

THREAD PROTECTOR

RELATED APPLICATION

The present application claims the benefit of 35 U.S.C. 111(b) provisional application Serial No. 60/086,446 filed May 22, 1998 and entitled Thread Protector, hereby incorporated
5 herein by reference.

BACKGROUND OF THE INVENTION

The invention relates to protectors for protecting the ends of pipe, and particularly for protecting the threads on the ends of pipe.

Pipes, such as pipes used for oil and gas drilling and production, are often produced in
10 sections and are connectable at their ends. One type of connection involves the use of a male threaded portion at one end (the pin end) of a section of pipe that is threadingly engageable with a female threaded portion at the end (the box end) of another section of pipe.

The ends of the pipe, including the threads, are subject to damage when not in actual use, such as from contact with other objects, or from being dropped, during transportation
15 and storage. Such damage may render the pipe faulty or unusable, resulting in delay, hardship and increased expense. Devices known as "thread protectors" are commonly used to protect the ends of the pipe, particularly the pipe threads thereon, from such damage. A "pin end" thread protector is connected to and protects the pin end of the pipe and a "box end" thread protector is connected to and protects the box end of the pipe. The thread
20 protectors are designed to prevent damage to the respective pipe ends when the pipe impacts other objects, the ground or otherwise is subjected to external impact. Example prior art thread protectors are disclosed in U. S. Patents 4,957,141; 5,195,562; and 5,244,015, all to Dreyfuss et al., and 4,809,752 to Strodter, all of which are hereby incorporated herein by reference in their entireties.

25 An industry standard for thread protectors for premium pipe is the "Shell®" test. A specification for the Shell test entitled "Shell Oil Specification for Thread Protectors March 1988" is attached hereto and hereby incorporated herein by reference in its entirety. The Shell test is also described in Technical Paper ADC/SPE 17209 entitled "Performance Evaluation of Commercially Available Thread Protectors," authored by E.J.C. Spruijt and
30 also hereby incorporated herein by reference in its entirety (the first two pages of the Paper are attached hereto). The Shell test subjects the thread protector and pipe to an impact energy to determine if the thread protector being tested can protect the pipe ends from damage. One type of Shell test simulates installing the thread protector on the pipe, raising the pipe off the

ground, and then dropping the pipe axially to evaluate the effectiveness of the thread protector by determining whether the end of the steel pipe was damaged. The Shell test requires that the thread protector prevent the pipe ends from damage during different tests at varying temperatures. Since the pipe is used in various environments and thus exposed to a wide range of temperatures, the test is performed at varying temperatures, such as 150° F, 70° F or ambient, and -50° F, to insure that the thread protector will protect the pipe when exposed to heat or cold over time. For testing pipes having nominal outer diameters of between 4 inches and 8 ¾ inches, for example, the thread protector and pipe may be subjected to 1200 ft/lbs of energy at temperatures of 150°F and again at 70° F (ambient). A third test subjects the thread protector and pipe to 600 ft/lbs of energy at a temperature of -50° F. For example, a section of pipe having a nominal outer diameter of between about 4.0 inches and about 8 3/4 inches with a weight of 430.4 lbs is dropped 33.6 inches transmitting 1205 ft/lb of impact energy onto the thread protector and pipe end. To determine the protective capacity of the protector, the pipe is inspected for damage. Damage may include dents, damaged threads, out-of-roundness, or other damage affecting the use of the pipe in the field. Although it is preferred that the thread protector not be damaged, damage to the thread protector is not a criteria in the Shell test. The Shell test for larger diameter pipe requires a larger impact, such as 1500 ft/lbs at 150° F and 70° F or ambient, and 800 ft/lbs at -50° F.

The thread protector must prevent substantial impact energy from reaching the pipe end to adequately protect the pipe from the impact energy. Prior art thread protectors have been designed as strong as possible to withstand the anticipated impact energy. Thus, prior art thread protectors are large, sturdy and rigid members which will prevent damage to the pipe and to the thread protector itself.

To provide this strength and rigidity, many prior art thread protectors are constructed of a composite of steel and plastic. One of the most commercial thread protectors is manufactured by Drilltec Patents and Technologies Company, Inc. and is known as Drilltec's ESPS™ protector. This protector includes an outer steel sleeve crimped over an inner plastic member. The steel sleeve has the effect of providing stiffness and rigidity to the protector, enabling it to withstand impact energy. The Drilltec protector is disclosed in U.S. Patents 4,957,141; 5,195,562; and 5,244,015. Other prior art thread protectors, such as Drilltec's STP™, Drilltec's SSP™ and Molding Specialties, Inc.'s Magnum model thread protectors are constructed of plastic and often include additives such as fibers or particles of another material, but without a steel sleeve. Figures 1A and 1B illustrate a pin end thread protector

and a box end thread protector, respectively, similar to that manufactured by Molding Specialties, Inc. for a pipe having a nominal outer diameter of 7 inches.

The prior art thread protectors are believed to have various disadvantages. Because these protectors are large and heavy, they require a substantial quantity of material, typically both steel and plastic, for their construction. The more material that is required to produce the protector, the greater the manufacturing cost. Prior art protectors are thus expensive. Further, the larger, bulkier and heavier the protector, the more difficult and time consuming the handling of the protectors and the greater the need for special handling equipment, particularly for large diameter pipe thread protectors.

Additionally, various prior art thread protectors constructed without a steel sleeve are believed to warp and become out-of-round or deformed, thus making it difficult or impossible for them to be installed onto the pipe end, thereby decreasing their usefulness. Further, typical prior art thread protectors constructed primarily of plastic are believed to be generally ineffective at withstanding significant impact energy. In particular, typical prior art thread protectors constructed of all plastic material, or plastic containing particles of other material, are believed to generally not pass the Shell test without being beefed up in size so as to use a substantial amount of material, thus substantially raising the cost of manufacturing the protector.

Thus, there remains a need for a thread protector capable of protecting pipe ends that requires less material and is thus more cost effective to manufacture (material and labor) than prior art thread protectors. Preferably, the thread protector does not include a steel sleeve and may be made of a material lighter than steel. Ideally, the thread protector could be designed to plastically deform under impact so that the impact energy is transformed into internal friction and thermal energy; the thread protector thus using up or substantially reducing the transmitted energy and preventing the energy from reaching or damaging the threads of the attached pipe. Especially well received would be a thread protector that is made substantially of plastic and that passes the Shell test. Further, the thread protector is preferably reduced in size and material than many prior art thread protectors, thereby reducing shipping and handling requirements.

The present invention overcomes one or more of these deficiencies in the prior art.

