

Composite article comprising aerogel particles and ceramic fibers

The present invention relates to a method for the preparation of a composite article (in particular a thin composite article) comprising aerogel particles and ceramic fibers as well as to a composite article obtainable by this method.

In many industrial and construction applications such as passive fire protection for structural steel beams, thermal insulation capability and temperature resistance at very high temperatures are required. UL1709 (Rapid Rise Fire Tests of Protection Materials for Structural Steel) requires a test temperature of 1093°C and ISO834 (cellulosic fire curve) requires temperature to reach 1110°C after a test period of 180 min. Novel insulation materials with thermal insulation capability and temperature resistance at elevated temperatures higher than 1100°C need to be developed.

In particular, it is desirable to have very thin insulating materials, often with a thickness not exceeding 3 mm, with thermal insulation capability and fire resistance. Such insulating materials are required in many industrial sectors, such as

- gaskets for ovens, stoves, heaters and other appliances
- non-ferrous ingot mould liners
- molten aluminium transfer systems
- refractory backup insulation in ladles, glass tanks, high-temperature furnaces, as well as in automotive and aerospace sectors, such as heat shields, cell-to-cell thermal runaway propagation barriers for EV batteries, battery pack and module fire and thermal protection.

Currently, various grades of ceramic fiber papers are applied as insulation materials for applications above 1000°C. On the one hand, the variations in chemical composition of ceramic fiber papers lead to different temperature resistance. Thus, ceramic fiber papers based on alkaline earth silicate (AES) are resistant to operating temperatures up to 1200°C, while ceramic fiber papers based on aluminum oxide (AO) can withstand 1600°C. On the other hand, the various chemical compositions lead to significant differences in material costs of ceramic fiber papers. The costs of ceramic fiber papers based on aluminum oxide are typically about 20 times the costs of ceramic fiber papers based on alkaline earth silicate. A sharp increase in material cost can be observed with the increase in the temperature resistance requirement.

In view of the prior art, the present invention serves to provide ceramic fiber papers with improved thermal insulation capability and temperature resistance at reduced costs.

The present inventors surprisingly found that this problem can be solved by incorporating aerogel into ceramic fiber papers after the fiber papers have been formed. This can be achieved by preparing an aerogel composition comprising an aerogel powder and an organic solvent and injecting or impregnating it into the fiber paper. Due to this approach, the use of binders can be reduced or even entirely avoided, while still obtaining an excellent attachment of the aerogel powder to the fibers of the fiber paper.

Thus, in a first aspect, the present invention relates to a method for the preparation of a composite article comprising aerogel particles and ceramic fibers, the method comprising:

- providing a fibrous article comprising ceramic fibers,
- providing an aerogel composition comprising an aerogel powder and an organic solvent,
- combining the fibrous article and the aerogel composition, and
- partially or completely removing the organic solvent to obtain the composite article.

The present invention furthermore relates to a composite article obtainable by this method.

In addition, the invention relates to a composite article comprising aerogel particles and ceramic fibers, wherein the composite article is obtainable by injecting or impregnating an

aerogel composition comprising an aerogel powder and an organic solvent, and optionally inorganic opacifiers and/or mineral fillers, into a fibrous article comprising ceramic fibers, and partially or completely removing the organic solvent to obtain the composite article.

In still a further aspect, the present invention relates to a composite article comprising aerogel particles and ceramic fibers, wherein one or more of the following requirements (i) to (vi) are fulfilled:

- (i) the composite article contains less than 15% by weight organic compounds;
- (ii) at least 50% of the fibers in the composite article have a length of 5 mm or more;
- (iii) the composite article contains less than 10% by weight binder;
- (iv) the composite article exhibits a total weight loss in thermogravimetric analysis (TGA) when being heated in a nitrogen atmosphere from 30°C to 1100°C with a temperature increase of 10 °C/min of less than 35% by weight;
- (v) the weight ratio of the one or more aerogels to the one or more fibers (aerogel/fiber) in the composite article is 1:8 or higher;
- (vi) the composite article has a burn-through time of 60 minutes or more, wherein the burn-through resistance is determined using the composite article in the form of a DIN A4 sheet with a thickness of 1 to 3 mm and treating the composite article at the centre of its first major surface with a flame having a temperature of 1400°C, using a soldering torch, wherein the burn-through time is the duration from start of the flame treatment until the centre of the second major surface reaches a temperature of 1000°C;

BRIEF DESCRIPTION OF THE FIGURES

- Figure 1: Aerogel-incorporated ceramic fiber paper (raw paper thickness 1 mm) (Example 1-1) a) top view; b) side view
- Figure 2: Aerogel-incorporated ceramic fiber paper (raw paper thickness 3 mm) (Example 1-3) a) top view; b) side view
- Figure 3: Soldering torch test setup
- Figure 4: Blank ceramic fiber paper (raw paper thickness 2 mm) after 20 sec flaming; a) front view; b) back view

- Figure 5: Aerogel-incorporated ceramic fiber paper (raw paper thickness 1 mm) after 60 min flaming; a) front view; b) back view
- Figure 6: Aerogel-incorporated ceramic fiber paper (raw paper thickness 3 mm) after 60 min flaming; a) front view; b) back view
- Figure 7: Comparison of the temperature increase of the back side middle part among a blank ceramic fiber paper (raw paper thickness 2 mm) and aerogel-incorporated ceramic fiber papers (raw paper thickness 1 mm and 3 mm).
- Figure 8: Blank ceramic fiber paper (raw paper thickness 1 mm) after 10 sec flaming; a) front view; b) close-up view of the burnt-through flamed area
- Figure 9: Blank ceramic fiber paper (raw paper thickness 3 mm) after 8 sec flaming; a) front view; b) close-up view of the burnt-through flamed area
- Figure 10: Aerogel-incorporated ceramic fiber paper (raw paper thickness 2 mm) after 60 min flaming; a) front view; b) close-up view of the flamed area
- Figure 11: Comparison of the temperature increase on the non-exposed side between a blank ceramic fiber paper (raw paper thickness 1 mm) and an aerogel-incorporated ceramic fiber paper (raw paper thickness 1 mm).
- Figure 12: Comparison of the temperature increase on the non-exposed side between a blank ceramic fiber paper (raw paper thickness 2 mm) and an aerogel-incorporated ceramic fiber paper (raw paper thickness 2 mm).
- Figure 13: Comparison of the temperature increase on the non-exposed side between a blank ceramic fiber paper (raw paper thickness 3 mm) and an aerogel-incorporated ceramic fiber paper (raw paper thickness 3 mm).

DEFINITION OF THE TERMS USED HEREIN

In the context of the present invention, the term "composite article" is to be understood as referring to any article which comprises one or more aerogel particles and one or more ceramic fibers. Thus, the term "composite" does not imply any limitations other than the presence of aerogel particles and ceramic fibers, which together form the article. It is to be understood that the aerogel particles and the ceramic fibers are not spatially distant. Rather, the aerogel particles are typically between and around the ceramic fibers. Preferably, the one

or more fibers form a woven or non-woven structure, in and around which the aerogel particles are present.

The composite article is typically in the form of batting, nonwovens, mats, felts or blankets, such as needled fiber blankets. It is preferably a nonwoven fiber blanket or a needled fiber blanket, wherein the aerogel particles are present. The term "nonwoven" is to be understood as also including needled fiber blankets. The composite article preferably has a thickness in the range of less than 3 mm, preferably in the range of 0.001 to less than 3 mm, more preferably in the range of 0.01 to 2.5 mm, even more preferably in the range of 0.01 to 2 mm. The extension in the other two dimensions is preferably each at least 5 times the thickness. It is to be understood that the term "dimension" as used herein refers to the three known space dimensions which are orthogonal to each other (such as understood in "3-dimensional").

The term "batting" as used herein refers to a layer or sheet of fibrous material, the fibrous material typically comprising the ceramic fibers.

The term "nonwoven" refers to any material containing fibers which is neither woven nor knitted.

The term "nonwoven fiber blanket" is to be understood as relating any material containing fibers which is neither woven nor knitted, wherein the material is in the form of a blanket.

The term "needled fiber blanket" is to be understood as relating to any material containing fibers wherein the fibers are needled and wherein the material is in the form of a blanket.

