower than the audio level at f_0 . Human vocal range during normal conversation is typically between 90 Hz to 400 Hz. The fundamental voice frequency and its higher harmonics present a complete vocal profile of a person. Therefore, without the vocal voice compensator 208, it is not ideal for a normal conversation to take place when a user is using the headphone 100. For example, if the passive isolation starts attenuating only from 200 Hz, it is evident that only a portion of the human vocal range is heard and the speech will be unclear. As a result, the vocal clarity compensator 208 is configured to restore the attenuated level of the ambient noise between f_0 and f_1 to 0 dB (see broken line of Figure 3) for audible speech during conversation to be received by the headphone 100 user.

Due to Helmholtz resonance, a typical feedback active noise cancellation headphone continuously produces high pitch noise at frequency f_1 . It should be noted that values of f_0 and f_1 are dependent on both construction and design of the earcups 102a, 102b. However, it is highly likely that both the values of f_0 and f_1 will fall within the human vocal range of between 90 Hz to 400 Hz. Therefore, it should be appreciated that in the restoration of the vocal signal by the vocal clarity compensator 208, it is recommended for frequencies at f_1 and higher to be filtered off. For optimum performance, the vocal clarity compensator 208 operates in the region from f_0 to f_1 to restore the attenuated

audio level. This effectively widens the audible frequency bandwidth to include the vocal range fundamental frequency and its second or third harmonics. As a result, this preserves the vocal range integrity and the user is able to enjoy a robust and clear conversation.

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A schematic diagram of the vocal clarity compensator 208 is shown in Figure 4 and this includes a multiple feedback (MFB) band pass filter 220 and a signal amplifier 222. The MFB filter 220 includes an op-amp U100 with a negative polarity input 226, a positive polarity input 228 tied to ground, and a filter output 230. The negative polarity input 226 is electrically coupled to a compensator input 224 via capacitors C100, C102 and resistors R100, R101. The compensator input 224 is connected to the second connector 204c of the first switching device 204. The MFB filter 200 includes feedback resistor R102 and feedback capacitor C101 which are coupled between the filter output 230 and the negative polarity input 226.

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The signal amplifier 222 includes op-amp U101 configured as an inverting amplifier. The op-amp U101 has a negative polarity input 232, a positive polarity input 234 tied to ground and an amplifier output 236 electrically coupled to the second connector 210c of the second switching device 210. A resistor R104 is coupled between the amplifier output 236 and the negative polarity input 232 and this together with the resistor R103 provides the gain for the inverting amplifier U101. The negative polarity input 232 is coupled to the filter output 230 of the MFB band pass filter 220 via a DC blocking capacitor C103.

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The MFB band pass filter 220 is configured to be high gain and high quality factor with mid-frequency centred at a selected frequency based on the passive isolation profile of the headset 100. The mid-frequency is centred between f_0 and f_1 , as shown in Figure 3 in order to avoid the Helmholtz resonance. Table 1 tabulates the components used in the circuitry shown in Figure 4 and their corresponding values so as to achieve the filter gain, quality factor and mid-frequency below:

Filter Gain, $K = -16.7$
 Quality Factor, $Q = 8.1$
 Mid-frequency, $f_m = 915 \text{ Hz}$

Components	Value
R100	5.6 K Ω
R101	1.2 K Ω
R102	300 K Ω
R103	4.7 K Ω
R104	47 K Ω
C100	1.0 μF
C101	15 nF
C102	6.8 nF
C103	1.0 μF

Table 1: Components value for circuitry shown in Figure 4

It should be appreciated that the values of various components in Table 1 are merely illustrative and should not be deemed to be limiting in any form or manner.

5 When the user of the headphone 100 wants to select the monitoring mode, the user selects the switches 204a, 210a accordingly so that the boosted feedback signal from the microphone amplifier 202 is now delivered to the vocal clarity compensator 208 and the ANC function of the ANC filter 206 is correspondingly disabled. This means that ambient signals or sound picked up by the
10 microphone 112 is conveyed to the vocal clarity compensator 208 instead of the ANC filter 206. As explained above, the vocal clarity compensator 208 is configured to restore the attenuated signals caused by the passive isolation, especially the signals within the vocal band.

15 Figure 5 is a graph showing the effects of the vocal clarity compensator 208. The graph includes a first frequency response 238 (broken lines) of a first speech signal without passing through the vocal clarity compensator 208 and it can be seen that ambient signals begin to be attenuated by the passive isolation (by the earcups 106a, 106b) from about 200Hz onwards. The graph
20 also includes a second frequency response 240 of a second speech signal which is passed through the vocal clarity compensator 208. Both the first and second speech signals are picked up by the microphone 112 and as it can be appreciated, the vocal clarity compensator 208 is able to boost or extend the frequency response 240 of the second speech signal between the frequencies
25 200Hz and 1KHz, and specifically, the vocal bandwidth is restored to 0dB at

about the 700 Hz mark as shown by juncture A. In this way, the vocal clarity compensator 208 is able to compensate for the attenuation by the passive isolation.

