

CONTROLLING PRODUCTION OF TRANSPORTATION
FUELS FROM RENEWABLE FEEDSTOCKS

STATEMENT REGARDING FEDERALLY SPONSORED
RESEARCH OR DEVELOPMENT

5 **[0001]** This invention was made under the support of the United States Government, United States Army Research Office, with financial support from DARPA, Agreement Number W911NF-07-C-0049. The United States Government has certain rights in the invention.

BACKGROUND OF THE INVENTION

10 **[0002]** This invention relates to a process for controlling the production of hydrocarbons useful as transportation fuels including diesel fuel and aviation fuel from renewable feedstocks such as the glycerides and free fatty acids found in materials such as plant oils, fish oils, animal fats, and greases. The process involves hydrogenation, decarboxylation, decarbonylation, and/or hydrodeoxygenation and optionally hydroisomerization, cracking, or
15 selective cracking, in one or more steps. Desired product specifications and yields are determined and reaction and fractionation conditions are set to achieve the specifications and yields.

[0003] As the demand for transportation fuel increases worldwide there is increasing interest in sources other than petroleum crude oil for producing diesel and aviation fuel. One
20 such source is what has been termed renewable feedstocks. These renewable feedstocks include examples such as plant oils such as corn, rapeseed, canola, soybean and algal oils, animal fats and oils such as tallow, fish oils and various waste streams such as yellow and brown greases and sewage sludge. The common feature of these feedstocks is that they are composed of glycerides and Free Fatty Acids (FFA). Another class of compounds appropriate
25 for these processes fatty acid alkyl esters (FAAE), such as fatty acid methyl ester (FAME). These types of compounds contain aliphatic carbon chains generally having from 8 to 24 carbon atoms. The aliphatic carbon chains in the glycerides, FFAs, or FAAEs can be saturated or mono-, di- or poly-unsaturated. Most of the glycerides in the renewable feed stocks will be triglycerides, but some of the glycerides in the renewable feedstock may be monoglycerides

or diglycerides. The monoglycerides and diglycerides can be processed along with the triglycerides.

[0004] There are reports in the art disclosing the production of hydrocarbons from plant oils. For example, US 4,300,009 discloses the use of crystalline aluminosilicate zeolites to convert plant oils such as corn oil to hydrocarbons such as gasoline and chemicals such as para-xylene. US 4,992,605 discloses the production of hydrocarbon products in the diesel boiling range by hydroprocessing vegetable oils such as canola or sunflower oil. Finally, US 2004/0230085 A1 discloses a process for treating a hydrocarbon component of biological origin by hydrodeoxygenation followed by isomerization.

[0005] The process herein comprises an optional pretreatment step, and one or more steps to hydrogenate, deoxygenate, hydroisomerize and optionally selectively hydrocrack the renewable feedstock, to generate both a diesel fuel component and an aviation fuel component. The specifications and relative yields of the diesel component and the aviation component are determined and the operating conditions of the isomerization and selective hydrocracking zone are determined in order to meet the specifications and yields of the products. The fractionation zone conditions are determined in order to separate the desired products at the desired yields. The diesel component and the aviation component may be suitable as fuels, used as components of blending pools, or may have one or more additives incorporated before being used as fuels.

SUMMARY OF THE INVENTION

[0006] The process herein is a process for controlling the production of a diesel component comprising hydrocarbons having boiling points in the diesel fuel range and an aviation component comprising hydrocarbons having boiling points in the aviation fuel range from a renewable feedstock. The process begins by identifying specifications required for the diesel component and for the aviation component; determining yields required for the diesel component and for the aviation component and that meet required specifications; determining isomerization and selective cracking conditions required in an isomerization and selective hydrocracking zone that result in the predetermined yields required for the diesel component and for the aviation component wherein the diesel component and the aviation component further meet the identified specifications; and determining operating conditions for a

fractionation zone that results in the separation of the diesel component and the aviation component at the required yields. The process further involves hydrogenating and deoxygenating the renewable feedstock by contacting the feedstock in a hydrogenation and deoxygenation zone with a hydrogenation and deoxygenation catalyst at hydrogenation and deoxygenation conditions to provide a hydrogenation and deoxygenation zone effluent comprising n-paraffins; isomerizing and selectively hydrocracking at least a portion of the n-paraffins in the hydrogenation and deoxygenation zone effluent by contacting with an isomerization and selective hydrocracking catalyst at the predetermined isomerization conditions in an isomerization and selective hydrocracking zone to generate branched-paraffins in an isomerization and selective hydrocracking zone effluent; and fractionating, in the fractionation zone, the isomerization and selective hydrocracking zone effluent the predetermined operating conditions of the fractionation zone to provide a first product stream comprising the diesel component, and a second product stream comprising the aviation component.

BRIEF DESCRIPTION OF THE DRAWINGS

[0007] FIG. 1 is a general flow scheme of one embodiment of the invention.

[0008] FIG. 2 is a general schematic of one embodiment of the invention to demonstrate possible control actions to implement in the process and their potential impact of the desired products.

DETAILED DESCRIPTION OF THE INVENTION

[0009] As stated, the present invention relates to a process for producing a first hydrocarbon product stream useful as diesel fuel or diesel fuel blending component and a second hydrocarbon product stream useful as aviation fuel or an aviation fuel blending component from a renewable feedstock such as those originating from plants or animals. The present invention involves controlling such a production process in order to produce the desired fuels as provided in industry, government, or military standards. Different types of diesel fuels or aviation fuels may be produced, and the controlled process provides a technique to enable an operator to produce different fuel types at different times or different relative yields at different times. For example, should the demand for aviation fuel increase

relative to diesel fuel, the control process allows an operator to adjust the relative yields of aviation fuel and diesel fuel to meet changing demands.

[0010] The term renewable feedstock is meant to include feedstocks other than those obtained directly from petroleum crude oil. Another term that has been used to describe at least a portion of this class of feedstocks is biorenewable feedstocks. The renewable feedstocks that can be used in the present invention include any of those which comprise glycerides, fatty acid alkyl esters (FAAE), and free fatty acids (FFA). Examples of these feedstocks include, but are not limited to, canola oil, corn oil, soy oils, rapeseed oil, soybean oil, colza oil, tall oil, sunflower oil, hempseed oil, olive oil, linseed oil, coconut oil, castor oil, peanut oil, palm oil, mustard oil, cottonseed oil, tallow, yellow and brown greases, lard, train oil, fats in milk, fish oil, algal oil, sewage sludge, cuphea oil, camelina, oil, jatropha oil, curcas oil, babassu oil, palm kernel oil, crambe oil, fatty acid methyl esters, lard, and the like. The glycerides, FAAES and FFAs of the typical vegetable or animal fat contain aliphatic hydrocarbon chains in their structure which have 8 to 24 carbon atoms with many of the oils containing high concentrations of fatty acids with 16 and 18 carbon atoms. Mixtures or co-feeds of renewable feedstocks and petroleum derived hydrocarbons may also be used as the feedstock. Other feedstock components which may be used, especially as a co-feed component in combination with the above listed renewable feedstocks, include spent motor oils and industrial lubricants, used paraffin waxes, liquids derived from gasification of coal, biomass, or natural gas followed by a downstream liquefaction step such as Fischer-Tropsch technology; liquids derived from depolymerization, thermal or chemical, of waste plastics such as polypropylene, high density polyethylene, and low density polyethylene; and other synthetic oils generated as byproducts from petrochemical and chemical processes. Mixtures of the above feedstocks may also be used as co-feed components. One advantage of using a co-feed component is transformation of what has been considered to be a waste product from a petroleum based process into a valuable co-feed component to the current process. Another option is to decrease operating expenses by lowering the recycle ratio around the deoxygenation reactor.

