

METHOD TO DEFINE DESIRED MOTION TRAJECTORIES OF EXOSKELETON FOR MOVEMENT OF A USER WITH FUNCTIONAL IMPAIRMENT OF THE SUPPORT-MOTOR APPARATUS, WALKING ASSISTANCE DEVICE FOR THIS USER AND CONTROL METHOD FOR THIS DEVICE

5 The invention relates to the medical equipment, in particular to the methods to define desired exoskeleton motion trajectories, user walking assistance devices and methods to control walking assistance in pre-determined in advance motion modes of users with support-motor apparatus functional impairment, with limited excursion or complete non-motility of the lower extremities at normal functioning of the upper
10 extremities and upper body part. The invention provides possibility of the walking of a user with support-motor apparatus functional impairment on horizontal and inclined surfaces, as well as stair flights and crossing over obstacles with the walking pattern analogous to the walking pattern of a healthy person, as well as it can be applied for conduction of rehabilitation and recreational procedures.

15 There is a known method to define desired motion trajectories of exoskeleton for motion of a user with support-motor apparatus functional impairment, not having the possibility of independent motion due to limited excursion of the lower extremities, wherein control signals to the exoskeleton drives are generated according to the readings of force sensors installed on the clamping elements of motorized exoskeleton to the user legs [US
20 7731670 B2 patent, publ. in 2010].

 This method is impossible to be used for users with complete non-motility of lower extremities, for example, for users with paraplegia due to impossibility for them to create muscle force in legs, and for users with limited excursion of lower extremities it is impossible to ensure setting of desired walking pattern analogous to the walking pattern of
25 a person without support-motor apparatus functional impairment.

 The closest to the proposed invention in terms of method to define desired motion trajectories of exoskeleton for motion in sagittal plane for a user with support-motor apparatus functional impairment is the method to define desired motion trajectory of exoskeleton in the Cartesian coordinate system for motion in sagittal plane in pre-
30 determined in advance motion modes of users with support-motor apparatus functional impairment using exoskeleton, comprising a housing equipped with clamps for attachment to the user trunk, left and right foot rest, each of which comprises pivotally connected corresponding femoral and shank sections and foot step equipped with corresponding clamps for attachment to the legs of the user and configured to rotate in sagittal plane,

wherein upper ends of the corresponding femoral sections are pivotally connected with the left and, respectively, right end of the exoskeleton housing, wherein hip and knee pivotal joints are equipped with sensors of relative angle rotation of adjacent sections and are configured motorized, as well as on-board controller connected to the sensors of relative angle rotation of adjacent sections and control inputs of motorized joints drives, wherein according to this method using motion capture system, comprising serially connected measuring devices unit to collect and transfer the captured motion parameters data, captured motion parameters data processing unit and captured motion parameters storage unit the output of which is connected to the output of motion capture system, ensure measuring of Cartesian coordinates of pre-selected human body points in the process of motion [A. P. Aliseychik, I.A. Orlov, V.E. Pavlovskiy, V.V. Pavlovskiy, A.K. Platonov., Mechanics and control of exoskeletons for lower extremities for neurorehabilitation of spinal patients. - "XI All-Russian convention on fundamental problems of theoretical and applied mechanics" CD-ROM, Kazan, August 20–24, 2015, p.133–135].

In this method the user's motion manner is formed as a set of time functions of the exoskeleton intersection angles, which does not allow changing the motion parameters - step length, leg rise height and walking rhythm.

The technical result, for achievement of which the proposed method is intended, is the calculation of time-dependent parameters of the desired motion trajectory, allowing to exactly define the desired motion trajectory of the exoskeleton in sagittal plane Cartesian coordinates system for the motion of user with support-motor apparatus functional impairment with motion manner close to the motion manner of a person without support-motor apparatus functional impairment, as well as change the step parameters (step length, leg rise height and walking rhythm).

There is a known walking assistance device for a user with support-motor apparatus functional impairment in pre-determined in advance motion modes comprising exoskeleton equipped with one or several executive mechanisms connected with various sections of the exoskeleton connected to the corresponding body parts of the user, wherein the device provides: receiving of input data indicating the desired sequence motion; obtaining of programmed data movements providing execution of one or more sequential instructions required for performance of relative movements of executive mechanisms for execution of the above instructions and movement of one or more sections of the exoskeleton according to the relative movements of the drive for each instruction [application PCT WO 2011002306 A1, publ. 2011].

In this device, the input signal, which is sent to the drives and defines the motion of the exoskeleton, is step-staired, thus affecting the smoothness of walking in the exoskeleton and does not allow to form control inputs to the exoskeleton drives, which provide close to natural walking pattern, therefore, having a negative impact on the ergonomic characteristics of the walking assistance device for a user with support-motor apparatus functional impairment.

The closest to this invention in terms of device is the walking assistance device for a user with support-motor apparatus functional impairment in pre-determined in advance motion modes comprising exoskeleton of lower extremities, wherein exoskeleton includes pelvic section, left and right foot rest, each of which consists of femoral and shank sections and foot steps, wherein adjacent sections are connected using corresponding pivotal joints providing the possibility of their rotation in sagittal plane and equipped with sensors of relative angle rotation integrated in the current angles and angular velocity measurement unit, wherein hip and knee pivotal joints are configured motorized and equipped with corresponding drives, for example, electric drives, as well as on-board controller connected with sensors of relative angle rotation of adjacent sections and control inputs of motorized joints drives, wherein foot steps are equipped with foot rest reaction sensors integrated in the foot rest reaction measurement unit and mounted in the heel and toe-cap of the foot step, additionally, walking assistance device comprises left and right hand rests and control device including desired exoskeleton angles and angular velocity calculation unit, external moment evaluation unit and unit of calculation and generation of control signals to the exoskeleton drives connected to the control inputs of corresponding drives, wherein the input of desired exoskeleton angles and angular velocity calculation unit is connected to the first input of the control device, the third input of which is connected to the output of the current angles and angular velocity measurement unit [RU 2364385 patent, publ. in 2009].

This device has the following disadvantages:

- the drive signals to the exoskeleton drives are the signals of electromyographic sensors taken off the unaffected extremity, therefore this device and its control method cannot be used by users with no muscular activity (complete paresis), including paraplegics;
- signals from these sensors do not provide proportionality in terms of angles in pivots;
- the input signal, which is sent to the drives and defines the motion of the exoskeleton, is stair-stepped, thus affecting the smoothness of walk in the exoskeleton;

- when generating the control signal to the exoskeleton drives, the influence of the user muscle tiredness on the value of the myographic signal is not taken into account, thus affecting the accuracy of the exoskeleton motion;

- mathematical model of the user exoskeleton put on used in the control signals generation unit when generating signals to the exoskeleton drives does not take into account the influence of the moment created due to the oscillations of the user trunk, the weight of which is approximately half of the body weight.

The above factors restrict functional capabilities of the device and do not allow to form control impact on the exoskeleton drives which provide walking pattern close to natural, having a negative impact on the ergonomic characteristics of the walking assistance device for a user with support-motor apparatus functional impairment.

The closest to this invention in terms of control method of this walking assistance device is control method of the walking assistance device for a user with support-motor apparatus functional impairment in pre-determined in advance motion modes comprising exoskeleton of lower extremities, including pelvic section, left and right foot rest, each of which consists of femoral and shank sections and foot steps, wherein adjacent sections are connected using corresponding pivotal joints providing the possibility of their rotation in sagittal plane and equipped with sensors of relative angle rotation integrated in the current angles and angular velocity measurement unit, wherein hip and knee pivotal joints are configured motorized and equipped with corresponding drives, for example, electric drives, as well as on-board controller connected with sensors of relative angle rotation of adjacent sections and control inputs of motorized joints drives, wherein foot steps are equipped with foot rest reaction sensors integrated in the foot rest reaction measurement unit and mounted in the heel and toe-cap of the foot step, additionally, walking assistance device comprises left and right hand rests and control device comprising desired exoskeleton angles and angular velocity calculation unit, external moment evaluation unit and unit of calculation and generation of control signals to the exoskeleton drives connected to the control inputs of corresponding drives, wherein the input of desired exoskeleton angles and angular velocity calculation unit is connected to the first input of the control device, the third input of which is connected to the output of the current angles and angular velocity measurement unit, wherein according to this method the current angles and angular velocities in hip and knee joints and foot rest reaction forces are measured [RU 2364385 patent, publ. in 2009].

This method used for control of the above walking assistance device for a user with support-motor apparatus functional impairment determines the restriction of functional capabilities and does not allow the provision of high ergonomic characteristics of the device as it is impossible to be applied for rendering of assistance to walking of users with complete loss of support-motor apparatus functions, and when used by users with partial loss of the above functions it cannot provide the user with walking pattern close to natural.

Claimed technical results as per device and method 2

The technical result, for achievement of which this invention is intended in terms of the walking assistance device for a user with support-motor apparatus functional impairment and method for control of this device, is the enhancement of functional capabilities and improvement of ergonomic characteristics of the device through provision of possibility to control the correct (close to the walking pattern of a person without support-motor apparatus functional impairment) walking pattern for users with complete or partial loss of motion activity of muscles and setting, possibility of setting and change, using remote control during motion along the desired trajectories, of such step parameters as length, rise height and walking rhythm, as well as increase of the exoskeleton motion precision on this trajectories.

Other technical results, for achievement of which this invention is intended in terms of the device implementation are:

- provision of possibility of the device use for assistance to the walking both with complete and partial paraplegia;
- provision of possibility of restoration of correct walking pattern of the user with possibility of choice of various walking parameters (length, rise height and rhythm of steps) for provision of possibility of various operation modes of the device - motion on flat, inclined, stepped surfaces, as well as crossing over obstacles, walking on the spot
- provision of possibility of smooth, smooth motion along the desired trajectories of hip and ankle pivots defined in the Cartesian coordinates.

