

Description**BACKGROUND OF THE INVENTION****Field of the Invention**

This invention relates generally to geophysical data acquisition systems, and in particular to a geophysical field acquisition system with circuitry which increases effective system bandwidth. Still more particularly, the invention relates to a geophysical acquisition system having circuitry which may be configured by operator control during seismic exploration operations to increase the effective bandwidth of the combination of earth acting as a filter to seismic signals and the geophysical acquisition system.

Description of the Prior Art

Recording systems for providing a permanent record, typically on magnetic tape, of geophysical data acquired in field operations are well known. For the purpose of this disclosure the term "geophysical data" includes data acquired in a land prospecting environment, where the sensors may be seismometers, geophones, or other types of sensors, as well as data acquired in a marine prospecting environment where the sensors may be hydrophones or the like. A typical digital field recording system is that disclosed in U.S. Patent No. 3,819,864.

Various designs of geophysical acquisition systems (also called seismographs and field acquisition systems) exist, the simplest being fixed systems where amplifier gain is preset and constant. Such prior art systems have a preamplifier stage, an analog gain stage, low-cut filters, notch filters, and high-cut anti-alias filters for each channel. A multiplexer switches the data channel sequentially to an analog to digital (A/D) converter which outputs a binary signal proportional to the input voltage.

One example of a prior art geophysical acquisition system is that described in U.S. patent 4,321,675. Such system includes one or more channels including an input stage responsive to seismic signals, an A/D converter which has a predetermined effective dynamic range, and a recorder for storing representations of such seismic signals. U.S. patent 3,684, 968 discloses an example of a floating point amplifier which may be used with system.

An important parameter of such geophysical acquisition systems is their dynamic range. Dynamic range is defined as the difference in dB between the largest input signal that can be processed and recorded, i.e., the signal having an amplitude just below that which would cause saturation in some element of the system, and the smallest signal which can be properly recorded by the system, generally considered to be a signal to noise ratio of 1. Dynamic range is commonly expressed as the ratio of the largest to the smallest signal and is typically expressed in decibels or dB.

The number of steps the A/D converter breaks the signal into defines the precision of the system. If it is broken into 12 bits, the system is more precise than if it is broken into 8 bits. An A/D converter is designed to accept a certain maximum voltage. It is important to amplify seismic signals (geophysical data) until the maximum voltages applied to the A/D converter are as close to (but not greater than) that value as possible. Using as many of the bits of the digital word as possible increases its significance. The significance of the digital word relates to the number of bits recorded above the system noise level. In other words, to take full advantage of the geophysical acquisition system, from a "significance" point of view, the signal must be amplified before the A/D stage with the gain of the amplifier being set as high as possible without saturating the electronics. The electronics become saturated when the largest voltage applied to the A/D converter is too big for converter full scale.

At any specific gain setting, a digital system can operate only within a defined input voltage range without the signal being either below the noise level or above saturation. The minimum detectable voltage is the larger of the threshold voltage for the least significant bit or the system noise level. The maximum detectable voltage is the level at which the A/D converter becomes saturated and outputs its largest possible digital number. Signals above the maximum level are truncated, either in their analog state or after conversion to digital form.

The systems typically used for petroleum exploration are designed to adjust their gains automatically according to the incoming signal and also to record the gain setting. These are floating-point systems where the number is recorded in exponent-mantissa scientific notation. The output from the A/D converter is the mantissa and the gain setting is the exponent. Binary gain systems were the first of these systems; an example is Texas Instruments' DFS III which is gain ranged in 6 dB increments (single bit shifts). The digital number is recorded as a 15-bit word and the gain is recorded in a 4-bit exponent. With binary gain

systems, several (from 15 to 60) calls to shift are required before gain is increased. A single call is needed to decrease gain.

The next generation of gain ranging amplifier recording systems was the instantaneous floating-point (IFP) system. Only one call is required to increase gain by any amount. The Texas Instruments DFS IV and DFS V are examples of such instruments. The gain increment for these instruments is 12 dB (2-bit shift) but could have other step ratios as well, such as 2:1 (6 dB) and 8:1 (18 dB).

When the processing of the digital signals is accomplished using digital filters and the like, the effective dynamic range of a signal that can be recorded from a maximum significance point of view, is less than the actual dynamic range of signals applied to the A/D converter. For a 16 bit A/D converter (15 bit mantissa, 1 bit sign), the effective dynamic range of the A/D converter and digital processing elements of the system is between 40 and 50 dB.

When an explosive source generates a seismic signal into the earth, the signal is actually a composite signal or sum of many different oscillatory signals or waves which propagate into the earth and are reflected or refracted back toward the geophones of the geophysical acquisition system. The spectrum of the generated signal depends on the weight and type of explosive, its shape and the material around it. In typical land seismic explorations, the energy peak of the generated spectrum is in the 10 to 30 Hz range, with a typical value of 15 Hz. At frequencies higher than the peak, the energy decreases at about 6 dB per octave. The shape of the generated energy spectrum of compressed air ("air gun") and mass impact devices is similar to that of an explosive source.

The spectrum of vibratory sources (e.g., Vibroseis, a trademark of Conoco, Inc.) can be controlled by the use of nonlinear sweep signals. The high frequency energy of resulting source seismic signals can be increased.

For any spectrum of seismic waves input into the earth by one of the sources mentioned above, the earth responds as an attenuation filter. The frequency components of multiple frequency seismic waves have a propagation velocity which is about the same for any frequency, but each frequency of the composite wave is attenuated at about .5 dB per its wavelength. The number of dB of attenuation for each component of the wave doubles with each doubling of frequency. A doubling of the attenuation as measured in number of dB is equivalent to an exponential increase in attenuation. Thus, as a function of frequency, the seismic waves (having a generated energy spectrum) are attenuated exponentially with increases in frequency.

The waves propagating through the earth are also attenuated exponentially as a function of time. As a result, the attenuation spectrum of the earth (considered as a signal filter) changes exponentially with time and frequency. At any specific time, the energy spectrum of the returning waves is acted on by the "earth filter" and sensors which typically reaches a maximum level in a frequency range from about 10 to 40 Hz and then decays exponentially with frequency. Considering the generated spectrum of frequencies, as acted on by the "earth filter" and sensor at any particular time after source initiation, is like taking a "snapshot" of the energy content of returning waves from a certain depth in the earth, considering that the propagation velocity of elastic waves is fairly well known. The later in time the snapshot is taken, the deeper the "look" into the formation.

In view of the "effective dynamic range" of the A/D converter and digital processing systems of a modern geophysical acquisition system, the "effective system bandwidth" of the combination of the "earth filter" and the seismic acquisition system can be approximated. At any time after seismic energy is applied to the earth, the maximum signal amplitude of the spectrum is determined, recognizing that the gain of the gain ranging amplifier is set to produce a near maximum signal level to the A/D converter. The effective dynamic range, in dB, is then subtracted from the level of the maximum signal level in dB to produce a signal level in dB, below the maximum signal level, to establish an attenuation level of the earth-acquisition system, below which signals can not be measured with full "significance" as defined above. That lower signal level, or significance level, then allows determination of the effective earth-acquisition system bandwidth, defined as the band of seismic signals which may be recorded with full significance. The effective bandwidth so defined changes with each snapshot or time after the seismic signals are generated and input into the earth.

It is important that the effective bandwidth of the earth-acquisition system be as wide as possible so that earth layers of smaller relative thickness may be resolved. Resolution may be defined as the limit at which two features can be distinguished from the effects of one feature. An acquisition system which enhances the effective bandwidth of the earth-acquisition system simply has more earth layer resolving capability than one with less effective bandwidth.

Low-cut filters have been used in the prior art to enhance effective system bandwidth. Knapp and Stepples describe a cut-off frequency of 80 Hz, 24 dB/octave low-cut filter prior to digitizing for a

geophysical acquisition system in GEOPHYSICS, Vo. 51, No. 2 (February 1986) at page 288. Knapp and Steeples suggest that the filter cut-off frequency should not be so high and the roll off slope so steep as to filter away all of the signal, but it is also important that it be high enough to attenuate high-amplitude, low frequency signal and low-frequency noise that might mask low amplitude signals.