SUMMARY OF THE INVENTION

In accordance with the invention, there is provided a thread protector for protecting threads on the end of a pipe, the thread protector having a base portion with a first end having

a threaded portion extending therefrom and threadably engageable with the pipe and a second end having an elongated annular bumper extending axially therefrom. The elongated bumper has an average length of at least about 1.1 inches and preferably at least about 2 inches. The ratio of the length to the average width of the elongated bumper is at least about 1.2 and preferably about 3 or more.

The base, threaded portion and elongated annular bumper may be constructed primarily of non-metallic material, such as high density polyethylene material. The base, threaded portion and elongated annular bumper may be constructed of material that has a minimum izod impact yield, or break point of about 5.6 ft-lb/inch. The thread protector is preferably capable of passing the Shell test.

The elongated bumper preferably has an inner taper forming a conical interior portion. The elongated bumper may include a plurality of cut-outs each having an average width of between approximately 1/32 inch and approximately 1/8 inches. The cut-outs may be slots that intersect the terminal end of the elongated bumper.

The elongated bumper may include at least two bumper arms. The elongated bumper may include at least one base tear starter.

In an alternate embodiment, the bumper may have at least one taper along its length forming an angle of at least about 1.8 degrees. In another embodiment, the ratio of the average length of the elongated bumper to the maximum outer diameter of the thread protector is at least about 0.20. In yet another embodiment, the ratio of the average length of the bumper to the nominal outer diameter of the pipe may be at least about 0.22.

Other objects and advantages of the invention will be apparent from the following description.

BRIEF DESCRIPTION OF THE DRAWINGS

For a detailed description of preferred embodiments of the invention, reference will now be made to the accompanying drawings wherein:

Figure 1A is a partial cross-sectional view of a prior art pin end thread protector;

Figure 1B is a partial cross-sectional view of a prior art box end thread protector;

Figure 2 is a partial cross-sectional view of one embodiment of a pin end thread protector made in accordance with the present invention;

Figure 3 is a enlarged view of a portion of the thread protector Figure 2 showing the base and thread members of the protector;

Figure 4 is a side view of an alternative embodiment of the terminal end of the bumper of the pin end thread protector shown in Figure 2;

Figure 5 is a side view of another alternative embodiment of the bumper of the pin end thread protector shown in Figure 2 having open cut-outs made in accordance with the present invention;

Figure 6 is a side view of still another alternative embodiment of the bumper of the pin end thread protector shown in Figure 2 having enclosed cut-outs made in accordance with the present invention;

Figure 7 is a partial cross-sectional view of another embodiment of the pin end thread protector of Figure 2 with no cover;

Figure 8 is a partial cross-sectional view of still another embodiment of the pin end thread protector of Figure 2 with a disc-like cover;

Figure 9 is a graph showing the percent strain of a test piece of Phillips 66 Marlex HXM 50100 polyethylene material as stress (psi) is applied to the material to its yield point;

Figure 10 is an enlargement of the graph shown in Figure 9 for percentage strain in the range of 0 to 20% for the Phillips 66 Marlex HXM 50100 polyethylene material as stress (psi) is applied to the material;

Figure 11 is a partial cross-sectional view of one embodiment of a box end thread protector made in accordance with the present invention;

Figure 12 is a perspective view of a pin end thread protector made in accordance with the present invention showing the dissipation of impact energy in the protector after impact;

Figure 13 is a partial cross-sectional view of another embodiment of a pin end thread protector having multiple bumpers and base tear starters made in accordance with the present invention;

Figure 14 is a perspective view of the thread protector of Figure 13;

Figure 15 is a partial cross-sectional view of another embodiment of a box end thread protector having multiple bumpers and base tear starters made in accordance with the present invention;

Figure 16 is a perspective view of the thread protector of Figure 15;

Figure 17 is a partial cross-sectional view of another embodiment of a pin end thread protector made in accordance with the present invention;

Figure 18 is a partial cross-sectional view of another embodiment of a box end thread protector made in accordance with the present invention;

Figure 19 is a partial cross-sectional view of still another embodiment of a pin end thread protector made in accordance with the present invention;

Figure 20 is a partial cross-sectional view of still another embodiment of a box end thread protector made in accordance with the present invention;

5 Figure 21 is a partial cross-sectional view of yet still another embodiment of a box end thread protector made in accordance with the present invention;

Figure 22 is a partial cross-sectional view of still yet another embodiment of a box end thread protector made in accordance with the present invention.

DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

10 Preferred embodiments of the invention are shown in the above-identified figures and described in detail below. In describing the preferred embodiments, like or identical reference numerals are used to identify common or similar elements. The figures are not necessarily to scale and certain features and certain views of the figures may be shown exaggerated in scale or in schematic form in the interest of clarity and conciseness.

15 Referring now to Figure 2, there is shown one embodiment of a pin end thread protector 50 of the present invention capable of protecting male threads 42 on the exterior 44 of a pin end 46 of pipe 48. Pipe 48 shown in Figure 2 has a nominal outer diameter of 7 inches. The thread protector 50 includes a base 56, a box 52 projecting axially from the base 56 in one direction and engageable with the pin end 46 of pipe 48, and a bumper 62
20 projecting axially from the base 56 in the opposite direction. The box 52 extends from one side of the base 56 to one end 50a of the protector 50, while the bumper 62 extends from the other side of the base 56 to the other end 50b of the protector 50.

The base 56 is an annular portion located generally at the mid-portion of protector 50 and proximate to the terminal end 49 of the pipe 48. The base 56 may, for example, have a
25 generally rectangular cross-section with a thickness 56a and a height 56b, and includes an internal annular surface, or seat, 57 for seating against the terminal end 49 of the pipe 48 when the protector 50 is installed on the pipe 48. The seat 57 preferably has a radial width which is at least as great as the radial width of the terminal end 49 of pipe 48.

The bumper 62 of the present invention is an elongated sleeve-like annular member
30 extending from the base 56 and having a height, or length, L and a thickness W. The length L of the bumper 62 is measured from the terminal end 64 of the bumper 62 to the other end 63 of the bumper 62 adjacent the base 56. It should be appreciated that the other end 63 of the bumper 62 is not distinct and is loosely defined as the point where the bumper 62 first

begins a taper A₂ as hereinafter defined. As shown in Figure 4, the terminal end 64 of the bumper 62 need not be even, forming varying lengths L₁, L₂ . . . L_n around the terminal end 64. In such an embodiment, the reference "L" refers to the average length of the varying lengths L₁, L₂ . . . L_n. If the bumper 62 has differing thicknesses W₁, W₂ . . . W_n, or is tapered, as shown for example in Figure 2, the reference "W" refers to an average thickness or width of bumper 62.