[0011] Two hydrocarbon products are generated by the current process; a diesel component and an aviation component. The diesel component comprises hydrocarbons having a boiling point in the diesel range and may be used directly as a fuel, may be blended with other

components before being used as diesel fuel, or may receive additives before being used as a diesel fuel. The aviation component comprises hydrocarbons having a boiling point in the aviation range, which includes jet range, and may be used directly as aviation fuel or may be used as a blending component to meet the specifications for a specific type of aviation fuel, or may receive additives before being used as an aviation fuel. Depending upon the application, various additives may be combined with the aviation component or the diesel component generated in order to meet required specifications for different specific fuels. In particular, the aviation fuel composition generated herein complies with, is a blending component for, or may be combined with one or more additives to meet at least one of: ASTM D 1655 Specification for Aviation Turbine Fuels Defense Stan 91--91 Turbine Fuel, Aviation Kerosene Type, Jet A-1 NATO code F-35, F-34, F-37 Aviation Fuel Quality Requirements for Jointly Operated Systems (Joint Checklist) A combination of ASTM and Def Stan requirements GOST 10227 Jet Fuel Specifications (Russia) Canadian CAN/CGSB-3.22 Aviation Turbine Fuel, Wide Cut Type Canadian CAN/CGSB-3.23 Aviation Turbine Fuel, Kerosene Type MIL-DTL-83133, JP-8, MIL-DTL-5624, JP-4, JP-5 QAV-1 (Brazil) Especificacao de Querosene de Aviacao No. 3 Jet Fuel (Chinese) according to GB6537 DCSEA 134A (France) Carbureacteur Pour Turbomachines D'Aviation, Type Kerosene Aviation Turbine Fuels of other countries, meeting the general grade requirements for Jet A, Jet A-1, Jet B, and TS-1 fuels as described in the IATA Guidance Material for Aviation Turbine Fuel Specifications. The aviation fuel is generally termed "jet fuel" herein and the term "jet fuel" is meant to encompass aviation fuel meeting the specifications above as well as to encompass aviation fuel used as a blending component of an aviation fuel meeting the specifications above. Additives may be added to the jet fuel in order to meet particular specifications. One particular type of jet fuel is JP-8, defined by Military Specification MIL-DTL-83133, which is a military grade type of highly refined kerosene based jet propellant specified by the United States Government. The fuel produced from glycerides or FAA as described herein is very similar to isoparaffinic kerosene or iPK, also known as a synthetic paraffinic kerosene (SPK) or synthetic jet fuel.

[0012] The control of the process allows for an operator to select the specific type of aviation fuel or blending component or diesel fuel or blending component to be produced and thus the specifications of the fuels/components and the relative yields of each so long as the yields selected allow the fuel specifications to be met. Then the operating conditions of the

isomerization and selective hydrocracking zone, described below, are determined so that the effluent of the zone comprises the hydrocarbons necessary to meet the desired fuel specifications. The operating conditions of a fractionation zone, also described below, are determined so that the hydrocarbons produced in the isomerization and selective cracking zone are separated into two product streams, a first product stream comprising the hydrocarbons in the diesel boiling range and meeting the specifications selected for the diesel component, and the second product stream comprising the hydrocarbons in the aviation boiling range and meeting the specification selected for the aviation component. A small byproduct stream of light hydrocarbons is also generated. This stream can be converted to useful hydrogen via standard steam reforming if desired.

[0013] The control process provides operators with a great deal of flexibility. Different grades of standards of fuels may be produced at different times as the market demands change, and the relative yields of the diesel component and the aviation component may be changed with market demands as well. Feedstock availability and pricing may also result in a need to control the process. The steps of the control process may be executed periodically as the operator desires in order to accommodate changing desires for different fuel specifications or yields.

[0014] Renewable feedstocks used in the present invention may contain a variety of impurities. For example, tall oil is a by product of the wood processing industry and tall oil contains esters and rosin acids in addition to FFAs. Rosin acids are cyclic carboxylic acids. The renewable feedstocks may also contain contaminants such as alkali metals, e.g. sodium and potassium, phosphorous as well as solids, water and detergents. An optional first step is to remove as much of these contaminants as possible. One possible pretreatment step involves contacting the renewable feedstock with an ion-exchange resin in a pretreatment zone at pretreatment conditions. The ion-exchange resin is an acidic ion exchange resin such as AmberlystTM-15 and can be used as a bed in a reactor through which the feedstock is flowed through, either upflow or downflow. Another technique includes contacting the renewable feedstock with a bleaching earth, such as bentonite clay, in a pretreatment zone.

[0015] Another possible means for removing contaminants is a mild acid wash. This is carried out by contacting the renewable feedstock with an acid such as sulfuric, nitric, phosphoric, or hydrochloric in a reactor. The acid and renewable feedstock can be contacted

either in a batch or continuous process. Contacting is done with a dilute acid solution usually at ambient temperature and atmospheric pressure. If the contacting is done in a continuous manner, it is usually done in a counter current manner. Yet another possible means of removing metal contaminants from the renewable feedstock is through the use of guard beds which are well known in the art. These can include alumina guard beds either with or without demetallation catalysts such as nickel or cobalt. Filtration and solvent extraction techniques are other choices which may be employed. Hydroprocessing such as that described in USAN 11/770,826 is another pretreatment technique which may be employed.

[0016] With the specifications of the products being determined, the relative yields of the products being determined, the operating conditions of the isomerization and selective hydrocracking zone and fraction zone being determined and set; the feedstock is flowed to a reaction zone comprising one or more catalyst beds in one or more reactors. The term feedstock is meant to include feedstocks that have not been treated to remove contaminants as well as those feedstocks purified in a pretreatment zone or oil processing facility. In the reaction zone, the feedstock is contacted with a hydrogenation or hydrotreating catalyst in the presence of hydrogen at hydrogenation conditions to hydrogenate the olefinic or unsaturated portions of the aliphatic hydrocarbon chains. Hydrogenation or hydrotreating catalysts are any of those well known in the art such as nickel or nickel/molybdenum dispersed on a high surface area support. Other hydrogenation catalysts include one or more noble metal catalytic elements dispersed on a high surface area support. Non-limiting examples of noble metals include Pt and/or Pd dispersed on gamma-aluminas. Hydrogenation conditions include a temperature of 200°C to 300°C and a pressure of 1379 kPa absolute (200 psia) to 4826 kPa absolute (700 psia). Other operating conditions for the hydrogenation zone are well known in the art. Note that a lower temperature zone is not necessary because the higher temperature hydrotreating conditions will also cause hydrogenation.

[0017] The hydrogenation and hydrotreating catalysts enumerated above are also capable of catalyzing decarboxylation, decarbonylation, and/or hydrodeoxygenation of the feedstock to remove oxygen. Decarboxylation, decarbonylation, and hydrodeoxygenation are herein collectively referred to as deoxygenation reactions. Deoxygenation conditions include a relatively low pressure of 1724 kPa absolute (250 psia) to 10,342 kPa absolute (1500 psia), with embodiments in the range of 3447 kPa (500 psia) to 6895 kPa (1000 psia) or below

4826 kPaa (700 psia); a temperature of 200°C to 460°C with embodiments in the range of 288°C to 345°C; and a liquid hourly space velocity of 0.25 to 4 hr⁻¹ with embodiments in the range of 1 to 4 hr⁻¹. Since hydrogenation is an exothermic reaction, as the feedstock flows through the catalyst bed the temperature increases and decarboxylation, decarbonylation, and hydrodeoxygenation will occur. Although the hydrogenation reaction is exothermic, some feedstocks may be highly saturated and not generate enough heat internally. Therefore, some embodiments may require external heat input. Thus, it is envisioned and is within the scope of this invention that all the reactions occur simultaneously in one reactor or in one bed. Alternatively, the conditions can be controlled such that hydrogenation primarily occurs in one bed and decarboxylation, decarbonylation, and/or hydrodeoxygenation occurs in a second or additional bed(s). If only one bed is used, it may be operated so that hydrogenation occurs primarily at the front of the bed, while decarboxylation, decarbonylation and hydrodeoxygenation occurs mainly in the middle and bottom of the bed. Finally, desired hydrogenation can be carried out in one reactor, while decarboxylation, decarbonylation, and/or hydrodeoxygenation can be carried out in a separate reactor. However, the order of the reactions is not critical to the success of the process.