As used herein, the term "blanket" typically refers to an article which extends into one dimension less than in the other two dimensions. Preferably, it refers to an article which extends in one dimension only up to 1000 mm, preferably up to 500 mm, more preferably up to 100 mm, while extending at least 5 times as much in each of the other two dimensions. In other words, the term "blanket" typically refers to flat articles, or oblong articles. Preferably the term "blanket" refers to articles having a thickness in the range of less than 3 mm which are sometimes also referred to as "paper".

Unless otherwise explicitly indicated, the use of singular or plural forms should be understood as allowing the presence of "one or more" of the nouns being in singular or plural form. In particular, the term "fibrous article comprising ceramic fibers" refers to a "fibrous article comprising one or more ceramic fibers". Similarly, the term "aerogel composition comprising an aerogel powder and an organic solvent" is to be understood as also including the case where more than one (type of) aerogel powder and/or more than one (type of) organic solvent are comprised in the aerogel composition. Mixtures of different types of aerogel powders and/or mixtures of different types of organic solvents may be used.

As used herein, the term "aerogel" refers to a porous material derived from a gel, in which the liquid component of the gel has been replaced with a gas essentially without collapse of the gel structure. Preferably, the "aerogel" is a silica aerogel. Such silica aerogels typically have a density of 0.1 g/cm³ or less, preferably 0.05 g/cm³ or less, and can be prepared by the well-known Stöber process. In the present invention, the "aerogel" is preferably a silica aerogel which is obtainable according to the process described in EP 2 722 311 A2, preferably as defined in claim 22 thereof.

In the present invention, the term "aerogel particle" preferably refers to silica aerogel particles which are obtainable according to the process described in EP 2 722 311 A2, preferably as defined in claim 22 thereof. Aerogel particles suitable for use in the present invention are, e.g., commercially available as "Jios AeroVa", wherein the "D20 Grade" is preferred. "Jios AeroVa D20 Grade" is described as having a D95 particle size range of less than 20 µm, a bulk density of 0.03 to 0.1 g/cm³, a thermal conductivity of 0.017 to 0.022 W/m·K, a surface area of 600 to 800 m²/g, and a porosity of more than 90%.

The term "heterophase reaction" preferably refers to any reaction conducted in a system containing more than one phase e.g. in a system composed of two non-mixable phases i.e. an aqueous phase and a phase which is not mixable with the aqueous phase, which is preferably a non-polar solvent phase. The reactions i.e. the creation of the first structures start at the interface between the different phases. Accordingly, it does not relate to reactions in which

all reactants are dissolved in the same solvent. An example of a "heterophase reaction" is an emulsion reaction, suspension reaction or dispersion reaction.

The term "ceramic" preferably refers to any material which is inorganic, non-metallic and preferably amorphous. It typically relates to one or more inorganic materials selected from oxides, nitrides and carbides, including any mixtures thereof. Preferably, the "ceramic" material contains at least 90 wt.-% (preferably at least 95 wt.-%, more preferably 99 wt.-%) of a total of one or more oxides, nitrides and/or carbides of silicon, aluminium, cerium, zirconium and/or alkaline earth metal(s).

The term "fiber" as used herein preferably refers to an article which extends in a first dimension at least 10 times more than in any of the other two dimensions. The first dimension preferably corresponds to the length direction of the fiber.

The term "fibrous article" refers to any article comprising one or more fibers. Examples therefore include fiber sheets, batting, nonwovens, mats, felts and needled fiber blankets. Preferred examples are a nonwoven fiber blanket or a needled fiber blanket. The fibrous article preferably has a thickness in the range of less than 3 mm, preferably in the range of 0.001 to less than 3 mm, more preferably in the range of 0.01 to 2.5 mm, even more preferably in the range of 0.01 to 2 mm, while extending at least 5 times as much in each of the other two dimensions.

As used herein, the term "aerogel composition" relates to any mixture comprising an aerogel powder and an organic solvent. Preferably, the "aerogel composition" is a mixture comprising the aerogel powder dispersed in an organic solvent. In other words, the "aerogel composition" is preferably an "aerogel dispersion".

The term "dispersion" as used herein preferably relates to a mixture wherein solid particles of one material are dispersed in a continuous phase of another material which is liquid. The terms solid and liquid as used herein refer to the state of a material at a temperature of 25°C and a pressure of 1 atm. Being "dispersed" preferably describes a state where the particles do not readily settle in the continuous phase of the liquid.

As used herein, the term "organic solvent" refers to any organic compound which is liquid at a temperature of 20°C and a pressure of 1 atm. Preferred examples of organic solvents include hydrocarbon solvents and alcohols including any mixtures thereof. Hydrocarbons are understood to be organic compounds consisting of carbon and hydrogen atoms.

The term "organic compound" as used herein relates to any compounds containing at least one carbon-hydrogen bond.

Terms such as "comprise" or "contain", such as in "A comprises B", are used herein to express an open definition of a composition etc. Accordingly, "A comprises B" is to be understood as indicating that A comprises at least B but may furthermore contain any number and amount of other components. In contrast, the term "consists of" such as in "A consists of B" typically indicates that A does not contain components other than B.

Terms such as "preferably" indicate that a certain feature may or may not be fulfilled. Such terms therefore precede optional features. Generally, if the feature is fulfilled, it is expected that additional beneficial effects may result.

The term "injecting" as used herein refers to the action of introducing (typically with force) a fluid (such as the aerogel composition) into a solid material (such as the fiber-containing article). A suitable approach for "injecting" is, e.g., described in EP 3 023 528 A1.

The term "impregnating" or "soaking" as used herein refers to the action of introducing (typically without force) a fluid (such as the aerogel composition) into a solid material (in particular a solid porous material, such as the fibrous article). The "impregnating" or "soaking" can for example be achieved either by placing the article to be impregnated or soaked in a container which contains the typically liquid material with which the article is to be impregnated or in a way that the liquid is poured over the article to be impregnated or soaked.

As used herein, the term "binder" relates to any materials which are intended to provide adhesion between two solid materials. Preferably, the term "binder" relates to any materials

which serve to bind aerogel particles to each other and/or to ceramic fibers. The binders may be of organic or inorganic nature. Particular examples of binders include, but are not limited, to water glass, silicone-based binders and phenolic resin-based binders.

DETAILED DESCRIPTION OF THE PRESENT INVENTION

The present invention relates to a method for the preparation of a composite article comprising aerogel particles and ceramic fibers as well as to a composite article obtainable by this method.

The method

The present invention concerns a method for the preparation of a composite article comprising aerogel particles and ceramic fibers, the method comprising:

- providing a fibrous article comprising ceramic fibers,
- providing an aerogel composition comprising an aerogel powder and an organic solvent,
- combining the fibrous article and the aerogel composition, and
- partially or completely removing the organic solvent to obtain the composite article.

The method is not limited to these steps and may include any number of additional steps before, between and after each of these steps. The steps mentioned above are thus not necessarily consecutive steps. However, it is preferred that they be conducted in the order specified. Furthermore, it is preferred that the steps be consecutive.

The steps of the method described herein may each include additional activities. For example, the step of providing an aerogel composition comprising an aerogel powder and an organic solvent may include providing the aerogel composition containing additional components other than the aerogel powder and the organic solvent. Furthermore, the step of combining the fibrous article and the aerogel composition may include combining not only the fibrous article and the aerogel composition but further articles, compositions etc.

The fibrous article and the aerogel composition are preferably combined by injecting, soaking or impregnating the aerogel composition into the fibrous article, more preferably by impregnating the aerogel composition into the fibrous article. Alternatively, in particular for thicker boards, injecting may be preferable. Suitable methods for injecting such a composition are known to the skilled person and, e.g., described in EP 3 023 528 A1.

Preferably, the partially or completely removing the organic solvent to obtain the composite article by drying includes drying at a temperature of 50 to 170°C for 1 to 8 hours, optionally followed by drying at 171°C to 230°C for 1 to 48 hours.

The composite article to be obtained by the method

The composite article obtainable by the method of the present invention preferably contains 15 to 70 wt.-% aerogel based on the total weight of the composite article. More preferred is 25 to 60 wt%, still more preferred is 35 to 50 wt% aerogel based on the total weight of the composite article.

The thickness of the composite article is typically in the range of less than 3 mm, preferably in the range of 0.001 to less than 3 mm, more preferably in the range of 0.01 to 2.5 mm, even more preferably in the range of 0.01 to 2 mm.