The elongated bumper 62 may have an inner taper along its length L forming a conical portion and thus have a cross-sectional area that is less than 100% of the rectangular cross-sectional area of the length L times the greatest thickness W of the bumper 62. For example, the bumper 62 may have a total taper along its length L forming an angle of greater than about 1.8 degrees. The exemplary bumper 62 of Figure 2 possesses a cross-sectional area that is less than about 80% of the total rectangular cross sectional area between ends 63, 64; an outer taper A₁ extending from about the mid-point 62c of the length L to the terminal end 64 of the bumper 62 of between about 4.0 - 5.0 degrees; a first inner tape A₂ extending from the end 63 of the bumper 62, or from the base 56, to about the mid-point 62c of the length L of between about 6.0 - 6.5 degrees; and a second inner taper A₃ of between about 8.0 - 8.5 degrees extending from about the mid-point 62c to the terminal end 64 of the bumper 62. Alternately, the bumper 62 may be viewed as having a non-uniform cross-section. In the embodiment of Figure 2, for example, the bumper 62 has thicknesses ranging from a thickness W₃ of about 0.55 inches, to a thickness W₂ of about 0.46 inches to a thickness W₁ of about 0.20 inches. The average thickness W of the bumper 62 is about 0.41 inches. It should be understood, however, that the thread protector 50 of the present invention is not limited to tapered elongated bumpers 62 or to any of the above specific examples.

The thread protector 50 is preferably constructed of a material that plastically deforms under impact so that the impact energy is transformed into internal friction and thermal energy; the thread protector 50 thus using up or substantially reducing the transmitted energy and preventing the energy from reaching or damaging the threads of the attached pipe 48. The thread protector 50 is thus preferably constructed of a material that will absorb substantial energy when subjected to external forces, such as the impact energy during the Shell test. The material absorbs the impact energy by deflecting, deforming or flexing and/or yielding or failing, each of these requiring energy. In the preferred embodiment of Figure 2, the thread protector 50 is constructed primarily of a material that has a substantial izod impact strength, as defined in the ASTM guidelines Designation D 256-93a entitled Standard Test Methods

for Determining the Pendulum Impact Resistance of Notched Specimens of Plastics, attached hereto and hereby incorporated herein by reference, and a substantial compressive strength, as defined in the ASTM guidelines Designation D 695-96 entitled Standard Test Method for Compressive Properties of Rigid Plastics, attached hereto and hereby incorporated herein by reference. Materials with these characteristics provide good energy absorption. See e.g. pages 11 and 12 of the Marlex Phillips 66 Brochure entitled "Engineering Properties of Marlex Resins", hereby incorporated herein by reference in its entirety. Other relevant reference materials include the Marlex Phillips 66 Brochures entitled "Polyethylene TIB 1 Properties & Processing" and "Blow Molding Resins: Information on Marlex Polyethylene Resins."

The thread protector 50 is preferably constructed primarily of a high density polyethylene material, such as Phillips 66 Marlex® HHM 5502 BN or HXM 50100. The nominal physical properties and mechanical properties of these materials are set forth on an attachment entitled "Nominal Physical Properties", hereby incorporated herein by reference. The Izod Impact yield, or break point of HHM 5501 is 5.6 ft-lb./inch at room temperature. Typical values for the tensile strength and elongation of various materials are also attached hereto and are hereby incorporated herein by reference. Additional information about HXM 50100 in the Marlex Brochure entitled "Polyethylene Data Sheet Marlex HXM 50100" is also attached hereto and hereby incorporated herein by reference.

Referring now to Figures 9 and 10, there are shown stress-strain graphs with curves 80a, 80b for the material HXM 50100. The curves 80a, 80b show properties for yield strength and ultimate strength of this material for use in the construction of a thread protector 50 made in accordance with the present invention. The curves 80a, 80b illustrate a tensile yield of 4100 psi, a tensile break of 2800 psi and an elongation at yield 9.7% and break 861 psi. The area 82a, 82b under the curves 80a, 80b represents the impact energy loss, or absorbed, to produce a given amount of deformation in the material. (Area = Force x Distance (or Work)) The graphs illustrate that the HMX 50100 material does not completely fail, but will deform and use up the energy from an external impact. Thus, external impact energy expended in a thread protector 50 constructed of this material in accordance with the present invention tends to absorb sufficient energy from the impact to dissipate a sufficient amount of that energy to avoid damage to the end of the attached pipe. Such characteristics tend to be maintained in the material throughout the range of temperatures and impact energy of the Shell test. It should be appreciated that the energy absorption, deflection and failure

characteristics of various materials, such as plastics, are difficult to measure with precision and may vary among even samples of the same type of material.

In other embodiments, the thread protector 50 may be constructed of low density polyethylene. Low density polyethylene generally possesses desirable deformation
5 characteristics in accordance with the present invention through low temperature ranges, such as -50°F . For yet another example, the protector 50 may be constructed of a plastic, such as high density polyethylene, with one or more additives such as a metal (e.g. aluminum), or metal and other material, dispersed in the plastic.

Referring again to Figure 2, the dimensions of bumper 62 may vary with the size of
10 the pipe 48 to be protected. The larger the pipe 48, the greater the protection required because of its increased weight. The following preferred dimensions have been found for pipe 48 having a nominal outer diameter 48a of 7.0 inches. The length L of the elongated bumper 62 made in accordance with the present invention is preferably at least about 1.1 inches and more preferably is at least about 2.0 inches. Further, the length L and thickness W
15 of the elongated bumper 62 preferably have a ratio of the length L to thickness W (L/W) of at least about 1.2 and preferably at least 3 or more. In the embodiment of Figure 2, for example, the length L is about 2.0 inches and the (average) thickness W is about 0.41 inches; the ratio L/W being about 4.88. Thus, the L and W may be varied so as to maintain the preferred L/W ratio. Additionally, the length L of the bumper 62 plus the height 56b of the base 56 is
20 preferably at least 1.75 inches. In the embodiment of Figure 2, for example, the height 56b is about .38 inches; $L + 56b$ thus being about 2.38 inches. The length L may also be based on its ratio with the outer diameter O_d of the thread protector 50. The ratio of length L to the outer diameter O_d of the thread protector 50 (L/O_d) may, in accordance with the present invention, be greater than about 0.15. For example, the outer diameter O_d of the protector 50
25 of Figure 2 is about 7.5 inches. The ratio L/O_d is thus about 0.27. Another method for measuring the length L of elongated bumper 62 may be the ratio of the length L to the nominal outer diameter 48a of the pipe 48 to be protected; the ratio $L/48a$ in accordance with the present invention being at least about 0.15. For example, the protector 50 of Figure 2, being designed for a pipe 48 having an nominal outer diameter of about 7.0 inches, has a ratio
30 $L/48a$ of about 0.29.

