

Description

The invention relates to a power supply circuit for supplying a load from input voltages of different magnitude, comprising a first series arrangement formed by a primary winding of a transformer and a main current path of a first semiconductor switch; a second series arrangement formed by a secondary winding of the transformer and a rectifier diode, this second series arrangement having terminals for connecting the load; a second transistor switch for switching the first semiconductor switch; and means for generating a signal which is a measure of the current through the primary winding.

Such a circuit can, for example, be used for charging a rechargeable battery or for supplying an electronic apparatus, it being possible to connect the apparatus without switching to voltage sources of different magnitude, for example to the electric power mains in different countries. Such a power supply circuit can more specifically be used in a rechargeable electric shaver in which the circuit produces the current for charging the battery or for supplying the motor.

A power supply circuit of the type referred to in the opening paragraph is disclosed in EP-B1-0030026. Said European Patent describes a power supply circuit in which, during the, so called, forward phase a current which flows through the primary winding, increases linearly with time and which current causes energy to be stored in the transformer. In the emitter line of a first transistor which constitutes the first semiconductor switch, a resistor is included across which a voltage is produced which is proportional to the primary current. The base-emitter junction of a second transistor is arranged in parallel with this resistor. This transistor constitutes the second semiconductor switch. The resistor constitutes said means for generating the signal which is a measure of the primary current. At a given value of the primary current the second transistor becomes conductive and consequently the first transistor is rendered non-conducting. This terminates the forward phase and the, so called, flyback phase starts. Because of the energy stored in the transformer a secondary current flows in the secondary winding during the flyback-phase. This current forms the charging current for the batteries or directly the supply current for the relevant apparatus. The secondary current decreases linearly with time. At the end of the flyback phase the first transistor is turned-on again, and another forward phase begins.

In the prior-art supply circuit a signal which linearly increases with time is applied during the forward phase to the control input of the second semiconductor switch. Due to this signal, the second semiconductor switch is driven relatively slowly in the conducting state. This implies that the instant at which the second

semiconductor switch becomes conductive and consequently the first semiconductor switch is rendered non-conducting is not accurately defined, so that also the turn-off value of the primary current is not accurately defined.

The invention has for its object to provide a power supply circuit in which the second semiconductor switch is turned-on rapidly.

Therefore, according to the invention, the power supply circuit is characterized in that an output of said means for generating a signal which is a measure of the current through the primary winding is connected to a first non-inverting input of a comparator, a second inverting input of which is connected to an output of means for fixing a reference voltage and an output of which is connected to a control input of the second transistor switch, and that the inverting input of the comparator is coupled via a capacitor to an output of the second transistor switch.

Not until the signal which is a measure of the primary current has reached a level determined by the reference voltage the comparator supplies a control signal by means of which the semiconductor switch is turned-on and consequently the first semiconductor switch is rendered conductive. Consequently, no signal is applied to the control input before the primary current has reached said level. Because a positive feedback circuit is established between the output of the second semiconductor switch and its control input, via the capacitor and the comparator, the second semiconductor switch becomes rapidly conductive and consequently the first semiconductor switch is rapidly rendered non-conducting. The turn-off value of the primary current is accurately determined thereby.

A fast turn-off of the first semiconductor switch has the advantage that this reduces the dissipation of energy in this switch to a considerable extent. Particularly for a compact apparatus, such as, for example, a shaver this is a considerable advantage as it reduces the necessity of cooling means.

An embodiment of the power supply circuit according to the invention in which the first semiconductor and second transistor switches are constituted by first and second transistors, is characterized in that the comparator is formed by a third transistor of a conductivity type opposite to that of the first and second transistors and whose base constitutes the inverting and the emitter the non-inverting input and the collector constitutes the output. Such a transistor is suitable for use as a comparator and is cheap.

Preferably, the power supply circuit according to the invention is characterized in that the means for fixing a reference voltage have a control input for receiving a signal which is a measure of the input voltage and that these means are arranged for supplying a reference voltage which is lower according as the input voltage is higher. Since the reference voltage sup-

plied depends in the manner described on the input voltage of the power supply circuit, the average intensity of the output current is kept constant within given tolerances at an appropriate choice of this voltage dependence.

A further embodiment of the power supply circuit according to the invention, is characterized in that the means for fixing a reference voltage are constituted by a circuit formed by a fourth transistor whose base-emitter junction is arranged in parallel with a first resistor, whose base-collector junction is arranged in parallel with a second resistor, the junction point of the collector of the fourth transistor with the second resistor constituting an output of the means for fixing a reference voltage, and the junction point between the base of the fourth transistor and the first and second resistors constituting a control input for receiving a control signal. The magnitude of the reference voltage thus generated is provided by the magnitude of the control voltage applied to the base of the fourth transistor. It should be noted that in EP-A-0188839 a power supply circuit is disclosed of this type in which the control input of the second semiconductor switch is coupled to means for generating a signal which is a measure of the current through the primary winding via what is commonly denoted to as a V_{BE} -multiplier. However, also in this known circuit the second semiconductor switch is driven only slowly in the conductive state, so that also in this circuit the turn-off value of the primary current is not accurately determined.