When the width of the composite article is W, the length of the composite article is L and the thickness of the composite article is T, the following requirement is preferably fulfilled by the composite article:

$$R = \frac{W \times L}{T^2}$$

wherein R is 100 or more, preferably 1000 or more, more preferably 10000 or more,
wherein W/L is preferably in a range of 1000/1 to 1/1000,
wherein W/T is preferably 10 or more, and

wherein L/T is preferably 10 or more.

In order to achieve excellent flame resistance, the composite article typically contains less than 15% by weight organic compounds, preferably less than 10% by weight organic compounds, more preferably less than 5% by weight organic compounds, even more preferably less than 2% by weight organic compounds, still more preferably less than 1% by weight organic compounds, most preferably less than 0.5% by weight organic compounds, based on the total weight of the composite article. The term organic compound typically relates to any compounds containing at least one carbon-hydrogen bond.

By the method of the present invention, it is possible to ensure that at least 50% of the fibers in the composite article have a length of 5 mm or more. Preferably at least 50% of the fibers in the composite article have a length of 10 mm or more, more preferably wherein at least 75% of the fibers in the composite article have a length of 5 mm or more, even more preferably wherein at least 75% of the fibers in the composite article have a length of 10 mm or more, still more preferably wherein at least 75% of the fibers in the composite article have a length of 15 mm or more, most preferably wherein at least 75% of the fibers in the composite article have a length of 20 mm or more.

To improve flame resistance and costs, the composite article typically contains less than 10% by weight binder, preferably less than 5% by weight binder, more preferably less than 2% by weight binder, even more preferably less than 1% by weight binder, still more preferably less than 0.5% by weight binder, most preferably less than 0.1% by weight binder. Furthermore, the reduction in the amount of binder may be beneficial for flame resistance, cohesion and insulating properties of the composite article as more fibers and/or aerogel can be incorporated in the composite article. The methods used in the prior art generally require the use of a binder to ensure the structural integrity of the composite articles by binding the fibers to each other and to the fillers. As the present invention allows the use of a fibrous article as a starting material, instead of a slurry of fibers and fillers, the amount of binder can be considerably reduced.

Due to the use of the inventive method, the composite article may exhibit a total weight loss, in thermogravimetric analysis (TGA) when being heated in a nitrogen atmosphere from 30°C to 1100°C with temperature ramp of 10 °C/min, of less than 35% by weight, preferably less than 30% by weight, more preferably less than 25% by weight, even more preferably less than 20% by weight, still more preferably less than 15% by weight, most preferably less than 10% by weight, based on the total weight of the composite article before the thermogravimetric analysis.

Furthermore, it is possible to achieve a weight ratio of the one or more aerogels to the one or more fibers (aerogel/fiber) in the composite article is 1:8 or higher, preferably 1:4 or higher, more preferably 1:2 or higher, even more preferably 1:1 or higher. In the prior art methods, which are typically based on drying a dispersion of fibers, the amount and length of fibers which can stably be included in the fiber blankets is severely limited, i.a. due to the required use of a considerable amount of binder.

The composite article may further comprise inorganic opacifiers and/or mineral fillers. Accordingly, it is preferred that the step of providing an aerogel composition comprising an aerogel powder and an organic solvent, is a step of providing an aerogel composition comprising an aerogel powder and an organic solvent and inorganic opacifiers and/or mineral fillers.

The fibrous article

The fibrous article is preferably selected from batting, nonwovens, mats, felts and needled fiber blankets which are preferably prepared via an air-lay or a carding process, wherein the fibrous article is preferably a nonwoven fiber blanket or a needled fiber blanket. The fibrous article preferably contains 90 wt.-% or more, more preferably 95 wt.-% or more, even more preferably 98 wt.-% or more, of ceramic fibers.

It is furthermore preferred that the fibrous article, in particular if it has a thickness of 3 mm or more, has a density of 20 to 300 kg/m³, preferably 50 to 200 kg/m³, more preferably 80 to 150 kg/m³.

In particular when the fibrous article has a thickness of less than 3 mm, it is preferred that the fibrous article has a density of 50 to 350 kg/m³, preferably 80 to 300 kg/m³, more preferably 100 to 250 kg/m³.

Examples of fibrous articles typically having a thickness of more than 3 mm are (amounts in wt.-%):

Fiberfrax Duraback by Unifrax, having a recommended operating temperature of 982°C, available with a density of 64 kg/m³ (typically having a chemical composition including 31-35% Al₂O₃, 50-54% SiO₂, 5% ZrO₂, 1.30% Fe₂O₃, 1.70% TiO₂, 0.50% MgO, and ≤7.5% CaO);

Fiberfrax Durablanket S by Unifrax, having a recommended operating temperature of 1177°C, available with densities of 64, 96 and 128 kg/m³ (typically having a chemical composition including 43-47% Al₂O₃, 53-57% SiO₂, <1% Fe₂O₃, and <1% TiO₂);

Fiberfrax Durablanket HP-S by Unifrax, having a recommended operating temperature of 1204°C, available with densities of 64, 96 and 128 kg/m³ (typically having a chemical composition including 43-47% Al₂O₃, and 53-57% SiO₂);

Fiberfrax Durablanket 2600 by Unifrax, having a recommended operating temperature of 1343°C, available with densities of 96 and 128 kg/m³ (typically having a chemical composition including 29-31% Al₂O₃, 53-55% SiO₂, 15-17% ZrO₂);

Fiberfrax PH blanket by Unifrax, having a recommended operating temperature of 1177°C, available with a density of 96 kg/m³ (typically having a chemical composition including 43-47% Al₂O₃, 53-55% SiO₂, <1% Fe₂O₃, and <1% TiO₂);

Fiberfrax Moist Pak-D by Unifrax, having a recommended operating temperature of 1010°C, available with densities of 190-290 kg/m³ (typically having a chemical composition including 23-32% Al₂O₃ and 68-77% SiO₂);

Fiberfrax Fibermat Blanket by Unifrax, having a recommended operating temperature of 677°C, available with a density of 88 kg/m³ (typically having a chemical composition including 29-47% Al₂O₃, 52-57% SiO₂, and less than 18% ZrO₂);

Fibermax Mat by Unifrax, having a recommended operating temperature of 1566°C, available with a density of 24 kg/m³ (typically having a chemical composition including 72% Al₂O₃, 27% SiO₂, 0,02% Fe₂O₃, 0,001% TiO₂, 0,05% MgO, and 0,05% CaO);

Fibermax Needled Blanket by Unifrax, having a recommended operating temperature of 1600°C, available with densities of 100 and 130 kg/m³ (typically having a chemical composition including 72% Al₂O₃, 27% SiO₂, 0,02% Fe₂O₃, 0,001% TiO₂, 0,05% MgO, and 0,05% CaO);

Insulfrax LTX Blanket by Unifrax, having a recommended operating temperature of 1100°C, available with densities of 64, 96, 128 and 160 kg/m³ (typically having a chemical composition including <1% Al₂O₃, 61-67% SiO₂, <0,6% Fe₂O₃, 2,5-6,5% MgO, and 27-33% CaO);

Insulfrax S Blanket by Unifrax, having a recommended operating temperature of 1100°C, available with densities of 64, 96 and 128 kg/m³ (typically having a chemical composition including 61-67% SiO₂, 2-7% MgO, and 27-33% CaO);

Isofrax 1400 Blanket by Unifrax, having a recommended operating temperature of 1300°C, available with densities of 96, 128 and 160 kg/m³ (typically having a chemical composition including 70-80% SiO₂ and 18-27% MgO);

"CERAKWOOL New-Bio" by KCC, available with densities of 96, 128 and 160 kg/m³ (typically having a chemical composition including <1% Al₂O₃, 58-67% SiO₂, 2-8% MgO, and 26-34% CaO);

Superwool plus blanket SPB by New Fire, having a recommended operating temperature of 1050°C, available with densities of 96 and 128 kg/m³ (typically having a chemical composition including 62-68% SiO₂, 3-7% MgO, and 26-32% CaO);

Saffil Blanket & Mat by Unifrax, having a recommended operating temperature of 1600°C, available with densities of 35, 96 kg/m³ (typically having a chemical composition including 95-97% Al₂O₃ and 3-5% SiO₂);

isoTherm S Vlies by Frenzelit, having a recommended operating temperature of 1100°C (typically having a chemical composition including >94% SiO₂).