The material for the protector 50 may also vary with the size of the pipe 48 to be protected and the ultimate location for shipment of the pipe. The dimensions of the bumper 62 will also be influenced by the properties of the material selected for the protector 50, such

as the impact resistance, energy absorption, compressive strength, stiffness, temperature durability, tensile yield or other pertinent capabilities of the material of which the protector 50 is made. The preferred material for protector 50 is Phillips 66 Marlex HHM 5502 BN. For example, a protector 50 made of the preferred material and having a bumper 62 with a length of at least about 1.1 will pass the 1200 ft/lb Shell® test.

It should be understood that the material for protector 50 and the dimensions of bumper 62 need not meet more than one of the above criteria in accordance with the present invention; and, in each case, is not limited to the specific examples of the preferred embodiments provided. Further, it should be understood that the present invention is not limited to thread protectors 50 that pass the Shell test.

Referring now to Figures 2 and 3, the box 52, having ends 52a and 52b, is capable of threadingly engaging the pipe threads 42 of pin end 46. For example, the box 52 is shown having an internal bore 54 with a plurality of thread members 55 formed at least partially thereon. The thread members 55 are formed to be threadingly engageable with the pipe threads 42 and each have an approximate height H_1 and thickness T_1 (Figure 3). The height H_1 of thread member 55 is the distance from the crest to the root of the thread member 55 and the thickness T_1 is the distance between the centers of adjacent roots on each side of a thread member 55. The bore 54 and thread members 55 may be formed in any suitable shape and configuration to be threadingly matable with the pipe threads 42 on pipe 48. For example, the height H_1 and thickness T_1 of thread members 55 may be dimensioned to fit a certain type of pipe threads 42. It should be appreciated that pipe threads 42 may have one or more steps and may be straight or tapered.

The box 52 may also include an annular recess 58 formed in the bore 54 of the box 52 adjacent to the thread member 55a that is closest to the base 56. In addition, a second annular recess 58c may be formed in the bore 54 adjacent to the thread member 55b that is closest to the end 52a of box 52. The recesses 58 and 58c may be formed with any desired dimensions suitable for use with the present invention. In the embodiment of Figures 2 and 3, the recess 58 has a depth 58a of approximately equal to or slightly greater than the height H_1 of thread member 55. As an example, the thread members 55 in thread protector 50 of Figure 2 (for use with a pipe 48 having an nominal outer diameter 48a of about 7.0 inches) may be formed with a thickness T_1 of about 0.200 inches and a height H_1 of about 0.063, and the recess 58 formed with a depth 58a of approximately 0.200 inches. The width 58b of recess 58 may also be specifically dimensioned, such as 0.063 inches.

The inclusion of recess 58 in the box 52 of protector 50 allows formation of the thread members 55 in the box 52 such as by allowing a threading tool, an example being a tap device (not shown), to be moved in and out of the bore 54. Without the recess 58, as the threading tool completes the threading of the bore 54, a hair, string or shaving of material may be formed and remain in the box 52 after the threading tool is removed. Once the pipe 48 is threadingly engaged with the base 54, the shaving may become embedded in the pipe threads 42 and may prevent the pipe 48 from later being threaded into another device, such as a pipe joint (not shown), or may remain attached to the bore 54 and be very difficult to remove therefrom. The recess 58 may also serve as a grease pocket for retaining grease carried on the pipe threads 42.

Referring now to Figure 12, in operation, upon impact to the elongated bumper 62 and pipe end (not shown), the energy E from the impact spreads through the material of the bumper 62, such as in a fan-like pattern beginning at the terminal end 64. As the energy E propagates through the material of bumper 62 towards bumper end 63, the energy is absorbed and thus dissipates as the bumper 62 flexes, deforms and deflects. Because each of these processes requires energy, the amount of energy which can reach the pipe end (not shown) and cause damage is lessened. The energy of a relatively small external impact force to the terminal end 64 may be absorbed or dissipated in only a portion of the elongated bumper 62. A larger impact to the terminal end 64 or to another location on the elongated bumper 62 increases the flexing, deforming, and deflecting down the length L of the elongated bumper 62, which increases the absorption of energy. If the impact energy is great, it may be sufficient to crack, tear or fracture the bumper 62, and possibly even the base 56 or box 52. This failure of the material significantly enhances the absorption of energy such that when the impact energy reaches the pipe 48 (Figure 2) it is insufficient to damage the pipe 48.

In another aspect of the present invention, it may be desirable to configure the thread protector 50 to avoid premature cracking, yielding or failure. The protector 50 may, for example, be susceptible to yielding and failure (and thus premature failure) at locations on the protector 50 having a stress concentration, or radical change in stiffness, such as at abrupt changes in the geometry of the protector 50. Depending on various factors, such as, for example, the shape and configuration of the protector 50, the type of material used to construct the protector 50 and the size of the pipe 48 engaged by the protector 50, it may be desirable to make gradual transitions in stiffness across the thread protector 50, and to remove or reduce stress concentrations in the protector 50. For example, the thread protector

50 may be generally formed with slopes or tapers at various locations where abrupt geometric changes in the protector 50 occur. For another example, where stress concentrations may exist, such as at corners formed in the thread protector 50, additional corners may be formed proximate to the existing corners to reduce the stress concentration at each corner.

5 The embodiment of Figure 2 has specific features that assist in avoiding premature failure. The recess 58 may be a stress concentration location and thus a location on the protector 50 susceptible to failure. To assist in reducing that susceptibility, a groove 66 may be formed in the protector 50 proximate to the recess 58, such as an annular groove 67 formed into the cover 81. Further, the depth 66a (Figure 3) of the groove 66 may, if desired,
10 be minimized, effectively increasing the thickness of the base 56 and generally strengthening the protector 50 in that area.

 Additionally, an annular shoulder 68 may be formed between the groove 66 and recess 58, as shown, for example, in Figure 2. Increasing the height 68a of the shoulder 68 will generally increase the strength of the protector 50 at base 56 and assist in preventing
15 premature fracturing of the protector 50. The shoulder 68 may function as the seat 57 for seating against the terminal end 49 of the pipe 48. Further, the protector 50 may be configured such that the shoulder 68 forms a substantial seal with the terminal end 49 of the pipe 48, preventing moisture from entering the pipe end 46 when the pipe 48 is engaged with a protector 50 having a cover 81. In such instance, the width 68b of the shoulder 68 (Figure
20 3) may be formed to correspond with the thickness of the pipe end 49. In other configurations, the protector 50 may be formed so that the shoulder 68 does not seat against the terminal end 49 of the pipe 48 or form a seal therewith. The further the shoulder 68 is from the pipe 48, the better the energy absorption by the protector 50.