For achievement of the above technical result in terms of the method to define the desired trajectories of the exoskeleton motion for movement in sagittal plane of user with support-motor apparatus functional impairment, according to which using motion capture system comprising serially connected measuring devices unit to collect and transfer the captured motion parameters data, captured motion parameters data processing unit and

captured motion parameters storage unit, the output of which is connected to the output of motion capture system, ensure measuring of Cartesian coordinates of pre-selected human body points in the process of its motion, a person without support-motor apparatus functional impairment is used to measure the Cartesian coordinates of the pre-selected body points, and the points of intersection between the hip joint axis and ankle joints axes, lying in the frontal plane, with sagittal plane are used as the pre-selected body points, the Cartesian coordinates of which are measured. Wherein the above Cartesian coordinates are measured depending on time in the form of trajectories along the axes of the Cartesian coordinates system of the above sagittal plane during motion of the person for each of the pre-determined in advance motion mode, and saved in the captured motion parameters storage unit in the form of data arrays for each measured trajectory, wherein axis of ordinates of the above coordinates system of the sagittal plane is directed vertically, while axis of abscissas – along the course of exoskeleton motion, and further in the unit of captured motion parameters processing, input of which is connected to the output of the motion capture system, captured motion parameters processing is conducted, calculating, based on the above, being table set functions, data arrays of the Cartesian coordinates, the parameters and/or interpolation coefficients for each of the chosen in advance differentiable, interpolating the above trajectories, analytical functions, differentiated at least two times, for example, splines, including cubic splines, wherein the calculated parameters and/or interpolation coefficients are saved in the connected to the output of the unit of captured motion parameters processing storage unit of parameters and/or interpolation coefficients.

Wherein as the pre-determined in advance motion modes of a person without support-motor apparatus functional impairment are used the modes: “Walk on horizontal surface”, “Go upstairs”, “Go downstairs”, “Walk up the inclined surface”, “Walk down the inclined surface”, “Cross over an obstacle”, “Sit on a rest”, “Stand vertically with straightened legs”, “Stand up vertically with straightened legs from the “Sit on a rest” position”, “Sit down on a rest from “Stand vertically with straightened legs”.

For achievement of the above technical results in terms of known walking assistance device for a user with support-motor apparatus functional failure comprising exoskeleton of the lower extremities, including pelvic section and left and right foot rests each of which consists of femoral and shank sections and foot steps. Wherein the adjacent sections are connected using corresponding pivotal joints ensuring the possibility of their rotation in sagittal plane and equipped with the corresponding sensors of relative angle rotation integrated in the current angles and angular velocity measurement unit,

wherein hip and knee pivotal joints are configured motorized and equipped with corresponding drives, for example, electric drives, as well as on-board controller connected to the sensors of relative angle rotation of the adjacent sections and control inputs of the motorized joints drives.

5 Wherein the foot steps are equipped with foot rest reaction sensors integrated in the foot rest reaction unit and mounted in the heel and toe-cap of the foot steps, additionally, the walking assistance device comprises left and right hand rests and control device including desired exoskeleton angles and angular velocity calculation unit, external moment evaluation unit and of calculation and generation of control signals to the
10 exoskeleton drives, wherein the input of desired exoskeleton angles and angular velocity calculation unit is connected to the first input of the control device, the third input of which is connected to the output of the current angles and angular velocity measurement unit, it is supplemented with external computer of assistant-specialist configured with provision to assistant-specialist of possibility to input into the exoskeleton on-board controller the ratio
15 of shank length to femur length, shank length and mass-inertial characteristics of the user body segments with exoskeleton sections attached to them, motion mode selection and adjustment of such motion parameters as step length, leg rise height and walking rhythm, control panel configured with provision to the user of the possibility of motion mode selection and adjustment of such motion parameters as step length, leg rise height and
20 walking rhythm, unit of current measurement in electric drives comprising first, second, third, fourth current sensors of, respectively, first, second, third, fourth electric drives, unit of desired trajectories generation in the Cartesian coordinates system configured to input to it and store in it the time-dependent parameters and/or interpolation coefficients of the desired motion trajectories in the Cartesian coordinates system for pre-determined in
25 advance motion modes, the first input of which is connected to the first output of control device, while the second input – to the output of the foot rest reaction measurement unit, the first output – is connected to the first input of the control device, and the second output is configured to be connected to the input of the desired motion trajectories parameters determination system in the Cartesian coordinates system, the output of which is
30 configured to be connected to the third input of the unit of desired trajectories generation in the Cartesian coordinates system, the fourth input of which is configured to be connected to the output of the external computer of the assistant-specialist, wherein the control device is supplemented with the unit of desired motion acceleration generation along the trajectories in the Cartesian coordinates system, the first input of which is
35 connected to the first input of the control device, the desired angular acceleration calculator, the first input of which is connected to the output of the unit of desired

acceleration generation of motion along the trajectories, and the second input – to the output of unit of the desired angles and angular velocities generation, unit of calculation of angular acceleration to the exoskeleton drives, wherein the first input of the unit of calculation of angular acceleration to the exoskeleton drives is connected to the output of the unit of desired angular acceleration calculation, and the second input – to the output of the unit of desired angles and angular velocity calculation unit, unit of calculation of the exoskeleton current Cartesian coordinates vector, the input of which is connected to the third input of the control device, and the output – to the second input of unit of desired acceleration generation of motion along the trajectories in the Cartesian coordinates system, housing angular motion evaluation unit, the input of which is connected to the output of the unit of calculation of the exoskeleton current Cartesian coordinates, and the output – to the fourth input of the external moment evaluation unit, the fifth input of which is connected through the second input of the control device to the output of the foot rest reaction calculation unit, wherein the first input of the control signals generation unit is connected to the output of the external moment evaluation unit, the first input of which is connected to the output of the unit of calculation of angular acceleration to the exoskeleton drives, and the second input – to the third input of the control device also connected with the third input of the exoskeleton drives angular acceleration calculation unit and to the second input of the control signal generation unit, the third input of which is connected to the output of the exoskeleton drives angular acceleration calculation unit, the fourth input – to the fourth input of the control device also connected with the third input of external moment evaluation unit, and the output to the output of the control device connected to control inputs of the drives equipped with current sensors of the electric drives of the motor current measurement unit, wherein the fourth input of the control device is connected to the output of the electric motors current measurement unit.

For achievement of the above technical results in terms of the control method of the walking assistance device for a user with support-motor apparatus functional impairment in pre-determined in advance motion modes on the basis of the exoskeleton in the known control method of the walking assistance device for a user comprising the exoskeleton of the lower extremities including pelvic section, left and right foot rests each of which consists of femoral and shank sections and foot steps, wherein the adjacent sections are connected using corresponding pivotal joints providing the possibility of their rotation in sagittal plane and equipped with corresponding sensors of relative angle rotation integrated in the current angles and angular velocities measurement unit, wherein hip and knee pivotal joints are configured motorized and equipped with corresponding drives, for example, electric drives, as well as on-board controller connected with sensors

of relative angle rotation of adjacent sections and control inputs of the motorized joints drives, wherein the foot steps are equipped with foot rest reaction sensors integrated in the foot rest reaction measurement unit and mounted in the heel and toe-cap of the foot step, additionally walking assistance device comprises left and right hand rests and control device including desired exoskeleton angles and angular velocity calculation unit, external moment evaluation unit and unit of calculation and generation of control signals to the exoskeleton drives connected to control inputs of corresponding drives, wherein the input of desired exoskeleton angles and angular velocity measurement unit is connected to the first input of the control device, the third input of which is connected to the output of current angles and angular velocity measurement unit.

Wherein, according to this method, the current angles and angular velocities in hip and knee joints and foot rest reaction forces are measured, the walking assistance device for a user with support-motor apparatus functional impairment is supplemented with external computer of assistant-specialist, configured with provision to the assistant-specialist of the possibility of input to the on-board controller the ratio of shank length to femur length, shank length and mass-inertial characteristics of the user body segments with exoskeleton sections attached to them, selection of the motion mode and adjustment of such motion parameters as step length, leg rise height and walking rhythm, control panel configured with provision to the user of the possibility of selection of the step length, leg rise height and walking rhythm, electric motors current measurement unit comprising the first second, third, fourth current sensors of, respectively, the first, second, third and fourth electric drives, unit of desired trajectories generation in the Cartesian coordinates system configured to input in it and store in it the time-dependent parameters and/or interpolation coefficients of the desired motion trajectories in the Cartesian coordinates system for pre-determined in advance motion modes, the first input of which is connected to the output of the control panel, and the second input – to the output of the foot rest reaction measurement unit, the first output is connected to the first input of the control device, and the second output is configured to be connected to the input of desired motion trajectories parameters determination system in the Cartesian coordinates system, the output of which is configured to be connected to the third input of desired trajectories generation unit in the Cartesian coordinates system, the fourth input of which is configured to be connected to the output of the external computer of the assistant-specialist,

wherein the control device is supplemented with a unit of desired motion acceleration generation along the trajectories in the Cartesian coordinates system, the first input of which is connected to the first input of the control device, the desired angular

acceleration calculator, the first input of which is connected to the output of the unit of calculation of desired motion acceleration along the trajectories, and the second input – to the output of the unit of the desired angles and angular velocities generation unit, unit of angular acceleration calculation to exoskeleton drives.

5 Wherein the first input of the unit of angular acceleration calculation to the exoskeleton drives is connected to the output of the unit of desired angular acceleration calculation, and the second input – to the unit of desired angles and angular velocities generation, current exoskeleton Cartesian coordinate vector calculation unit, the input of which is connected to the third input of the control device, and the output – to the second
10 input of the unit of desired motion acceleration generation along the trajectories in the Cartesian coordinates system, housing angular motion evaluation unit, the input of which is connected to the output of unit of the exoskeleton current Cartesian coordinate calculation, and the output – to the fourth input of external moment evaluation unit, the fifth input of which is connected through the second input of the control device to the
15 output of the foot rest reaction measurement unit, wherein the first input of the control signals generation unit is connected to the output of the external moment evaluation unit, the first input of which is connected to the unit of angular acceleration calculation to the exoskeleton drives, and the second input – to the third input of the control device, also connected to the third input of the unit of calculation of angular accelerations to the
20 exoskeleton drives and to the second input of the control signals generation unit, the third input of which is connected to the output of the unit of calculation of angular accelerations to the exoskeleton drives, the fourth input – to the fourth input of the control device, also connected with the third input of the external moment evaluation unit, and output – to the output of the control device, connected to the drives control inputs, equipped with current
25 sensors of electric motors of the motors current measurement unit, wherein the fourth input of the control device is connected to the output of the electric motors current measurement unit.