[0018] The reaction product from the hydrogenation and deoxygenation reactions will comprise both a liquid portion and a gaseous portion. The liquid portion comprises a hydrocarbon fraction comprising n-paraffins and having a large concentration of paraffins in the 15 to 18 carbon number range. Different feedstocks will have different distributions of paraffins. A portion of this hydrocarbon fraction, after separation from the gaseous portion, may be used as the hydrocarbon recycle described above. Although this hydrocarbon fraction is useful as a diesel fuel or diesel fuel blending component, additional fuels, such as aviation fuels or aviation fuel blending components which typically have a concentration of paraffins in the range of 9 to 15 carbon atoms, may be produced with additional processing. Also, because the hydrocarbon fraction comprises essentially all n-paraffins, it will have poor cold flow properties. Many diesel and aviation fuels and blending components must have better cold flow properties and so the reaction product is further reacted under isomerization conditions to isomerize at least a portion of the n-paraffins to branched paraffins.

[0019] The gaseous portion of the reaction product from the hydrogenation and deoxygenation zone comprises hydrogen, carbon dioxide, carbon monoxide, water vapor,

propane nitrogen or nitrogen compounds and perhaps sulfur components such as hydrogen sulfide or phosphorous component such as phosphine. The effluent from the deoxygenation zone is conducted to a hot high pressure hydrogen stripper. One purpose of the hot high pressure hydrogen stripper is to selectively separate at least a portion of the gaseous portion of the effluent from the liquid portion of the effluent. As hydrogen is an expensive resource, to conserve costs, the separated hydrogen is recycled to the first reaction zone containing the deoxygenation reactor. Also, failure to remove the water, carbon monoxide, and carbon dioxide from the effluent may result in poor catalyst performance in the isomerization zone. Water, carbon monoxide, carbon dioxide, any ammonia or hydrogen sulfide are selectively stripped in the hot high pressure hydrogen stripper using hydrogen. The hydrogen used for the stripping may be dry, and free of carbon oxides. The temperature may be controlled in a limited range to achieve the desired separation and the pressure may be maintained at approximately the same pressure as the two reaction zones to minimize both investment and operating costs. The hot high pressure hydrogen stripper may be operated at conditions ranging from a pressure of 689 kPa absolute (100 psia) to 13,790 kPa absolute (2000 psia), and a temperature of 40°C to 350°C. In another embodiment the hot high pressure hydrogen stripper may be operated at conditions ranging from a pressure of 1379 kPa absolute (200 psia) to 4826 kPa absolute (700 psia), or 2413 kPa absolute (350 psia) to 4882 kPa absolute (650 psia), and a temperature of 50°C to 350°C. The hot high pressure hydrogen stripper may be operated at essentially the same pressure as the reaction zone. By “essentially”, it is meant that the operating pressure of the hot high pressure hydrogen stripper is within 1034 kPa absolute (150 psia) of the operating pressure of the reaction zone. For example, in one embodiment the hot high pressure hydrogen stripper separation zone is no more than 1034 kPa absolute (150 psia) less than that of the reaction zone.

[0020] The effluent enters the hot high pressure stripper and at least a portion of the gaseous components, are carried with the hydrogen stripping gas and separated into an overhead stream. The remainder of the deoxygenation zone effluent stream is removed as hot high pressure hydrogen stripper bottoms and contains the liquid hydrocarbon fraction having components such as normal hydrocarbons having from 8 to 24 carbon atoms. A portion of this liquid hydrocarbon fraction in hot high pressure hydrogen stripper bottoms may be used as the hydrocarbon recycle described below.

[0021] Hydrogen is a reactant in the reactions above, and to be effective, a sufficient quantity of hydrogen must be in solution to most effectively take part in the catalytic reaction. Past processes have operated at high pressures in order to achieve a desired amount of hydrogen in solution and readily available for reaction. If hydrogen is not available at the reaction site of the catalyst, the coke forms on the catalyst and deactivates the catalyst. To solve this problem, the pressure is often raised to insure enough hydrogen is available to avoid coking reactions on the catalyst. However, higher pressure operations are more costly to build and to operate as compared to their lower pressure counterparts. The present invention allows for the operating pressure to be in the range of 1379 kPa absolute (200 psia) to 4826 kPa absolute (700 psia) which is lower than that found in many previous operations. In another embodiment the operating pressure is in the range of 2413 kPa absolute (350 psia) to 4481 kPa absolute (650 psia), and in yet another embodiment operating pressure is in the range of 2758 kPa absolute (400 psia) to 4137 kPa absolute (600 psia). Furthermore, the rate of reaction is increased resulting in a greater amount of throughput of material through the reactor in a given period of time. Lower operating pressures provide an additional advantage in increasing the decarboxylation reaction while reducing the hydrodeoxygenation reaction. The result is a reduction in the amount of hydrogen required to remove oxygen from the feedstock component and produce a finished product. Hydrogen can be a costly component of the feed and reduction of the hydrogen requirements is beneficial from an economic standpoint.

[0022] In one embodiment of the invention, the desired amount of hydrogen is kept in solution at lower pressures by employing a large recycle of hydrocarbon. Other processes have employed hydrocarbon recycle in order to control the temperature in the reaction zones since the reactions are exothermic reactions. However, the range of recycle to feedstock ratios used herein is set based on the need to control the level of hydrogen in the liquid phase and therefore reduce the deactivation rate. The amount of recycle is determined not on temperature control requirements, but instead, based upon hydrogen solubility requirements. Hydrogen has a greater solubility in the hydrocarbon product than it does in the feedstock. By utilizing a large hydrocarbon recycle the solubility of hydrogen in the liquid phase in the reaction zone is greatly increased and higher pressures are not needed to increase the amount of hydrogen in solution and avoid catalyst deactivation at low pressures. In one embodiment

of the invention, the volume ratio of hydrocarbon recycle to feedstock is from 2:1 to 8:1. In another embodiment the ratio is in the range of 3:1 to 6:1 and in yet another embodiment the ratio is in the range of 4:1 to 5:1. The ranges of suitable volume ratios of hydrocarbon recycle to feedstock are described in pending application USAN 12/193,149. Suitable ranges for hydrogen solubility were shown to begin at a recycle to feed ratio of 2:1. From recycle to feed ratios of 2:1 through 6:1 the simulation of USAN 12/193,149 showed that the hydrogen solubility remained high. Thus, the specific ranges of vol/vol ratios of recycle to feed for this embodiment is determined based on achieving a suitable hydrogen solubility in the deoxygenation reaction zone.

[0023] In another embodiment, instead of recycling hydrocarbon, one or more of the co-feed components discussed above may be used to provide the solubility of hydrogen and temperature control. Depending upon the relative costs of the hydrocarbon and the co-feed component, one embodiment may be more economic than the other. It is important to note that the recycle or co-feed is optional and the process does not require recycle or co-feed. Complete deoxygenation and hydrogenation may be achieved without recycle or co-feed components. In still another embodiment, the process may be conducted with continuous catalyst regeneration in order to counteract the catalyst deactivation effects of the lower amounts of hydrogen in solution or the higher operating conditions.

[0024] Although the hydrocarbons may be useful as a diesel fuel, or a diesel fuel blending component, because they comprises essentially all n-paraffins, they will have poor cold flow properties. To improve the cold flow properties of the liquid hydrocarbon fraction, the reaction product can be contacted with an isomerization catalyst under isomerization conditions in an isomerization and selective hydrocracking zone to at least partially isomerize the n-paraffins to isoparaffins.