Identification of Objects of the Invention

It is a general object of this invention to provide an apparatus and method for increasing the effective bandwidth of a geophysical data acquisition system for recording seismic signals returning from the earth.

It is another object of the invention to provide a Low-cut filter in a geophysical data acquisition system which increases effective system bandwidth but simultaneously allows recording of low frequency signals returning from deep within the earth.

It is still another object of the invention to provide in a geophysical data acquisition system an attenuation limited low-cut filter having an operator selectable cut-off frequency, and maximum attenuation level at low frequencies to increase effective system bandwidth.

It is another object of the invention to provide in a geophysical data acquisition system a filter having a substantially constant gain below a lower cut-off frequency, gain increasing with increasing frequency in a transitional band above the lower cut-off frequency, and a constant gain above the upper limit of the transition band.

It is another object of the invention to provide in a geophysical acquisition system a spectral shaping filter disposed in the input stage of the system so as to minimize system input noise while simultaneously enhancing effective system bandwidth.

Another object of the invention is to provide in a geophysical acquisition system a spectral shaping filter having an operator selectable lower cut-off frequency, and gain boost following such lower cut-off frequency to increase effective earth/acquisition system bandwidth.

It is still another object of the invention to provide a method of geophysical field operations whereby a field operating specialist may determine the spectral characteristics of the earth and adjust attenuation limited low-cut filter and spectral shaping filter parameters in order to enhance the spectral characteristics of the seismic acquisition system to signals returning from a specific energy source and earth location, thereby increasing the resolution of signals acquired.

The invention is set out in independent claims 1 and 8, with further embodiments in dependent claims.

BRIEF DESCRIPTION OF THE DRAWINGS

The objects, advantages and features of the invention will become more apparent by reference to the drawings which are appended hereto and wherein like numerals indicate like parts and wherein an illustrative embodiment of the invention is shown, of which:

Figure 1 is a block diagram of a typical prior art geophysical data acquisition system;

Figure 2 is a block diagram of the geophysical data acquisition system of the invention incorporating an input stage with a spectral shaping filter followed by an attenuation limited low-cut filter;

Figure 3A is an embodiment of an input stage incorporating a single ended spectral shaping filter characterized by low cut-off frequency and gain boost above such low cut-off frequency;

Figure 3B is an embodiment of an input stage incorporating a single ended spectral shaping filter characterized by operator selectable low cut-off frequency and gain boost above such frequency;

Figure 4A is an embodiment of a differential input stage incorporating a spectral shaping filter characterized by an operator selectable low cut-off frequency and an operator selectable gain boost above such frequency;

Figure 4B is a schematic drawing of a preferred embodiment of a differential input stage of the geophysical acquisition system of Figure 2 including a spectral shaping filter characterized by operator selectable low cut-off frequency and gain boost above such frequency;

Figure 5 is a graph of gain versus log frequency of a spectral shaping boost filter with operator selectable low cut-off frequency and gain boost;

Figure 6 is an example of the attenuation spectra of the earth and sensor at a number of times following seismic signal generation, the example showing the effective system bandwidth enhancement of a spectral shaping filter;

Figure 7A is an embodiment of an attenuation limited low-cut filter characterized by a cut-off frequency and a fixed level of attenuation at low frequencies below such cut-off frequency;

Figure 7B is a graph of attenuation versus log frequency showing the frequency response of the circuit of Figure 7A;

Figure 7C is a schematic drawing of a preferred embodiment of an attenuation limited filter of the geophysical acquisition system of Figure 2 including two stages of the filters illustrated in Figure 7A and characterized by operator selectable low cut-off frequency and attenuation level at low frequencies; and

Figure 8 is an example of the attenuation spectra of the earth and sensor at a number of times following seismic signal generation, the example showing the effective system bandwidth enhancement of an attenuation limited low-cut filter at one of those times.

10 DESCRIPTION OF THE INVENTION

Figure 1 is a block diagram of a typical prior art geophysical data acquisition system. The input to such a system is normally provided by a cable comprised of a plurality of twisted pair signal conductors. In the case of land seismic prospecting, each twisted pair is connected at some remote location to a geophone or geophone group. In the case of marine prospecting, the twisted pairs are enclosed in a streamer which is towed behind a prospecting boat and are connected at remote locations to hydrophones or hydrophone groups. In either case a plurality of channels of data are available to be recorded by the data collection system. Each twisted pair provides a differential signal which is not referenced to ground.

With reference to Figure 1, one such signal is coupled to an input stage or preamplifier 25 of a channel of the data collection system by leads 1 and 2. The signal enters differential amplifier 3 which, in turn, provides a differential output on lines 5 and 6 to differential amplifier 7. Amplifier 7 is designed to provide a high common mode rejection and to convert the differential signal to a single ended signal on line 8. Amplifiers 3 and 7 comprise an input stage or preamplifier 25. Preferably amplifier 3 should have a lower equivalent input noise and a high gain. The high gain amplifies the received signals to a sufficiently high level such that the noise contributed by the following devices is insignificant relative to the noise contribution of amplifier 3. Amplifier 7 typically has a gain near unity.

Other means for coupling the cable signals to the data collection system are known including those disclosed in U.S. Patent Nos. 3,778,759 and 3,972,020.

The preamplifier output is coupled by lead 8 to low-cut filter 9. The function of low-cut filter 9 is to attenuate low frequency signals. Line 10 couples the output of the low-cut filter to a high-cut filter 11. The high-cut filter attenuates high frequencies and typically has a slope of 72 dB per octave. Since the analog signals are to be sampled and digitized at a later point in the system, the steep slope of high-cut filter 11 is used to assure that frequencies above one-half the sampling frequency are attenuated to prevent significant frequency folding.

The output of high-cut filter 11 is coupled by lead 12 to notch filter 13. The reject band of notch filter 13 is centered at the power line frequency so as to attenuate any pickup from nearby power lines. High-cut filters and notch filters are well known in the art and require no further discussion here. In some systems it has been known for the notch filter to precede the high-cut filter or for the high-cut filter to precede the low-cut filter.

The output of the notch filter is coupled by lead 14 to the input of a low drift DC amplifier 15. Typically, the amplifier 15 has a gain of near unity and a low output impedance. The low drift requirement stems from the fact that the remainder of the data acquisition system is DC coupled. The output of amplifier 15 is coupled by lead 16 to multiplexer switch 17. Multiplexer switch 17 is typically a semiconductor switch which is closed for a very brief time period so as to provide a sample of the data from the illustrated channel via lead 18 to the input of gain ranging amplifier 19.

That portion of the data collection system described to this point, that is the channel between the input signal and line 18, is duplicated for each channel of input data to be recorded by the system. The various multiplexer switches such as switch 17 are successively closed for brief periods so as to provide on lead 18 a continuous succession of analog samples from the various data channels.

These various samples, after amplification by amplifier 19, are coupled by line 21 to analog-to-digital converter 20. The digitized output signals are coupled by lead 23 to a recorder 22 which, in the preferred embodiment, comprises a magnetic tape recorder. The geophysical data recording system as outlined above provides on magnetic tape digitized samples of the multichannel analog data received from the cable.

Most high quality analog-to-digital converters in current use have a dynamic range of 80 to 90 dB but may exceed 120 dB. Gain ranging amplifier 19 has the capability to automatically adjust its gain for each new data sample as the sample is received on lead 18. The gain is adjusted so as to ensure that the amplified signal appearing on lead 21 will fall within the acceptable range of the analog-to-digital converter.

The actual gain setting of amplifier 19 is provided to recorder 22 on line 25 for recording along with the corresponding digitized sample appearing on line 23. One example of a suitable gain ranging amplifier is that disclosed in U.S. Patent No. 3,684,968. Specific embodiments of various components illustrated in Figure 1 appear in a digital field system supplied by Texas Instruments Incorporated of Dallas, Texas under the trademark DFS V.

Figure 2 is a block diagram of the geophysical acquisition system according to the invention. It is similar to that of Figure 1, but incorporates an input stage 30 including a spectral shaping filter and further incorporates an attenuation limited low-cut filter stage 33. The system of Figure 2 incorporates a high line pickup eliminator circuit 40 which feeds analog information back to the gain ranging amplifier 19' via D/A converter 42. The high line pickup eliminator 40, obviating the need for a prior art notch filter, is described in pending U.S. application 835,140 assigned to the assignee of this invention. Its operation is not described here. An additional low-cut filter 13' is provided in the channel to filter extremely low frequencies.