Wherein, according to the proposed control method of the walking assistance device for a user with support-motor apparatus functional impairment, the ratio of shank
30 length to femur length, shank length are measured and mass-inertial characteristics of the user body segments measurement is conducted directly or indirectly with exoskeleton sections attached to them and via the external computer of the assistant-specialist and the fourth input of the unit of the desired trajectories generation in the Cartesian coordinate system of the on-board controller are input into the unit of the desired trajectories
35 generation in the Cartesian coordinate system of the on-board controller and through it –

into the system of determination of the desired motion trajectories parameters in the Cartesian coordinate system such measured user parameters as shank length, the ratio of shank length to femur length and mass-inertial characteristics of the user body segments with exoskeleton put on, and according to the specified ratio of shank length to femur length of the user data obtaining from the system of desired motion trajectories determination in the Cartesian coordinate system is conducted, which are input in the desired trajectories generation unit in the Cartesian coordinate system in the form of arrays of parameters (coefficients) of interpolation of interpolating functions obtained for a person without support-motor apparatus functional impairment during his/her movement in each of the pre-determined in advance modes, mode is set using the external computer of the assistant-specialist or control panel from the series of pre-determined in advance modes, numeric values of interpolating functions are calculated and scaled by way of their multiplication by the coefficients equal to the ratio between the shank length of the user with support-motor apparatus functional impairment and the shank length of a person without support-motor apparatus functional impairment, desired step parameters are set from control panel or external computer of the assistant-specialist by way of scaling of the interpolating trajectories corresponding to the user represented in the Cartesian coordinate system by corresponding coefficients, as well as for changing of the time of leg carrying over (walking rhythm) – by way of scaling of these functions time axis.

Wherein, scaling is conducted both for each particular coordinate and for their combinations, in the current exoskeleton Cartesian coordinate calculation unit the vector of the current exoskeleton Cartesian coordinates is calculated, based on the obtained measurements of angles and angular velocities in hip and knee joints, in the unit of desired trajectories generation in the Cartesian coordinates system the desired trajectories of hip and ankle pivots of the exoskeleton depending on time, by way of calculation based on the stored time-dependent parameters (coefficients) values arrays of the numeric values of interpolating functions recorded in the Cartesian coordinate system; the vector of the desired angles and angle velocities is calculated based on the previously calculated values of the vector of the desired trajectories and their first derivatives, in the unit of desired motion acceleration generation along the trajectories in the Cartesian coordinate system the vector of desired acceleration for motion along the trajectory in the Cartesian coordinate system is calculated based on the previously calculated values of the position and velocity vector in the Cartesian coordinate system and the vector of desired trajectories and their first and second derivatives, in the desired angles and angular velocities generation unit, the vector of desired angular acceleration is calculated based on the vector of desired acceleration for motion along the trajectory in the Cartesian

coordinate system and vector of desired angles and angular velocities, in the desired exoskeleton drives angular acceleration generation unit the vector of desired angular acceleration to the exoskeleton drives is calculated, based on previously calculated vector of desired angular velocities, vector of desired angles and angular velocities, vector of current angles and angular velocities value in the pivotal joints, in the external moment evaluation unit the vector of external moment is calculated based on previously calculated vector of desired angular accelerations to the drives, vectors of current angles and angular acceleration values in pivotal joints, vector of foot rest reaction, measured vector of the exoskeleton drives currents and taking into account mass-inertial characteristics of the user body segments with exoskeleton put on, and the vector of control signals to the drives of exoskeleton is calculated in generated in the unit of control signals generation to the drives of exoskeleton based on previously calculated vector of current angles values, external moment vector and measured vector of current angles and angular velocities values in pivotal joints, vectors of the exoskeleton drives currents.

Wherein as the pre-determined in advance motion modes of a person with support-motor apparatus functional impairment are used the modes: "Walk on horizontal surface", "Go upstairs", "Go downstairs", "Walk up the inclined surface", "Walk down the inclined surface", "Cross over an obstacle", "Sit on a rest", "Stand vertically with straightened legs", "Stand up vertically with straightened legs from the "Sit on a rest" position", "Sit down on a rest from "Stand vertically with straightened legs".

Wherein the unit of desired motion trajectories generation in the Cartesian coordinate system and control device are implemented in software in the on-board controller of the exoskeleton

Fig. 1 shows the external appearance of a walking assistance device for a user with support-motor apparatus functional impairment, Fig.2 – kinematic diagram of this device, Fig. 3 – functional diagram of the exoskeleton desired motion trajectories parameters determination system in the Cartesian coordinate system, and Fig. 4 – functional diagram of the walking assistance device for a user.

Fig. 5–9 shows motion trajectory in sagittal plane of several points of lower extremities of a person without support-motor apparatus functional impairment in the Cartesian coordinate system obtained experimentally using Vicon motion video capture system.

Fig. 5 – shows motion trajectories in the Cartesian coordinate system of hip, knee and ankle joints and toes of the transferred legs, and Fig. 6 – hip, knee and ankle joints and toes of the support leg.

5 Fig.7 – shows motion trajectories in the Cartesian coordinates system of the hip and ankle joints of the portable leg for the trajectory with initial step length (shown with dotted line) and trajectory with step length reduced by 30% (shown with full line).

Fig.8 – shows supporting trajectory (full line) of the leg transfer along the leg rise axis and the trajectory of accelerated (dotted line) by 30% leg transfer, Fig.9 – shows supporting trajectory of transfer along the axis of longitudinal leg transfer and trajectory of
10 leg transfer accelerated by 30%.

In Fig.1-9 the following is indicated:

- 1 – exoskeleton of lower extremities;
- 2 – pelvic section;
- 3 and 4 – respectively, left and right foot rests;
- 15 5 and 6 – respectively, left and right femoral sections;
- 7 and 8 – respectively, left and right shank sections;
- 9 and 10 – respectively, left and right foot steps;
- 11 – left hip pivotal joint;
- 12 – left knee pivotal joint;
- 20 13 – left ankle pivotal joint;
- 14 – right hip pivotal joint;
- 15 – right knee pivotal joint;
- 16 – right ankle pivotal joint;
- 17 – sensor of relative angle rotation of the left femoral section;
- 25 18 – sensor of relative angle rotation of the left shank section;
- 19 – second output of the unit 41 of desired trajectories generation in the Cartesian coordinate system;

- 20 – sensor of relative angle rotation of the right femoral section;
- 21 – sensor of relative angle rotation of the right shank section;
- 22 – third output of the unit 41 of desired trajectories generation in the Cartesian coordinate system;
- 5 23 – drive of the left hip pivotal joint;
- 24 – drive of the right hip pivotal joint;
- 25 – drive of the left knee pivotal joint;
- 26 – drive of the right knee pivotal joint;
- 27, 28, 29 and 30 – first, second, third and, respectively, fourth foot rest reaction force
- 10 sensor;
- 31 – foot rest reaction measurement unit;
- 32 – control panel;
- 33 and 34 – left and, respectively, right hand rests;
- 35 – control device;
- 15 36 – desired exoskeleton angles and angular velocities calculation unit;
- 37 – desired exoskeleton angles and angular velocities calculation unit 36 input;
- 38 – first input of the control device 35;
- 39 – third input of the control device 35;
- 40 – external moment evaluation unit;
- 20 41 – unit of desired trajectories generation in the Cartesian coordinate system;
- 42 – first input of the unit 41 of desired trajectories generation in the Cartesian coordinate system;
- 43 – desired motion trajectories parameters determination system in the Cartesian coordinate system;
- 25 44 – desired motion acceleration generation unit along the trajectories in the Cartesian coordinate system;

- 45 – first input of the desired motion acceleration generation unit 44 along the trajectories in the Cartesian coordinate system;
- 46 – desired angular accelerations calculation unit;
- 47 – first input of the desired angular accelerations calculation unit 46;
- 5 48 – exoskeleton drives desired angular accelerations calculation unit;
- 49 and 50 – first and, respectively, second inputs of the exoskeleton drives desired angular accelerations calculation unit 48;
- 51 – vector of the exoskeleton current Cartesian coordinates calculation unit;
- 52 – exoskeleton drives control signal generation unit;
- 10 53 – second input of the unit 41 of desired trajectories generation in the Cartesian coordinate system;
- 54 – second input of the desired angular accelerations calculation unit 46;
- 55 – second input of the desired motion acceleration generation unit 44 along the trajectories in the Cartesian coordinate system;
- 15 56 – first input of the exoskeleton drives control signal generation unit 52;
- 57 and 58 – first and, respectively, second inputs of external moment evaluation unit 40;
- 59 – third input of the exoskeleton drives desired angular accelerations calculation unit 48;
- 60, 61, 62 – second, third and, respectively, fourth inputs of the exoskeleton drives control signal generation unit 52;
- 20 63 – fourth input of the control device 35;
- 64 – third input of external moment evaluation unit 40;
- 65 – electric drives current measurement unit;
- 66, 67, 68 and 69 – first, second, third and, respectively, fourth 69 sensors of current of the first 23, second 24, third 25 and, respectively, fourth 26 electric drives;
- 25 70 – current angles and angular velocities measurement unit;
- 71 – user torso angular motion evaluation unit;

- 72 – user torso angular motion evaluation unit input;
- 73 – fourth input of external moment evaluation unit 40;
- 74 – fifth input of external moment evaluation unit 40;
- 75 – fifth input of the control device 35;
- 5 76 – storage unit of the exoskeleton desired motion trajectories parameters and/or interpolation coefficients in the Cartesian coordinate system;
- 77 – motion capture system;
- 78 – measuring devices unit to collect and transfer the captured motion parameters data;
- 10 79 – captured motion parameters data processing unit;
- 80 – captured motion parameters storage unit;
- 81 – captured motion parameters processing unit;
- 82 – crutch handle;
- 83 – first output of the unit 41 of desired trajectories generation in the Cartesian
- 15 coordinate system;
- 84 – fourth output of the unit 41 of desired trajectories generation in the Cartesian coordinate system;
- 85 – on-board controller;
- 86 – external computer of the assistant-specialist;
- 20 87 – desired motion trajectories in the Cartesian coordinate system determination controller;
- 88 and 89 – first and, respectively, second outputs of the external computer 86 of the assistant;
- 90 – sixth input of external moment evaluation unit 40;
- 25 Method to define the desired exoskeleton motion trajectories in the Cartesian coordinate system for the movement in sagittal plane in pre-determined in advance motion

modes of user with support-motor apparatus functional impairment is implemented for the exoskeleton 1 including pelvic 2 section and left 3 and right 4 foot rests each of which consists of femoral 5 (6) and shank 7 (8) sections and foot steps 9 (10).