5 In use, when the user of the headphone 100 is listening to the audio being streamed from the audio source 218 to the earcups 102a, 102b, the switch 204a of the first switching device 204 and the switch 210a of the second switching device 210 are selected to be connected to the respective first connectors 204b, 210b. The microphone 112 picks up the ambient signals,
10 which would mostly be the low frequency components since the high frequency components are blocked by the passive isolation provided by the ear cushion 106a, 106b. The microphone 112 then delivers the picked up ambient signals as the feedback signal to the microphone amplifier 202 and then to the ANC filter 206 so that an anti-phase signal of the feedback signal is produced to
15 cancel out the ambient signals picked up by the microphone 112.

When the user wants to engage in a conversation or listen to the ambient sound without having to remove the headphone 100, the user selects the switch 204a of the first switching device 204 and the switch 210a of the second switching
20 device 210 to connect to the respective second contacts 204c, 210c and the feedback signal from the microphone 112 is then delivered to the vocal clarity compensator 208, instead of the ANC filter 206. The vocal clarity compensator 208 processes the feedback signal (from the microphone amplifier 202) to boost the gain of the feedback signal so that the user is able to hear a clearer ambient
25 sound and thus, have a more robust conversation.

As an alternative to the configuration of Figure 4, wider vocal bandwidth may be restored if cascaded MFB bandpass filters are used and Figure 6 shows an example. To elaborate, with reference to Figure 6, there are two MFB filters 220', 220" of Figure 4 cascaded in parallel with an input coupled to the second connector 204c of the first switching device 204. The outputs of the cascaded MFB filters 220', 220" are coupled to a signal amplifier 222' which has a similar configuration as the signal amplifier 222 of Figure 4 and which also functions as a summer/adder. The cascaded MFB filters 220', 220" are able to provide enhance voice clarity as compared to the single filter configuration of Figure 4. The values of the various components of the cascaded MFB filters 220', 220" and the signal amplifier 222 are selected based on the desired effect and this would be within the knowledge of a person skilled in the art. Specifically, each band pass filter 220', 220" has its own parameters so that the mid-frequency is centred at different locations in the frequency band. In this way, the circuit design is able to compensate wider bandwidth and restore the vocal clarity. Further, when the MFB band pass filters 220', 220" are cascaded in parallel connection, each filter compensates the selected mid-frequency and even wider bandwidth may be restored.

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As it can be appreciated from the described embodiment, by having the microphone 112, which is mounted or disposed near the speaker driver 108, pick up ambient sounds (both undesired ambient noise and desired ambient sound such as voice communication), this simplifies the circuitry of the active cancellation circuit 200. Depending on the mode of the active cancellation

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circuit 200, the ambient sound picked up is either used to create the anti-phase signal to cancel out the ambient sounds actively or used to boost the frequency response of certain components of the ambient sound. In other words, the microphone 112 actually serves a dual purpose of picking up undesired and
5 desired ambient sounds.

The described embodiment should not be construed as limitative. For example, although it is preferred for the microphone 112 to face the ear of the user, the microphone 112 may be arranged in other positions to pick up the ambient
10 sound, regardless of whether the sound is desired (eg. voice) or undesired ambient sound.

The vocal clarity compensator 208 is described as a band pass filter but a high pass filter is also possible. The described embodiment provides two examples
15 of the MFB filter but it is envisaged that multiple MFB filters may be cascaded to provide enhanced voice clarity. The same applies if high pass filters are used.

The ear cushion 106a, 106b are described to be circumaural but may include other types such as intra-aural and supra-aural.

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Having now fully described the invention, it should be apparent to one of ordinary skill in the art that many modifications can be made hereto without departing from the scope as claimed.

CLAIMS

1. A noise reduction circuit with monitoring functionality for a headphone having at least one speaker driver, the circuit comprising:
5 a microphone configured to convert ambient sound into a corresponding electrical ambient signal, the microphone being disposed adjacent to the speaker driver's diaphragm;
an active noise reduction path configured to provide active noise reduction of the ambient sound based on the corresponding electrical
10 ambient signal;
a vocal signal compensation path configured to restore attenuated signals within the vocal range of the corresponding electrical ambient signal to increase audibility of vocal signals of the ambient sound; and
a switching device arranged to selectively deliver the corresponding
15 electrical ambient signal to the active noise reduction path or to the vocal signal compensation path.
2. A noise reduction circuit according to claim 1, wherein the vocal signal compensation path comprises a vocal clarity compensator configured to
20 enhance the frequency response of the attenuated signal within the vocal range.
3. A noise reduction circuit according to claim 2, wherein the vocal clarity compensator includes a band pass filter and a signal amplifier coupled to
25 the band pass filter's output.

4. A noise reduction circuit according to claim 2, wherein the vocal clarity compensator includes more than one band pass filter cascaded in parallel.
5. A noise reduction circuit according to claim 2, wherein the vocal clarity compensator includes a high pass filter.
6. A noise reduction circuit according to claim 2, wherein the frequency response is dependent on both construction and design of earcups of the headphone, the frequency response being between 200 Hz and 1 KHz of the vocal range.
7. A noise reduction circuit according to claim 1, further comprising a microphone amplifier arranged to amplify the corresponding electrical ambient signal, and wherein the switching device is arranged to receive the amplified corresponding electrical ambient signal.
8. A noise reduction circuit according to claim 1, wherein the active noise reduction path includes an active-noise cancellation filter.
9. A noise reduction circuit according claim 1 wherein the microphone is arranged to face the user.

10. A noise reduction circuit according to claim 1, wherein the microphone is arranged at the front of the speaker driver's diaphragm.
11. A headphone comprising the noise reduction circuit of claim 1.