Another further embodiment of the power supply circuit according to the invention is characterized in that the means for fixing a reference voltage comprise a current mirror circuit having a primary and secondary branch, the current-mirror circuit being arranged such that the current flowing through each of the two branches is substantially proportional to the input voltage. By feeding the secondary branch from a constant supply voltage and by incorporating in the secondary branch a resistor across which a voltage is generated which is proportional to the input voltage, the reference voltage source produces a reference voltage which decreases linearly with an increasing input voltage.

The power supply circuit according to the invention, is preferably characterized in that the second series arrangement of the secondary winding and the rectifier diode provided with terminals for connection of the load is arranged in series with the main current path of the first semiconductor switch. In this preferred embodiment the load, which is arranged in parallel with the secondary winding, is not only supplied from the transformer during the flyback phase, but also directly during the forward phase by the primary current from the applied input voltage. The power supply circuit according to the invention may be further characterized in that the means for generating a signal which is a measure of the current through the

primary winding are arranged between the first semiconductor switch and the second series arrangement. In this situation the termination of the forward phase also depends on the storage battery voltage, so that the charging current of the storage battery decreases at higher battery voltage levels.

A power supply circuit according to the invention is eminently suitable for integration, at least partly, in an integrated circuit. An integrated circuit for use in a power supply circuit according to the invention preferably comprises the second semiconductor switch, the comparator and the reference voltage source.

The invention will now be described by way of example, in greater detail with reference to the accompanying drawing, in which

Fig. 1 is a first circuit diagram of the power supply circuit according to the invention,

Fig. 2 is a second circuit diagram, in which the load is arranged in series with the main current path of the first semiconductor switch,

Fig. 3 shows a first embodiment of a power supply circuit according to the invention, and

Fig. 4 shows a second embodiment of a power supply circuit according to the invention.

Fig. 1 shows the circuit diagram of a self-oscillating power supply circuit according to the invention.

The primary winding N_1 of a transformer TR, the main current path of a transistor T_1 and a current measuring resistor R_1 are arranged in series between the positive input terminal 1 and the negative input terminal 2. This first transistor T_1 constitutes the first semiconductor switch. The base of the first transistor is coupled to the negative input terminal 2 via the main current path of the second transistor T_2 which constitutes the second semiconductor switch. The base of the second transistor T_2 is connected to the output of a comparator CP an inverting input 5 of which is connected to the output of means for fixing a reference voltage, for example a reference voltage source RS and a second, non-inverting, input 6 is connected to that terminal of the current measuring resistor R_1 that faces the first transistor. The base of the first transistor T_1 is further coupled to the positive input terminal 1 via a starter resistor R_2 . The secondary winding N_2 of the transformer TR is arranged in series with a rectifier diode D_1 between two terminals 3 and 4. A load L which, for example, is formed by a series arrangement of two rechargeable batteries A_1 and A_2 with which a motor M can be arranged in parallel via a switch S is connected to the two terminals 3 and 4. The junction point 7 of the secondary winding N_2 and the rectifier diode D_1 is coupled to the base of the first transistor T_1 via a positive feedback circuit formed by a series arrangement of a resistor R_3 and a capacitor C_1 . The collector of the second transistor T_2 , and consequently the base of the first transistor T_1 , is coupled via the capacitor C_2 to the inverting in-

put 5 of the comparator CP. Finally, an input 8 of the reference voltage source is connected to the positive input terminal 1 via the resistor R_4 .

At a constant value of the input voltage the circuit operates as follows. After the application of an input voltage, a d.c. voltage or a rectified a.c. voltage to the input terminals 1 and 2 a small current starts flowing through the starter resistor R_2 into the base of the first transistor T_1 . This transistor is partly rendered conductive thereby, so that a small primary current starts flowing through the primary winding N_1 of the transformer TR. This primary current induces a voltage across the secondary winding N_2 , which induced voltage generates a current in the positive feedback circuit formed by the resistor R_3 and the capacitor C_1 , which current is fed to the base of the transistor T_1 causing this transistor to become conductive to an increased extent. Via the positive feedback circuit the first transistor is thus driven rapidly to the fully conductive state, whereafter a primary current which linearly increases with time flows through the primary winding N_1 . Together with the primary current a voltage, which also increases linearly with time, is produced across the current measuring resistor R_1 . This voltage is applied to the non-inverting input 6 of the comparator CP. A reference voltage which is obtained from the reference voltage source RS is applied to the inverting input 5 of the comparator. As soon as the voltage across the current measuring resistor R_1 has reached a level determined by the reference voltage, the comparator changes state and a signal becomes available at the output of the comparator CP in response to which the second transistor T_2 is rendered conductive. This causes the voltage at the base of the first transistor T_1 to be decreased, so that this transistor is cut-off and the primary current stops flowing. This phase of a cycle is called the forward phase.