Examples of fibrous articles typically having a thickness of less than 3 mm are (amounts in wt.-%):

Fiberfrax Paper FT, having a recommended operating temperature of 1250°C, available with densities of 200-240 kg/m³ (typically having a chemical composition including 46-50% Al₂O₃ and 50-54% SiO₂);

Fiberfrax Paper DS, having a recommended operating temperature of 1250°C, available with densities of 160-200 kg/m³ (typically having a chemical composition including 46-50% Al₂O₃ and 50-54% SiO₂);

Fiberfrax Paper H, having a recommended operating temperature of 1400°C, available with densities of 180-280 kg/m³ (typically having a chemical composition including 48-58% Al₂O₃ and 42-52% SiO₂);

Fiberfrax Durafelt LD, having a recommended operating temperature of 1250°C, available with densities of 110-190 kg/m³ (typically having a chemical composition including 46-52% Al₂O₃ and 48-54% SiO₂);

Fiberfrax Durafelt HD, having a recommended operating temperature of 1250°C, available with densities of 200-300 kg/m³ (typically having a chemical composition including 42-50% Al₂O₃ and 50-58% SiO₂);

Fiberfrax Durafelt Z, having a recommended operating temperature of 1400°C, available with densities of 200-300 kg/m³ (typically having a chemical composition including 28-32% Al₂O₃, 52-56% SiO₂ and 14-18% ZrO₂);

Morgan Kaowool 1260 Paper, having a recommended operating temperature of 1260°C, available with density of 190 kg/m³ (typically having a chemical composition including 47% Al₂O₃ and 52% SiO₂);

Morgan Kaowool 500 Paper, having a recommended operating temperature of 1176°C, available with densities of 192-224 kg/m³ (typically having a chemical composition including 47% Al₂O₃ and 53% SiO₂);

Morgan Kaowool 700 Paper, having a recommended operating temperature of 1176°C, available with densities of 176-208 kg/m³ (typically having a chemical composition including 47% Al₂O₃ and 53% SiO₂);

Morgan Kaowool 900 Paper, having a recommended operating temperature of 1176°C, available with densities of 160-192 kg/m³ (typically having a chemical composition including 47% Al₂O₃ and 53% SiO₂);

Morgan Kaowool 2000 Paper, having a recommended operating temperature of 1176°C, available with densities of 176-224 kg/m³ (typically having a chemical composition including 47% Al₂O₃ and 53% SiO₂);

Morgan Kaowool 2600 Paper, having a recommended operating temperature of 1343°C, available with densities of 160-208 kg/m³ (typically having a chemical composition including 35% Al₂O₃, 51% SiO₂ and 14% ZrO₂);

Insulfrax Paper, having a recommended operating temperature of 1200°C, available with a density of 150 kg/m³ (typically having a chemical composition including less than 1% Al₂O₃, 61-67% SiO₂, 2.5-6.5% MgO and 27-33% CaO);

Flexilite-MC Paper, having a recommended operating temperature of 1260°C, available with a density of 150 kg/m³ (typically having a chemical composition including 70-80% SiO₂ and 18-27% MgO);

Isofrax 1260C Paper, having a recommended operating temperature of 1260°C, available with densities of 140-160 kg/m³ (typically having a chemical composition including 70-80% SiO₂ and 18-27% MgO);

Morgan Superwool Plus Paper, having a recommended operating temperature of 1000°C, available with densities of 180-250 kg/m³ (typically having a chemical composition including 62-68% SiO₂, 3-7% MgO and 26-32% CaO);

Morgan Superwool HT Paper, having a recommended operating temperature of 1150°C, available with densities of 180-250 kg/m³ (typically having a chemical composition including 70-80% SiO₂ and 18-26% CaO);

Saffil 1600 Paper, having a recommended operating temperature of 1600°C, available with densities of 140-200 kg/m³ (typically having a chemical composition including more than 90% Al₂O₃ and less than 8% SiO₂);

Morgan Kaowool 1600 Paper, having a recommended operating temperature of 1600°C, available with a density of 150 kg/m³ (typically having a chemical composition including 88% Al₂O₃ and 9% SiO₂);

Morgan Kaowool 3000 Paper, having a recommended operating temperature of 1538°C, available with densities of 112-160 kg/m³ (typically having a chemical composition including 95% Al₂O₃ and 5% SiO₂);

Frenzelit isoTherm S Vlies, having a recommended operating temperature of 1100°C, (typically having a chemical composition including more than 94% SiO₂).

Among these, the following are preferred:

Fiberfrax Paper DS, Fiberfrax Paper H, Fiberfrax Durafelt LD, Kaowool 1260 Paper, Kaowool 900 Paper, Kaowool 2600 Paper, Insulfrax Paper, Isofrax 1260C Paper, Superwool Plus Paper, Superwool HT Paper, Saffil 1600 Paper, Kaowool 1600 Paper, Kaowool 3000 Paper, and isoTherm S Vlies.

The ceramic fibers

The ceramic fibers may generally be structured into three classes of fibers

- a) ceramic fibers containing 80 wt.-% or more of alumina,
- b) ceramic fibers containing 2 to less than 80 wt.-% alumina, and
- c) ceramic fibers containing less than 2 wt.-% alumina.

a) ceramic fibers 80 wt.-% or more of alumina:

This first type of ceramic fibers typically contains 80 wt.-% or more of alumina, preferably 85 wt.-% or more of alumina, preferably 90 wt.-% or more of alumina, or even 95 wt.-% or more of alumina, based on the total weight of the ceramic fibers, wherein the content of alumina is preferably 99 wt.-% or less, more preferably 98 wt.-% or less, even more preferably 97 wt.-% or less, based on the total weight of the ceramic fibers.

The ceramic fibers may further contain 0 to 20 wt.-% of silica, preferably 1 to 20 wt.-% of silica, more preferably 1 to 15 wt.-% of silica, even more preferably 1 to 10 wt.-% of silica, still more preferably 2 to 9 wt.-% of silica, based on the total weight of the ceramic fibers.

It is preferred that these ceramic fibers contain less than 3 wt.-% of components other than silica and alumina, preferably less than 2 wt.-% of components other than silica and alumina, or even less than 1 or 0.5 wt.-% of components other than silica and alumina, based on the total weight of the ceramic fibers.

b) ceramic fibers containing 2 to less than 80 wt.-% alumina:

This second type of ceramic fibers typically contains 2 to less than 80 wt.-% alumina, preferably 15 to less than 80 wt.-% alumina, more preferably 20 to 75 wt.-% alumina, based on the total weight of the ceramic fibers.

The ceramic fibers may further contain 10 to 98 wt.-% of silica, preferably 15 to 90 wt.-% of silica, more preferably 20 to 85 wt.-% of silica, even more preferably 25 to 80 wt.-% of silica, based on the total weight of the ceramic fibers.

For example, the ceramic fibers may contain 30 to 35 wt.-% of alumina, 50 to 55 wt.-% of silica and a total of ZrO_2 , Fe_2O_3 , TiO_2 , MgO and CaO of 4 to 20 wt.-%, based on the total weight of the ceramic fibers. Alternatively, the ceramic fibers may contain 42 to 48 wt.-% of alumina and 52 to 58 wt.-% of silica, based on the total weight of the ceramic fibers; or the ceramic fibers may contain 42 to 58 wt.-% of alumina and 52 to 58 wt.-% of silica, based on the total weight of the ceramic fibers. Furthermore, the ceramic fibers may contain 28 to 32 wt.-% of alumina, 52 to 56 wt.-% of silica and 14 to 18 wt.-% of ZrO_2 , based on the total weight of the ceramic fibers. It is furthermore possible that the ceramic fibers contain 22 to 34 wt.-% of alumina and 66 to 78 wt.-% of silica, based on the total weight of the ceramic fibers. In a further alternative example, the ceramic fibers contain 66 to 78 wt.-% of alumina, 22 to 34 wt.-% of silica, based on the total weight of the ceramic fibers.