[0025] Catalysts and conditions for isomerization are well known in the art. See for example US 2004/0230085 A1 which is incorporated by reference in its entirety. The conditions used for the isomerization are predetermined so that the proper degree of isomerization and selective cracking are achieved to meet the predetermined specifications of the desired products. Isomerization can be carried out in a separate bed of the same reaction zone, i.e. same reactor, described above or the isomerization can be carried out in a separate reactor. The product of the deoxygenation reaction zone is contacted with an isomerization

catalyst in the presence of hydrogen at isomerization conditions to isomerize the normal paraffins to branched paraffins. In some embodiments, only minimal branching is required, enough to overcome cold-flow problems of the normal paraffins. In other embodiments, a greater amount of isomerization is desired. The predominate isomerization product is generally a mono-branched hydrocarbon. Along with the isomerization, some hydrocracking of the hydrocarbons will occur. The more severe the conditions of the isomerization zone, the greater the amount of hydrocracking of the hydrocarbons. The hydrocracking occurring in the isomerization zone results in a wider distribution of hydrocarbons than resulted from the deoxygenation zone and increased levels of hydrocracking produces higher yields of hydrocarbons in the aviation fuel boiling range.

[0026] The isomerization of the paraffinic hydrocarbons can be accomplished in any manner known in the art or by using any suitable catalyst known in the art. Suitable catalysts comprise a metal of Group VIII (IUPAC 8-10) of the Periodic Table and a support material. Suitable Group VIII metals include platinum and palladium, each of which may be used alone or in combination. The support material may be amorphous or crystalline. Suitable support materials include aluminas, amorphous aluminas, amorphous silica-aluminas, ferrierite, ALPO-31, SAPO-11, SAPO-31, SAPO-37, SAPO-41, SM-3, MgAPSO-31, FU-9, NU-10, NU-23, ZSM-12, ZSM-22, ZSM-23, ZSM-35, ZSM-48, ZSM-50, ZSM-57, MeAPO-11, MeAPO-31, MeAPO-41, MeAPSO-11, MeAPSO-31, MeAPSO-41, MeAPSO-46, ELAPO-11, ELAPO-31, ELAPO-41, ELAPSO-11, ELAPSO-31, ELAPSO-41, laumontite, cancrinite, offretite, hydrogen form of stillbite, magnesium or calcium form of mordenite, and magnesium or calcium form of partheite, each of which may be used alone or in combination. ALPO-31 is described in US 4,310,440. SAPO-11, SAPO-31, SAPO-37, and SAPO-41 are described in US 4,440,871. SM-3 is described in US 4,943,424; US 5,087,347; US 5,158,665; and US 5,208,005. MgAPSO is a MeAPSO, which is an acronym for a metal aluminumsilicophosphate molecular sieve, where the metal Me is magnesium (Mg). Suitable MeAPSO-31 catalysts include MgAPSO-31. MeAPSOs are described in US 4,793,984, and MgAPSOs are described in US 4,758,419. MgAPSO-31 is a preferred MgAPSO, where 31 means a MgAPSO having structure type 31. Many natural zeolites, such as ferrierite, that have an initially reduced pore size can be converted to forms suitable for olefin skeletal isomerization by removing associated alkali metal or alkaline earth metal by ammonium ion exchange and calcination to produce the substantially

hydrogen form, as taught in US 4,795,623 and US 4,924,027. Further catalysts and conditions for skeletal isomerization are disclosed in US 5,510,306, US 5,082,956, and US 5,741,759.

[0027] The isomerization catalyst may also comprise a modifier selected from the group consisting of lanthanum, cerium, praseodymium, neodymium, samarium, gadolinium, terbium, and mixtures thereof, as described in US 5,716,897 and US 5,851,949. Other suitable support materials include ZSM-22, ZSM-23, and ZSM-35, which are described for use in dewaxing in US 5,246,566 and in the article entitled "New molecular sieve process for lube dewaxing by wax isomerization," written by S. J. Miller, in Microporous Materials 2 (1994) 439-449. The teachings of US 4,310,440; US 4,440,871; US 4,793,984; US 4,758,419; US 4,943,424; US 5,087,347; US 5,158,665; US 5,208,005; US 5,246,566; US 5,716,897; and US 5,851,949 are hereby incorporated by reference.

[0028] US 5,444,032 and US 5,608,968 teach a suitable bifunctional catalyst which is constituted by an amorphous silica-alumina gel and one or more metals belonging to Group VIIIA, and is effective in the hydroisomerization of long-chain normal paraffins containing more than 15 carbon atoms. US 5,981,419 and 5,908,134 teach a suitable bifunctional catalyst which comprises: (a) a porous crystalline material isostructural with beta-zeolite selected from boro-silicate (BOR-B) and boro-alumino-silicate (Al-BOR-B) in which the molar $\text{SiO}_2:\text{Al}_2\text{O}_3$ ratio is higher than 300:1; (b) one or more metal(s) belonging to Group VIIIA, selected from platinum and palladium, in an amount comprised within the range of from 0.05 to 5% by weight. Article V. Calemme et al., App. Catal. A: Gen., 190 (2000), 207 teaches yet another suitable catalyst.

[0029] The isomerization catalyst may be any of those well known in the art such as those described and cited above. In general, isomerization conditions include a temperature of 150°C to 360°C and a pressure of 1724 kPa absolute (250 psia) to 4726 kPa absolute (700 psia). In another embodiment the isomerization conditions include a temperature of 300°C to 360°C and a pressure of 3102 kPa absolute (450 psia) to 3792 kPa absolute (550 psia). Other operating conditions for the isomerization zone are well known in the art, and the specific operating conditions used are predetermined and are dependant upon the desired product specifications and relative yields of the products.

[0030] The catalysts suitable for the isomerization of the paraffinic hydrocarbons and the conditions of the isomerization zone also operate to cause some hydrocracking of the

hydrocarbons. Therefore, although a main product of the hydrogenation, deoxygenation, and isomerization steps is a paraffinic hydrocarbon fraction suitable for use as diesel fuel or as a blending component for diesel fuel, a second paraffinic hydrocarbon suitable for use as an aviation fuel, or as a component for aviation fuel is also generated. As illustrative of this concept, a concentration of paraffins formed from renewable feedstocks typically has 15 to 18 carbon atoms, but additional paraffins may be formed to provide a range of from 8 to 24 carbon atoms. A portion of the normal paraffins are isomerized to branched paraffins, but the carbon number range of paraffins does not alter with isomerization alone. However, some hydrocracking will occur concurrently with the isomerization, generating paraffins having boiling points from 150°C to 300°C which is lower than that of the majority of C15 to C18 paraffins produced in the deoxygenation reaction zone. The 150°C to 300°C boiling point range meets many aviation fuel specifications and can therefore be separated from the other boiling point ranges after the isomerization zone in order to produce an aviation fuel. This will lower the overall yield of diesel fuel but allows the production of two fuel products: a diesel fuel and an aviation fuel. The process severity in the isomerization zone controls the potential yield of product for aviation fuel, the amount of light products that are not useful for diesel fuel or aviation fuel, and the isomerized/normal ratio of both aviation and diesel range fuel. The hydrocracking is controlled through catalyst choice and reaction conditions in an attempt to restrict the degree of hydrocracking occurring. Ideally, each paraffin molecule would experience only a single hydrocracking event and ideally that single hydrocracking event would result in at least one paraffin in the C9 to C15 carbon number range. Careful choice of catalyst and control of the process conditions in the isomerization zone both maximizes paraffin products in the aviation fuel range while minimizing the production of the light paraffins that are not useful for either diesel fuel or aviation fuel applications.