Wherein the adjacent sections 2-5, 5-7, 7-9, 2-6, 6-8 and 8-10 are connected using
5 corresponding pivotal joints 11, 12, 13, 14, 15 and 16 ensuring the possibility of their rotation in sagittal plane and equipped with the corresponding sensors 17, 18, 20, 21 of relative angle rotation integrated in the current angles and angular velocity measurement unit 70, wherein hip 11 and 14 and knee 12 and 15 pivotal joints are configured motorized and equipped with corresponding drives 23, 24 and 25, 26, for example, electric drives, as
10 well as on-board controller 85 connected to the sensors 17, 18, 20, 21 of relative angle rotation of the adjacent sections and control inputs of the motorized joints drives 23, 24 and 25, 26.

Wherein, according to this method, the motion capture system 77, which includes serially connected measuring devices unit 78 to collect and transfer the captured motion
15 parameters data, the captured motion parameters data processing unit 79, the captured motion parameters storage unit 80, the output of which is connected to the output of the motion capture system 77, ensures measuring of Cartesian coordinates of pre-selected human body points in the process of motion, wherein motion capture system 77 is used in the scope of desired trajectories parameters determination system in the Cartesian
20 coordinate system 43, and a person without support-motor apparatus functional impairment is used to measure the Cartesian coordinates of the pre-selected body points, and the points of intersection between the hip joint axis and ankle joints axes, lying in the frontal plane, with sagittal plane are used as the pre-selected body points, the Cartesian coordinates of which are measured.

25

Wherein the above Cartesian coordinates are measured depending on time in the form of trajectories along the axes of the Cartesian coordinates system of the above sagittal plane during motion of the above person for each of the pre-determined in advance motion mode, and saved in the captured motion parameters storage unit 80 in
30 the form of data arrays for each measured trajectory, wherein axis of ordinates of the above coordinates system of the sagittal plane is directed vertically, while axis of abscissas – along the course of exoskeleton motion.

Further in the captured motion parameters processing unit 81 integrated into the desired motion trajectories parameters determination system 43 in the Cartesian
35 coordinates system, the input of which is connected to the output of the motion capture

system 77, processing of the parameters and/or interpolation coefficients of the captured motion is conducted, calculating, based on the above arrays of table set time functions of the Cartesian coordinates, the parameters and/or interpolation coefficients for each of the chosen in advance differentiable, interpolating the above trajectories, analytical functions, differentiated at least two times, for example, splines, including cubic splines.

Wherein the calculated parameters and/or interpolation coefficients are recorded in the storage unit 76 of the exoskeleton desired motion trajectories parameters and/or interpolation coefficients in the Cartesian coordinate system connected to the output of the captured motion parameters processing unit 81 and integrated in the desired motion trajectories parameters determination system 43 in the Cartesian coordinate system.

Wherein the above measurements, processing of data obtained as the result of these measurements and storage of the results of these data processing are conducted for a group of people with various ratio of shank length to femur length, wherein preserving the data on the above ratios and shank length for each person in this group.

Wherein the captured motion parameters processing unit 81 and storage unit 76 of the exoskeleton desired motion trajectories parameters and/or interpolation coefficients in the Cartesian coordinate system should preferably be implemented in software in the controller 87 of desired motion trajectories system determination in the Cartesian coordinate.

Wherein as the pre-determined in advance motion modes of a person without support-motor apparatus functional impairment are used the modes: "Walk on horizontal surface", "Go upstairs", "Go downstairs", "Walk up the inclined surface", "Walk down the inclined surface", "Cross over an obstacle", "Sit on a rest", "Stand vertically with straightened legs", "Stand up vertically with straightened legs from the "Sit on a rest" position", "Sit down on a rest from "Stand vertically with straightened legs".

Walking assistance device for a user with support-motor apparatus functional impairment in pre-determined in advance motion modes, comprising exoskeleton 1 of the lower extremities, includes pelvic 2 section and left 3 and right 4 foot rests each of which consists of femoral 5 (6) and shank 7 (8) sections and foot steps 9 (10). Wherein the adjacent sections 2-5, 5-7, 7-9, 2-6, 6-8 and 8-10 are connected using corresponding pivotal joints 11, 12, 13, 14, 15 and 16 ensuring the possibility of their rotation in sagittal plane and equipped with the corresponding sensors 17, 18, 20, 21 of relative angle rotation integrated in the current angles and angular velocity measurement unit 70.

Wherein hip 11 and 14 and knee 12 and 15 pivotal joints are configured motorized and equipped with corresponding drives 23, 24 and 25, 26, for example, electric drives, as well as on-board controller 85 connected with sensors 17, 18, 20, 21 of relative angle

rotation of adjacent sections and control inputs of the motorized joints drives 23, 24 and 25, 26, wherein the foot steps 9 and 10 are equipped with first 27, second 28, third 29 and fourth 30 foot rest reaction sensors integrated in the foot rest reaction measurement unit 31 and mounted in the heel 27, (29) and toe-cap 28, (30) of the foot steps 9 (10).

5 Additionally, the walking assistance device comprises left 33 and right 34 hand rests and control device 35, including exoskeleton 1 desired angles and angular velocities calculation unit 36, external moment evaluation unit 40 and control signals to the exoskeleton 1 drives generation unit 52 connected to the control inputs of the corresponding drives, wherein exoskeleton 1 desired angles and angular velocities
10 calculation unit 36 input 37 is connected to the first input 38 of the control device 35, third input 39 of which is connected to the output of current angles and angular velocities measurement unit 70.

 Additionally, walking assistance device for a user with support-motor apparatus functional impairment comprises external computer 86 of the assistant-specialist
15 configured to provide the assistant-specialist with the possibility of input into the on-board controller 85 of the exoskeleton 1 of the ratio of shank length to femur length, shank length and mass-inertial characteristics of the user body segments with exoskeleton sections attached to them, motion mode selection and adjustment of such motion parameters as step length, leg rise height and walking rhythm,
20 control panel 32, configured to provide the user with the possibility of motion mode selection and adjustment of such motion parameters as step length, leg rise height and walking rhythm and electric drives current measurement unit 65, comprising first 66, second 67, third 68, fourth 69 current sensors of, respectively, first 23, second 24, third 25 and fourth 26 electric drives.

25 Additionally, walking assistance device for a user with support-motor apparatus functional impairment comprises the desired Cartesian trajectories generation unit 41, configured to input to it and store in it the time-dependent parameters and/or interpolation coefficients of the desired Cartesian trajectories for pre-determined in advance motion modes, the first input 42 of which is connected to the output of control panel 32, and the
30 second input 53 – to the output of the foot rest reaction measurement unit 31, first output 83 is connected to the first input 38 of control device 35, and the second output 19 is configured with the possibility to connect to the input of the desired motion Cartesian trajectories parameters determination system 43, the output of which is configured with the possibility to connect to the third input 22 of the the desired Cartesian trajectories

generation unit 41, the fourth input 84 of which is configured with the possibility to connect to the first 88 output of the external computer 86 of the assistant-specialist, the second output 89 of which is configured with the possibility to connect to the sixth input 90 of the external moment evaluation unit 40.

5 Wherein the control device 35 comprises the desired motion acceleration generation unit 44 along the trajectories in the Cartesian coordinate system, the first input 45 of which is connected to the first input 38 of the control device 35, desired angular accelerations calculation unit 46, the first input 47 of which is connected to the output of the desired trajectory accelerations generation unit 44, and the second input 54 – to the
10 output of desired exoskeleton angles and angular velocities calculation unit 36, unit 48 of calculation of desired angle accelerations to the exoskeleton 1 drives, the first input 49 of which is connected to the output of the desired angular accelerations calculation unit 46, and the second input 50 – to the output of the desired exoskeleton angles and angular velocities calculation unit 36, vector of the exoskeleton 1 current Cartesian coordinates
15 calculation unit 51, the input of which is connected to the third input 39 of the control device 35, and the output to the second 55 input of the desired motion accelerations generation unit 44 along the trajectories in the Cartesian coordinate system.

 Additionally, the walking assistance device comprises user torso angular motion evaluation unit 71, the input 72 of which is connected to the output of current exoskeleton
20 Cartesian coordinates vector calculation unit 51, and the output – to the fourth 73 input of the external moment evaluation unit 40, the fifth input 74 of which through the second input 75 of the control device 35 is connected to the output of the foot rest reaction measurement unit 31.

 Wherein, the first input 56 of the exoskeleton drives control signal generation unit
25 52 is connected to the output of the external moment evaluation unit 40, the first input 57 of which is connected to the output of the exoskeleton drives desired angular accelerations calculation unit 48, and the second input 58 – to the third input 39 of the control device 35, also connected to the third input 59 of the exoskeleton drives desired angular accelerations calculation unit 48 and to the second 60 input of the exoskeleton
30 drives control signal generation unit 52, the third input 61 of which is connected to the output of the exoskeleton drives desired angular accelerations calculation unit 48, the fourth input 62 – to the fourth input 63 of the control device 35, also connected to the third input 64 of the external moment evaluation unit 40, and the output – to the output of the control device 35, connected to the control inputs of the drives 23, 24, 25, 26 equipped
35 with sensors 66, 67, 68, 69 of current of electric motors of the electric motors current

measurement unit 65, wherein the fourth 63 input of the control device 35 is connected to the output of electric motors currents measurement unit 65.