Figure 3A is a schematic diagram of an input stage 30 with a differential amplifier 43 followed by a single ended embodiment of a spectral shaping filter 50. Figure 5 is a gain versus log frequency graph that describes in general the gain versus frequency characteristics of the spectral shaping circuit 50 of Figure 3A as well as the circuits of Figures 3A, 3B, 4A, and 4B. The input stage 30 preferably has a gain of G_1 at DC frequency, a lower cut-off frequency f_1 followed by a gain which increases with increasing frequency until a boost gain of G_2 is approached at a cut-off frequency of f_2 . Cut-off frequency is defined herein as the 3 dB point above or below the straight line approximation to the gain or attenuation response on a gain or attenuation versus log frequency graph.

An important feature of this invention is the placement of the spectral shaping circuit 50 in input stage 30. Typically, the higher the gain of the input stage is, the lower the equivalent input noise of the system. Placing the spectral shaping circuit 50 in the input stage provides gain boost before any of the higher noise circuits which follow, resulting in a lower equivalent system noise than if a spectral shaping circuit were to be placed in the system following the input stage.

Seismic signals returning from the earth are applied from a sensor such as a geophone to leads 1, 2 (Figure 3A) to differential amplifier 43 which may have a gain of 4 or more. The output on lead 44 is applied to the positive input of an operational amplifier 51 of spectral shaping circuit 50. Circuit 50 includes resistance/capacitance (RC) feedback network which applies the output signal on lead 55 to the negative input of operational amplifier 51 via lead 56. The DC gain G_1 of spectral shaping circuit 50 is dependent on the ratio of R_1 to the sum of R_1 , R_2 and R_5 . The high frequency gain G_2 is a function of the resistors R_1 , R_2 , R_3 and R_5 . The gain between cut-off frequencies f_1 and f_2 rises at slopes approaching 6 dB/octave (20 dB/decade) rate. The lower cut-off frequency f_1 is a function of the capacitor C_1 and the resistors R_1 , R_2 , R_3 and R_5 . Selecting the lower cut-off frequency f_1 , the DC gain G_1 , and the difference in gain, or gain boost ($G_2 - G_1$) in dB determines the proper numerical values for R_1 , R_2 , R_3 , R_5 and C_1 .

The input stage of Figure 3B is of identical form as that of Figure 3A except that the resistor and capacitor values in the circuit of Figure 3B, analogous to those of Figure 3A, may be changed in value by means of switches S_1 , S_2 , S_3 , S_4 and S_5 . Three values of capacitance C_1 may be inserted in the circuit by closing either switch S_4 or S_5 or closing both switches S_4 and S_5 . One of four values for R_3 may be inserted in the circuit 50 by opening or closing switches S_2 and S_3 to insert or not insert R_3'' or R_3''' in parallel with R_3' . The switch S_1 may be closed to a number of different points 201-204 to change the amount of output signal on output lead 55 that is fed back to the negative input of operational amplifier 51 via lead 56. Representative values for resistors and capacitors of Figure 3B follow in Table I.

TABLE I

R_1	87 ohms
R_2'	261 ohms
R_2''	1,044 ohms
R_2'''	4,176 ohms
R_5	25,056 ohms
R_3'	1,516 ohms
R_3''	1,129 ohms
R_3'''	566 ohms
C_1'	1 μ F
C_1''	1.625 μ F

With the values of the resistors and capacitors shown in Table I, it is evident that switch S_1 controls the DC gain G_1 of the circuit.

If switch S_1 is connected to positions 200, 201, 203 or 204, the effective R_1 (R_1 eff) and R_2 (R_2 eff) of Figure 3B equivalent to R_1 and R_2 of Figure 3A are as follows in Table II, with the DC gain of circuit 50 tabulated.

TABLE II

Switch Position	DC Gain	R_1 Eff	R_2 Eff
201	5.5	5568	0
202	22	1392	4176
203	88	348	5220
204	352	87	5481

Switches S_2 and S_3 control the boost gain ($G_2 - G_1$) in dB above DC gain G_1 for the circuit.

With the notation of R_3 referring to the amount of resistance inserted in series with the capacitors C_1' or C_1'' , the amount of gain boost from the DC gain is tabulated below in Table III.

TABLE III

Switch Positions of S_2 and S_3	Approx. Boost (dB)	Approx. Boost (gain)	R_3
S_2 & S_3 open	12	4.01	1516
S_2 closed	18	8.0	647
S_2 & S_3 closed	24	16.01	302
S_3 closed	----- (not used) -----		

Switches S_4 and S_5 control the lower cut-off frequency f_1 of the circuit. With the notation C_1 referring to the amount of capacitance inserted in series with combinations of resistors R_3' and R_3'' and R_3''' , the lower cut-off frequency f_1 is tabulated for the switch positions of S_4 and S_5 in Table IV. The upper cut-off frequency f_2 which also results is tabulated.

TABLE IV

Switch Position of S_4 and S_5	Capacitance C_1 (μ f)	$R_3 = 3030 + 12\text{dB}$		$R_3 = 1294 + 18\text{dB}$		$R_3 = 603 + 24\text{dB}$	
		f_1	f_2	f_1	f_2	f_1	f_2
S_4 closed, S_5 open	1.0	26.2	105.0	30.6	246.0	32.8	527.4
S_4 open, S_5 closed	1.625	16.1	64.7	18.8	151.3	20.2	324.5
S_4 closed, S_5 closed	2.625	10.0	40.0	11.65	93.7	12.5	200.9

Tables II, III, and IV demonstrate that by appropriate manipulation of switches $S_1 - S_5$, the DC gain G_1 , the lower cut-off frequency f_1 , and the boost gain $G_2 - G_1$ in dB added by circuit 50 (and of course of circuit 30) of Figure 3B may be set, under operator control during field operations.

Figure 4A illustrates the spectral shaping input stage 30 in an embodiment of the circuit which directly accepts the differential input signal on leads 1 and 2. Amplifiers 60, 61 may be transistors with the leads 1 and 2 connected to the bases B thereof. The outputs of the collectors C of amplifiers 60, 61 are applied differentially from leads 64 and 65 to operational amplifier 70. The output of amplifier 70 (which is the output of the spectral shaping input stage 30 of the embodiment of Figure 4A) is applied to the positive inputs (or emitters) of amplifiers 61 and 60 via functionally identical feedback networks as the feedback network illustrated in Figure 3B. Switches S_1 and S_1' are ganged together to ensure that the DC gain selected by appropriate ratios of R_1 and R_2' , R_2'' and R_2''' are the same. The cut-off frequency f_1 is selected in the same way as for Figure 3B by selecting the positions of switches S_4 and S_5 to bring $C_1''/2$ or $C_1'/2$ or $C_1''/2$ and $C_1''/2$ into the circuit. Spectral boost, expressed in dB, as high frequency gain G_2

minus by low frequency gain G_1 , is selectable by positioning switches S_2 and S_3 to put $2R_3''$ in parallel with $2R_3'$, or $2R_3'''$ in parallel with $2R_3'$ or both $2R_3''$ and $2R_3'''$ in parallel with resistor $2R_3'$. The values of the resistors and capacitors of Table I correspond to those shown in Figure 4A.

The common mode signal appearing at point P between 1 meg resistors R_8 and R_9 is applied via operational amplifier 71 via resistors R_{10} and R_{11} for application to the emitters of transistor amplifiers 60 and 61. Resistors R_{10} and R_{11} of Figure 4A are preferably 2087 ohms. Transistors 60, 61 are each one-half of a commercially available two transistor package MAT-01 and operational amplifier 70 is a commercially available circuit LT1008.

Figure 4B shows the preferred embodiment of the spectral shaping input stage of Figure 4A. Transistors 60 and 61 are each one-half of the commercially available package MAT-01. The transistors are supplied from a 15 volt source through 100K ohm resistors R_{12} and R_{13} . The operational amplifier 70 is a commercially available circuit LT1008. The common mode operational amplifier 71, having a 10 volt reference source applied to its positive input, is one-half of a commercially available circuit LF442.