Since the collector of the second transistor T_2 is coupled via the capacitor C_2 to the inverting input of the comparator the voltage drop across this collector is conveyed to the input of the comparator. This causes the voltage difference between the two inputs of the comparator to increase and consequently the control current for the base of the second transistor T_2 supplied by the comparator. As a result thereof the second transistor becomes increasingly conductive which causes the voltage at its collector to decrease still further. Consequently, because of the positive feedback due to the capacitor C_2 , the second transistor T_2 is very rapidly rendered conductive, as a result of which the first transistor T_1 is also driven very rapidly out of its conducting state. The value of the primary current at which the forward phase is terminated is consequently determined very accurately.

During the forward phase the rectifier diode D_1 is in the non-conducting state. After the primary current has ended, the polarity of the voltage across the secondary winding N_2 changes state, so that the rectifier

diode becomes conductive. The energy stored in the transformer is thereafter transferred in the form of a current to the load L, for example for charging the batteries A_1 and A_2 . During this phase, denoted the fly-back phase, the current decreases linearly to zero, whereafter the transistor T_1 is switched on again via the positive feedback circuit formed by N_3 and C_1 and a subsequent forward phase starts.

At a different, higher value of the input voltage the primary current increases during the forward phase to a different, faster, extent. Since the average output current at a fixed load is determined by the period of the cycle and the energy level of the transformer, the average output current through the load increases, at a high input voltage, because of the increasing frequency. This effect, an input voltage-dependent output current, is not wanted. To suppress this voltage dependence a voltage which is proportional to the input voltage is applied to an input 8 of the reference voltage source via a resistor R_4 . The reference voltage source RS is arranged such that the reference voltage supplied is lower according as the voltage at the input 8 is higher. In response to the lower reference voltage the primary current reaches the level at which the first transistor T_1 is turned-off via the second transistor T_2 at an earlier instant. Consequently, the forward phase is shortened, so that the average output current remains the same in spite of the higher input voltage across the terminals 1 and 2.

It should be noted that the signal applied to the reference voltage source, which is a measure of the magnitude of the input voltage can be obtained in a different manner, for example from the junction point 7 of the secondary winding N_2 and the rectifier diode D_1 , or can be generated with the aid of additional elements, for example an auxiliary coil. During the forward phase the voltage across the point 7 is proportional to the input voltage via the turns ratio.

Fig. 2 is a second circuit diagram of the power supply circuit according to the invention, in which however the load L is arranged in series with the main current path of the first semiconductor switch T_1 . This circuit diagram comprises the same elements as the circuit diagram of Fig. 1. These elements are given the same reference numerals.

The mode of operation of this circuit is substantially equal to the mode of operation of the circuit described in the foregoing. After the first transistor T_1 has been rendered conductive via the starter resistor R_2 and the positive feedback circuit formed by the resistor R_3 and the capacitor C_1 , the primary current whose intensity increases linearly does not only flow through the primary winding N_1 of the transformer TR, the main current path of the transistor T_1 and the current measuring resistor R_1 , but also through the load L. The load is consequently also fed during the forward phase. In all further aspects the operation of the circuit described in the foregoing is identical to that of

the circuit and will therefore not be described in greater detail.

Fig. 3 shows an embodiment of a circuit according to the invention. In this circuit the elements corresponding to the preceding circuit diagrams are given the same reference numerals.

The power supply circuit is connected to the mains voltage via the rectifier bridge G and the smoothing filter comprising the coil L_1 and the capacitors C_3 and C_4 . One of the input lines of the rectifier bridge G incorporates the resistor F which acts as a fuse and limits the interrupts the switch-on and transient currents in the case of excessive mains currents.

Similar to what has been described in the foregoing, this embodiment is based on a first series arrangement of the primary winding N_1 of the transformer TR, the first semiconductor switch T_1 and the current measuring resistor R_1 and a second series arrangement of the secondary winding N_2 of the transformer and the rectifier diode D_1 which is arranged in parallel with the load L. The load L is arranged in series with the first series arrangement between the current measuring resistor and the negative input terminal 2 of the power supply circuit. A snubber circuit formed by the Zener diode D_2 and diode D_3 is arranged parallel to the primary winding N_1 to suppress voltage peaks on switch-off of the current through the primary winding of the transformer. The starter resistor R_2 is not directly connected to the positive input terminal but is arranged in parallel with the collector-base junction of the first transistor T_1 used as the first semiconductor switch.