 For another example of a feature that assists in avoiding premature failure, the area of
25 intersection 70 (Figure 2) of the elongated bumper 62 and the base 56 may be a location of significant change in stiffness. In the embodiment of Figure 2, the end 63 of the elongated bumper 62 is connected to the base 56 at the area of intersection 70. To assist in reducing the dramatic change in stiffness, the base 56 may be formed with a relatively significant width 56a and thickness 56b. Further, the end 63 of the bumper 62 may be tapered, having an
30 increased width W_3 proximate to the intersection 70, assisting in reducing stress concentrations and decreasing the extreme stiffness of the protector 50 in that area.

 Referring again to Figure 2, the thread protector 50 may be constructed with any desirable overall dimensions and material, such as to correspond with different sizes of pipes

48. For example, different sizes of thread protectors 50 may be made to fit pipes 48 having nominal outer diameters 48a ranging from 2 3/8 inches to 20 inches. Further, the thread protector 50 may be constructed to have a minimal weight. For example, a thread protector 50 capable of passing the Shell test and protecting threads 42 on the end 46 of a premium
5 grade pipe 48 having an nominal outer diameter 48a of about 7.0 inches may be formed having a weight of about 2.43 pounds.

The thread protector 50 may be formed by any suitable manufacturing process, such as by injection molding. The thread protector 50 may, for example, be made as a single integral molding. It should be taken into account that the type of manufacturing process used
10 may affect the energy absorption, deflection and failure characteristics of the thread protector 50.

Now referring to Figures 5 and 6, the elongated bumper 62 may include a plurality of cut-outs 72 to increase energy absorption of the protector 50. The cut-outs 72 provide a stress concentration to encourage the material of the protector 50 proximate to the cut-outs 72
15 to tear upon impact, thereby redistributing the impact energy over a large volume of protector material and also using up impact energy, further minimizing the transmission of impact energy to the attached pipe (not shown). The cut-outs 72 may be formed in any suitable shape, quantity and location in the wall of the bumper 62. In Figure 5, for example, each cut-out 72 preferably forms a slot 76 that intersects the terminal end 64 of the elongated bumper
20 62 at its end 74. The slots 76 are thus open at their ends 74. Each slot 76 extends through the thickness of the bumper 62 and has a narrow width (not shown). Each cut-out 72 of the embodiment of Figure 5, for example, has an average width of between approximately 1/32 inch and approximately 1/8 inch.

The corners C at the ends 73, 74 of the cut-outs 72 may be left sharp and not rounded
25 to enhance the cracking and tearing of the material. In the embodiment of Figure 5, the cut-outs 72 extend partially across the length L of the elongated bumper 62 and terminate at angles 78 at their ends 73.

In Figure 6, the cut-outs 72 are internal cracks, or slots, 76a having ends 73a, 74a both disposed in the elongated bumper 62. The internal slots 76a are thus closed and have corners
30 C formed at ends 73a, 74a. The internal slots 76a are shown also extending through the thickness of the bumper 62, having narrow widths (not shown) and having corners C that are sharp and not rounded.

Referring to Figure 8, in another aspect of the invention, the bumper 62 may include two or more installation slots 62d, which may be used with a tool for threading and unthreading the protector 50 from the pipe 48, as is well known in the art. The embodiment of Figure 8, for example, includes four installation slots 62d that are about 0.75 inches wide and about 0.50 inches deep, which are engageable with the tool, such as a standard installation bar, for rotating the protector 50 on and off the pipe 48.

Referring now to Figures 2, 7 and 8, the central opening 51 of the protector 50 may be entirely or partially covered or uncovered. For example, the protector 50 may be completely open, such as shown in Figure 7. In other embodiments, as shown for example in Figure 8, the protector 50 may include a central cover 81 extending from the base 56. The central cover 81 may be formed to partially or completely cover the opening 51, such as the disc-like cover 81a of Figure 8. For example, when the central cover 81 completely covers the opening 51, debris cannot enter the pipe end 46 from outside the protector 50. In yet other configurations, as shown, for example in Figure 2, the central cover 81 may be a recessed member 82. The recessed member 82 may be formed with any desirable shape or configuration. In Figure 2, the recessed member 82 is a cup-like member 84 extending from the base 56 that allows the thread protector 50 and pipe 48 to be lifted. A device, such as a hook (not shown), may be inserted into the cup-like member 84 when the pipe 48 and connected thread protector 50 are in a non-vertical position to lift and/or lower the protector 50 and pipe 48.

Referring now to Figure 11, an embodiment of a box end thread protector 100 capable of protecting female threads 42 on the interior 45 of a box end 47 of pipe 48 made in accordance with the present invention is shown. The above description of the pin end thread protector 50 and its use generally applies equally to the protector 100, except as otherwise described herein. The thread protector 100 includes a base 156, a pin 152 projecting axially from the base 156 in one direction and engageable with the box end 47 of the pipe 48, and an elongated bumper 162 projecting axially from the base 156 in the opposite direction. The pin 152 thus extends to the one end 100a of the protector 100, while the bumper 162 extends to the other end 100b of the protector 100.

The base 156 is a portion of the protector 100 located proximate to the terminal end 49 of the pipe 48. The base 156 may include an annular surface, or seat, 57 that faces and may abut the terminal end 49 of the pipe 48 when the pipe 48 is engaged with the protector 100. The seat 57 preferably has a radial width which is at least as large as the radial width of

the terminal end 49 of the pipe 48. This allows seat 57 to protect the terminal end 49 from damage. The base 156 may be formed with a generally rectangular, or square, cross section, having a height 156b extending from the seat 57 to the end 163 of the bumper 162 proximate to the beginning of the taper, and a thickness 156a, such as shown in Figure 11. In other
5 embodiments (not shown), the base 156 may be merely the cross-section of the protector 100 adjacent the location of the seat 57, in which instances the elongated bumper 162 extends substantially directly from the seat 57.

The length L of the bumper 162 of protector 100 Figure 11 is measured from the terminal end 164 of the bumper 162 to the opposite end 163 of the bumper 162, or to the base
10 156. Again it should be appreciated that the other end 163 of the bumper 162 is not distinct and is loosely defined as the point where the bumper 162 first begins a taper As as hereinafter defined. If the bumper 162 has differing thicknesses $W_1, W_2 \dots W_n$, or is tapered, as shown for example in Figure 11, the reference "W" refers to the average thickness of bumper 162.

The length L of the elongated bumper 162 made in accordance with the present
15 invention may be at least about 1.5 inches. Further, the length L of the bumper 162 plus the height 156b of the base 156 may be at least 1.8. In the preferred embodiment of Figure 11, for example, the length L of bumper 162 is at least about 1.8 inches and the length L of the bumper 162 plus the height 156b of the base 156 is at least about 1.9 inches and preferably over 2.2.