Switches S_1 and S_1' are voltage controlled field effect transistor (FET) switches corresponding to switches S_1 and S_1' of Figure 4A. Voltage applied individually to leads 80-83 cause the corresponding FETs to conduct, thereby connecting the emitters of transistors 61 and 60 to the positions between the resistors R_1 , R_2' , R_2'' , R_2''' and R_5 .

Switches S_2 and S_3 are voltage controlled FETs corresponding to switches S_2 and S_3 of Figure 4A. Voltage applied individually or simultaneously to leads 90 and 91 closes switches S_2 and S_3 . Switches S_4 and S_5 are voltage controlled FETs corresponding to switches S_4 and S_5 of Figure 4A. Voltage applied individually or simultaneously to leads 92 and 93 closes FET switches S_4 and S_5 .

Voltages applied to leads 80 through 83 serve to set the gain G_1 of the input stage 30. (Gains G_1 , G_2 and lower cut-off frequency, f_1 , are defined schematically in Figure 5). A voltage applied to lead 80 achieves a "low gain G_1 "; a voltage applied to lead 81 achieves a "medium low gain G_1 "; a voltage applied to lead 82 achieves a "medium high gain G_1 "; and a voltage applied to lead 83 achieves a "high gain G_1 ".

A voltage applied to lead 92 sets low cut-off frequency f_1 to a relatively high value (see Table IV above). A voltage applied to lead 93 provides a lower low cut-off frequency f_1 . A voltage applied to both leads 92 and 93 provides a still lower low cut-off frequency. No voltage applied to leads 90 or 91 provides a low gain boost from gain G_1 to gain G_2 . A voltage applied to lead 91 provides a medium gain boost from gain G_1 to gain G_2 . A voltage applied to 90 and 91 provides a high gain boost. The voltages applied to leads 80-83 and 90-93 are preferably applied from a digital computer subject to operator control.

Figure 6 illustrates the attenuation spectra of a typical section of earth as a function of time after a seismic generation. The dashed line curves represent the attenuation of the earth to seismic waves as a function of time and frequency. Time is treated as a parameter such that each time attenuation curve may be considered a "snap shot" of the frequency attenuation of the earth. The maximum point on the various curves are marked as A_1 , A_2 , etc. In the system of Figure 2, the gain ranging amplifier 19' automatically adjusts its gain such that a maximum amplitude of the composite seismic signal will not be greater than a maximum signal recognizable by A/D converter 70'. For each of the time curves of Figure 6, the dynamic range of AD converter 70' and digital processing steps following the AD converter is taken as 48 dB to determine the effective system bandwidth. (Of course, the 48 dB is only an example for explaining the beneficial aspects of this invention.) For example, for the $T=1$ sec. spectrum, measured from maximum point A_2 results in line 301, which extends to point P_1 , at about 127Hz. For returning seismic waves which are received 1 second following seismic generation, the bandwidth of the earth, (considering the seismic acquisition system of Figure 2 to be in a flat bandwidth configuration over the frequencies of interest) is about 127Hz.

The solid curve above each earth and sensor spectrum (dashed) curve, show the result of applying spectral boosting with the circuits of Figure 3B or 4B. For this example, 24dB of spectral boost with the lower cut-off frequency set at about 20Hz was applied. It is seen that for the $T=1$ sec. spectrum, spectral boosting results in approximately 23Hz additional bandwidth. Enhanced bandwidth of each spectrum at later times from seismic generation is also achieved, but of course, the increase in effective earth/acquisition system bandwidth is proportionately less. The effective earth/acquisition system bandwidth at $T=3$ is increased from about 51Hz to about 54Hz, a 3Hz increase.

In operation, a seismic exploration specialist first makes a test shot, records the returning seismic signals from the earth, and then determines the frequency where the spectral peak occurs at a time such as $T=1.0$ or 2.0 seconds after seismic generation. Such spectral peak may be determined using fast fourier transform techniques. The low cut-off frequency f_1 of the circuits of Figures 3B or 4B should be set at a frequency about the same as or greater than the frequency of the determined spectral peak. The amount of boost gain is then selected to optimally enhance the effective system bandwidth for a particular depth of

interest.

Turning now to Figure 7A, a preferred circuit 100 which is embodied in duplicate stages (Figure 7C) of low-cut filter 35 is illustrated. The circuit of Figure 7A is a modified second-order low-cut filter which has an attenuation versus log frequency response as illustrated in Figure 7B. The response of the circuit is similar to an ordinary low-cut filter with an increasing attenuation with decreasing frequency below the cut-off frequency f_c . However, the attenuation limit A in dB is reached at DC (zero frequency) after a maximum attenuation A_{max} is reached at a frequency

$f_{A_{max}}$

below the cut-off frequency f_c .

Although the preferred embodiment of the attenuation limited low-cut filter of the invention is shown in Figures 7A and 7C and its frequency response is shown in Figure 7B, other attenuation limited low-cut filters may be used. Such other filters would have a frequency response characterized by a substantially constant attenuation at low frequencies and a decreasing attenuation with frequency higher than a cut-off frequency corresponding to frequency

$f_{A_{max}}$

of Figure 7B.

With the circuit 100 of Figure 7A, the variable resistor R_B is adjusted to set-up desired stop band floor attenuation limit A. The variable resistors R_{2A} and R_{4A} are adjusted to set the low cut-off frequency f_c . Table V below indicates the cut-off frequencies and attenuation limits in dB achieved for the various switch settings of Figure 7A. Switches $S_{20} - S_{60}$ of variable resistor R_{2A} are ganged with switches $S_{20}' - S_{60}'$ of variable resistor R_{4A} . Table V assumes the following resistor values and capacitor values. A "1" indicates that a switch is closed; a "0" indicates that it is open.

$R_5 = 1,000$ ohms $C_{639} = .15\mu f$

$R_{10} = 249,088$ ohms $C_{638} = .15\mu f$

$R_{20} = 296,716$ ohms

$R_{30} = 129,625$ ohms $R_{B1} = 29,698$ ohms

$R_{40} = 62,585$ ohms $R_{B2} = 13,887$ ohms

$R_{50} = 30,016$ ohms

$R_{60} = 13,905$ ohms

$2R_5 = 2,000$ ohms

$2R_{10} = 498,176$ ohms

etc.

TABLE V

GANGED SWITCHES
S20-S60 and S20'-S60'

	S60 S60'	S50 S50'	S40 S40'	S30 S30'	S20 S20'	$f_{c \text{ nom}}$
10	0	0	0	0	0	3.0
	0	0	0	0	1	5.5
	0	0	0	1	0	8.7
	0	0	0	1	1	11.2
	0	0	1	0	0	14.7
15	0	0	1	0	1	17.1
	0	0	1	1	0	20.2
	0	0	1	1	1	22.6
	0	1	0	0	0	27.0
	0	1	0	0	1	29.3
20	0	1	0	1	0	32.3
	0	1	0	1	1	34.6
	0	1	1	0	0	38.0
	0	1	1	0	1	40.2
	0	1	1	1	0	43.2
25	0	1	1	1	1	45.4
	1	0	0	0	0	52.9
	1	0	0	0	1	55.1
	1	0	0	1	0	57.9
	1	0	0	1	1	60.1
30	1	0	1	0	0	63.2
	1	0	1	0	1	65.3
	1	0	1	1	0	68.0
	1	0	1	1	1	70.1
	1	1	0	0	0	73.9
35	1	1	0	0	1	75.9
	1	1	0	1	0	78.6
	1	1	0	1	1	80.6
	1	1	1	0	0	83.5
	1	1	1	0	1	85.5
40	1	1	1	1	0	88.0
	1	1	1	1	1	90.0

45	Switches S80 and S90		Attenuation A	Cut-Off Frequency $f_{c \text{ nom}}$
	S80	S90		
	0	0	infinity	
	1	0	-24 dB	$1.06 f_c$
	0	1	-18 dB	$1.12 f_c$
50	1	1	-15.2 dB	$1.15 f_c$

As Table V shows, the attenuation limited low-cut filter may be varied to produce three different attenuation limits A and a plurality of cut-off frequencies f_c varying from about 3Hz to 104Hz. The frequency of maximum attenuation

$$f_{A_{\max}}$$

as indicated in the graph of Figure 7B is related to the cut-off frequency f_c by a factor K. The factor K is the ratio of maximum attenuation frequency

$$f_{A_{\max}}$$

to the normal cut-off frequency f_c of the circuit. Table VI relates the attenuation limit A to the factor K, the octave ratio (the number of octaves below f_c where

$$f_{A_{\max}}$$

occurs) and the maximum attenuation $A_{\max}$ in dB.