Wherein, according to the present method for control of the above walking assistance device for a user with support-motor apparatus functional impairment, the ratio of shank length to femur length, shank length and mass-inertial characteristics of the user body segments with exoskeleton sections attached to them are measured and through external computer 86 of the assistant-specialist and the fourth input 84 of the desired trajectories generation unit 41 in the Cartesian coordinate system of the on-board controller 85 are input into the unit 41 of desired trajectories generation in the Cartesian coordinate system of the on-board controller 85 and through it into the desired motion trajectories parameters determination system 43 in the Cartesian coordinate system such measured user parameters as shank length, the ratio of shank length to femur length and mass-inertial characteristics of the user body segments with exoskeleton 1 put on, according to the input user ratio of shank length to femur length data extract is conducted from the desired motion trajectories parameters determination system 43 in the Cartesian coordinate system, which are entered into the desired trajectories generation unit 41 in the Cartesian coordinate system in the form of parameters (coefficients) arrays of interpolation of interpolating functions obtained for a person without support-motor apparatus functional impairment during his/her movement in each of the pre-determined in advance modes, from the external computer 86 of the assistant-specialist of control panel 32 the user motion mode is set, numeric values of interpolating functions are calculated and scaled by way of their multiplication by the coefficient equal to the ratio between the shank length of the user with support-motor apparatus functional impairment and the shank length of a person without support-motor apparatus functional impairment, desired step parameters are set from control panel or external computer of the assistant-specialist by way of scaling of the interpolating trajectories corresponding to the user represented in the Cartesian coordinate system by corresponding coefficients, as well as for changing of the time of leg carrying over (walking rhythm) – by way of scaling of these functions time axis, wherein, scaling is conducted both for each particular coordinate and for their combinations, the vector of the current exoskeleton Cartesian coordinates is calculated, based on the obtained measurements of angles and angular velocities in hip and knee joints, the desired motion trajectories of hip and ankle pivots of the exoskeleton are generated depending on time, by way of calculation based on the stored and time-dependent parameters (coefficients) values arrays of the numeric values of interpolating functions recorded in the Cartesian coordinate system; the vector of the desired angles and angle velocities is calculated based on the previously calculated values of the vector

of the desired trajectories and their first derivatives; the vector of desired accelerations for motion along the trajectory in the Cartesian coordinate system is calculated based on the previously calculated values of the position and velocity vector in the Cartesian coordinate system and the vector of desired trajectories and their first and second derivatives; the
5 vector of desired angular acceleration is calculated based on the vector of desired acceleration for motion along the trajectory in the Cartesian coordinate system and the vector of desired angles and angular velocities; the vector of desired exoskeleton drives angular accelerations is calculated, based on the previously calculated vector of desired angular accelerations, vector of desired angles and angular velocities, vector of current
10 pivotal joints angles and angular velocities values; the vector of external moment is calculated based on previously calculated vector of desired angular accelerations to the drives, the vector of current angles and angular acceleration values in pivotal joints, the vector of measured exoskeleton drives currents and considering the mass-inertia characteristics of segments of the user body with the exoskeleton put on it, and the vector
15 of the exoskeleton drives control signals is calculated and generated on the basis of previously calculated vector of current pivotal joints angles and angular velocities values, vector of exoskeleton drives current and vector of foot rest reaction.

Wherein as the pre-determined in advance motion modes of a person with support-motor apparatus functional impairment are used the modes: "Walk on horizontal
20 surface", "Go upstairs", "Go downstairs", "Walk up the inclined surface", "Walk down the inclined surface", "Cross over an obstacle", "Sit on a rest", "Stand vertically with straightened legs", "Stand up vertically with straightened legs from the "Sit on a rest" position", "Sit down on a rest from "Stand vertically with straightened legs".

Wherein the unit 41 of desired motion trajectories generation in the Cartesian
25 coordinate system and control device 35 are implemented in software in the on-board controller 85 of the exoskeleton 1.

Description of the use principles of the walking assistance device for a user with support-motor apparatus functional impairment

30 Operation of the walking assistance device for a user with support-motor apparatus functional impairment can be conventionally characterized by three stages:

– preparation, at which data arrays are formed that clearly characterize the walking (walking pattern) in the Cartesian coordinate system of a person without support-motor apparatus functional impairment for pre-determined in advance motion modes, which is
35 the desired trajectory of motion in the same Cartesian coordinate system of user with

support-motor apparatus functional impairment for the same pre-determined in advance motion modes;

– measurements and adjustment stage at which the measurement is conducted of the required geometric and mass-inertial characteristics of user with support-motor apparatus

5 functional impairment and input of the measured data is conducted into the exoskeleton on-board controller, as well as exoskeleton motion mode and walking parameters (step length, leg rise height, walking rhythm) are set;

– stage of control effects generation to the exoskeleton drives at which calculation of control signals and generation of control signals to the exoskeleton drives are performed.

10 **Preparation stage**

According to the proposed method to define the desired motion trajectories of the exoskeleton for movement in the sagittal plane in pre-determined in advance of user with support-motor apparatus functional impairment motion capture is conducted of a person without support-motor apparatus functional impairment (Fig.5, 6), storage of the captured
15 motion in the Cartesian coordinates is conducted, parameters and/or interpolation coefficients of the desired motion trajectories in the Cartesian coordinate system in sagittal plane in the same pre-determined in advance motion modes of a person without support-motor apparatus functional impairment are calculated and used. Additionally, this person without support-motor apparatus functional impairment should have the same ratio
20 of shank length to femur length as the user with support-motor apparatus functional impairment. Additionally, their shank length should be recorded.

For implementation of the method to define the desired exoskeleton motion trajectories, the desired exoskeleton motion trajectories parameters determination system 43 in the Cartesian coordinate system is used, comprising the following technical means:

25 motion capture system 77, comprising serially connected measuring devices unit 78 to collect and transfer the captured motion parameters data, captured motion parameters data processing unit 79 and the captured motion parameters storage unit 80, the output of which is connected to the output of the motion capture system 77 and serially connected captured motion parameters processing unit 81, the input of which is connected to the
30 output of motion capture system 77 and storage unit 76 for the desired exoskeleton motion trajectories parameters and/or interpolation function coefficients , where data on the ratio of shank length to femur length of a person without support-motor apparatus functional impairment are also recorded.

Thus, in the unit 76 the accumulation and storage is conducted of the calculated parameters and/or interpolation coefficients of the desired trajectories both for the group of people with various ratios of shank length to femur length, wherein preserving the data on the above ratios and shank length for each person of this group, and for the trajectories corresponding to various pre-determined in advance motion modes (walking on flat, inclined and stepped surfaces, as well as modes of lowering and standing up from the rest).

It is preferable that the captured motion parameters processing unit 81 and storage unit 76 of the exoskeleton desired motion trajectories parameters and/or interpolation coefficients in the Cartesian coordinate system are implemented in the desired motion trajectories in the Cartesian coordinate system determination controller 87.

Wherein as the pre-determined in advance motion modes of a person without support-motor apparatus functional impairment are used the modes: "Walk on horizontal surface", "Go upstairs", "Go downstairs", "Walk up the inclined surface", "Walk down the inclined surface", "Cross over an obstacle", "Sit on a rest", "Stand vertically with straightened legs", "Stand up vertically with straightened legs from the "Sit on a rest" position", "Sit down on a rest from "Stand vertically with straightened legs".

Measurements and adjustment stage

At the stage of measurements and adjustment measurements and input into the exoskeleton on-board controller of the anthropometric and mass-inertial parameters of the user with support-motor apparatus functional impairment. These measurements are conducted by assistant-specialist who inputs the into the exoskeleton 1 on-board controller 85 using external computer 86.

Thus, according to shank length and shank length/femur length ratio measured by the assistant-specialist, which through the fourth input 84 of the unit 41 of desired motion trajectories generation in the Cartesian coordinate system, the second output 19 of the above unit 41 and input of the desired motion trajectories parameters determination system 43 in the Cartesian coordinate system are input, and through the output of the above system 43 the extract of arrays of parameters and/or interpolation coefficients of the desired trajectories corresponding to the input ration for all pre-determined in advance person motion mode is conducted.

After that trajectories scaling is conducted, which are presented in the Cartesian coordinate system, by the coefficient of shank length of a person without support-motor

apparatus functional impairment and user with support-motor apparatus functional impairment, and interpolation coefficients of the desired trajectories for the user are calculated. Obtained coefficients clearly determine the desired trajectory of the exoskeleton movement in sagittal plane for movement in pre-determined in advance motion modes of user with support-motor apparatus functional impairment, and further it is used as the reference in the process of the exoskeleton motion.

After setting of the walking parameters (step length, leg rise height, walking rhythm) scaling is conducted of the interpolated trajectories corresponding to the user, presented in the Cartesian coordinate system, by the corresponding coefficients, all for changing of time of leg transfer (walking rhythm) – by way of scaling of the time axis of these functions, wherein scaling is conducted both for each particular coordinate and their combination. Reference and scaled trajectories are shown in Figures 7–9.

Stage of control effects generation to the exoskeleton drives

From literature sources [V.V. Beletskiy. Biped walking. Model tasks of dynamics and control. Moscow: Nauka, 1984. 268 pages. Pages 219–220] it is known that dynamic model of exoskeleton with integrated and attached to it lower body part of the user during motion in sagittal plane can be described by the equations taking into account the user trunk motion,

$$D(\theta)\ddot{\theta} + H(\theta, \dot{\theta}) + G(\theta) + R(\theta) = W(\tau_e + \tau_h) \quad (1)$$

where D – [7x7] matrix describing the inertia of exoskeleton with a person integrated in it, H – [7x1] vector of Coriolis and centrifugal forces, G – [7x1] vector of gravity forces, $R(\theta)$ – [7x1] vector of foot rest reaction of the support leg, W – [7x4] – a certain matrix, τ_e – [4x1] vector of control moments produced by the drives, τ_h – [6x1] vector of external impact moments, $\theta, \dot{\theta}, \ddot{\theta}$ – [7x1] vectors of generalized coordinates, velocities and accelerations. Vector θ [7x1] consists of Cartesian coordinates of hip joint x_{pel}, y_{pel} , user torso inclination angle ψ and vector of intersection angles $\mathcal{G}(t) = [\alpha_1(t), \beta_1(t), \alpha_2(t), \beta_2(t)]'$ in hip 11 and 14 and knee 12 and 15 pivotal joints of support and transferred legs.