The dimensions of the elongated bumper 162 may vary with the size of the pipe 48 to
20 be protected. The following preferred dimensions have been found for pipe 48 having a nominal outer diameter of 7.0 inches. The length L and thickness W of the elongated bumper 162 made in accordance with the present invention may be formed such that the ratio of the length L to thickness W (L/W) is at least about 2.0 and preferably over 3. In the embodiment
25 of Figure 11, for example, the length L is about 1.8 inches and the average thickness W is about 0.45 inches; the ratio L/W thus being about 4.0. The length L may also be measured based on its ratio with another variable, such as for example the outer diameter O_d of the thread protector 100. The ratio of length L to the outer diameter O_d of the thread protector 100 (L/O_d) may, in accordance with the present invention, be greater than about 0.20. For
30 example, the outer diameter O_d of the protector 100 of Figure 11 is about 7.7 inches. The ratio L/O_d is thus about 0.23. Another method for measuring the length L of elongated bumper 162 may be the ratio of the length L to the nominal outer diameter 48a of the pipe 48 to be protected; the ratio $L/48a$ in accordance with the present invention being at least about

0.22. For example, the protector 100 of Figure 11 is matable with a pipe 48 having an nominal outer diameter 48a of about 7.0 inches; the ratio $L/48a$ thus being about 0.26.

It should be understood that the bumper 162 need not meet more than one of the above criteria in accordance with the present invention; and, in each case, is not limited to the specific examples provided.

Still referring to Figure 11, the elongated bumper 162 may be at least partially tapered along its length L and have a cross-sectional area that is less than 100% of the rectangular cross-sectional area of the length L times the greatest thickness W of the bumper 162. For example, the bumper 162 may have a total taper along its length L forming an angle of at least about 1.8 degrees. The exemplary bumper 162 of Figure 11, for example, possesses a cross-sectional area that is about 70% of the total rectangular cross-sectional area between ends 163, 164; an outer taper A₄ extending from about the mid-point 162c of the length L to the terminal end 164 of the bumper 162 of between about 4.0 - 5.0 degrees, and an inner taper A₅ of between about 12.0 - 13.0 degrees extending from the terminal end 164 to the end 163 of the bumper 162. In another embodiment, the bumper 162 may be formed with tapers similar to tapers A₁, A₂ and A₃ of bumper 62 described above with respect to protector 50 of Figure 2. Alternately, the bumper 162 may be viewed as having a non-uniform cross-section. In the embodiment of Figure 11, for example, the bumper 162 has thicknesses ranging from a thickness W₃ of about 0.68 inches to a thickness W₁ of about 0.20 inches. The average thickness W of the bumper 162 is about 0.45 inches. It should be understood, however, that the thread protector 100 of the present invention is not limited to tapered elongated bumpers 162 or to any of the above specific examples.

The pin 152, having ends 152a, 152b, respectively, is capable of at least partially engaging the box end 47 and pipe threads 42 of pipe 48. For example, the pin 152 of the embodiment of Figure 11 is shown having an outer surface 154 with a plurality of thread members 155 formed at least partially thereon. The thread members 155 are formed to be matable with the pipe threads 42 and may be shaped and sized similarly as described above with respect to thread members 55 of protector 50.

Still referring to Figure 11, the thread protector 100 may be constructed in any desirable overall size, such as to correspond with different sizes of pipes 48. For example, different sized thread protectors 100 may be made to fit pipes 48 having nominal outer diameters 48a of ranging from 2 3/8 inches to 20 inches. Further, the thread protector 100 may be constructed to have a minimal weight. For example, the thread protector 100 for

passing the Shell test and protecting premium quality pipe having an nominal outer diameter 48a of about 7.0 inches may be formed having a weight about 1.75 pounds.

The option of including a groove 66 and shoulder 68 as described above with respect to protector 50 (Figure 2) is not applicable to thread protector 100. Further, referring still to
5 Figure 11, the central opening 51 of the protector 100 may be entirely or partially covered or uncovered, similarly as described above with respect to protector 50. In the embodiment of Figure 11, the central cover 81 extends from the end 152a of pin 152.

Figures 17-22 illustrate exemplary embodiments of the present invention for pipes of different diameters. Figure 17 illustrates a pin thread protector 400 for the pin end 46 of a
10 pipe 48 having a nominal diameter 48a of 5.5 inches. The bumper length L is approximately 2.0 inches and the average bumper width W is approximately 0.48 inches providing a W/L ratio of 4.19. The outside diameter O_d is approximately 6.20 inches providing a L/O_d of approximately 0.32 and a L/48a of approximately 0.36. The base length 56b is approximately 0.20 inches providing an impact travel distance D of 2.19 inches between
15 terminal bumper end 64 and shoulder 57 adjacent the terminal end 49 of the pipe 48. End width W₁ is approximately 0.32 inches and the base width W₃ is approximately 0.63 inches. The cross-sectional area of bumper 62 with the inner conical portion 402 is approximately 75% of a rectangular area of base width W₃ times bumper length L.

Figure 18 illustrates a box thread protector 410 for the box end 47 of a pipe 48 having
20 a nominal diameter 48a of 5.5 inches. The bumper length L is approximately 1.20 inches and the average bumper width W is approximately 0.38 inches providing a W/L ratio of 3.19. The outside diameter O_d is approximately 6.27 inches providing a L/O_d of approximately 0.19 and a L/48a of approximately 0.22. The base length 156b is approximately 1.08 inches providing an impact travel distance D of 2.28 inches between terminal bumper end 164 and
25 shoulder 157 adjacent the terminal end 49 of the pipe 48. Shoulder 157 is formed in part by an annular retention flange 159 extending outwardly from base 156 to ensure that the terminal end 49 of the pipe 48 is covered by shoulder 157 and therefore protected. It should be appreciated that the outer diameter O_d of pipe 48 will vary due to differences in thread types and pipe dimensions. End width W₁ is approximately 0.25 inches and the base width
30 W₃ is approximately 0.50 inches. The cross-sectional area of bumper 62 with the inner conical portion 402 is approximately 75% of a rectangular area of base width W₃ times bumper length L.

Figure 19 illustrates a pin thread protector 420 for the pin end 46 of a pipe 48 having a nominal diameter 48a of 7-5/8 inches. The bumper length L is approximately 2.06 inches and the average bumper width W is approximately 0.52 inches providing a W/L ratio of 3.94. The outside diameter is approximately 8.14 inches providing a L/O_d of approximately 0.25 and a L/48a of approximately 0.27. The base length 56b is approximately 0.43 inches providing an impact travel distance D of 2.50 inches between terminal bumper end 64 and shoulder 157 adjacent the terminal end 49 of the pipe 48. End width W₁ is approximately 0.37 inches and the base width W₃ is approximately 0.68 inches. The cross-sectional area of bumper 62 with the inner conical portion 402 is approximately 71% of a rectangular area of base width W₃ times bumper length L.