TABLE VI

A(dB)	K	Octave ratio	$A_{\max}$ (dB)
-15.2	2.22	1.15	-20
-18	3.22	1.56	-24
-24	3.67	1.88	-33

Figure 7C illustrates the preferred embodiment of the attenuation limited low-cut filter 35 of Figure 2. Two identical circuits 100, as shown in Figure 7A and specified above in Tables V and VI are placed in series. The switches S20-S60, S20'-S60', and S80 and S90 are voltage controlled field effect transistors like those of Figure 4B. Voltages applied to five leads L1-L5 to variable resistors R2A and R4A for each circuit 100 control switches S20-S60 and S20'-S60'. Two leads L7 and L8 for each circuit 100 control switches S80 and S90. Bypass switches S100 are controlled by lead L6. Operational amplifiers 106 are preferably commercially available LT1012 operational amplifiers.

Figure 8, like Figure 6 illustrates the attenuation spectra of typical sections of earth as a function of time from a seismic generation. The dashed line curves represent the attenuation of the earth to seismic waves as a function of time and frequency. As with Figure 6, time is treated as a parameter such that each time attenuation curve may be considered a "snapshot" of the frequency attenuation of the earth. The T=2.0 curve shows the least attenuation of the earth (the maximum point A4) to occur at about 16Hz. The 48 dB effective dynamic range of the A/D converter/digital processing system results in an "effective system bandwidth" of about 74Hz at point P₃.

By inserting the attenuation limited low-cut filter circuit 35 of Figure 7C, the combined earth and sensor attenuation and attenuation limited low-cut filter (assuming for illustration purposes that the spectral boost circuit 30 is not present) results in an attenuation curve 500. The point of maximum signal strength occurs at the point A7 at about 8Hz. The frequency at which the combined curve 500 falls to 48 dB below point A7 is point P4 at about 98Hz. For the T=2 second snapshot, the resulting increase in effective system bandwidth is about 24Hz. The increase in effective system bandwidth at earlier snapshots is greater; for later in time snapshots (i.e., T=3.0 sec.), the increase in effective system bandwidth is reduced slightly due to the attenuation at low frequencies.

In operation, a seismic exploration specialist controls the shape of curve 500 by adjusting the attenuation and cut-off frequencies of circuits 100 of circuit 35 (Figure 7C) by applying digital control voltages to leads 21-28 effectively controlling the switches S20-S60, S20'-S60', S80, S90 and S100.

Impulse sources have an excess of low frequencies due to both the spectra of the source generated energy and the earth attenuation as described above. The specialist determines the frequency of the spectral peak by examining an FFT (fast fourier transform) plot of a test shot. The attenuation limited low-cut filter parameters are then set to provide the greatest attenuation portion (i.e., $A_{\max}$ of Figure 7B) at approximately the peak of the test spectra. The frequency f_c of the attenuation limited low-cut filter is then

set according to the relationship:

f_0 = frequency of test spectral peak K

5 where K is defined as above with reference to Table VI. The attenuation limit (A in dB) is selected depending on the depth of the formation that is desired to be mapped with increased resolution. The low frequency loss at the attenuation limit reduces the maximum depth from which low frequency reflections can be obtained. The highest attenuation produces the greatest increase in bandwidth and the best shallow depth resolution, but deep low frequency reflections are attenuated.

10 Vibrated sources (such as Vibroseis equipment) convert a majority of their energy into surface waves which propagate at low velocity along the surface of the earth and interfere with the reflections that are arriving from the buried layers of interest. These horizontally traveling waves are usually controlled by the combination of source arrays (multiple vibrators in a line) and receiver arrays which tend to reject horizontally traveling waves. These long arrays tend to "smear" the reflections due to elevation differences within the array and due to reflections that arrive at an angle. This smearing acts as a high frequency filter. 15 If the array is reduced, the interfering surface waves use a large portion of the dynamic recording range.

The attenuation limited low-cut filter of the invention can be used to reduce the amplitude of the surface wave. The surface wave problem is best analyzed with a noise analysis which determines the apparent arrival velocity and time of arrival of the interference. Careful examination of the period of these waves gives 20 a rough approximation of the spectral peak. A more accurate spectral peak determination method is to make an FFT analysis over the arrival time and offset of the interference of interest. Once the spectral peak is determined the choice of filters is the same as described for the impulse source.

Of course both the spectral shaping filter of circuit 30 and the attenuation limited low-cut filters 100 of circuit 35 may have their parameters set, as described above, to enhance the earth-acquisition system 25 bandwidth so as to increase the effective system bandwidth for higher resolution of zones of buried layers in the earth.

Various modifications and alterations in the described system and method will be apparent to those skilled in the art of the foregoing description which does not depart from the scope of the invention as claimed. For this reason, these changes are desired to be included in the appended claims. The appended 30 claims recite the only limitations to the present invention. The descriptive manner which is employed for setting forth the embodiments is to be interpreted as illustrative and not limitative.

Claims

- 35 1. A geophysical data acquisition system channel, for use in recording geophysical data for earth formations, said earth formations having different spectral characteristics in response to a specific energy source at different locations on the earth, the channel including an input stage responsive to seismic signals and a recorder (22') for storing representations of said signals, and having an A/D converter having a predetermined effective dynamic range, said channel characterized by 40 means for adjusting under operator control the spectral characteristics of said channel so that the total spectrum of the combination of the earth and the channel is enhanced thereby increasing the resolution of signals acquired.
2. The channel of claim 1 wherein said means for adjusting said spectral characteristics includes a 45 boosting circuit (30) comprising,
 - means for providing a first gain for seismic signals of high frequencies above a higher cut-off frequency f_2 , (S1, R1, R2, R3, R5),
 - means for providing a falling gain for seismic signals of frequencies below said higher cut-off frequency, characterized in that the channel also includes means for providing a second gain for 50 seismic signals of low frequencies below a lower cut-off frequency f_1 , (S1, RA, R2, R5), and
 - means for setting under operator control, the frequency of said lower cut-off frequency and the amount of rising gain between said lower cut-off frequency f_1 and said upper cut-off frequency f_2 (S1, S2, S3, S4, S5).
- 55 3. The channel according to claim 2 wherein said means for providing a first gain, means for providing a second gain, and means for providing a falling gain include,
 - a differential amplifier means (43) with differential inputs for accepting geophysical signals across two input leads (1,2) and for generating single ended amplified intermediate signals proportional to the



set according to the relationship:

f_c = frequency of test spectral peak K

5 where K is defined as above with reference to Table VI. The attenuation limit (A in dB) is selected depending on the depth of the formation that is desired to be mapped with increased resolution. The low frequency loss at the attenuation limit reduces the maximum depth from which low frequency reflections can be obtained. The highest attenuation produces the greatest increase in bandwidth and the best shallow depth resolution, but deep low frequency reflections are attenuated.

10 Vibrated sources (such as Vibroseis equipment) convert a majority of their energy into surface waves which propagate at low velocity along the surface of the earth and interfere with the reflections that are arriving from the buried layers of interest. These horizontally traveling waves are usually controlled by the combination of source arrays (multiple vibrators in a line) and receiver arrays which tend to reject horizontally traveling waves. These long arrays tend to "smear" the reflections due to elevation differences
15 within the array and due to reflections that arrive at an angle. This smearing acts as a high frequency filter. If the array is reduced, the interfering surface waves use a large portion of the dynamic recording range.

The attenuation limited low-cut filter of the invention can be used to reduce the amplitude of the surface wave. The surface wave problem is best analyzed with a noise analysis which determines the apparent arrival velocity and time of arrival of the interference. Careful examination of the period of these waves gives
20 a rough approximation of the spectral peak. A more accurate spectral peak determination method is to make an FFT analysis over the arrival time and offset of the interference of interest. Once the spectral peak is determined the choice of filters is the same as described for the impulse source.