In contradistinction to the preceding circuit diagrams, the positive feedback circuit between the junction point 7 of the secondary winding N_2 with the rectified diode D_1 and the base of the transistor T_1 is assembled from a series arrangement of two resistors R_3 and R_5 with interposed capacitor C_1 . A Zener diode D_4 whose anode faces the emitter of the transistor is provided between the junction point of the resistor R_5 with the capacitor C_1 and the emitter of the first transistor T_1 . The Zener diode D_4 limits the maximum voltage which can be applied to the base of the first transistor T_1 . As a result thereof the transistor T_1 cannot be saturated too much so that the delay which occurs at the turn-off of the first transistor T_1 after the second transistor T_2 has been rendered conductive is limited. The effect of the Zener diode D_4 is independent of the input voltage.

The second semiconductor switch transistor T_2 , for switching the first transistor T_1 , is driven from the comparator CP. This comparator is constituted by the PNP-transistor T_4 whose emitter is the non-inverting input 6 and whose base is the inverting input 5. At the beginning of the forward phase the PNP-transistor T_4 is non-conducting. During the forward phase the voltage at the non-inverting input 6, the emitter of the

transistor, increases linearly until the difference between this voltage and the voltage, determined by the reference voltage source, at the inverting input 5, the base of the transistor, has become that large that the PNP-transistor T_4 starts conducting a signal which is applied to the base of the second transistor T_2 , then becomes available at the collector of the PNP-transistor, the output of the comparator. Because of the non-linear characteristic of the PNP-transistor T_4 the signal applied to the base of the transistor T_2 increases rapidly. This causes this transistor to become conductive as a result of which the first transistor T_1 is cut-off and the forward phase is terminated.

A second capacitor C_2 is provided between the base of the PNP-transistor T_4 and the base of the first transistor T_1 .

When, after the PNP-transistor T_4 has become slightly conductive also the second transistor T_2 is rendered conductive to some extent, the voltage at the collector of the second transistor decreases. This decrease in voltage is conveyed to the base of the PNP-transistor T_4 via the capacitor C_2 . As a result thereof the base-emitter voltage of T_4 increases, so that this PNP-transistor is rendered conductive to a greater extent. In its turn the transistor T_4 now renders the second transistor T_2 more conductive. Thus the second transistor T_2 is rapidly rendered conductive, causing the first transistor T_1 to be rapidly cut-off.

The means R_8 for fixing a reference voltage are based on a transistor T_3 . A first resistor R_8 is arranged parallel to the base-emitter junction of this transistor and a second resistor R_9 is arranged parallel to the base-collector junction. The emitter of the transistor T_3 is connected to that end of the first transistor T_1 that is remote from the current measuring resistor R_1 . The output of R_8 is constituted by the junction point of the collector of the transistor T_3 and the second resistor R_9 . This junction point is connected to the base of the PNP-transistor T_4 .

The means R_8 operate as follows. During the beginning of the forward phase the transistor T_3 is non-conducting. The output is connected to a voltage which is equal to the voltage across that end of the current measuring resistor R_1 that faces the first transistor, which voltage has been transferred via the comparator. Consequently, a voltage equal to the voltage across the resistor R_1 is present across the means R_8 . When the primary current increases, the voltage across the first resistor R_8 will increase proportionally thereto and consequently also the base-emitter voltage of the transistor T_3 until the transistor T_3 starts conducting. A further increase of the voltage across the resistor R_1 is then accompanied by an increasing current through the transistor T_3 , the voltage remaining the same. The voltage at the input of the comparator consequently does not increase any further, so that a constant reference voltage has been

obtained during the remaining portion of the forward phase. The forward phase is ended as soon as the voltage difference between the inputs 5 and 6 of the comparator has increased to such a high value that the PNP-transistor T_4 starts conducting. The primary current then stops. The voltage across the resistor R_1 disappears, in responses to which also the voltage across the means R_8 and across the resistor R_1 decreases to zero. The transistor T_3 then changes again to the cut-off state.

The above description is based on the situation in which there is a connection between the junction point of the base of the transistor T_4 and the first and second resistors R_8 and R_9 and an external voltage source. However, in the presence of an external voltage source applying voltage to this junction point, a bias voltage will be applied across a first resistor R_8 , and consequently across the base-emitter junction of T_3 , which causes the transistor T_3 to start conducting at a lower voltage across the current measuring resistor R_1 . The maximum voltage at the output of the means R_8 is consequently also lower and the forward phase is terminated at a lower value of the primary current.