Figure 20 illustrates a box thread protector 430 for the box end 47 of a pipe 48 having a nominal diameter 48a of 7-5/8 inches. The bumper length L is approximately 1.94 inches and the average bumper width W is approximately 0.51 inches providing a W/L ratio of 3.80. The outside diameter O_d is approximately 7.66 inches providing a L/O_d of approximately 0.25 and a L/48a of approximately 0.25. The base length 156b is approximately .29 inches providing an impact travel distance D of 2.23 inches between terminal bumper end 164 and shoulder 157 adjacent the terminal end 49 of the pipe 48. End width W₁ is approximately 0.30 inches and the base width W₃ is approximately 0.72 inches. The cross-sectional area of bumper 62 with the inner conical portion 402 is approximately 71% of a rectangular area of base width W₃ times bumper length L.

Figure 17 is also illustrative of a pin thread protector for the pin end 46 of a pipe 48 having a nominal diameter 48a of 9-5/8 inches. The bumper length L is approximately 2.09 inches and the average bumper width W is approximately 0.59 inches providing a W/L ratio of 3.56. The outside diameter O_d is approximately 10.71 inches providing a L/O_d of approximately 0.20 and a L/48a of approximately 0.22. The base length 56b is approximately 0.46 inches providing an impact travel distance of 2.55 inches between terminal bumper end 64 and shoulder 157 adjacent the terminal end 49 of the pipe 48. End width W₁ is approximately 0.43 inches and the base width W₃ is approximately 0.74 inches. The cross-sectional area of bumper 62 with the inner conical portion 402 is approximately 66% of a rectangular area of base width W₃ times bumper length L.

Figure 21 illustrates a box thread protector 440 for the box end 47 of a pipe 48 having a nominal diameter 48a of 9-5/8 inches. The bumper length L is approximately 2.06 inches and the average bumper width W is approximately 0.52 inches providing a W/L ratio of 3.96.

The outside diameter O_d is approximately 9.86 inches providing a L/O_d of approximately 0.21 and a $L/48a$ of approximately 0.21. The base length 156b is approximately 0.20 inches providing an impact travel distance D of 2.26 inches between terminal bumper end 164 and shoulder 157 adjacent the terminal end 49 of the pipe 48. End width W_1 is approximately 0.25 inches and the base width W_3 is approximately 0.79 inches. The cross-sectional area of bumper 62 with the inner conical portion 402 is approximately 66% of a rectangular area of base width W_3 times bumper length L .

Figure 17 also illustrates a pin thread protector for the pin end 46 of a pipe 48 having a nominal diameter 48a of 13-3/8 inches. The bumper length L is approximately 2.03 inches and the average bumper width W is approximately 0.55 inches providing a W/L ratio of 3.71. The outside diameter O_d is approximately 14.02 inches providing a L/O_d of approximately 0.14 and a $L/48a$ of approximately 0.15. The base length 56b is approximately 0.41 inches providing an impact travel distance of 2.44 inches between terminal bumper end 64 and shoulder 157 adjacent the terminal end 49 of the pipe 48. End width W_1 is approximately 0.40 inches and the base width W_3 is approximately 0.70 inches. The cross-sectional area of bumper 62 with the inner conical portion 402 is approximately 70% of a rectangular area of base width W_3 times bumper length L .

Figure 22 illustrates a box thread protector 450 for the box end 47 of a pipe 48 having a nominal diameter 48a of 13-3/8 inches. The bumper length L is approximately 1.79 inches and the average bumper width W is approximately 0.44 inches providing a W/L ratio of 4.03. The outside diameter O_d is approximately 13.91 inches providing a L/O_d of approximately 0.13 and a $L/48a$ of approximately 0.13. The base length 156b is approximately 0.47 inches providing an impact travel distance of 2.26 inches between terminal bumper end 164 and shoulder 157 adjacent the terminal end 49 of the pipe 48. End width W_1 is approximately 0.25 inches and the base width W_3 is approximately 0.64 inches. The cross-sectional area of bumper 62 with the inner conical portion 402 is approximately 70% of a rectangular area of base width W_3 times bumper length L .

Figures 13-16 illustrate other exemplary embodiments of the present invention. The pin end thread protector 250 of Figures 13 and 14 is useful for protecting male threads 42 on the exterior 44 of a pin end 46 of pipe 48, while the box end thread protector 300 of Figures 15 and 16 is useful for protecting female threads 42 on the interior 45 of a box end 47 of pipe 48. The protectors 250, 300 of the embodiment of Figures 13-16 are generally similar to the

exemplary embodiments of protectors 50 and 100 described above with respect to Figures 2-12, except as otherwise described herein.

Referring to Figure 13, the base 256 is a portion of the protector 250 located proximate to the terminal end 49 of the pipe 48. The base 256 may be formed with a generally rectangular, or square, cross section. In the embodiment of Figure 13, for example, the base 256 has a thickness 256a and a height 256b. The base 256 may include a seat 257 that abuts the terminal end 49 of the pipe 48 when the pipe 48 is engaged with the protector 250. In the embodiment of Figures 13 and 14, a cover 281 is shown extending from the base 256. The box 252 is capable of threadingly engaging the pipe threads 42 of pin end 46. For example, the box 252 is shown having an internal bore 254 with a plurality of thread members 255 formed at least partially thereon.

The outer surface 253 of the base 256 of protector 250 may be formed with one or more base tear starters 259. The base tear starters 259 may be formed in any suitable shape, quantity and location on the base 256. For example, the base tear starters 259 in the embodiment of Figure 13 include a pair of annular channels 260a, 260b formed into the outer surface 253 around the circumference of the base 256 and extending partially into the thickness 256a of the base 256. However, the protector 250 may instead be formed with one, or more than two, base tear starters 259 or channels 260a, 260b.

The elongated bumper 262 of protector 250 may include two or more axially extending bumper arms 286. In the embodiment of Figure 13, two bumper arms 286 are included, the bumper arms 286 being annular outer and inner elongated ring shaped portions 288a, 288b. Further, the two or more bumper arms 286 may be formed with different lengths L. For example, the radially outermost ring shaped portion 288a of the embodiment of Figure 13 has a length L₁, and the ring shaped portion 288b has a length L₂ that is smaller length L₁.

Upon impact to the bumper 262, the impact energy may be transmitted between the two or more bumper arms 286. In Figures 13 and 14, for example, the outer annular elongated ring shaped portion 288a may flex, bend or deform upon external impact thereto. The impact energy may travel around the outer ring shaped portion 288a and transfer to the inner ring shaped portion 288b, causing it to flex, bend or deform. Before reaching the base 256 or box 252, the energy may be substantially dissipated or absorbed.