Of course both the spectral shaping filter of circuit 30 and the attenuation limited low-cut filters 100 of circuit 35 may have their parameters set, as described above, to enhance the earth-acquisition system
25 bandwidth so as to increase the effective system bandwidth for higher resolution of zones of buried layers in the earth.

Various modifications and alterations in the described system and method will be apparent to those skilled in the art of the foregoing description which does not depart from the scope of the invention as claimed. For this reason, these changes are desired to be included in the appended claims. The appended
30 claims recite the only limitations to the present invention. The descriptive manner which is employed for setting forth the embodiments is to be interpreted as illustrative and not limitative.

Claims

- 35 1. A geophysical data acquisition system channel, for use in recording geophysical data for earth formations, said earth formations having different spectral characteristics in response to a specific energy source at different locations on the earth, the channel including an input stage responsive to seismic signals and a recorder (22') for storing representations of said signals, and having an A/D converter having a predetermined effective dynamic range, said channel characterized by
40 means for adjusting under operator control the spectral characteristics of said channel so that the total spectrum of the combination of the earth and the channel is enhanced thereby increasing the resolution of signals acquired.
2. The channel of claim 1 wherein said means for adjusting said spectral characteristics includes a
45 boosting circuit (30) comprising,
 - means for providing a first gain for seismic signals of high frequencies above a higher cut-off frequency f_2 , (S1, R1, R2, R3, R5),
 - means for providing a falling gain for seismic signals of frequencies below said higher cut-off frequency, characterized in that the channel also includes means for providing a second gain for
50 seismic signals of low frequencies below a lower cut-off frequency f_1 , (S1, RA, R2, R5); and
 - means for setting under operator control, the frequency of said lower cut-off frequency and the amount of rising gain between said lower cut-off frequency f_1 and said upper cut-off frequency f_2 (S1, S2, S3, S4, S5).
- 55 3. The channel according to claim 2 wherein said means for providing a first gain, means for providing a second gain, and means for providing a falling gain include,
 - a differential amplifier means (43) with differential inputs for accepting geophysical signals across two input leads (1,2) and for generating single ended amplified intermediate signals proportional to the



signals applied between said input leads,

an amplifier means (51) having said amplified intermediate signals applied to one of its input terminals, said amplifier having a portion of its output applied via a frequency sensitive network to another of its input terminals, for producing output signals, and

whereby said output signal relative to said signals applied across said two input terminals are characterized by a second gain at low frequencies, a first gain at high frequencies, and a rising gain between a lower cut-off frequency f_1 and a higher cut-off frequency f_2 .

4. The channel of claim 1 wherein said means for adjusting said spectral characteristics includes an attenuation limited low-cut filter comprising
 - means for producing a (R2A, R4A) a cut-off frequency f_c such that signal of frequency below f_c are increasingly attenuated with decreasing frequency below said cut-off frequency f_c and for limiting attenuation (RB) of such signals at low frequency approaching zero frequency, and
 - means for setting, under operator control the level of said limited attenuation and said cut-off frequency f_c .
5. The channel of claim 4 wherein
 - said attenuation limited low-cut filter is characterized by an input-output response having a region of maximum attenuation (A_{max}) below said cut-off frequency f_c , said maximum attenuation being greater than or equal to said limited attenuation.
6. The channel of claims 4 or 5 wherein said attenuation limited low-cut filter is a second-order low-cut filter.
7. The channel of claim 1 wherein said means for adjusting said spectral characteristics includes
 - a boosting circuit (30) comprising
 - means for providing a first gain for seismic signals of high frequencies above a higher cut-off frequency f_2 , (S1, R1, R2, R3, R5),
 - means for providing a falling gain for seismic signals of frequencies below said higher cut-off frequency, characterized in that the channel also includes means for providing a second gain for seismic signals of low frequencies below a lower cut-off frequency f_1 , (S1, RA, R2, R5), and
 - means for setting under operator control, the frequency of said lower cut-off frequency and the amount of rising gain between said lower cut-off frequency f_1 and said upper cut-off frequency f_2 (S1, S2, S3, S4, S5), and
 - an attenuation limited low-cut filter (35) comprising
 - means for producing a (R2A, R4A) a cut-off frequency f_c such that signal of frequency below f_c are increasingly attenuated with decreasing frequency below said cut-off frequency f_c and for limiting attenuation (RB) of such signals at low frequency approaching zero frequency, and
 - means for setting, under operator control the level of said limited attenuation and said cut-off frequency f_c .
8. A method of adjusting the total combination of earth and geophysical data acquisition system channel spectrum characteristics so as to increase the resolution of signals acquired by the channel, comprising the steps of
 - determining the spectral characteristics of the earth, and
 - adjusting under operator control the spectral characteristics of said channel so that the total spectrum of the combination of the earth and the channel is enhanced.
9. The method of claim 8 wherein said adjusting step includes the sub-steps of
 - providing a first gain for seismic signals of high frequencies above a higher cut-off frequency f_2 ,
 - providing a falling gain for seismic signals of frequencies below said higher cut-off frequency,
 - providing a second gain for seismic signals of low frequencies below a lower cut-off frequency f_1 , and
 - adjusting the frequency of said lower cut-off frequency, the amount of gain between said lower cut-off frequency f_1 and said upper cut-off frequency f_2 .
10. The method of claim 8 wherein said adjusting step includes the sub-steps of
 - providing a cut-off frequency f_c such that signals of frequency below f_c are increasingly attenuated



with decreasing frequency below said cut-off frequency f_c ,
 providing limiting attenuation of such signals at low frequencies approaching zero frequency, and
 adjusting the level of said limited attenuation and said cut-off frequency f_c .

- 5 11. The method of claim 8 wherein said adjusting step includes the sub-steps of
 providing a first gain for seismic signals of high frequencies above a higher cut-off frequency f_2 ,
 providing a falling gain for seismic signals of frequencies below said higher cut-off frequency.
 providing a second gain for seismic signals of low frequencies below a lower cut-off frequency f_1 ,
 and
 10 adjusting the frequency of said lower cut-off frequency, the amount of gain between said lower cut-
 off frequency f_1 and said upper cut-off frequency f_2 , and
 providing a cut-off frequency f_c such that signals of frequency below f_c are increasingly attenuated
 with decreasing frequency below said cut-off frequency f_c ,
 providing limiting attenuation of such signals at low frequencies approaching zero frequency, and
 15 adjusting the level of said limited attenuation and said cut-off frequency f_c .