[0031] Fuel specifications are typically not based upon carbon number ranges. Instead, the specifications for different types of fuels are often expressed through acceptable ranges of chemical and physical requirements of the fuel. For example, aviation turbine fuels, a kerosene type fuel including JP-8, are specified by MIL-DTL-83133, JP-4, a blend of gasoline, kerosene and light distillates, is specified by MIL-DTL-5624 and JP-5 a kerosene type fuel with low volatility and high flash point is also specified by MIL-DTL-5624, with the written specification of each being periodically revised. Often a distillation range from 10

percent recovered to a final boiling point is used as a key parameter defining different types of fuels. The distillations ranges are typically measured by ASTM Test Method D 86 or D2887. Therefore, blending of different components in order to meet the specification is quite common. While the aviation fuel product of the present invention may meet aviation fuel specifications, it is expected that some blending of the product with other blending components may be required to meet the desired set of fuel specifications. In other words, one product of this invention is a composition which may be used with other components to form a fuel meeting at least one of the specifications for aviation fuel such as JP-8. The desired aviation fuel product is a highly paraffinic distillate fuel component having a paraffin content of at least 75% by volume.

[0032] The catalysts of the subject process can be formulated using industry standard techniques. It may be manufactured in the form of a cylindrical extrudate having a diameter of from 0.8 to 3.2 mm (1/32in to 1/8 in). The catalyst can be made in any other desired form such as a sphere or pellet. The extrudate may be in forms other than a cylinder such as the form of a well-known trilobe or other shape which has advantages in terms of reduced diffusional distance or pressure drop.

[0033] The stream obtained after all reactions have been carried out, the final effluent stream, is now processed through one or more separation steps to obtain at least two purified hydrocarbon product streams, one useful as a diesel fuel or diesel fuel blending component and a second useful as aviation fuel or an aviation fuel blending component. At least a third lighter stream of components not useful as diesel or aviation fuel is also separated.

[0034] With the effluent stream of the isomerization and selective hydrocracking zone comprising both a liquid component and a gaseous component, various portions of which may be recycled, multiple separation steps may be employed. For example, hydrogen may be first separated in a isomerization effluent separator with the separated hydrogen being removed in an overhead stream. Suitable operating conditions of the isomerization effluent separator include, for example, a temperature of 230°C and a pressure of 4100 kPa absolute (600 psia). If there is a low concentration of carbon oxides, or the carbon oxides are removed, the hydrogen may be recycled back to the hot high pressure hydrogen stripper for use both as a rectification gas and to combine with the remainder as a bottoms stream. The remainder is passed to the isomerization reaction zone and thus the hydrogen becomes a component of the

isomerization reaction zone feed streams in order to provide the necessary hydrogen partial pressures for the reactor. The hydrogen is also a reactant in the deoxygenation reactors, and different feedstocks will consume different amounts of hydrogen. The isomerization effluent separator allows flexibility for the process to operate even when larger amounts of hydrogen are consumed in the first reaction zone. Furthermore, at least a portion of the remainder or bottoms stream of the isomerization effluent separator may be recycled to the isomerization reaction zone to increase the degree of isomerization.

[0035] The remainder of the isomerization effluent after the removal of hydrogen still has liquid and gaseous components and is cooled, by techniques such as air cooling or water cooling and passed to a cold separator where the liquid component is separated from the gaseous component. Suitable operating conditions of the cold separator include, for example, a temperature of 20 to 60°C and a pressure of 3850 kPa absolute (560 psia). A water byproduct stream is also separated. At least a portion of the liquid component, after cooling and separating from the gaseous component, may be recycled back to the isomerization zone to increase the degree of isomerization. Prior to entering the cold separator, the remainder of the isomerization and selective hydrocracking zone effluent may be combined with the hot high pressure hydrogen stripper overhead stream, and the resulting combined stream may be introduced into the cold separator.

[0036] The liquid component contains the hydrocarbons useful as diesel fuel and aviation fuel, termed diesel fuel range hydrocarbons and aviation fuel range hydrocarbons, respectively, as well as smaller amounts of naphtha and LPG. The separated liquid component is further purified in a product fractionation zone which separates lower boiling components and dissolved gases into an LPG and naphtha stream; an aviation range product; and a diesel range product. Suitable operating conditions of the product distillation zone include a temperature of from 20 to 200°C at the overhead and a pressure from 0 to 1379 kPa absolute (0 to 200 psia). The conditions of the distillation zone may be adjusted to control the relative amounts of hydrocarbon contained in the aviation range product stream and the diesel range product stream.

[0037] The LPG and naphtha stream may be further separated in a debutanizer or depropanizer in order to separate the LPG into an overhead stream, leaving the naphtha in a bottoms stream. Suitable operating conditions of this unit include a temperature of from 20

to 200°C at the overhead and a pressure from 0 to 2758 kPa absolute (0 to 400 psia). The LPG may be sold as valuable product or may be used in other processes such as a feed to a hydrogen production facility. Similarly, the naphtha may be used in other processes, such as the feed to a hydrogen production facility.

5 [0038] In another embodiment, a single fraction column may be operated to provide four streams, with the hydrocarbons suitable for use in a diesel fuel removed from the bottom of the column, hydrocarbons suitable for use in an aviation fuel removed from a first side-cut, hydrocarbons in the naphtha range being removed in a second side-cut and the propane and light ends being removed in an overhead from the column. In yet another embodiment, a first
10 fractionation column may separate the hydrocarbons useful in diesel and aviation fuels into a bottoms stream, and propane, light ends, and naphtha into an overhead stream. A second fractionation column may be used to separate the hydrocarbons suitable for use in a diesel fuel into a bottoms stream of the column and hydrocarbons suitable for use in an aviation fuel into an overhead stream of the column, while a third fractionation column may be employed
15 to separate the naphtha range hydrocarbons from the propane and light ends. Also, dividing wall columns may be employed.

[0039] The operating conditions of the one or more fractionation columns may be used to control the amount of the hydrocarbons that are withdrawn in each of the streams as well as the composition of the hydrocarbon mixture withdrawn in each stream. Typical operating
20 variables well known in the distillation art include column temperature, column pressure (vacuum to above atmospheric), reflux ratio, and the like. The result of changing column variables, however, is only to adjust the vapor temperature at the top of the distillation column. Therefore the distillation variables are adjusted with respect to a particular feedstock in order to achieve a temperature cut point to give a product that meets desired properties.

25 Table 1 shows the effect on product properties from two hydrocarbon feeds by adjusting the final boiling temperature. The feeds A and B were processed from the same vegetable feedstock under identical hydrogenation and deoxygenation conditions but somewhat different isomerization and selective hydrocracking conditions. As a result feeds A and B differed in the iso/normal ratio and cloud point. Initial boiling point of the aviation fuel cut
30 remained constant (150°C). The examples in Table 1 clearly show that achieving the desired kerosene (jet fuel) product is a function not only of specific boiling range but also

isomerized/normal paraffin ratio. The required freeze point changes for a specific aviation fuel. For example, Freeze point specification for JP-8 jet fuel is -47°C . Therefore the desired operating parameters for the isomerization reactor and the distillation column must develop with respect to the specific product desired.

TABLE 1

Ex.	Feed	Aviation Cut End B.P. ($^{\circ}\text{C}$)	Aviation product (iso/normal)	Freeze Point ($^{\circ}\text{C}$)
1	A	285	n.a.	- 32
2	A	270	n.a	- 44
3	A	265	4.4	- 48
4	B	275	6.5	- 49

[0040] With the present invention, at least 10 wt.-% of aviation fuel or aviation fuel blending component can be recovered. The wt.-% of diesel fuel ranges from 10 to 80 wt.-%. Therefore, wide flexibility in the relative amounts of diesel range fuel and aviation range fuel is achieved. The balance of the product is the naphtha and the light ends. Higher amounts of aviation range fuel is produced by increasing the severity of the isomerization reactor. As the process severity increase, more hydrocracking occurs in the isomerization reaction zone, shifting a portion of the diesel fuel to aviation fuel and the lighter materials. The remaining diesel fraction will also have a higher degree of isomerization.