If impact energy reaches the base 256, base tear starters 259 provide stress concentrations to encourage the material of the protector 250 proximate to the starters 259 to

flex or tear, thereby redistributing the impact energy over a large volume of base 256 material and also using up impact energy, further minimizing the transmission of impact energy to the attached pipe (not shown). With the embodiment shown in Figures 13-14, for example, the protector 250 may crack or fail at the annular channels 260a, 260b, instead of allowing
5 energy to be transmitted to the pipe 48.

The above description of the pin end thread protector 250 made with reference to Figures 13 and 14 and its use applies generally equally to the box end protector 300, such as shown in Figures 15 and 16, except as otherwise described herein. The thread protector 300 (Figure 15) includes a base 356, a pin 352 projecting axially from the base 356 in one
10 direction and engageable with the box end 47 of the pipe 48, and an elongated bumper 362 projecting axially from the base 356 in the opposite direction. The pin 352 thus extends to one end 300a of the protector 300, while the bumper 362 extends to the other end 300b.

Still referring to Figure 15, the base 356 is a portion of the protector 300 located proximate to the terminal end 49 of the pipe 48. The base 356 may be formed with a
15 generally rectangular, or square, cross section. In the embodiment of Figure 15, for example, the base 356 has a thickness 356a and a height 356b. The base 356 may include a seat 357 that abuts the terminal end 49 of the pipe 48 when the pipe 48 is engaged with the protector 300. In the embodiment of Figures 15 and 16, a cover 381 is shown extending from the base 356.

The base of annular channel 260b and the seat 357 form an annular retention flange
20 359 having a depth and a height in proportion to the thickness of the pin 352 and its terminal end 49. The retention flange 359 remains in place, in tact, and against the terminal end 49 of pin 352 upon impact by another object against the end of thread protector 300. The protector 300 is easily removed from the pipe 352 since no major stresses pass through the
25 retention flange 359. With the retention flange 300 in place, there is no damage to the terminal end 49 of the pipe 352. Also the retention flange 359 prevents the ingress of foreign matter and therefore prevents environmental damage.

The pin 352, having ends 352a, 352b, is capable of at least partially engaging the box end 47 and pipe threads 42 of pipe 48. For example, the pin 352 of the embodiment of Figure
30 15 is shown having a plurality of thread members 355 formed at least partially thereon. The thread members 355 may be formed similarly as described above with respect to protector 100 of Figure 11.

While preferred embodiments of the present invention have been shown and described, modifications thereof can be made by one skilled in the art without departing from the spirit or teachings of this invention. The embodiments described herein are exemplary only and are not limiting. The particular features of the embodiments described above are exemplary of the invention and may be useful with different embodiments not necessarily having all of the same features. For example, the base 56 of the protector 50 of the embodiment of Figure 2 may be formed with base tear starters 259 (Figure 13) and the elongated bumper 262 of the embodiment of Figure 14 may be formed with cut-outs 72 (Figure 5). Many variations and modifications are possible and are within the scope of the invention. Accordingly, the scope of protection is not limited to the embodiments described herein.

**CLAIMS**

I claim:

1. A protector for protecting the end of a pipe, comprising:
 - a body;
 - 5 said body having a connector to connect with the pipe;
 - said body having a bumper;
 - said bumper having a configuration and being made of a substantially non-metallic material; and
 - 10 said configuration and material being capable of dissipating 1200 ft/lbs of energy at ambient and at 150°F.
2. The protector of claim 1 wherein said material is a high density polyethylene.
3. The protector of claim 2 wherein said polyethylene has the izod impact strength and the compressive properties of HHM 5502.
4. The protector of claim 1 wherein said bumper is a generally sleeve-like member
15 having a length of at least 2 inches.
5. The protector of claim 1 wherein
 - said body has a base portion;
 - said connector is a threaded portion extending axially from a first end of said base portion and engageable with the pipe, and
 - 20 said bumper is an elongated annular member extending axially from a second end of said base portion and having an average length and average thickness, said average length being at least about 1.1 inches and the ratio of said average length to said average thickness being at least about 1.2.
6. The thread protector of claim 5 wherein said elongated annular bumper is conical.
- 25 7. The thread protector of claim 5 wherein said base, threaded portion and elongated annular bumper are constructed primarily of non-metallic material.
8. The thread protector of claim 5 wherein said base, threaded portion and elongated annular bumper pass the Shell test.
9. The thread protector of claim 5 wherein said base, threaded portion and elongated
30 annular bumper are constructed primarily of high density polyethylene material.
10. The thread protector of claim 5 wherein said base, threaded portion and elongated annular bumper are constructed of material that has an izod impact break point of about 5.6 ft-lb/inch.



11. The thread protector of claim 5 wherein said elongated bumper includes a plurality of cut-outs.
12. The thread protector of claim 11 wherein said cut-out has an average width of between approximately 1/32 inch and approximately 1/8 inch.
- 5 13. The thread protector of claim 11 wherein said elongated bumper has a terminal end and said cut-out comprises a slot intersecting with said terminal end of said elongated bumper.
14. The thread protector of claim 5 wherein said elongated bumper includes at least two bumper arms.
- 10 15. The thread protector of claim 5 wherein said elongated bumper includes at least one base tear starter.
16. A thread protector for protecting threads on the end of a pipe, the thread protector having a maximum outer diameter, comprising:
- a base portion having a first length and first and second ends;
 - 15 a threaded portion extending axially from said first end of said base portion and threadably engageable with the pipe;
 - an elongated annular bumper extending axially from said second end of said base portion and having an average length; and
 - said first length and said average length totaling at least two inches.
- 20 17. A thread protector for protecting threads on the end of a pipe comprising:
- a base portion having first and second ends;
 - a threaded portion extending axially from said first end of said base portion and threadably engageable with the pipe; and
 - an elongated annular bumper extending axially from said second end of said
 - 25 base portion and having an average length and an average width, wherein the ratio of said average length to said average width is at least 2.
18. A thread protector for protecting threads on the end of a pipe, comprising:
- a base portion having first and second ends;
 - a threaded portion extending axially from said first end of said base portion
 - 30 and threadably engageable with the pipe; and
 - an elongated annular bumper extending axially from said second end of said base portion, said elongated annular bumper having a maximum length and a



maximum width, said elongated annular bumper having a cross-section which is at least 80% less said maximum length times said maximum width.



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(57) Abstract

A thread protector (50) for protecting threads (42) on the end of a pipe (48) includes a base portion (84), a threaded portion (54) extending axially from a first end of the base portion (52a) and threadably engageable with the pipe and an elongated annular bumper (62) extending axially from a second end (50b) of the base portion. The elongated bumper (62) has an average length and width such that the ratio of the length to the width is at least 2. The base and elongated bumper have a total length of at least two inches.