Patentansprüche

- 20 1. Ein geophysikalischer Datenerfassungssystemkanal, zur Verwendung bei der Aufzeichnung geophysika-
 lischer Daten für Erdformationen, wobei die Erdformationen als Reaktion auf eine spezifische Energie-
 quelle an verschiedenen Stellen der Erde unterschiedliche Spektraleigenschaften aufweisen, wobei der
 Kanal eine Eingangsstufe, die auf seismische Signale anspricht und ein Registrierinstrument (22') zur
 Speicherung der Darstellungen der Signale umfaßt sowie einen A/D-Umsetzer mit einem festgelegten
 25 wirksamen Dynamikbereich, wobei der Kanal durch eine Einrichtung zur Einstellung der Spektraleigen-
 schaften des Kanals unter Selbstkontrolle gekennzeichnet ist, so daß das Gesamtspektrum der der
 Kombination der Erde und des Kanals verbessert wird, wodurch die Auflösung der erfaßten Daten
 erhöht wird.
- 30 2. Kanal nach Anspruch 1, wobei die Einrichtung zur Einstellung der Spektraleigenschaften einen Verstar-
 kerkreis (30) aufweist, der folgendes umfaßt:
 eine Einrichtung zur Bereitstellung einer ersten Verstärkung für seismische Signale hoher Frequen-
 zen oberhalb einer oberen Grenzfrequenz f_2 , (S1, R1, R2, R3, R5),
 eine Einrichtung zur Bereitstellung einer fallenden Verstärkung für seismische Signale von Frequen-
 35 zen unterhalb der oberen Grenzfrequenz, dadurch gekennzeichnet, daß der Kanal ferner eine Einrich-
 tung zur Bereitstellung einer zweiten Verstärkung für seismische Signale niedriger Frequenzen unter-
 halb einer unteren Grenzfrequenz f_1 , (S1, RA, R2, R5), umfaßt und
 eine Einrichtung zur Einstellung unter Selbstkontrolle, der Frequenz der unteren Grenzfrequenz und
 des Ausmaßes der ansteigenden Verstärkung zwischen der unteren Grenzfrequenz f_1 und der oberen
 Grenzfrequenz f_2 (S1, S2, S3, S4, S5).
- 40 3. Kanal nach Anspruch 2, wobei die Einrichtung zur Bereitstellung einer ersten Verstärkung, die
 Einrichtung zur Bereitstellung einer zweiten Verstärkung und die Einrichtung zur Bereitstellung einer
 fallenden Verstärkung folgendes umfassen:
 eine Differentialverstärkereinrichtung (43) mit Differentialeingängen zum Empfang geophysikali-
 45 scher Daten über zwei Eingangsleitungen (1, 2) und zur Erzeugung einzelner Zwischensignale, die
 proportional zu den Signalen sind, die zwischen den Eingangsleitungen angelegt werden,
 eine Verstärkereinrichtung (51), wobei einem der Eingangsanschlüsse der Einrichtung die verstärk-
 ten Zwischensignale zugeführt werden, wobei ein Teil der Ausgabe des Verstärkers zur Erzeugung von
 Ausgangssignalen über ein frequenzempfindliches Netz einem anderen Eingangsanschluß zugeführt
 50 wird und
 wobei die Ausgangssignale relativ zu den über beide Eingangsschlüsse angelegten Signalen
 gekennzeichnet sind, durch eine zweite Verstärkung bei niedrigen Frequenzen, eine erste Verstärkung
 bei hohen Frequenzen und eine ansteigende Verstärkung zwischen einer unteren Grenzfrequenz f_1 und
 einer oberen Grenzfrequenz f_2 .
- 55 4. Kanal nach Anspruch 1, wobei die Einrichtung zur Einstellung der Spektraleigenschaften einen schwä-
 chungsbegrenzten Tiefpaßfilter aufweist, der folgendes umfaßt:
 eine Einrichtung zur Erzeugung (R2A, R4A) einer Grenzfrequenz f_c , so daß Signale von Frequenzen



unterhalb von f_c mit einer abnehmenden Frequenz unterhalb der Grenzfrequenz f_c zunehmend geschwächt werden und zur begrenzenden Schwächung (RB) dieser Signale bei einer niedrigen Frequenz, die sich der Nullfrequenz nähert und

eine Einrichtung zur Einstellung der Höhe der begrenzten Schwächung und der Grenzfrequenz f_c unter Selbstkontrolle.

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5. Kanal nach Anspruch 4, wobei der genannte schwächungsbegrenzte Tiefpaßfilter durch eine Eingabe-Empfindlichkeit gekennzeichnet ist, mit einem Bereich der maximalen Schwächung (A_{max}) unterhalb der Grenzfrequenz f_c , wobei die maximale Schwächung größer oder gleich der begrenzten Schwächung ist.

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6. Kanal nach Anspruch 4 oder 5, wobei der schwächungsbegrenzte Tiefpaßfilter einen Tiefpaßfilter zweiter Ordnung darstellt.

7. Kanal nach Anspruch 1, wobei die Einrichtung zur Einstellung der Spektraleigenschaften folgendes aufweist:

15

einen Verstärkerkreis (30) mit

einer Einrichtung zur Bereitstellung einer ersten Verstärkung für seismische Signale hoher Frequenzen oberhalb einer oberen Grenzfrequenz f_2 , (S1, R1, R2, R3, R5),

20

einer Einrichtung zur Bereitstellung einer fallenden Verstärkung für seismische Signale von Frequenzen unterhalb der oberen Grenzfrequenz, dadurch gekennzeichnet, daß der Kanal ferner eine Einrichtung zur Bereitstellung einer zweiten Verstärkung für seismische Signale niedriger Frequenzen unterhalb einer unteren Grenzfrequenz f_1 , (S1, RA, R2, R5), umfaßt und

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einer Einrichtung zur Einstellung unter Selbstkontrolle, der Frequenz der unteren Grenzfrequenz und der Höhe der ansteigenden Verstärkung zwischen der unteren Grenzfrequenz f_1 und der oberen Grenzfrequenz f_2 (S1, S2, S3, S4, S5) und

einem schwächungsbegrenzten Tiefpaßfilter (35) mit

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einer Einrichtung zur Erzeugung (R2A, R4A) einer Grenzfrequenz f_c , so daß Signale von Frequenzen unterhalb von f_c mit einer abnehmenden Frequenz unterhalb der Grenzfrequenz f_c zunehmend geschwächt werden und zur begrenzenden Schwächung (RB) dieser Signale bei einer niedrigen Frequenz, die sich der Nullfrequenz nähert und

einer Einrichtung zur Einstellung der Höhe der begrenzten Schwächung und der Grenzfrequenz f_c unter Selbstkontrolle.

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8. Verfahren zur Einstellung der Gesamtkombination der Spektraleigenschaften des Kanals des Datenerfassungssystems für Erde und geophysikalische Daten, um die Auflösung der von dem Kanal erfaßten Signale zu erhöhen, wobei das Verfahren folgende Schritte umfaßt:

Ermittlung der Spektraleigenschaften der Erde und

40

Einstellung der Spektraleigenschaften des Kanals unter Selbstkontrolle, so daß das Gesamtspektrum der Kombination der Erde und des Kanals verbessert wird.

9. Verfahren nach Anspruch 8, wobei der Einstellungsschritt folgende Unterschritte umfaßt:

45

Bereitstellung einer ersten Verstärkung für seismische Signale hoher Frequenzen oberhalb einer oberen Grenzfrequenz f_2 ,

Bereitstellung einer fallenden Verstärkung für seismische Signale von Frequenzen unterhalb der oberen Grenzfrequenz,

Bereitstellung einer zweiten Verstärkung für seismische Signale niedriger Frequenzen unterhalb einer unteren Grenzfrequenz f_1 und

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Einstellung der Frequenz der unteren Grenzfrequenz, der Höhe der Verstärkung zwischen der unteren Grenzfrequenz f_1 und der oberen Grenzfrequenz f_2 .

10. Verfahren nach Anspruch 8, wobei der Einstellungsschritt folgende Unterschritte umfaßt:

55

Bereitstellung einer Grenzfrequenz f_c , so daß Signale von Frequenzen unterhalb von f_c mit einer abnehmenden Frequenz unterhalb der Grenzfrequenz f_c zunehmend geschwächt werden,

Bereitstellung einer begrenzten Schwächung dieser Signale bei niedrigen Frequenzen, die sich der Nullfrequenz nähern, und

Einstellung der Höhe der begrenzten Schwächung und der Grenzfrequenz f_c .



11. Verfahren nach Anspruch 8, wobei der Einstellungsschritt folgende Unterschritte umfaßt:

- Bereitstellung einer ersten Verstärkung für seismische Signale hoher Frequenzen oberhalb einer oberen Grenzfrequenz f_2 ,
- Bereitstellung einer fallenden Verstärkung für seismische Signale von Frequenzen unterhalb der oberen Grenzfrequenz,
- Bereitstellung einer zweiten Verstärkung für seismische Signale niedriger Frequenzen unterhalb einer unteren Grenzfrequenz f_1 und
- Einstellung der Frequenz der unteren Grenzfrequenz, der Höhe der Verstärkung zwischen der unteren Grenzfrequenz f_1 und der oberen Grenzfrequenz f_2 und
- Bereitstellung einer begrenzten Schwächung dieser Signale bei niedrigen Frequenzen, die sich der Nullfrequenz nähern und
- Einstellung der Höhe der begrenzten Schwächung und der Grenzfrequenz f_0 .