[0041] Table 2 shows the general effect of increasing process condition severity of the isomerization reactor on the amount of diesel fuel, aviation fuel, and light products produced. In the first case maximum diesel is produced and all hydrocarbons in the aviation fuel range remain in the diesel fuel fraction. The isomerization severity remains the same in the second case but now the aviation fuel is separated in a fractionation zone. Diesel fuel amount is decreased while 10 wt.-% to 20 wt.-% aviation fuel is removed. In case three the severity of the isomerization zone is increased and higher hydrocracking levels result in more aviation fuel and less diesel. Also, since the hydrocracking reaction is not totally selective the amount of light products also increase. The severity of the isomerization reactor can be increased through many approaches, including higher temperatures, lower space velocity, different pressure, different hydrogen concentrations, or any combination of these. The last case

results in maximum aviation fuel at the highest process severity. At such conditions little diesel fuel remains while the production of lights increase substantially.

TABLE 2

Case	Process Severity	Diesel Fuel (wt%)	Aviation Fuel (wt%)	Light materials (wt%)
#1 Maximum diesel fuel	Mild	70-80%	0%	20-30%
#2 Minimum production of lights with some aviation fuel production	Mild	60-70%	10-20%	20-30%
#3 Higher aviation fuel yields with diesel production	Elevated	40-50%	20-25%	25-40%
#4 Highest aviation fuel yields while minimizing lights	High	30-40%	30-35%	25-40%
#5 Maximum aviation fuel	Severe	<10%	40-45%	45-50%

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[0042] A portion of the product diesel-range hydrocarbon is recycled to the hydrogenating and deoxygenating reaction zone. The recycle stream may be taken from the product hydrocarbon stream after the hydrogenating and deoxygenating reactor(s) and separation of gaseous components, and recycled back to the hydrogenating and deoxygenating reactor(s). Or the recycle stream may be taken from the effluent of a separation unit, such as a hot high pressure separator, located between the deoxygenation reaction zone and the isomerization reaction zone. A portion of a hydrocarbon stream from, for example, a hot high pressure separator or a cold high pressure separator, may also be cooled down if necessary and used as cool quench liquid between the beds of the deoxygenation reaction zone to further control the heat of reaction and provide quench liquid for emergencies. The recycle stream may be introduced to the inlet of the deoxygenation reaction zone and/or to any subsequent beds or reactors. One benefit of the hydrocarbon recycle is to control the temperature rise across the individual beds. However, as discussed above, the amount of hydrocarbon recycle herein is determined based upon the desired hydrogen solubility in the reaction zone. Increasing the hydrogen solubility in the reaction mixture allows for successful operation at lower pressures, and thus reduced cost. Operating with high recycle and maintaining high levels of hydrogen in the liquid phase helps dissipate hot spots at the catalyst surface and reduces the formation of undesirable heavy components which lead to coking and catalyst deactivation.

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[0043] Optionally the process may employ a steam reforming zone in order to provide hydrogen to the hydrogenation/deoxygenation zone and isomerization zone. The steam

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reforming process is a well known chemical process for producing hydrogen, and is the most common method of producing hydrogen or hydrogen and carbon oxide mixtures. A hydrocarbon and steam mixture is catalytically reacted at high temperature to form hydrogen, and the carbon oxides: carbon monoxide and carbon dioxide. Since the reforming reaction is strongly endothermic, heat must be supplied to the reactant mixture, such as by heating the tubes in a furnace or reformer. A specific type of steam reforming is autothermal reforming, also called catalytic partial oxidation. This process differs from catalytic steam reforming in that the heat is supplied by the partial internal combustion of the feedstock with oxygen or air, and not supplied from an external source. In general, the amount of reforming achieved depends on the temperature of the gas leaving the catalyst; exit temperatures in the range of 700°C to 950°C are typical for conventional hydrocarbon reforming. Pressures may range up to 4000 kPa absolute. Steam reforming catalysts are well known and conventional catalysts are suitable for use in the present invention.

[0044] Typically, natural gas is the most predominate feedstock to a steam reforming process. However, in the present invention, hydrocarbons that are too light for the desired products may be generated at any of the reaction zones. For example, in the deoxygenation zone, propane is a common by product. Other C1 to C3 paraffins may be present as well. These lighter components may be separated from the desired portion of the deoxygenation effluent and routed to the steam reforming zone for the generation of hydrogen. Similarly, paraffins having eight or less carbon atoms from the effluent of the isomerization zone may be conducted to the reforming zone. Therefore, the lighter materials from the deoxygenation, isomerization and hydrocracking zones are directed, along with stream, to a reforming zone. In the reforming zone, the lighter hydrocarbons and steam are catalytically reacted to form hydrogen and carbon oxides. The steam reforming product may be recycled to any of the reaction zones to provide at least hydrogen to the reaction zone. Optionally, the hydrogen may be separated from the carbon oxides generated in the steam reforming reaction, and the separated hydrogen may be recycled to any of the reaction zones. Since hydrogen is an expensive resource, generating at least a portion of the required hydrogen from the undesired products of the reaction zones can decrease the cost of the process. This feature becomes more valuable when an external source of hydrogen is not readily available.

[0045] In an alternative embodiment, catalytic reforming may be employed instead of steam reforming. In a typical catalytic reforming zone, the reactions include dehydrogenation, dehydrocyclization, isomerization, and hydrocracking. The dehydrogenation reactions typically will be the dehydroisomerization of alkylcyclopentanes to alkylcyclohexanes, the
5 dehydrogenation of paraffins to olefins, the dehydrogenation of cyclohexanes to alkylcycloparaffins and the dehydrocyclization of acyclic paraffins and acyclic olefins to aromatics. The isomerization reactions included isomerization of n-paraffins to isoparaffins, the hydroisomerization of olefins to isoparaffins, and the isomerization of substituted aromatics. The hydrocracking reactions include the hydrocracking of paraffins. The aromatization of the n-
10 paraffins to aromatics is generally considered to be highly desirable because of the high octane rating of the resulting aromatic product. In this application, the hydrogen generated by the reactions is also a highly desired product, for it is recycled to at least the deoxygenation zone. The hydrogen generated is recycled to any of the reaction zones, the hydrogenation/deoxygenation zone, the isomerization zone, and or the selective hydrocracking
15 zone.

[0046] Turning to FIG. 1, the operator determines the specifications of the aviation component and the diesel component to be produced. The operator then determines the yield of each component to be produced while still meeting the desired specifications. With those parameters now set, the operator determines the operating conditions of the isomerization and
20 selective hydrogenation zone and the operating conditions of the fractionation zone to control the slate of hydrocarbons being produced and separated so that the specifications and yields are met. Then a renewable feedstock stream 2, which may pass through an optional feed surge drum, is combined with recycle gas stream 68 and recycle stream 16 to form combined feed stream 20, which is heat exchanged with reactor effluent and then introduced into
25 deoxygenation reactor 4. The heat exchange may occur before or after the recycle is combined with the feed. Deoxygenation reactor 4 may contain multiple beds shown as 4a, 4b and 4c. Deoxygenation reactor 4 contains at least one catalyst capable of catalyzing decarboxylation and/or hydrodeoxygenation of the feedstock to remove oxygen. Deoxygenation reactor effluent stream 6 containing the products of the decarboxylation and/or hydrodeoxygenation reactions is
30 removed from deoxygenation reactor 4 and heat exchanged with stream 20 containing feed to the deoxygenation reactor. Stream 6 comprises a liquid component containing largely normal

paraffin hydrocarbons in the diesel boiling range and a gaseous component containing largely hydrogen, vaporous water, carbon monoxide, carbon dioxide and propane.