It is preferred that these ceramic fibers contain less than 2 wt.-% of components other than those indicated above, preferably less than 1 wt.-% of components other than those indicated above, even more preferably less than 0.5 wt.-% of components other than those indicated above, based on the total weight of the ceramic fibers.

c) ceramic fibers containing less than 2 wt.-% alumina:

Ceramic fibers of this type typically contain less than 2 wt.-% alumina, preferably less than 1 wt.-% alumina, more preferably less than 0.5 wt.-% alumina, based on the total weight of the ceramic fibers. Alumina may even be absent from these ceramic fibers.

These ceramic fibers typically further contain 50 to 85 wt.-% silica and 15 to 50 wt.-% alkaline earth metal oxide, preferably 55 to 85 wt.-% silica and 15 to 45 wt.-% alkaline earth metal oxide, more preferably 60 to 82 wt.-% silica and 18 to 40 wt.-% alkaline earth metal oxide, based on the total weight of the ceramic fibers. Alternatively, ceramic fibers of this type may contain 55 to 72 wt.-% silica and 28 to 45 wt.-% alkaline earth metal oxide, preferably 60 to

70 wt.-% silica and 30 to 40 wt.-% alkaline earth metal oxide, based on the total weight of the ceramic fibers. Another type of these ceramic fibers contains 65 to 85 wt.-% silica and 15 to 35 wt.-% alkaline earth metal oxide, preferably 70 to 80 wt.-% silica and 20 to 30 wt.-% alkaline earth metal oxide, based on the total weight of the ceramic fibers.

The alkaline earth metal oxide is preferably selected from MgO and CaO or a combination thereof. In some embodiments, the ratio of the CaO in the alkaline earth metal oxide is 75 wt.-% or more, or even 85 wt.-% or more, based on the total amount of alkaline earth metal oxide.

In any of the ceramic fibers described herein, the content of any components of the ceramic fibers other than those indicated is preferably less than 4 wt.-%, more preferably less than 3 wt.-%, still more preferably less than 2 wt.-%, even more preferably less than 1 wt.-% or even less than 0.5 wt.-%, based on the total weight of the ceramic fibers.

The solvent

The organic solvent used in the method of the present invention is typically a hydrocarbon solvent, preferably selected from C₃₋₁₆ saturated, unsaturated or partially saturated hydrocarbons or mixtures thereof, more preferably selected from C₃₋₁₀ saturated straight, branched or cyclic hydrocarbons or mixtures thereof, even more preferably selected from C₃₋₁₀ linear or branched alkanes or mixtures thereof, still more preferably selected from C₅₋₇ linear or branched alkanes or mixtures thereof, still even more preferably selected from hexanes or heptanes or mixtures thereof, most preferably n-hexane.

Alternatively, the organic solvent used in the present invention is an alcohol solvent, preferably selected from C₂₋₁₂ saturated, unsaturated or partially saturated alcohols or mixtures thereof, more preferably selected from C₂₋₁₂ saturated straight, branched or cyclic alcohols or mixtures thereof, even more preferably selected from C₂₋₁₂ saturated straight, branched or cyclic monohydric alcohols or mixtures thereof, still more preferably selected from C₂₋₆ saturated straight, branched or cyclic monohydric alcohols (such as ethanol, 1-

propanol, 2-propanol, butanols, pentanols (including cyclopentanol) or hexanols (including cyclohexanol)) or mixtures thereof, still even more preferably selected from propanols or mixtures thereof, most preferably 2-propanol.

Furthermore, the organic solvent may be a mixture of one or more hydrocarbon solvent(s) and one or more alcohol solvent(s) indicated above.

The aerogel

The aerogel may be any inorganic aerogel. Preferably, it comprises or consists of one or more selected from silicon oxide, aluminum oxide, zirconium oxide, titanium oxide, hafnium oxide and yttrium oxide. More preferably, the aerogel comprises or consists of silicon oxide. Even more preferably the aerogel is silica aerogel.

The aerogel typically has a porosity of 85% or higher, more preferably a porosity of 90% or higher, as determined by isotherm adsorption and desorption. More specifically, porosity is determined by measuring pore volume and pore size distribution of aerogel by using the BJH (Barret-Joyner-Halenda) adsorption and desorption isotherm method.

The specific surface area of the aerogel is typically 300 m²/g or higher. Preferably it is 400 m²/g or higher, preferably 500 m²/g or higher, preferably 600 m²/g or higher, and preferably 2000 m²/g or less, more preferably 1500 m²/g or less, even more preferably 1000 m²/g or less, still more preferably 800 m²/g or less, as determined by DIN ISO 9277 2003-05 (Determination of the specific surface area of solids by gas adsorption using the BET method).

In the present invention, it is preferable that the powder of the aerogel has a median particle size (d₅₀) in the range of 1 to 50 µm, preferably 5 to 40 µm, more preferably 10 to 30 µm, even more preferably 15 to 25 µm, as measured by laser diffraction, preferably using a Malvern Mastersizer.

The powder of the aerogel may, e.g., be obtained from a heterophase reaction. In such a case, it is preferred that the powder of the aerogel is silica aerogel powder obtained by mixing and

reacting de-ionized water, water glass, an organosilane compound, an inorganic acid, and an organic solvent, which is preferably a non-polar organic solvent, to obtain silica hydrogel primary particles. The silica hydrogel primary particles are then solvent-substituted and the solvent-substituted gel particles are dried under ambient pressure to obtain silica aerogel powder. It is preferred that no further grinding or sieving treatment is performed. Such a heterophase reaction method is known to the skilled person and, e.g., described in EP 2 722 311.

The aerogel powder is preferably prepared in the form of particles instead of a monolith. Thus, preferable the aerogel powder used in the present invention has been obtained by a process which does not include grinding of the aerogel material. More preferably, the aerogel powder is in the form of primary particles (optionally including secondary particles). Accordingly, no grinding or sieving treatment is needed for generating the aerogel powder. Furthermore, it is preferred that the aerogel powder is dried under ambient pressure, e.g. 1 atm, instead of using a supercritical drying process which is sometimes employed in the production of aerogel according to the prior art.

The aerogel composition

The aerogel composition comprises the aerogel powder and the organic solvent. It is to be understood that the aerogel composition may contain further components. To achieve efficient distribution of the aerogel powder in the fibrous article, the aerogel composition is preferably a dispersion of the aerogel powder in the organic solvent.

The aerogel composition typically contains 2 to 20 wt.-% aerogel, preferably 4 to 18 wt.-% aerogel, more preferably 6 to 18 wt.-% aerogel, even more preferably 10 to 18 wt.-% aerogel, based on the total weight of the aerogel composition. The remainder is preferably the organic solvent.

It is preferred that the combined content of aerogel powder and organic solvent in the aerogel composition is 90 wt.-% or more, preferably 95 wt.-% or more, more preferably 97 wt.-% or more, even more preferably 98 wt.-% or more, still more preferably 99 wt.-% or more, most

preferably 99.5 wt.-% or more, or even 99.8 wt.-% or more, based on the total weight of the aerogel composition.

Alternatively, if the method involves the use of inorganic opacifiers and/or mineral fillers, the aerogel composition is preferably a dispersion of the aerogel powder, inorganic opacifiers and/or mineral fillers in the organic solvent. Other components may or may not be contained in the aerogel composition. The inorganic opacifiers typically comprise or consist of one or more selected from iron oxide, zirconium oxide, titanium oxide, silicon carbide and graphite (graphite preferably being contained in the composite article in an amount of less than 5 wt.%, preferably less than 2 wt.%, more preferably less than 1 wt.% based on the total weight of the composite article). Among these, iron oxide, zirconium oxide, titanium oxide and/or silicon carbide are preferred. Preferably the inorganic opacifiers comprise or consist of one or more selected from iron oxide, zirconium oxide and silicon carbide, more preferably wherein the inorganic opacifier is iron oxide or silicon carbide.

The mineral fillers preferably comprise or consist of one or more selected from metal hydroxides and hydrated carbonates. Preferably, the mineral fillers comprise or consist of one or more selected from aluminum hydroxides, magnesium hydroxides, hydromagnesites and hydrocalcites. More preferably, the mineral fillers are one or both selected from magnesium dihydroxide and aluminum trihydroxide.