In the embodiment shown in Fig. 3 the external voltage is supplied by the secondary winding N_2 of the transformer. Via the turns ratio this secondary voltage which is proportional to the input voltage connected to the power supply circuit so that the external voltage applied to the reference voltage source is higher according as the input voltage increases. The bias voltage across the resistor R_8 is influenced by the voltage divider formed by the first resistor R_8 and the current-limiting resistor R_4 .

Fig. 4 shows a second embodiment of a power supply circuit according to the invention. In this circuit the reference voltage source is constituted by a current mirror circuit. In all further respects the circuit is equal to the circuit described in the foregoing, the elements are given the same reference numerals and are not described in greater detail here.

In this embodiment the means for fixing a reference voltage are constituted by a reference voltage source RS which is assembled from two series arrangements between the two input terminals 1 and 2 of the power supply circuit. One series arrangement is formed by a resistor R_{10} in series with the collector-emitter path of a fifth transistor T_5 . The base and the collector of the transistor T_5 are interconnected so that the transistor is arranged as a diode. The second series arrangement comprises two resistors R_{11} and R_{12} arranged in series with the collector-emitter path of a sixth transistor T_6 . A Zener diode D_5 whose anode is connected to the junction point of the two resistors R_{11} and R_{12} and whose cathode is connected to the emitter of transistor T_6 is arranged in parallel with the resistor R_{12} and the main current path of transistor T_6 . The base of transistor T_6 is connected to the base of

transistor T_5 .

When a voltage is applied across the input terminals 1 and 2 a current starts flowing through the primary branch, formed by the resistor R_{10} and the transistor T_5 . A base-emitter voltage V_{BE} will then be produced across the base-emitter junction of the fifth transistor T_5 , in correspondence with the current intensity. Consequently the same base-emitter voltage V_{BE} is present across the base-emitter junction of the sixth transistor T_6 so that in this, secondary, branch of the current mirror a current will flow of the same intensity as that in the primary branch. Because of the Zener diode D_5 the junction point of the two resistors R_{11} and R_{12} carried a constant voltage equal to the break-down voltage of the Zener diode. The voltage at the junction point of the resistor R_{12} with the collector of the sixth transistor T_6 is consequently equal to the difference between the Zener voltage and the voltage across the resistor R_{12} . In view of the action of the current mirror this voltage is equal to the product of the resistance value of R_{12} and the current through the primary branch of the current mirror. Since the current through the primary branch is proportional to the input voltage across the terminals 1 and 2 the voltage at the collector of the sixth transistor T_6 is lower according as the value of input voltage is higher. The voltage at the collector of the transistor T_6 is applied as a reference voltage to the inverting input 5 of the comparator CP.

Finally it should be noted that the means for fixing a reference voltage as described in the foregoing and shown in the Figures have an output voltage which linearly depends on the input voltage of the power supply circuit. It is of course possible to use means which have a non-linear dependence. In that situation it is possible to adapt the input voltage-output current characteristic to a desired behaviour. Moreover, the invention is not limited to a specific comparator. In addition to the comparator described a different comparator known to a person skilled in the art can alternatively be used, for example a push-pull amplifier.

Claims

1. A power supply circuit for supplying a load (L) from input voltages of different magnitude, comprising a first series arrangement formed by a primary winding (N_1) of a transformer (TR) and a main current path of a first semiconductor switch (T_1); a second series arrangement formed by a secondary winding (N_2) of the transformer and a rectifier diode (D_1), this second series arrangement having terminals (3, 4) for connecting the load (L); a second transistor switch (T_2) for switching the first semiconductor switch; and means (R_1) for generating a signal which is a measure of the current flowing through the pri-



obtained during the remaining portion of the forward phase. The forward phase is ended as soon as the voltage difference between the inputs 5 and 6 of the comparator has increased to such a high value that the PNP-transistor T_4 starts conducting. The primary current then stops. The voltage across the resistor R_1 disappears, in responses to which also the voltage across the means R_s and across the resistor R_1 decreases to zero. The transistor T_3 then changes again to the cut-off state.

The above description is based on the situation in which there is a connection between the junction point of the base of the transistor T_4 and the first and second resistors R_8 and R_9 and an external voltage source. However, in the presence of an external voltage source applying voltage to this junction point, a bias voltage will be applied across a first resistor R_8 , and consequently across the base-emitter junction of T_3 , which causes the transistor T_3 to start conducting at a lower voltage across the current measuring resistor R_1 . The maximum voltage at the output of the means R_s is consequently also lower and the forward phase is terminated at a lower value of the primary current.

In the embodiment shown in Fig. 3 the external voltage is supplied by the secondary winding N_2 of the transformer. Via the turns ratio this secondary voltage which is proportional to the input voltage connected to the power supply circuit so that the external voltage applied to the reference voltage source is higher according as the input voltage increases. The bias voltage across the resistor R_8 is influenced by the voltage divider formed by the first resistor R_8 and the current-limiting resistor R_4 .