[0047] Deoxygenation reactor effluent stream 6 is then directed to hot high pressure hydrogen stripper 8. Make up hydrogen in line 10 is divided into two portions, stream 10a and 10b. Make up hydrogen in stream 10a is also introduced to hot high pressure hydrogen stripper 8. In hot high pressure hydrogen stripper 8, the gaseous component of deoxygenation reactor effluent 6 is selectively stripped from the liquid component of deoxygenation reactor effluent 6 using make-up hydrogen 10a and recycle hydrogen 28. The dissolved gaseous component comprising hydrogen, vaporous water, carbon monoxide, carbon dioxide and at least a portion of the propane, is selectively separated into hot high pressure hydrogen stripper overhead stream 14. The remaining liquid component of deoxygenation reactor effluent 6 comprising primarily normal paraffins having a carbon number from 8 to 24 with a cetane number of 60 to 100 is removed as hot high pressure hydrogen stripper bottom 12.

[0048] A portion of hot high pressure hydrogen stripper bottoms forms recycle stream 16 and is combined with renewable feedstock stream 2 to create combined feed 20. Another portion of recycle stream 16, optional stream 16a, may be routed directly to deoxygenation reactor 4 and introduced at interstage locations such as between beds 4a and 4b and or between beds 4b and 4c in order, or example, to aid in temperature control. The remainder of hot high pressure hydrogen stripper bottoms in stream 12 is combined with hydrogen stream 10b to form combined stream 18 which is routed to isomerization and selective hydrocracking reactor 22. Stream 18 may be heat exchanged with isomerization reactor effluent 24.

[0049] The product of the isomerization and selective hydrocracker reactor containing a gaseous portion of hydrogen and propane and a branched-paraffin-enriched liquid portion is removed in line 24, and after optional heat exchange with stream 18, is introduced into hydrogen separator 26. The overhead stream 28 from hydrogen separator 26 contains primarily hydrogen which may be recycled back to hot high pressure hydrogen stripper 8. Bottom stream 30 from hydrogen separator 26 is air cooled using air cooler 32 and introduced into product separator 34. In product separator 34 the gaseous portion of the stream comprising hydrogen, carbon monoxide, hydrogen sulfide, carbon dioxide and propane are removed in stream 36 while the liquid hydrocarbon portion of the stream is removed in stream 38. A water byproduct stream 40 may also be removed from product separator 34. Stream 38 is introduced to product

stripper 42 where components having higher relative volatilities are separated into stream 44, components within the boiling range of aviation fuel is removed in stream 45, with the remainder, the diesel range components, being withdrawn from product stripper 42 in line 46. Stream 44 is introduced into fractionator 48 which operates to separate LPG into overhead 50 leaving a naphtha bottoms 52. Any of optional lines 72, 74, or 76 may be used to recycle at least a portion of the isomerization zone effluent back to the isomerization zone to increase the amount of n-paraffins that are isomerized to branched paraffins.

[0050] The vapor stream 36 from product separator 34 contains the gaseous portion of the isomerization effluent which comprises at least hydrogen, carbon monoxide, hydrogen sulfide, carbon dioxide and propane and is directed to a system of amine absorbers to separate carbon dioxide and hydrogen sulfide from the vapor stream. Because of the cost of hydrogen, it is desirable to recycle the hydrogen to deoxygenation reactor 4, but it is not desirable to circulate the carbon dioxide or an excess of sulfur containing components. In order to separate sulfur containing components and carbon dioxide from the hydrogen, vapor stream 36 is passed through a system of at least two amine absorbers, also called scrubbers, starting with the first amine absorber zone 56. The amine chosen to be employed in first amine scrubber 56 is capable of selectively removing at least both the components of interest, carbon dioxide and the sulfur components such as hydrogen sulfide. Suitable amines are available from DOW and from BASF, and in one embodiment the amines are a promoted or activated methyldiethanolamine (MDEA). See US 6,337,059, hereby incorporated by reference in its entirety. Suitable amines for the first amine absorber zone from DOW include the UCARSOLTM AP series solvents such as AP802, AP804, AP806, AP810 and AP814. The carbon dioxide and hydrogen sulfide are absorbed by the amine while the hydrogen passes through first amine scrubber zone and into line 68 to be recycled to the first reaction zone. The amine is regenerated and the carbon dioxide and hydrogen sulfide are released and removed in line 62. Within the first amine absorber zone, regenerated amine may be recycled for use again. The released carbon dioxide and hydrogen sulfide in line 62 are passed through second amine scrubber zone 58 which contains an amine selective to hydrogen sulfide, but not selective to carbon dioxide. Again, suitable amines are available from DOW and from BASF, and in one embodiment the amines are a promoted or activated MDEA. Suitable amines for the second amine absorber zone from DOW include the UCARSOLTM HS series solvents such as HS101, HS 102, HS103, HS104, HS115. Therefore

the carbon dioxide passes through second amine scrubber zone 58 and into line 66. The amine may be regenerated which releases the hydrogen sulfide into line 60. Regenerated amine is then reused, and the hydrogen sulfide may be recycled to the deoxygenation reaction zone.

Conditions for the first scrubber zone includes a temperature in the range of 30 to 60°C. The first absorber is operated at essentially the same pressure as the reaction zone. By

“essentially” it is meant that the operating pressure of the first absorber is within 1034 kPa absolute (150 psia) of the operating pressure of the reaction zone. For example, the pressure of the first absorber is no more than 1034 kPa absolute (150 psia) less than that of the reaction zone. The second amine absorber zone is operated in a pressure range of from 138 kPa absolute (20 psia) to 241 kPa absolute (35 psia). Also, at least the first the absorber is operated at a temperature that is at least 1°C higher than that of the separator. Keeping the absorbers warmer than the separator operates to maintain any light hydrocarbons in the vapor phase and prevents the light hydrocarbons from condensing into the absorber solvent.

[0051] The following examples are presented in illustration of this invention and are not intended as undue limitations on the generally broad scope of the invention as set out in the claims.

[0052] Refined, bleached, and deodorized (RBD) soybean oil was hydrogenated and deoxygenated in a pilot plant by flowing the oil down over a fixed-bed deoxygenation catalyst at 315°C, 3447 kPag (500 psig), a LHSV of 1.0 h⁻¹, and a H₂/HC of 711 std m³/m³ (4000 scf/bbl). A sulfur source was added to stabilize the catalyst. The side products of propane, CO_x, and water were separated from the paraffinic product which was composed almost entirely of C₁₅ to C₁₈ n-paraffins. The yield of this n-paraffin product was 83% in the deoxygenation reactor.

[0053] The paraffin product described above was isomerized and hydrocracked in a pilot plant by flowing the product over a fixed bed isomerization catalyst at various process conditions as shown in Table 3 below. In all cases the H₂/HC was 444 std m³/m³ (2500 scf/bbl). Table 3 shows only the amounts of products produced in the isomerization reactor, not the total amount after both deoxygenation and isomerization. In Case 1 no aviation fuel was removed in the fractionation zone and represents high yields of diesel fuel since all of the lighter components for aviation fuel are kept in the diesel product. Case 2 was conducted at the same process conditions as case 1 but aviation fuel was separated resulting in 13 wt.-%

aviation fuel with a corresponding decrease in the yield of diesel fuel to 71 wt.-%. For Case 3 the isomerization reactor was run at a higher bed temperature resulting in increased isomerization and higher amounts of hydrocracking. As noted above, the higher iso/normal ratios allows a broader temperature range for the aviation cut and the increasing the overall yield of aviation fuel. For Case 4 the isomerization zone process severity was decreased by raising the space velocity which resulted in lower yields of aviation fuel and higher yields of diesel fuel. Case 5 was run at higher temperatures and lower space velocity than Case 4 resulting in a significant increase in the amount of yield of aviation fuel, substantially less yield of diesel fuel, and higher isomerization levels for each fuel. In the final case aviation fuel is maximized to 43% with only 5% diesel remaining though a combination of higher temperature, lower space velocity and higher pressure than case 1. The production of lights increased to >50% and the isomerization level of both fuels was very high.