It is preferred that the inorganic opacifiers and the mineral fillers are not in the form of aerogel(s). It is in particular preferred that the bulk density of the inorganic opacifiers, and more preferably also of the mineral fillers, is at least 0.1 g/cm^3 , tested according to DIN EN ISO 787-11 and/or that the specific surface area of the inorganic opacifiers, and more preferably also of the mineral fillers, is $300 \text{ m}^2/\text{g}$ or less, tested according to DIN ISO 9277 2003-05 (BET method). Alternatively or in addition, is furthermore preferred that the inorganic opacifiers, and more preferably also the mineral fillers, are chemically different from the material used as the aerogel. It is to be understood that any combination of the inorganic opacifiers, and of the mineral fillers, mentioned herein may be used.

In the case of containing inorganic opacifiers and/or mineral fillers, the aerogel composition

preferably contains 2 to 20 wt.-% aerogel, preferably 4 to 18 wt.-% aerogel, more preferably 6 to 18 wt.-% aerogel, even more preferably 10 to 18 wt.-% aerogel, based on the total weight of the aerogel composition, the remainder preferably being organic solvent and inorganic opacifiers and mineral fillers.

In the case of containing inorganic opacifiers and/or mineral fillers, the combined content of aerogel powder and organic solvent in the aerogel composition is typically 50 wt.-% or more, preferably 75 wt.-% or more, more preferably 85 wt.-% or more. Furthermore, the combined content of inorganic opacifiers and mineral fillers in the aerogel composition is typically 50 wt.-% or less, preferably 25 wt.-% or less, more preferably 15 wt.-% or less, based on the total weight of the aerogel composition.

The composite article obtainable by the method

The present invention furthermore relates to a composite article obtainable by the method according to the present invention. It is to be understood that this composite article exhibits the properties resulting from the method of the present invention. Accordingly, any of the features set out herein with respect to the method of the invention, including any preferred ranges, also apply with respect to the composite article of the present invention.

For example, the composite article preferably contains 15 to 70 wt.-% aerogel based on the total weight of the composite article. The thickness of the composite article is preferably in the range of 0.01 mm to less than 3 mm. However, the present invention is also applicable to composite articles having a thickness in the range of 3 mm to 500 mm.

It is to be understood that any known fillers may be contained in the composite article of the present invention without any particular limitation. However, the composite article contains preferably less than 15% by weight organic compounds and preferably less than 10% by weight binder. The composite article preferably exhibits a total weight loss, in thermogravimetric analysis (TGA) when being heated in a nitrogen atmosphere from 30°C to 1100°C with temperature ramp of 10 °C/min, of less than 35% by weight.

Preferably at least 50% of the fibers in the composite article have a length of 5 mm or more. It is furthermore preferred that the weight ratio of the one or more aerogels to the one or more fibers (aerogel/fiber) in the composite article is 1:8 or higher. As will be understood, the composite article may further comprise inorganic opacifiers and/or mineral fillers as specified herein.

The composite article may be defined in further ways, either by referring to its method of production or to its properties.

Accordingly, the composite article of the present invention may be defined as comprising aerogel particles and ceramic fibers, wherein the composite article is obtainable by injecting or impregnating an aerogel composition comprising an aerogel powder and an organic solvent, and optionally inorganic opacifiers and/or mineral fillers, into a fibrous article comprising ceramic fibers, and partially or completely removing the organic solvent to obtain the composite article.

In addition or alternatively, the composite article may be defined as comprising aerogel particles and ceramic fibers, wherein one or more of the following requirements (i) to (vi) are fulfilled:

- (i) The composite article contains less than 15% by weight organic compounds, based on the total weight of the composite article. The content of organic compounds is preferably less than 10% by weight, more preferably less than 2% by weight, even more preferably less than 5% by weight. The term organic compound relates to any compounds containing at least one carbon-hydrogen bond.
- (ii) At least 50% of the fibers in the composite article have a length of 5 mm or more. Preferably at least 50% of the fibers in the composite article have a length of 10 mm or more. More preferably at least 75% of the fibers in the composite article have a length of 5 mm or more. Even more preferably at least 75% of the fibers in the composite article have a length of 10 mm or more. Still more preferably at least 75% of the fibers in the composite article have a length of 15 mm or more. Most preferably at least 75% of the

fibers in the composite article have a length of 20 mm or more.

- (iii) The composite article contains less than 10% by weight binder, based on the total weight of the composite article. The content of binder in the composite article contains less than 10% by weight binder, preferably less than 5% by weight binder, more preferably less than 2% by weight binder, even more preferably less than 1% by weight binder, still more preferably less than 0.5% by weight binder, most preferably less than 0.1% by weight binder.
- (iv) The composite article exhibits a total weight loss in thermogravimetric analysis (TGA) when being heated in a nitrogen atmosphere from 30°C to 1100°C with a temperature increase of 10 °C/min of less than 35% by weight. The total weight loss in thermogravimetric analysis is preferably less than 30% by weight, more preferably less than 25% by weight, even more preferably less than 20% by weight, still more preferably less than 15% by weight, most preferably less than 10% by weight, based on the weight of the composite article before the thermogravimetric analysis.
- (v) The weight ratio of the one or more aerogels to the one or more fibers (aerogel/fiber) in the composite article is 1:8 or higher. Preferably, the weight ratio of the one or more aerogels to the one or more fibers (aerogel/fiber) in the composite article is higher than 1:8, preferably 1:4 or higher, more preferably 1:2 or higher, even more preferably 1:1 or higher.
- (vi) The composite article has a burn-through time of 60 minutes or more. Preferably, the composite article has a burn-through time of 60 minutes or more, preferably 120 minutes or more, even more preferably 180 minutes or more, still more preferably 240 minutes or more. The burn-through resistance is determined using the composite article in the form of a DIN A4 sheet with a thickness of 1 to 3 mm and treating the composite article at the centre of its first major surface with a flame having a temperature of 1400°C, using a soldering torch, wherein the burn-through time is the duration from start of the flame treatment until the centre of the second major surface reaches a temperature of 1000°C.

The composite article may fulfil one or any number of possible combinations of requirements (i) to (vi). For example, the composite article preferably fulfils requirement (i), or requirement (ii), or requirement (iii), or requirement (iv), or requirement (v), or requirement (vi). Alternatively, it is preferred that two requirements be fulfilled, such as (i) and (ii), (ii) and (iii), (iii) and (iv), (iv) and (v), (v) and (vi), (i) and (iii), (ii) and (iv), (iii) and (v), (iv) and (vi), (i) and (iv), (ii) and (v), (iii) and (vi), (i) and (v), (ii) and (vi), or (i) and (vi). Alternatively, it is preferred that three requirements be fulfilled, such as (i) and (ii) and (iii), (i) and (ii) and (iv), (i) and (ii) and (v), (i) and (ii) and (vi), (i) and (iii) and (iv), (i) and (iii) and (v), (i) and (iii) and (vi), (i) and (iv) and (v), (i) and (iv) and (vi), (i) and (v) and (vi), (ii) and (iii) and (iv), (ii) and (iii) and (v), (ii) and (iii) and (vi), (ii) and (iv) and (v), (ii) and (iv) and (vi), (ii) and (v) and (vi), (iii) and (iv) and (v), (iii) and (iv) and (vi), (iii) and (v) and (vi), or (iv) and (v) and (vi). Alternatively, it is preferred that four, five or six of these requirements be fulfilled.

It is to be understood that also the composite article according to these alternative definitions may further comprise inorganic opacifiers and/or mineral fillers. The composite article preferably contains 15 to 70 wt.-%, more preferably 25 to 60 wt%, still more preferably 35 to 50 wt% aerogel, based on the total weight of the composite article. Preferably, the composite article has a thickness in the range of less than 3 mm, preferably in the range of 0.001 to less than 3 mm, more preferably in the range of 0.01 to 2.5 mm, even more preferably in the range of 0.01 to 2 mm. In addition, when the width of the composite article is W, the length of the composite article is L and the thickness of the composite article is T, the following requirement is preferably fulfilled:

$$R = \frac{W \times L}{T^2}$$

wherein R is 100 or more, preferably 1000 or more, more preferably 10000 or more,

wherein W/L is preferably in a range of 1000/1 to 1/1000,

wherein W/T is preferably 10 or more, and

wherein L/T is preferably 10 or more.

It is to be understood that the composite article of the present invention may contain further components, such as inert fillers or pigments, flame retardants, flame and smoke suppressors, binders. These are preferably added by including them in the aerogel composition.