Revendications

1. Voie d'un système d'acquisition de données géophysiques, destinée à être utilisée pour une opération d'enregistrement de données géophysiques afférentes à des formations de terrain, lesdites formations possédant des caractéristiques spectrales différentes en réponse à une source d'énergie spécifique disposée en différents emplacements sur le terrain,
 - ladite voie comprenant un étage d'entrée sensible à des signaux sismique, un enregistreur (22') pour stocker des représentations de ces signaux et un convertisseur analogique-numérique ayant une plage dynamique effective déterminée,
 - ladite voie étant caractérisée en ce qu'elle comporte des moyens, mis en oeuvre par un opérateur, pour ajuster ses caractéristiques spectrales de telle manière que le spectre total de la combinaison formée par le terrain et par la voie soit élargi, augmentant ainsi la résolution des signaux acquis.
2. Voie selon la revendication 1, dans laquelle les moyens pour ajuster lesdites caractéristiques spectrales comportent un circuit de valorisation (30) comprenant:
 - des moyens pour fournir un premier gain aux signaux sismiques ayant des fréquences élevées, situées au-delà d'une fréquence de coupure haute f_2 (S1, R1, R2, R3, R5),
 - des moyens pour fournir un gain décroissant aux signaux sismiques ayant des fréquences situées en-deçà de ladite fréquence de coupure haute,
 - caractérisée en ce qu'elle comprend également:
 - des moyens pour fournir un second gain aux signaux sismiques ayant des fréquences basses situées en deçà d'une fréquence de coupure basse f_1 (S1, RA, R2, R5);
 - et des moyens, adaptés à être mis en oeuvre par un opérateur, pour fixer la valeur de ladite fréquence de coupure basse et la valeur du gain croissant entre ladite fréquence de coupure basse f_1 et ladite fréquence de coupure haute f_2 (S1, S2, S3, S4, S5).
3. Voie selon la revendication 2, dans laquelle les moyens pour fournir un premier gain, les moyens pour fournir un second gain et les moyens pour fournir un gain décroissant comprennent:
 - un étage amplificateur différentiel (43) ayant des entrées différentielles pour accepter des signaux sismiques sur deux conducteurs d'entrée (1, 2) et pour produire sur une sortie unique des signaux intermédiaires amplifiés proportionnels aux signaux appliqués entre les deux conducteurs d'entrée;
 - un étage amplificateur (51) recevant sur l'une de ses deux bornes d'entrée lesdits signaux intermédiaires amplifiés, cet étage amplificateur ayant une partie de ses signaux de sortie appliquée à une autre de ses bornes d'entrée, via un réseau sensible aux fréquences, afin de produire des signaux de sortie;
 - caractérisée en ce que lesdits signaux de sortie présentent vis-à-vis des signaux appliqués entre lesdites deux bornes d'entrée, un second gain à des fréquences basses, un premier gain à des fréquences hautes et un gain croissant entre une fréquence de coupure basse f_1 et une fréquence de coupure haute f_2 .
4. Voie selon la revendication 1, dans laquelle lesdits moyens pour ajuster lesdites caractéristiques spectrales comportent un filtre d'atténuation limitée opérant à partir d'une fréquence de coupure basse, qui comprend:



- des moyens pour produire une fréquence de coupure f_c (R2A, R4A) telle que les signaux de fréquence inférieure à f_c aient une atténuation croissante avec une fréquence décroissant en dessous de ladite fréquence f_c et pour limiter l'atténuation (RB) de tels signaux à des fréquences approchant la fréquence zéro, et
 - des moyens, mis en oeuvre par un opérateur, pour fixer le niveau de cette atténuation limitée et la valeur de cette fréquence de coupure f_c .
- 5
5. Voie selon la revendication 4, dans laquelle le filtre d'atténuation limitée opérant en deçà d'une fréquence de coupure basse est caractérisée en ce que sa fonction de transfert présente une région d'atténuation maximale (Amax) au-dessous de ladite fréquence de coupure f_c , ladite atténuation maximale étant supérieure ou au moins égale à ladite atténuation limitée.
- 10
6. Voie selon les revendications 4 ou 5, dans laquelle ledit filtre d'atténuation limitée à fréquence de coupure basse est un filtre du second ordre à fréquence de coupure.
- 15
7. Voie selon la revendication 1, dans laquelle les moyens pour ajuster lesdites caractéristiques spectrales comportent un circuit de valorisation (30) comprenant:
- des moyens pour fournir un premier gain aux signaux sismiques ayant des fréquences situées en dessous d'une fréquence de coupure haute f_2 (R1, R2, R3, R4, R5);
 - des moyens pour fournir un gain décroissant aux signaux sismiques ayant des fréquences situées en dessous de ladite fréquence de coupure haute,
 - caractérisée en ce que la dite voie comporte également:
 - des moyens pour fournir un second gain pour les signaux sismiques ayant des fréquences basses situées en dessous d'une fréquence de coupure basse f_1 (S1, RA, R2, R5);
 - des moyens, mis en oeuvre par un opérateur, pour fixer la valeur de ladite fréquence de coupure basse et la valeur du gain croissant entre ladite fréquence de coupure basse f_1 et ladite fréquence de coupure haute f_2 (S1, S2, S3, S4, S5),
 - un filtre d'atténuation limitée (35) en dessous d'une fréquence de coupure basse comprenant:
 - des moyens pour produire une fréquence de coupure f_c (R2A-R4A) telle que les signaux de fréquences inférieures à f_c aient une atténuation croissante lorsque leur fréquence décroît en dessous de ladite fréquence de coupure f_c et pour limiter l'atténuation (RB) de tels signaux aux fréquences basses approchant la fréquence zéro;
 - des moyens, mis en oeuvre par un opérateur, pour fixer le niveau de ladite atténuation limitée et la valeur de ladite fréquence de coupure f_c .
- 20
- 25
- 30
- 35
8. Procédé pour ajuster la combinaison formée par les caractéristiques du terrain et d'une voie d'un système d'acquisition de données géophysiques, de manière à augmenter la résolution des signaux acquis par la voie, caractérisé en ce qu'il comprend les étapes suivantes:
- déterminer les caractéristiques spectrales du terrain;
 - faire ajuster par un opérateur les caractéristiques spectrales de la voie du système d'acquisition de telle manière que le spectre total de la combinaison formée par le terrain et ladite voie soit élargi.
- 40
9. Procédé selon la revendication 8, dans lequel lesdites étapes comprennent les sous-étapes suivantes:
- fournir un premier gain à des signaux sismiques ayant des fréquences élevées situées au-delà d'une fréquence de coupure haute f_2 ;
 - fournir un gain décroissant aux signaux sismiques ayant des fréquences situées en deçà de ladite fréquence de coupure haute;
 - fournir un second gain aux signaux sismiques ayant des fréquences situées en deçà d'une fréquence de coupure basse f_1 ;
 - ajuster la valeur de ladite fréquence de coupure basse, le montant du gain entre ladite fréquence de coupure basse f_1 et ladite fréquence de coupure haute f_2 .
- 45
- 50
10. Procédé selon la revendication 8, dans lequel ladite étape d'ajustement comprend les sous-étapes suivantes:
- fournir une fréquence de coupure f_c telle que les signaux de fréquences situées en deçà de f_c aient une atténuation croissante lorsque leur fréquence décroît en deçà de ladite fréquence de coupure f_c ;
- 55



- fournir une atténuation limitée aux signaux de fréquence basse approchant la fréquence zéro;
- ajuster le niveau de ladite atténuation limitée et la valeur de ladite fréquence de coupure f_c .

11. Procédé selon la revendication 8, dans lequel l'étape d'ajustement comprend les sous-étapes suivantes:

- fournir un premier gain aux signaux sismiques de fréquences hautes situées au-delà d'une fréquence de coupure haute f_2 ;
- fournir un gain décroissant aux signaux sismiques ayant des fréquences situées en deçà de ladite fréquence de coupure haute;
- fournir un second gain aux signaux sismiques ayant des fréquences basses situées en deçà d'une fréquence de coupure basse f_1 ;
- ajuster la valeur de ladite fréquence de coupure basse, le montant du gain entre ladite fréquence de coupure basse f_1 et ladite fréquence de coupure haute f_2 ;
- fournir une fréquence de coupure f_c telle que les signaux de fréquences situées au-dessous de f_c aient une atténuation croissante lorsque leur fréquence décroît au-dessous de ladite fréquence de coupure f_c ;
- fournir une atténuation limitée aux signaux ayant des fréquences basses approchant la fréquence zéro;
- ajuster le niveau de ladite atténuation limitée et la valeur de ladite fréquence de coupure f_c .