Fig. 4 shows a second embodiment of a power supply circuit according to the invention. In this circuit the reference voltage source is constituted by a current mirror circuit. In all further respects the circuit is equal to the circuit described in the foregoing, the elements are given the same reference numerals and are not described in greater detail here.

In this embodiment the means for fixing a reference voltage are constituted by a reference voltage source RS which is assembled from two series arrangements between the two input terminals 1 and 2 of the power supply circuit. One series arrangement is formed by a resistor R_{10} in series with the collector-emitter path of a fifth transistor T_5 . The base and the collector of the transistor T_5 are interconnected so that the transistor is arranged as a diode. The second series arrangement comprises two resistors R_{11} and R_{12} arranged in series with the collector-emitter path of a sixth transistor T_6 . A Zener diode D_5 whose anode is connected to the junction point of the two resistors R_{11} and R_{12} and whose cathode is connected to the emitter of transistor T_6 is arranged in parallel with the resistor R_{12} and the main current path of transistor T_6 . The base of transistor T_6 is connected to the base of

transistor T_5 .

When a voltage is applied across the input terminals 1 and 2 a current starts flowing through the primary branch, formed by the resistor R_{10} and the transistor T_5 . A base-emitter voltage V_{BE} will then be produced across the base-emitter junction of the fifth transistor T_5 , in correspondence with the current intensity. Consequently the same base-emitter voltage V_{BE} is present across the base-emitter junction of the sixth transistor T_6 so that in this, secondary, branch of the current mirror a current will flow of the same intensity as that in the primary branch. Because of the Zener diode D_5 the junction point of the two resistors R_{11} and R_{12} carries a constant voltage equal to the break-down voltage of the Zener diode. The voltage at the junction point of the resistor R_{12} with the collector of the sixth transistor T_6 is consequently equal to the difference between the Zener voltage and the voltage across the resistor R_{12} . In view of the action of the current mirror this voltage is equal to the product of the resistance value of R_{12} and the current through the primary branch of the current mirror. Since the current through the primary branch is proportional to the input voltage across the terminals 1 and 2 the voltage at the collector of the sixth transistor T_6 is lower according as the value of input voltage is higher. The voltage at the collector of the transistor T_6 is applied as a reference voltage to the inverting input 5 of the comparator CP.

Finally it should be noted that the means for fixing a reference voltage as described in the foregoing and shown in the Figures have an output voltage which linearly depends on the input voltage of the power supply circuit. It is of course possible to use means which have a non-linear dependence. In that situation it is possible to adapt the input voltage-output current characteristic to a desired behaviour. Moreover, the invention is not limited to a specific comparator. In addition to the comparator described a different comparator known to a person skilled in the art can alternatively be used, for example a push-pull amplifier.

Claims

1. A power supply circuit for supplying a load (L) from input voltages of different magnitude, comprising a first series arrangement formed by a primary winding (N_1) of a transformer (TR) and a main current path of a first semiconductor switch (T_1); a second series arrangement formed by a secondary winding (N_2) of the transformer and a rectifier diode (D_1), this second series arrangement having terminals (3, 4) for connecting the load (L); a second transistor switch (T_2) for switching the first semiconductor switch; and means (R_1) for generating a signal which is a measure of the current flowing through the pri-



- mary winding, characterized in that the output of said means (R_1) is connected to a first non-inverting input (6) of a comparator (CP) a second inverting input (5) of which is connected to an output of means for fixing a reference voltage (RS) and an output of which is connected to a control input of the second transistor switch (T_2), and that the inverting input of the comparator (CP) is coupled via a capacitor to an output of the second transistor switch (T_2).
2. A power supply circuit as claimed in Claim 1, the first semiconductor and second transistor switches being constituted by first and second transistors, characterized in that the comparator (CP) is constituted by a third transistor (T_4) of a conductivity type opposite to that of the first and second transistors (T_1 , T_2) and whose base constitutes the inverting input (5) and the emitter constitutes the non-inverting input (6) and the collector forms the output.
 3. A power supply circuit as claimed in Claim 1 or 2, characterized in that the means for fixing a reference voltage (R_s) have a control input for receiving a signal which is a measure of the input voltage and that these means (R_s) are arranged for supplying a reference voltage which is lower according as the input voltage is higher.
 4. A power supply circuit as claimed in Claim 1, 2 or 3, characterized in that the means for fixing a reference voltage (RS) are constituted by a circuit of a fourth transistor (T_3) whose base-emitter junction is arranged in parallel with a first resistor (R_6), whose base-collector junction is arranged in parallel with a second resistor (R_8), the junction point of the collector of the fourth transistor with the second resistor constituting an output of the means (R_s) for fixing a reference voltage, and the junction point of the base of the fourth transistor and the first and second resistors constitute a control input for receiving a control signal.
 5. A power supply circuit as claimed in Claim 1, 2, or 3, characterized in that the means for fixing a reference voltage (RS) include a current mirror circuit having a primary and a secondary branch, the current mirror circuit being arranged such that the current flowing through each of the two branches (R_{10} , T_6 ; R_{12} , T_8) is substantially proportional to the input voltage.
 6. A power supply circuit as claimed in any one of the preceding Claims, characterized in that the second series arrangement of the secondary winding (N_2) and the rectifier diode (D_1) provided with terminals (3, 4) for connecting the load (L), is arranged in series with the main current path of the first semiconductor switch (T_1).
 7. A power supply circuit as claimed in Claim 6, characterized in that the means (R_1) for generating a signal which is a measure of the current through the primary winding are arranged between the first semiconductor switch (T_1) and the second series arrangement (N_2).
 8. A shaver provided with a power supply circuit as claimed in any one of the Claims 1 to 7.