The composite article of the present invention may furthermore be coated with various other materials and/or combined with other materials, such as wovens or laminates, to form further composites.

The present invention may be summarized by the following items 1 to 60:

1. A method for the preparation of a composite article comprising aerogel particles and ceramic fibers, the method comprising:
providing a fibrous article comprising ceramic fibers,
providing an aerogel composition comprising an aerogel powder and an organic solvent,
combining the fibrous article and the aerogel composition, and
partially or completely removing the organic solvent to obtain the composite article.
2. The method for the preparation of a composite article according to item 1, wherein the composite article further comprises inorganic opacifiers and/or mineral fillers, wherein the step of providing an aerogel composition comprising an aerogel powder and an organic solvent, is a step of providing an aerogel composition comprising an aerogel powder and an organic solvent and inorganic opacifiers and/or mineral fillers.
3. The method for the preparation of a composite article according to item 1 or 2, wherein the fibrous article is selected from batting, nonwovens, mats, felts and needled fiber blankets, wherein the fibrous article is preferably a nonwoven fiber blanket or a needled fiber blanket.
4. The method for the preparation of a composite article according to any one of items 1 to 3, wherein the fibrous article has a density of 50 to 350 kg/m³, preferably 80 to 300 kg/m³, more preferably 100 to 250 kg/m³.

5. The method for the preparation of a composite article according to any one of the preceding items, wherein the ceramic fibers contain 80 wt.-% or more of alumina, preferably 85 wt.-% or more of alumina, preferably 90 wt.-% or more of alumina, based on the total weight of the ceramic fibers, wherein the content of alumina is preferably 99 wt.-% or less, more preferably 98 wt.-% or less, even more preferably 97 wt.-% or more, based on the total weight of the ceramic fibers.
6. The method for the preparation of a composite article according to item 5, wherein the ceramic fibers further contain 0 to 20 wt.-% of silica, preferably 1 to 20 wt.-% of silica, more preferably 1 to 15 wt.-% of silica, even more preferably 1 to 10 wt.-% of silica, still more preferably 2 to 9 wt.-% of silica, or even 2 to 6 wt.-% of silica, based on the total weight of the ceramic fibers.
7. The method for the preparation of a composite article according to item 5, wherein the ceramic fibers contain less than 3 wt.-% of components other than silica and alumina, preferably less than 2 wt.-% of components other than silica and alumina, even more preferably less than 1 wt.-% of components other than silica and alumina, based on the total weight of the ceramic fibers.
8. The method for the preparation of a composite article according to any one of items 1 to 4, wherein the ceramic fibers contain 2 to less than 80 wt.-% alumina, preferably 15 to less than 80 wt.-% alumina, more preferably 20 to 75 wt.-% alumina, based on the total weight of the ceramic fibers.
9. The method for the preparation of a composite article according to item 8, wherein the ceramic fibers further contain 10 to 98 wt.-% of silica, preferably 15 to 90 wt.-% of silica, more preferably 20 to 85 wt.-% of silica, even more preferably 25 to 80 wt.-% of silica, based on the total weight of the ceramic fibers.
10. The method for the preparation of a composite article according to item 8 or 9, wherein the ceramic fibers contain 30 to 35 wt.-% of alumina, 50 to 55 wt.-% of silica and a total of ZrO_2 , Fe_2O_3 , TiO_2 , MgO and CaO of 4 to 20 wt.-%, based on the total weight of the

ceramic fibers.

11. The method for the preparation of a composite article according to item 8 or 9, wherein the ceramic fibers contain 42 to 58 wt.-% of alumina and 52 to 58 wt.-% of silica, based on the total weight of the ceramic fibers.
12. The method for the preparation of a composite article according to item 8 or 9, wherein the ceramic fibers contain 28 to 32 wt.-% of alumina, 52 to 56 wt.-% of silica and 14 to 18 wt.-% of ZrO_2 , based on the total weight of the ceramic fibers.
13. The method for the preparation of a composite article according to item 8 or 9, wherein the ceramic fibers contain 22 to 34 wt.-% of alumina, 66 to 78 wt.-% of silica, based on the total weight of the ceramic fibers.
14. The method for the preparation of a composite article according to item 8 or 9, wherein the ceramic fibers contain 66 to 78 wt.-% of alumina, 22 to 34 wt.-% of silica, based on the total weight of the ceramic fibers.
15. The method for the preparation of a composite article according to any one of items 1 to 4, wherein the ceramic fibers contain less than 2 wt.-% alumina, preferably less than 1 wt.-% alumina, more preferably less than 0.5 wt.-% alumina, based on the total weight of the ceramic fibers.
16. The method for the preparation of a composite article according to item 15, wherein the ceramic fibers further contain 50 to 85 wt.-% silica and 15 to 50 wt.-% alkaline earth metal oxide, preferably 55 to 85 wt.-% silica and 15 to 45 wt.-% alkaline earth metal oxide, more preferably 60 to 82 wt.-% silica and 18 to 40 wt.-% alkaline earth metal oxide, based on the total weight of the ceramic fibers.
17. The method for the preparation of a composite article according to item 15, wherein the ceramic fibers further contain 55 to 72 wt.-% silica and 28 to 45 wt.-% alkaline earth metal oxide, preferably 60 to 70 wt.-% silica and 30 to 40 wt.-% alkaline earth metal

oxide, based on the total weight of the ceramic fibers.

18. The method for the preparation of a composite article according to item 15, wherein the ceramic fibers further contain 65 to 85 wt.-% silica and 15 to 35 wt.-% alkaline earth metal oxide, preferably 70 to 80 wt.-% silica and 20 to 30 wt.-% alkaline earth metal oxide, based on the total weight of the ceramic fibers.
19. The method for the preparation of a composite article according to any one of items 16 to 18, wherein the alkaline earth metal oxide is selected from MgO and CaO or a combination thereof, wherein the content of the CaO in the alkaline earth metal oxide is preferably 75 wt.-% or more, more preferably 85 wt.-% or more, based on the total amount of alkaline earth metal oxide.
20. The method for the preparation of a composite article according to any one of items 8 to 14 and 16 to 19, wherein the content of any components of the ceramic fibers other than those indicated in the respective items is less than 4 wt.-%, preferably less than 3 wt.-%, even more preferably less than 2 wt.-%, even more preferably less than 1 wt.-%, or even less than 0.5 wt.-%, based on the total weight of the ceramic fibers.
21. The method for the preparation of a composite article according to any one of the preceding items, wherein the organic solvent is a hydrocarbon solvent, preferably selected from C₃₋₁₆ saturated, unsaturated or partially saturated hydrocarbons or mixtures thereof, more preferably selected from C₃₋₁₀ saturated straight, branched or cyclic hydrocarbons or mixtures thereof, even more preferably selected from C₃₋₁₀ linear or branched alkanes or mixtures thereof, still more preferably selected from C₅₋₇ linear or branched alkanes or mixtures thereof, still even more preferably selected from hexanes or heptanes or mixtures thereof, most preferably n-hexane.
22. The method for the preparation of a composite article according to any one of items 1 to 20, wherein the organic solvent is an alcohol solvent, preferably selected from C₂₋₁₂ saturated, unsaturated or partially saturated alcohols or mixtures thereof, more preferably selected from C₂₋₁₂ saturated straight, branched or cyclic alcohols or mixtures

thereof, even more preferably selected from C₂₋₁₂ saturated straight, branched or cyclic monohydric alcohols or mixtures thereof, still more preferably selected from C₂₋₆ saturated straight, branched or cyclic monohydric alcohols or mixtures thereof, still even more preferably selected from propanols or mixtures thereof, most preferably 2-propanol.