Using control panel 32 the required motion mode is selected from the series of pre-determined in advance motion modes. Using integrated in the current angles and angular velocities measurement unit 70 sensors 17, 20 and 18, 21 of relative angle rotation angles

and angular velocities of hip 11 and 14 and knee 12 and 15 pivotal joints are measured, and using integrated in the electric motors current measurement unit 65 sensors 66, 67, 68 and 69 of electric motors current measurement – electric drives electric motors 23, 24, 25, 26, respectively.

5 Simultaneously, using force sensors 27, 28, 29 and 30, integrated in the foot rest reaction measurement unit 31, data on the foot rest reaction in foot steps 9 and 10 are collected.

10 Additionally, on signal from control panel 32 from the storage unit 76 of the parameters and/or interpolation coefficients desired motion trajectories parameters determination system 43 to the memory of the unit 41 of desired trajectories generation in the Cartesian coordinate system parameters and/or interpolation coefficients are entered of motion trajectories of pre-determined in advance motion modes of a person without support-motor apparatus functional impairment with the same ratio of shank length to femur length as the user with impairment of the above functions and the shank length of a
15 person without impairment of above functions.

Assistance device requires adjustment to the anthropometric parameters of specific user – ratio of shank length/femur length and shank length, as well as his/her mass-dimensional parameters. Assistant inputs these user parameters into the unit 41 using external computer 86 of the assistant-specialist. Then, unit 41 receives from unit 43
20 a set of desired motion trajectories for various motion modes corresponding to the input user anthropometric parameters.

Motion start of the exoskeleton and step parameters are set by the assistant using external 86 computer and/or by user using control panel 32.

25 In the current exoskeleton Cartesian coordinates vector calculation unit 51, the vectors of current exoskeleton Cartesian coordinates are calculated, based on the obtained measurements of angles and angular velocities in hip 11 and 14 and knee 12 and 15 pivotal joints.

Relations between two ankle pivots and pelvic pivot for the case of single-support walking are of the form of [V.V. Beletskiy. Biped walking. Model tasks of dynamics and control.
30 Moscow: Nauka, 1984. 268 pages. Page 16]

$$Y = \Phi(\mathcal{I}) \quad (2)$$

$$\dot{Y} = \frac{d}{dt} \Phi(\mathcal{G}) \quad (3)$$

where vector $Y = [x_{pel}, y_{pel}, x_{1a}, y_{1a}, x_{2a}, y_{2a}]'$, which is considered as a time function.

In the unit 41, the desired trajectories of exoskeleton hip and ankle pivots motion are generated depending on time by way of calculation, based on stored and time-dependent parameters (coefficients) values array of numeric values of interpolating functions $\Xi(t)$ and their first $\dot{\Xi}(t)$ and second $\ddot{\Xi}(t)$ derivatives recorded in the Cartesian coordinate system.

The desired angles and angular velocities generation unit 36

calculates the vector of desired angles and angular velocities based on previously calculated values of the vector of desired trajectories and their first derivatives,

Relations **Error! Reference source not found.** assume the availability of inverse ratios [V.V. Beletskiy. Biped walking. - Moscow. Nauka, 1984, -286 pages. Page 16]

$$\mathcal{G}(t) = \Phi^{-1}(Y), \quad (4)$$

$$\dot{\mathcal{G}}(t) = \frac{d\Phi^{-1}(Y)}{dt} \quad (5)$$

Use of vectors $\Xi(t)$, $\dot{\Xi}(t)$, along with ratios **Error! Reference source not found.**, **Error! Reference source not found.** allows calculation of the desired angles $\mathcal{G}^*(t)$ and their first derivatives $\dot{\mathcal{G}}^*(t)$ according to formulas

$$\mathcal{G}^*(t) = \Phi^{-1}(\Xi), \quad (6)$$

$$\dot{\mathcal{G}}^*(t) = \frac{d}{dt} \Phi^{-1}(\Xi) \quad (7)$$

In the unit 44 for generation of the desired accelerations for motion along the trajectory, the vector of desired accelerations for motion along the trajectory in the

Cartesian coordinates system is calculated based on previously calculated values of the vector of position and velocity in the Cartesian coordinate system and the vector of desired trajectories and their first and second derivatives,

Stability of the exoskeleton motion along the trajectories is achieved through control forming in such a manner that deviation ε of the exoskeleton coordinates from the desired trajectory is a decreasing time function asymptotically tending to zero (for example, in the form of

$$\varepsilon = Y - \Xi(t) = A_1 e^{\lambda_1 t} + A_2 e^{\lambda_2 t}, \quad \lambda_1, \lambda_2 < 0).$$

Determining the vector from it $\dot{Y}$ after double differentiation we obtain the second derivative

$$\ddot{Y}^*(t) = (\lambda_1 + \lambda_2)(\dot{Y}(t) - \dot{\Xi}(t)) - \lambda_1 \lambda_2 (Y(t) - \Xi(t)) + \ddot{\Xi}(t), \quad (8)$$

ensuring smooth motion along the trajectories in hip and ankle pivots. Vector values λ_1, λ_2 are set in the form of negative real numbers and are set-up coefficients and adjusting parameters determined by dynamic characteristics of the user-exoskeleton human-machine system.

In the desired angular accelerations calculation unit 46 the vector of desired angular accelerations are calculated based on the vector of desired acceleration for motion along the trajectory in the Cartesian coordinate system and vector of desired angles and angular velocities.

Vector $\ddot{Y}^*(t)$ is used for calculation of the vector of desired angular accelerations $\ddot{\mathcal{G}}^*(t)$. For that, by differentiating the formula **Error! Reference source not found.** and inserting the vector $\ddot{Y}^*(t)$ and vectors $Y^*(t) = \Xi(t)$, $\dot{Y}^*(t) = \dot{\Xi}(t)$, in it we calculate the vector components $\ddot{\mathcal{G}}^*(t)$.

Obtained expressions for the desired second derivatives as per angles $\ddot{\mathcal{G}}^*(t)$ are formed taking into account possible deviations of the exoskeleton from the desired trajectories in the Cartesian coordinates.

5 In the unit 48 the vector of desired angular accelerations to the drives are calculated based on the previously calculated vector of desired angular accelerations, vector of desired angles and angular velocities, vector of current values of angles and angular velocities in pivotal joints,

Next level of algorithm formation ensuring improvement of the drive system control quality,
10 consists in calculation of the vector components of angular acceleration $\ddot{\mathcal{G}}(t)$ for their working off by the drive system, which is formed taking into account possible errors occurring during exoskeleton drive system operation

$$\ddot{\mathcal{G}}(t) = (\mu_1 + \mu_2)(\dot{\mathcal{G}}(t) - \dot{\mathcal{G}}^*(t)) - \mu_1\mu_2(\mathcal{G}(t) - \mathcal{G}^*(t)) + \ddot{\mathcal{G}}^*(t), \quad (9)$$

where $\mu_1, \mu_2 < 0$ – vectors of control parameters the values of which are determined by
15 the drive dynamics. It allows provision of the smooth exoskeleton motion along the desired trajectories and increases the accuracy of the motion implementation.

In the unit 71 evaluation of the body angular motion is conducted. Operator body is the weightiest object which certainly requires consideration of its motion. In the present embodiment of method for control the operator ψ body angular motion is evaluated
20 based on the formula (V.V. Beletskiy. Biped walking. Model tasks of dynamics and control. Moscow: Nauka, 1984. 268 pages, Page 65, V.V. Beletskiy, E.K. Lavrovskiy Model task of biped walking./ Solid body mechanics, No.2, 1981. Page 25)

$$\psi(t) = -\frac{ML}{2K_r} \left[ch\omega t - \frac{1 + ch\omega T_{step}}{sh\omega T_{step}} sh\omega t \right] - \frac{Mx_{pel}}{K_r}, \quad (10)$$

$$\omega^2 = \frac{K_r g}{J + K_r h}, \quad K_r = m_t r.$$

where m_t – trunk weight;

25 J – trunk moment of inertia;

r – distance from the trunk mass center to the pelvis;

M – user body weight;

L – step length;

h – height of pelvis point movement;

5 T_{step} – step period,

from where the first and second derivatives of this angle can be obtained. Evaluation ψ of angle and its derivatives is used for evaluation of external moment which is mainly created due to the operator body oscillations.

10 In the external moment evaluation unit 40 the vector of external moment is calculated based on the previously calculated vectors of desired angular accelerations to the drives, vector of current values of angles and angular velocities in pivotal joints and measured vector of the exoskeleton drives currents,

For provision of the smooth exoskeleton motion it is necessary to take into account the equations of dynamics together with evaluation of oscillating body movements.

15 Exoskeleton drive system can be a hydro drive, pneumatic drive or electric drive.

It is known [V.V. Titov, I.V. Shardyko, I.Yu. Dalyaev. Implementation of force-torque control for two-stage manipulator./ Visnik NTUU “KPI”. Series of machine equipment No.2 (68). 2013. Page 150] that the electric drive dynamics is described by the equations

$$\left\{ \begin{array}{l} \tau_m(t) = C_m \cdot i_m(t); \\ e(t) = C_e \cdot \dot{\alpha}; \\ u(t) = e(t) + R_m \cdot i_m(t) + \frac{di_m(t)}{dt} \cdot L_m; \\ J_m \cdot \ddot{\alpha} = \tau_m(t) - \tau_{mext}(t) - \tau_{fric}(\dot{\alpha}, \tau_m - \tau_{mext}, t); \end{array} \right.$$

20

Where τ_m – motor moment, C_m , C_e – moment and electric constant of the motor respectively, e – motor back electromotive force, R_m , L_m = motor resistance and armature inductance, J_m – motor rotor moment of inertia, τ_{mext} – external moment on the motor shaft, $\ddot{\alpha}$, $\dot{\alpha}$ – acceleration and angular rotation rate of the motor shaft α , τ_{fric} – force of friction on the motor shaft, u – feed voltage on the motor windings.