Patentansprüche

1. Speiseschaltung zum Speisen einer Last (L) aus Eingangsspannungen unterschiedlicher Größe mit einer ersten Reihenschaltung aus einer Primärwicklung (N_1) eines Transformators (Tr) und einer Hauptstromstrecke eines ersten Halbleiterschalters (T_1), mit einer zweiten Reihenschaltung aus einer Sekundärwicklung (N_2) des Transformators und einer Gleichrichterdiode (D_1), wobei diese zweite Reihenschaltung mit Anschlußklemmen (3, 4) versehen ist zum Anschließen der Last (L); mit einem zweiten Transistorschalter (T_2) zum Schalten des ersten Halbleiterschalters; und mit Mitteln (R_1) zum Erzeugen eines Signals, das ein Maß für den Strom durch die Primärwicklung ist, dadurch gekennzeichnet, daß der Ausgang der genannten Mittel (R_1) mit einem ersten nicht-invertierenden Eingang (6) einer Vergleichsschaltung (CP) verbunden ist, von der ein zweiter invertierender Eingang (5) mit einem Ausgang von Mitteln verbunden ist zum Festlegen einer Bezugsspannung (RS) und von der ein Ausgang mit einem Steuereingang des zweiten Transistorschalters (T_2) verbunden ist, und daß der invertierende Eingang der Vergleichsschaltung (CP) über einen Kondensator mit einem Ausgang des zweiten Transistorschalters (T_2) gekoppelt ist.
2. Speiseschaltung nach Anspruch 1, wobei der erste Halbleiter- und der zweite Transistorschalter durch einen ersten und einen zweiten Transistor gebildet werden, dadurch gekennzeichnet, daß die Vergleichsschaltung (CP) durch einen dritten Transistor (T_4) gebildet wird, dessen Leitungstyp dem des ersten und zweiten Transistors (T_1 , T_2) entgegengesetzt ist, und dessen Basis den invertierenden Eingang (5) und dessen Emitter den nicht-invertierenden Eingang (6) und dessen Kollektor den Ausgang bildet.
3. Speiseschaltung nach Anspruch 1 oder 2, dadurch gekennzeichnet, daß die Mittel zum Festlegen einer Bezugsspannung (R_s) einen Steuer-



eingang aufweisen zum Empfangen eines Signals, das ein Maß der Eingangsspannung ist und daß diese Mittel (R_a) vorgesehen sind zum Liefern einer Bezugsspannung, die niedriger ist, je nachdem die Eingangsspannung höher ist.

4. Speiseschaltung nach Anspruch 1, 2 oder 3, dadurch gekennzeichnet, daß die Mittel zum Festlegen einer Bezugsspannung (RS) durch eine Schaltungsanordnung aus einem vierten Transistor (T_3) bestehen, dessen Basis-Emitter-Übergang parallel zu einem ersten Widerstand (R_8) liegt, dessen Basis-Kollektor-Übergang parallel zu einem zweiten Widerstand (R_9) liegt, wobei der Verbindungspunkt des Kollektors des vierten Transistors mit dem zweiten Widerstand einen Ausgang der Mittel (R_a) zum Festlegen einer Bezugsspannung bildet, und wobei der Verbindungspunkt der Basis des vierten Transistors und dem ersten und zweiten Widerstand einen Steuereingang zum Erhalten eines Steuersignals bildet.
5. Speiseschaltung nach Anspruch 1, 2 oder 3, dadurch gekennzeichnet, daß die Mittel zum Festlegen einer Bezugsspannung (RS) eine Stromspiegelschaltung mit einem primären und einem sekundären Zweig aufweisen, wobei der Strom durch jeden der beiden Zweige (R_{10} , T_5 ; R_{12} , T_6) zu der Eingangsspannung nahezu proportional ist.
6. Speiseschaltung nach einem der vorstehenden Ansprüche, dadurch gekennzeichnet, daß in Reihe mit der Hauptstromstrecke des ersten Halbleiterschalters (T_1) die zweite Reihenschaltung aus der Sekundärwicklung (N_2) und der Gleichrichterdioden (D_1) mit Anschlüssen (3, 4) zum Anschließen der Last (L) vorgesehen ist.
7. Speiseschaltung nach Anspruch 6, dadurch gekennzeichnet, daß die Mittel (R_1) zum Erzeugen eines Signals, das ein Maß für den Strom durch die Primärwicklung ist, sich zwischen dem ersten Halbleiterschalter (T_1) und der zweiten Reihenschaltung (N_2) befinden.
8. Rasiergerät mit einer Speiseschaltung nach einem der Ansprüche 1 bis 7.