TABLE 3

Process Example	Temperature C	Pressure kPa-gauge (psig)	LHSV (h-1)	Diesel wt% (i/n)	Aviation (wt%) (i/n)	Lights (wt%)
Case 1	345	4137 (600)	1	87% (4.0)	0%	13%
Case 2	345	4137 (600)	1	71% (2.9)	13% (4.4)	16%
Case 3	355	4137 (600)	1	55% (4.3)	22% (6.5)	23%
Case 4	352	3447 (500)	1.7	62% (2.3)	15% (2.3)	23%
Case 5	362	3447 (500)	1.6	29% (7.7)	26% (5.2)	45%
Case 6	355	4826 (700)	0.7	5% (15)	43% (10)	52%

[0054] Turning to FIG.2, a schematic is presented to illustrate possible control actions which may be taken in the operation of process. As used herein “EBP” means end-boiling-point and “IBP” means initial-boiling-point. Table 4 shows sample relationships between the possible control actions in FIG. 2 and the possible impact on the products. In FIG. 2, the process 200 results in the two desired products, diesel fuel 204 and aviation fuel 206. An operator, upon observing and possibly testing the diesel fuel 204 would determine whether

the diesel yield met the target, question 210. If the answer to question 210 was no, control may be exercised over the operating parameters of process 200 to result in a change to diesel fuel 204. In this case, one option is to lower the end boiling point cut of the aviation fuel from the fractionation zone. If the diesel yield target is now met in question 210, an operator would
5 proceed to ask whether the diesel cloud point specification has been met, question 240. If the answer is yes, the diesel product may be ready for sale. If the answer to question 240 is no, additional controls and adjustments may be exercised such as increasing the severity of the isomerization reaction or lowering the end boiling point cut of the of the aviation fuel from the fractionation zone, so that the cloud point specification of the diesel product is met.

10 **[0055]** Similarly, an operator, upon observing and possibly testing the aviation or jet fuel 206 would determine whether the aviation or jet fuel yield met the target, question 220. If the answer to question 220 was no, control may be exercised over the operating parameters of process 200 to result in a change to diesel fuel 204. In this case, one option is to increase the severity of the operating conditions of the isomerization reaction. If the aviation or jet fuel
15 yield target is now met in question 220, an operator would proceed to ask whether the aviation or jet fuel freeze point specification has been met, question 260. If the answer to question 240 is no, additional controls and adjustments may be exercised such as increasing the severity of the isomerization reaction or lowering the end boiling point cut of the aviation fuel from the fractionation zone, so that the freeze point specification of the aviation or jet
20 fuel product is met. Once the freeze point specification of the aviation or jet fuel is met, an operator would evaluate whether the flash point specification has been met, question 280. If the answer is yes, the aviation or jet product may be ready for sale. If the answer is no, one control option is to increase the initial boiling point of the aviation or jet cut from the fractionation zone, so that the flash point specification of the aviation or jet fuel product is
25 met.

TABLE 4

TYPE OF CONTROL (as shown on FIG. 2)	IMPACT
A	Higher Diesel Yields Lower jet Yields Lower Diesel Cloud Point
B	Higher Iso/Normal Ratio More Hydrocracking Lower Diesel Cloud Point Lower Jet Freeze Point Higher yield of Lights and Naphtha Impact on Jet Yield is variable
C	Higher Iso/Normal Ratio More Hydrocracking Lower Diesel Cloud Point Lower Jet Freeze Point Higher yield of Lights and Naphtha Lower Diesel Yield Higher Jet Yield.
D	Lower Jet Yield Higher Yield of Lights and Naphtha

FIG 2. and Table 4 merely illustrate one embodiment of the invention, and are not meant to limit the scope of the invention in any way. Other questions may be asked and other control actions may be employed; all within the scope of the invention.

CLAIMS:

1. A process for controlling the production of a diesel component comprising hydrocarbons having boiling points in the diesel fuel range and an aviation component comprising hydrocarbons having boiling points in the aviation fuel range from a renewable
5 feedstock comprising:

identifying specifications required for the diesel component and for the aviation component;

determining yields required for the diesel component and for the aviation component and that meet required specifications;

10 determining isomerization and selective cracking conditions required in an isomerization and selective hydrocracking zone that result in the predetermined yields required for the diesel component and for the aviation component wherein the diesel component and the aviation component further meet the identified specifications;

determining operating conditions for a fractionation zone that results in the separation
15 of the diesel component and the aviation component at the required yields;

hydrogenating and deoxygenating the renewable feedstock by contacting the feedstock in a hydrogenation and deoxygenation zone with a hydrogenation and deoxygenation catalyst at hydrogenation and deoxygenation conditions to provide a hydrogenation and deoxygenation zone effluent comprising n-paraffins;

20 isomerizing and selectively hydrocracking at least a portion of the n-paraffins in the hydrogenation and deoxygenation zone effluent by contacting with an isomerization and selective hydrocracking catalyst at the predetermined isomerization conditions in an isomerization and selective hydrocracking zone to generate branched-paraffins in an isomerization and selective hydrocracking zone effluent; and

25 fractionating, in the fractionation zone, the isomerization and selective hydrocracking zone effluent the predetermined operating conditions of the fractionation zone to provide a first product stream comprising the diesel component, and a second product stream comprising the aviation component.

2. The process of Claim 1 further comprising periodically repeating the process.

30 3. The process of Claim 1 wherein the specifications are those identified in industry standard, government, or military fuel standard requirements.

4. The process of Claim 1 wherein the yield required for the diesel component is from 30 wt.-% to 70 wt.-% and the yield required for the aviation component is from 10 wt.-% to 35 wt.-%.

5. The process of Claim 1 wherein the renewable feedstock comprises at least one component selected from the group consisting of fatty acid alkyl esters, canola oil, corn oil, soy oils, rapeseed oil, soybean oil, colza oil, tall oil, sunflower oil, hempseed oil, olive oil, linseed oil, coconut oil, castor oil, peanut oil, palm oil, mustard oil, cottonseed oil, tallow, yellow and brown greases, lard, train oil, fats in milk, fish oil, algal oil, sewage sludge, cuphea oil, camelina oil, jatropha oil, curcas oil, babassu oil, palm oil, crambe oil, and kernel oil.

6. The process of Claim 1 further comprising recycling a portion of the hydrogenation and deoxygenation zone effluent to the hydrogenation and deoxygenation zone wherein the hydrocarbon volume ratio recycle to feedstock is in the range of 2:1 to 8:1.

7. The process of Claim 1 further comprising co-feeding or mixing with the renewable feedstock, a component selected from the group consisting of a petroleum hydrocarbon feedstock, liquids derived from gasification of coal or natural gas followed by a downstream liquefaction; liquids derived from depolymerization, thermal or chemical, of waste plastics; and other synthetic oils generated as byproducts from petrochemical and chemical processes.

8. The process of Claim 1 wherein the hydrogenating and deoxygenating further generates at least propane which is separated from the hydrogenation and deoxygenation zone effluent and conducted to a steam reforming zone to produce at least hydrogen, and said hydrogen being recycled to at least the hydrogenation and deoxygenation zone.

9. The process of Claim 1 wherein the selective hydrocracking further provides hydrocarbons having 8 or less carbon atoms which are separated from hydrocarbons having 9 or more carbon atoms, the hydrocarbons having 8 or less carbon atoms being conducted to a steam reforming zone to produce at least hydrogen, said hydrogen being recycled to at least the hydrogenating and deoxygenating zone.

10. A diesel fuel or diesel fuel blending component and an aviation fuel or aviation fuel blending component as produced by the process of Claim 1.