25

On the other side, in case of electric drive the vector of external, in relation to the drive, moments obtained from the dynamics equation **Error! Reference source not found.** has the form of

$$\tau_e = -W^{-1} \left[D(\theta) \ddot{\theta} + H(\theta, \dot{\theta}) + G(\theta) + R(\theta) \right] - \tau_h(t) \quad , \quad (11)$$

- 5 where $\ddot{\theta} = [\ddot{Y}^*, \ddot{\psi}, \ddot{\theta}]$, can be found using evaluations taking into account mass-inertial [A.V. Voronov. Anatomical organization and biomechanical characteristics of muscles and joints of a lower extremity./ Moscow, Fizkultura, obrazovanie i nauka, 2003., Pages 11–12, 19–20; D.A. Winter, Biomechanics and motor control of human movement, 2005. JOHN WILEY & SONS, INC., P. 86, Table 4.1] characteristics of the mechanical system –
10 a person in exoskeleton, as well as based on the consideration of the drives dynamics and current vectors measurement going on in electromechanical drives. As a result

$$M_{dv}(t) = (\tau_{fric} + J_e \cdot T \ddot{\theta}(t)) \cdot j + W^{-1} \left[D(\theta) \ddot{\theta} + H(\theta, \dot{\theta}) + G(\theta) + R(\theta) \right] \quad (12)$$

- Here M_{dv} – moment developed by the motor at the reduction gear output shaft, C_m , J_e – electric motors parameters matrices, j – reduction coefficient matrix, i – current vector,
15 $T [7 \times 4]$ – vector translation matrix θ to the vector of the exoskeleton intersection angles, τ_{fric} – friction forces moment driven to the motors output shaft.

- In the control signals generation unit 52 the vector of control signals to the exoskeleton drives is calculated and generated based on the previously calculated vector of current angles, evaluated external moment vector and measured vector of current
20 angles and angular velocities value in the pivotal joints, as well as exoskeleton drives current vector.

Control voltage in case of electric drives is calculated as follows

$$u(t) = C_e \cdot T \cdot \dot{\theta} + C_m^{-1} R_e M_{dv} / j + \frac{di(t)}{dt} \cdot L_e \quad (13)$$

Similarly the control is organized for the drives of other types.

- 25 The above formulas are used to develop algorithms for generation of the desired trajectories of motion in the Cartesian coordinate system and the control signals to the

exoskeleton drives and are implemented in software in the exoskeleton on-board controller.

Thus, through significant differences of this invention from the prior art:

– possibility is provided for assistance to the walking of users both with partial and complete loss of support-motor apparatus functions, wherein user motion is conducted according to the set by the exoskeleton walking pattern of a person without support-motor apparatus functional impairment with kinematic characteristics (ratio of shank length to femur length) close to the user kinematic characteristics;

– possibility is provided for recovery of the correct walking pattern of the user with the possibility to change using control panel such walking parameters as step length, leg rise height and walking rhythm;

– possibility is provided of various user motion modes on horizontal, inclined and stepped surfaces, as well as crossing over of obstacles and walking on the spot through setting the exoskeleton for motion along the desired trajectories corresponding to the motion on the selected surface;

– through setting of desired angular accelerations according to exponential second-order model with negative actual control parameters the possibility is provided of smooth and smooth motion along the desired trajectories of hip and ankle pivots set in the Cartesian coordinates.

The above results confirm the achievement in this invention of technical results in relation of enhancement of functional capabilities and improvement of ergonomic characteristics of the device.

Patent research conducted by the applicant showed that there are no analogues to the present significant differences.

CLAIMS

1. Method to define desired trajectories of the exoskeleton in the Cartesian coordinate system for movement in sagittal plane in pre-determined in advance motion mode of user with support-motor apparatus functional impairment using exoskeleton including pelvic section, left and right foot rests each of which consists of femoral and shank sections and foot steps, wherein the adjacent sections are connected using corresponding pivotal joints providing the possibility of their rotation in sagittal plane and equipped with corresponding sensors of relative angle rotation integrated in the current angles and angular velocities measurement unit, wherein hip and knee joints are configured motorized and equipped with corresponding drives, for example, electric drives, as well as on-board controller connected with sensors of relative angle rotation of adjacent sections and control inputs of the motorized joints drives, wherein according to the present method using motion capture system including serially connected measuring devices unit to collect and transfer the captured motion parameters data, captured motion parameters data processing unit and captured motion parameters storage unit, the output of which is connected to the output of motion capture system, ensure measuring of Cartesian coordinates of pre-selected human body points in the process of its motion, characterized in that the motion capture system is used as a part of the desired Cartesian trajectories parameters determination system, and a person without support-motor apparatus functional impairment is used to measure the Cartesian coordinates of the pre-selected body points, and the points of intersection between the hip joint axis and ankle joints axes, lying in the frontal plane, with sagittal plane are used as the pre-selected body points, the Cartesian coordinates of which are measured, depending on time in the form of trajectories along the axes of the Cartesian coordinates system of the above sagittal plane during motion of the above person for each of the pre-determined in advance motion mode, and saved in the captured motion parameters storage unit in the form of data arrays for each measured trajectory, wherein axis of ordinates of the above coordinates system of the sagittal plane is directed vertically, while axis of abscissas – along the course of exoskeleton motion, and further in the integrated into the desired Cartesian trajectories parameters determination system captured motion parameters processing unit, the input of which is connected to the output of the motion capture system, processing is conducted of parameters and/or interpolation coefficients of the captured motion calculating, based on the above table set arrays of the time functions of the Cartesian coordinates, the parameters and/or interpolation coefficients for each of the

chosen in advance smooth, interpolating the above trajectories, analytic function, differentiated at least twice,

for example, splines, including cubic splines, wherein the calculated parameters and/or interpolation coefficients are saved in the desired exoskeleton Cartesian trajectories parameters and/or interpolation coefficients storage unit, connected to the output of the captured motion parameters processing unit and integrated into the desired Cartesian trajectories parameters determination system the of the , wherein the above measurements, processing of data obtained as the result of these measurements and storage of these data processing results are conducted for groups of people with various ratios of shank length to the femur length, wherein preserving the data on the above ratios and shank length for each person in this group.

2. Method according to claim 1, **characterized** in that the captured motion parameters processing unit and the desired exoskeleton Cartesian trajectories parameters and/or interpolation coefficients storage unit are implemented in software in the desired Cartesian trajectories determination controller.

3. Method according to claim 1, **characterized** in that as the pre-determined in advance motion modes of a person without support-motor apparatus functional impairment are used the modes: "Walk on horizontal surface", "Go upstairs", "Go downstairs", "Walk up the inclined surface", "Walk down the inclined surface", "Cross over an obstacle", "Sit on a rest", "Stand vertically with straightened legs", "Stand up vertically with straightened legs from the "Sit on a rest" position", "Sit down on a rest from "Stand vertically with straightened legs".

4. Walking assistance device for a user with support-motor apparatus functional impairment in pre-determined in advance motion modes, comprising the exoskeleton of lower extremities, including pelvic section and left and right foot rests, each of which consists of femoral and shank sections and foot steps, wherein adjacent sections are connected using corresponding pivotal joints providing the possibility of their rotation in sagittal plane and equipped with corresponding sensors of relative angle rotation integrated in the current angles and angular velocities measurement unit, wherein hip and knee joints are configured motorized and equipped with corresponding drives, for example, electric drives, as well as on-board controller connected with sensors of relative angle rotation of adjacent sections and control inputs of the motorized joints drives, wherein the foot steps are equipped with foot rest reaction sensors integrated in the foot rest reaction measurement unit and mounted in the heel and toe-cap of the foot step, additionally walking assistance device comprises left and right hand rests and control

device including desired exoskeleton angles and angular velocity calculation unit, external
 moment evaluation unit and unit of calculation and generation of control signals to the
 exoskeleton drives connected to control inputs of corresponding drives, wherein the input
 of desired exoskeleton angles and angular velocity measurement unit is connected to the
 5 first input of the control device, the third input of which is connected to the output of
 current angles and angular velocity measurement unit characterized in that it is
 supplemented with external computer of assistant-specialist configured with provision to
 the assistant specialist of possibility to input into the exoskeleton on-board controller the
 ratio of shank length to femur length, shank length and mass-inertial characteristics of the
 10 user body segments with exoskeleton sections attached to them, motion mode selection
 and adjustment of such motion parameters as step length, leg rise height and walking
 rhythm, control panel configured with provision to the user of the possibility of motion
 mode selection and adjustment of such motion parameters as step length, leg rise height
 and walking rhythm, unit of current measurement in electric drives comprising first,
 15 second, third, fourth current sensors of, respectively, first, second, third, fourth electric
 drives, unit of desired trajectories generation in the Cartesian coordinates system
 configured to input to it and store in it time-dependent parameters and/or interpolation
 coefficients of the desired motion trajectories in the Cartesian coordinates system for pre-
 determined in advance motion modes, the first input of which is connected to the first
 20 output of control device, while the second input – to the output of the foot rest reaction
 measurement unit, the first output – is connected to the first input of the control device,
 and the second output is configured to be connected to the desired Cartesian trajectories
 parameters determination system, the output of which is configured to be connected to the
 third input of the desired Cartesian trajectories generating unit, the fourth input of which is
 25 configured to be connected to the output of the external computer of the assistant-
 specialist, wherein the control device is supplemented with a desired Cartesian trajectory
 accelerations generation unit, the first input of which is connected to the first input of the
 control device, the desired angular acceleration calculation unit, the first input of which is
 connected to the output of the desired trajectory acceleration generation unit, and the
 30 second input – to the output of the desired angles and angular velocities generation unit,
 exoskeleton drives angular acceleration calculation unit, wherein the first input of the
 exoskeleton drives angular acceleration calculation unit is connected to the output of the
 desired angular acceleration calculation unit, and the second input – to the output of the
 desired angles and angular velocity calculation unit, current exoskeleton Cartesian
 35 coordinates vector calculation unit, the input of which is connected to the third input of the
 control device, and the output – to the second input of desired Cartesian trajectories

accelerations generation unit, user torso angular motion evaluation unit, the input of which is connected to the output of the current exoskeleton Cartesian coordinates calculation unit, and the output – to the fourth input of the external moment evaluation unit, the fifth input of which is connected through the second input of the control device to the output of the foot rest reaction calculation unit, wherein the first input of the control signals generation unit is connected to the output of the external moment evaluation unit, the first input of which is connected to the output of the exoskeleton drives angular acceleration calculation unit, and the second input – to the third input of the control device also connected with the third input of the exoskeleton drives angular acceleration calculation unit and to the second input of the control signal generation unit, the third input of which is connected to the output of the exoskeleton drives angular acceleration calculation unit, the fourth input – to the fourth input of the control device also connected with the third input of external moment evaluation unit, and the output to the output of the control device connected to control inputs of the drives equipped with current sensors of the electric drives of the motor current measurement unit, wherein the fourth input of the control device is connected to the output of the electric motors current measurement unit.