Revendications

1. Circuit d'alimentation d'une charge (L) à partir de tensions d'entrée de valeurs différentes, comportant un premier montage série formé par un enroulement primaire (N_1) d'un transformateur (TR) et un trajet de courant principal d'un pre-

mier commutateur semiconducteur (T_1); un second montage série formé par un enroulement secondaire (N_2) du transformateur et une diode redresseuse (D_1), ce second montage série ayant des bornes (3, 4) pour raccorder la charge (L); un second commutateur à transistor (T_2) pour commuter le premier commutateur semiconducteur; et des moyens (R_1) pour engendrer un signal qui est une mesure du courant traversant l'enroulement primaire, caractérisé en ce que la sortie desdits moyens (R_1) pour engendrer un signal qui est une mesure du courant traversant l'enroulement primaire est reliée à une première entrée non inverseuse (6) d'un comparateur (CP) dont une seconde entrée inverseuse (5) est reliée à une sortie de moyens pour fixer une tension de référence (RS) et dont une sortie est reliée à une entrée de commande du second commutateur à transistor (T_2), et en ce que l'entrée inverseuse du comparateur (CP) est couplée à travers un condensateur à une sortie du second commutateur à transistor (T_2).

2. Circuit d'alimentation selon la revendication 1, le premier commutateur semiconducteur et le second commutateur à transistor étant constitués par des premier et second transistors, caractérisé en ce que le comparateur (CP) est constitué par un troisième transistor (T_4) d'un second type de conductivité, opposé à celui des premier et second transistors (T_1 , T_2), troisième transistor dont la base constitue l'entrée inverseuse (5) et dont l'émetteur constitue l'entrée non inverseuse (6) et le collecteur forme la sortie.
3. Circuit d'alimentation selon la revendication 1 ou 2, caractérisé en ce que les moyens (RS) pour fixer une tension de référence présentent une entrée de commande pour recevoir un signal qui est une mesure de la tension d'entrée et en ce que ces moyens (RS) sont agencés pour fournir une tension de référence qui est plus basse à mesure que la tension d'entrée est plus élevée.
4. Circuit d'alimentation selon la revendication 1, 2 ou 3, caractérisé en ce que les moyens (RS) pour fixer une tension de référence sont constitués par un circuit formé d'un quatrième transistor (T_3), dont la jonction de base-émetteur est montée en parallèle avec une première résistance (R_8) dont la jonction de base-collecteur est montée en parallèle avec une seconde résistance (R_9), le point commun au collecteur du quatrième transistor et à la seconde résistance constituant une sortie des moyens (R_a) pour fixer une tension de référence et le point commun à la base du quatrième transistor et aux première et seconde résistances constituant une entrée de commande pour rece-



voir un signal de commande.

5. Circuit d'alimentation selon la revendication 1, 2 ou 3, caractérisé en ce que les moyens (RS) pour fixer une tension de référence comportent un circuit de miroir de courant présentant des branches primaire et secondaire, le circuit de miroir de courant étant disposé de façon que le courant traversant chacune des deux branches (R_{10} , T_5 ; R_{12} , T_6) soit sensiblement proportionnel à la tension d'entrée. 5 10
6. Circuit d'alimentation selon l'une quelconque des revendications précédentes, caractérisé en ce que le second montage série de l'enroulement secondaire (N_2) et de la diode redresseuse (D_1), muni de bornes (3, 4) pour raccorder la charge (11) est monté en série avec le trajet de courant principal du premier commutateur semiconducteur (T_1). 15 20
7. Circuit d'alimentation selon la revendication 6, caractérisé en ce que les moyens (R_1) pour engendrer un signal qui est une mesure du courant traversant l'enroulement primaire sont disposés entre le premier commutateur semiconducteur (T_1) et le second montage en série (N_2). 25
8. Rasoir électrique muni d'un circuit d'alimentation selon l'une quelconque des revendications 1 à 7. 30

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