5. Device according to claim 4, **characterized** in that desired Cartesian trajectories generation unit and control device are implemented in software in the on-board controller of the exoskeleton.

6. Device according to claim 4, **characterized** in that as the pre-determined in advance motion modes of a person with support-motor apparatus functional impairment are used the modes: "Walk on horizontal surface", "Go upstairs", "Go downstairs", "Walk up the inclined surface", "Walk down the inclined surface", "Cross over an obstacle", "Sit on a rest", "Stand vertically with straightened legs", "Stand up vertically with straightened legs from the "Sit on a rest" position", "Sit down on a rest from "Stand vertically with straightened legs".

7. Control method of the walking assistance device for a user with support-motor apparatus functional impairment in pre-determined in advance motion modes comprising exoskeleton of lower extremities, including pelvic section, left and right foot rest, each of which consists of femoral and shank sections and foot steps, wherein adjacent sections are connected using corresponding pivotal joints providing the possibility of their rotation in sagittal plane and equipped with sensors of relative angle rotation integrated in the current angles and angular velocity measurement unit, wherein hip and knee pivotal joints are configured motorized and equipped with corresponding drives, for example, electric drives, as well as on-board controller connected with sensors of relative angle rotation of adjacent sections and control inputs of motorized joints drives, wherein foot steps are

equipped with foot rest reaction sensors integrated in the foot rest reaction measurement unit and mounted in the heel and toe-cap of the foot step, additionally, walking assistance device comprises left and right hand rests and control device comprising desired exoskeleton angles and angular velocity calculation unit, external moment evaluation unit and unit of calculation and generation of control signals to the exoskeleton drives connected to the control inputs of corresponding drives, wherein the input of desired exoskeleton angles and angular velocity calculation unit is connected to the first input of the control device, the third input of which is connected to the output of the current angles and angular velocity measurement unit, wherein according to this method the current angles and angular velocities in hip and knee joints and foot rest reaction forces are measured, characterized in that the walking assistance device for a user with support-motor apparatus functional impairment is supplemented with external computer of assistant-specialist with provision to the assistant-specialist of the possibility of input to the on-board controller the ratio of shank length to femur length, shank length and mass-inertial characteristics of the user body segments with exoskeleton sections attached to them, motion mode selection and adjustment of such motion parameters as step length, leg rise height and walking rhythm, control panel configured with provision to the user of the possibility of motion mode selection and adjustment of such motion parameters as step length, leg rise height and walking rhythm, unit of current measurement in electric drives comprising first, second, third, fourth current sensors of, respectively, first, second, third, fourth electric drives, unit of desired trajectories generation in the Cartesian coordinates system configured to input to it and store in it the time-dependent parameters and/or interpolation coefficients of the desired motion trajectories in the Cartesian coordinates system for pre-determined in advance motion modes, the first input of which is connected to the first output of control device, while the second input – to the output of the foot rest reaction measurement unit, the first output is connected to the first input of the control device, and the second output is configured to be connected to the input of the desired motion trajectories parameters determination system in the Cartesian coordinates system, the output of which is configured to be connected to the third input of the desired Cartesian trajectories generation unit, the fourth input of which is configured to be connected to the output of the external computer of the assistant-specialist, wherein the control device is supplemented with a unit of acceleration for motion along the trajectories in the Cartesian coordinates system, the first input of which is connected to the first input of the control device, desired angular acceleration calculation unit, the first input of which is connected to the output of the desired trajectory acceleration generation unit, and the second input – to the output of desired angles and angular velocities generation unit,

exoskeleton drives angular acceleration calculation unit, wherein the first input of the
 exoskeleton drives angular acceleration calculation unit is connected to the output of the
 desired angular acceleration calculation unit, and the second input – to the output of the
 desired angles and angular velocity calculation unit, current exoskeleton Cartesian
 5 coordinates vector calculation unit, the input of which is connected to the third input of the
 control device, and the output – to the second input of desired Cartesian trajectories
 accelerations generation unit, housing angular motion evaluation unit, the input of which is
 connected to the output of the current exoskeleton Cartesian coordinates calculation unit,
 and the output – to the fourth input of the external moment evaluation unit, the fifth input of
 10 which is connected through the second input of the control device to the output of the foot
 rest reaction calculation unit, wherein the first input of the control signals generation unit is
 connected to the output of the external moment evaluation unit, the first input of which is
 connected to the output of the exoskeleton drives angular acceleration calculation unit,
 and the second input – to the third input of the control device also connected with the third
 15 input of the exoskeleton drives angular acceleration calculation unit and to the second
 input of the control signal generation unit, the third input of which is connected to the
 output of the exoskeleton drives angular acceleration calculation unit, the fourth input – to
 the fourth input of the control device also connected with the third input of external
 moment evaluation unit, and the output to the output of the control device connected to
 20 control inputs of the drives equipped with current sensors of the electric drives of the
 motor current measurement unit, wherein, the fourth input of the control device is
 connected to the output of electric motors current measurement unit, wherein, according
 to the proposed control method of the walking assistance device for a user with support-
 motor apparatus functional impairment, the ratio of shank length to femur length, shank
 25 length are measured and mass-inertial characteristics of the user body segments
 measurement is conducted directly or indirectly with exoskeleton sections attached to
 them and using the external computer of the assistant-specialist and the fourth input of the
 unit of the desired trajectories generation in the Cartesian coordinate system of the on-
 board controller are input into the unit of the desired trajectories generation in the
 30 Cartesian coordinate system of the on-board controller and through it – into the system of
 determination of the desired motion trajectories parameters in the Cartesian coordinate
 system such measured user parameters as shank length, the ratio of shank length to
 femur length and mass-inertial characteristics of the user body segments with exoskeleton
 put on, and according to the specified ratio of shank length to femur length of the user
 35 data obtaining from the system of desired motion trajectories determination in the
 Cartesian coordinate system is conducted, which are input in the desired trajectories

generation unit in the Cartesian coordinate system in the form of arrays of parameters (coefficients) of interpolation of interpolating functions obtained for a person without support-motor apparatus functional impairment during his/her movement in each of the pre-determined in advance modes, mode is set using the external computer of the assistant-specialist or control panel from the series of pre-determined in advance modes, numeric values of interpolating functions are calculated and scaled by way of their multiplication by the coefficient equal to the ratio between the shank length of the user with support-motor apparatus functional impairment and the shank length of a person without support-motor apparatus functional impairment, desired step parameters are set from control panel or external computer of the assistant-specialist by way of scaling of the interpolating trajectories corresponding to the user represented in the Cartesian coordinate system by corresponding coefficients, as well as for changing of the time of leg carrying over (walking rhythm) – by way of scaling of these functions time axis, wherein, scaling is conducted both for each particular coordinate and for their combinations, in the current exoskeleton Cartesian coordinate vector calculation unit, the vector of the current exoskeleton Cartesian coordinates is calculated, based on the obtained measurements of angles and angular velocities in hip and knee joints, in the unit of desired trajectories generation in the Cartesian coordinates system the desired trajectories of hip and ankle pivots of the exoskeleton depending on time, by way of calculation based on the stored time-dependent parameters (coefficients) values arrays of the numeric values of interpolating functions recorded in the Cartesian coordinate system; the vector of the desired angles and angle velocities is calculated based on the previously calculated values of the vector of the desired trajectories and their first derivatives, in the unit of desired motion acceleration generation along the trajectories in the Cartesian coordinate system the vector of desired acceleration for motion along the trajectory in the Cartesian coordinate system is calculated based on the previously calculated values of the position and velocity vector in the Cartesian coordinate system and the vector of desired trajectories and their first and second derivatives, in the desired angles and angular velocities generation unit the vector of desired angular acceleration is calculated based on the vector of desired acceleration for motion along the trajectory in the Cartesian coordinate system and vector of desired angles and angular velocities, in the desired exoskeleton drives angular acceleration generation the vector of desired angular acceleration to the exoskeleton drives is calculated, based on previously calculated vector of desired angular velocities, vector of desired angles and angular velocities, vector of current angles and angular velocities value in the pivotal joints in the external moment evaluation the vector of external moment is calculated based on previously calculated

vector of desired angular accelerations to the drives, vectors of current angles and angular acceleration values in pivotal joints, vector of foot rest reaction, measured vector of the exoskeleton drives currents and taking into account mass-inertial characteristics of the user body segments with exoskeleton put on, and the vector of control signals to the drives of exoskeleton is calculated in generated in the unit of control signals generation to the drives of exoskeleton based on previously calculated vector of current angles values, external moment vector and measured vector of current angles and angular velocities values in pivotal joints, vectors of the exoskeleton drives currents.

8. Method according to claim 7, **characterized** in that as the pre-determined in advance motion modes of a person with support-motor apparatus functional impairment are used the modes: "Walk on horizontal surface", "Go upstairs", "Go downstairs", "Walk up the inclined surface", "Walk down the inclined surface", "Cross over an obstacle", "Sit on a rest", "Stand vertically with straightened legs", "Stand up vertically with straightened legs from the "Sit on a rest" position", "Sit down on a rest from "Stand vertically with straightened legs".

9. Method according to claim 7, **characterized** in that the unit of desired motion trajectories generation in the Cartesian coordinate system and control device are implemented in software in the on-board controller of the exoskeleton.