23. The method for the preparation of a composite article according to any one of the preceding items, wherein the aerogel comprises or consists of one or more selected from silicon oxide, aluminum oxide, zirconium oxide, titanium oxide, hafnium oxide and yttrium oxide, preferably wherein the aerogel comprises or consists of silicon oxide, more preferably wherein the aerogel is silica aerogel.
24. The method for the preparation of a composite article according to any one of the preceding items, wherein the aerogel has a porosity of 85% or higher, more preferably a porosity of 90% or higher, as determined by isotherm adsorption and desorption.
25. The method for the preparation of a composite article according to any one of the preceding items, wherein the aerogel has a specific surface area of 300 m²/g or higher, preferably 400 m²/g or higher, preferably 500 m²/g or higher, preferably 600 m²/g or higher, and preferably 2000 m²/g or less, more preferably 1500 m²/g or less, even more preferably 1000 m²/g or less, as determined by DIN ISO 9277 2003-05 (Determination of the specific surface area of solids by gas adsorption using the BET method).
26. The method for the preparation of a composite article according to any one of the preceding items, wherein the powder of the aerogel has a median particle size (d₅₀) in the range of 1 to 50 µm, preferably 5 to 40 µm, more preferably 10 to 30 µm, even more preferably 15 to 25 µm, as measured by laser diffraction, preferably using a Malvern Mastersizer.
27. The method for the preparation of a composite article according to any one of the preceding items, wherein the powder of the aerogel is obtained from a heterophase reaction.

28. The method for the preparation of a composite article according to any one of the preceding items, wherein the powder of the aerogel is silica aerogel powder obtained by mixing and reacting de-ionized water, water glass, an organosilane compound, an inorganic acid, and an organic solvent, which is preferably a non-polar organic solvent, to obtain silica hydrogel primary particles, solvent-substituting the silica hydrogel primary particles, and drying the solvent-substitution completed gel particles under ambient pressure to obtain silica aerogel powder, preferably without any further grinding or sieving treatment .
29. The method for the preparation of a composite article according to item 1 or any one of items 3 to 28, wherein the aerogel composition is a dispersion of the aerogel powder in the organic solvent.
30. The method for the preparation of a composite article according to item 1 and any one of items 3 to 29, wherein the aerogel composition contains 2 to 20 wt.-% aerogel, preferably 4 to 18 wt.-% aerogel, more preferably 6 to 18 wt.-% aerogel , even more preferably 10 to 18 wt.-% aerogel, based on the total weight of the aerogel composition, the remainder preferably being organic solvent.
31. The method for the preparation of a composite article according to item 1 and any of items 3 to 30, wherein the combined content of aerogel powder and organic solvent in the aerogel composition is 90 wt.-% or more, preferably 95 wt.-% or more, more preferably 97 wt.-% or more, even more preferably 98 wt.-% or more, still more preferably 99 wt.-% or more, most preferably 99.5 wt.-% or more, or even 99.8 wt.-% or more.
32. The method for the preparation of a composite article according to any one of items 2 to 28, wherein the aerogel composition is a dispersion of the aerogel powder, inorganic opacifiers and/or mineral fillers in the organic solvent.

33. The method for the preparation of a composite article according to any one of items 2 to 28 and 32, wherein the inorganic opacifiers comprise or consist of one or more selected from iron oxide, zirconium oxide, titanium oxide, silicon carbide and graphite, preferably wherein the inorganic opacifiers comprise or consist of one or more selected from iron oxide, zirconium oxide, and silicon carbide, more preferably wherein the inorganic opacifier is iron oxide or silicon carbide.
34. The method for the preparation of a composite article according to any one of items 2 to 28, 32 and 33, wherein the mineral fillers comprise or consist of one or more selected from metal hydroxides and hydrated carbonates, preferably wherein the mineral fillers comprise or consist of one or more selected from aluminum hydroxides, magnesium hydroxides, hydromagnesites and hydrocalcites, more preferably wherein the mineral fillers are one or both selected from magnesium dihydroxide and aluminum trihydroxide.
35. The method for the preparation of a composite article according to any one of items 2 to 28 and 32 to 34, wherein the aerogel composition contains 2 to 20 wt.-% aerogel, preferably 4 to 18 wt.-% aerogel, more preferably 6 to 18 wt.-% aerogel, even more preferably 10 to 18 wt.-% aerogel, based on the total weight of the aerogel composition, the remainder preferably being organic solvent and inorganic opacifiers and mineral fillers.
36. The method for the preparation of a composite article according to any one of items 2 to 28 and 32 to 35, wherein the combined content of aerogel powder and organic solvent in the aerogel composition is 50 wt.-% or more, preferably 75 wt.-% or more, more preferably 85 wt.-% or more.
37. The method for the preparation of a composite article according to any one of items 2 to 28 and 32 to 36, wherein the combined content of inorganic opacifiers and mineral fillers in the aerogel composition is 50 wt.-% or less, preferably 25 wt.-% or less, more preferably 15 wt.-% or less.

38. The method for the preparation of a composite article according to any one of the preceding items, wherein the fibrous article and the aerogel composition are combined by injecting or impregnating the aerogel composition into the fibrous article.
39. The method for the preparation of a composite article according to any one of the preceding items wherein partially or completely removing the organic solvent to obtain the composite article by drying includes drying at a temperature of 50 to 170°C for 1 to 8 hours, optionally followed by drying at 171°C to 230°C for 1 to 48 hours.
40. The method for the preparation of a composite article according to any one of the preceding items, wherein the composite article contains 15 to 70 wt.-%, preferably 25 to 60 wt%, more preferably 35 to 50 wt%, aerogel, based on the total weight of the composite article.
41. The method for the preparation of a composite article according to any one of the preceding items, wherein the composite article has a thickness in the range of less than 3 mm, preferably in the range of 0.001 to less than 3 mm, more preferably in the range of 0.01 to 2.5 mm, even more preferably in the range of 0.01 to 2 mm.
42. The method for the preparation of a composite article according to any one of the preceding items, wherein when the width of the composite article is W, the length of the composite article is L and the thickness of the composite article is T, the following requirement is fulfilled:

$$R = \frac{W \times L}{T^2}$$

wherein R is 100 or more, preferably 1000 or more, more preferably 10000 or more,

wherein W/L is preferably in a range of 1000/1 to 1/1000,

wherein W/T is preferably 10 or more, and

wherein L/T is preferably 10 or more.

43. The method for the preparation of a composite article according to any one of the preceding items, wherein the composite article contains less than 15% by weight organic compounds, preferably less than 10% by weight organic compounds, more preferably less than 5% by weight organic compounds, wherein the term organic compound relates to any compounds containing at least one carbon-hydrogen bond.
44. The method for the preparation of a composite article according to any one of the preceding items, wherein at least 50% of the fibers in the composite article have a length of 5 mm or more, preferably wherein at least 50% of the fibers in the composite article have a length of 10 mm or more, more preferably wherein at least 75% of the fibers in the composite article have a length of 5 mm or more, even more preferably wherein at least 75% of the fibers in the composite article have a length of 10 mm or more, still more preferably wherein at least 75% of the fibers in the composite article have a length of 15 mm or more, most preferably wherein at least 75% of the fibers in the composite article have a length of 20 mm or more.
45. The method for the preparation of a composite article according to any one of the preceding items, wherein the composite article contains less than 10% by weight binder, preferably less than 5% by weight binder, more preferably less than 2% by weight binder, even more preferably less than 1% by weight binder, still more preferably less than 0.5% by weight binder, most preferably less than 0.1% by weight binder.
46. The method for the preparation of a composite article according to any one of the preceding items, wherein the composite article exhibits a total weight loss, in thermogravimetric analysis (TGA) when being heated in a nitrogen atmosphere from 30°C to 1100°C with temperature ramp of 10 °C/min, of less than 35% by weight, preferably less than 30% by weight, more preferably less than 25% by weight, even more preferably less than 20% by weight, still more preferably less than 15% by weight, most preferably less than 10% by weight.
47. The method for the preparation of a composite article according to any one of the preceding items, wherein the weight ratio of the one or more aerogels to the one or

more fibers (aerogel/fiber) in the composite article is 1:8 or higher, preferably 1:4 or higher, more preferably 1:2 or higher, even more preferably 1:1 or higher.

48. A composite article obtainable by the method according to any one of the preceding items.
49. A composite article comprising aerogel particles and ceramic fibers, wherein the composite article is obtainable by injecting or impregnating an aerogel composition comprising an aerogel powder and an organic solvent, and optionally inorganic opacifiers and/or mineral fillers, into a fibrous article comprising ceramic fibers, and partially or completely removing the organic solvent to obtain the composite article.
50. A composite article comprising aerogel particles and ceramic fibers, wherein one or more of the following requirements (i) to (vi) are fulfilled:
 - (i) the composite article contains less than 15% by weight organic compounds;
 - (ii) at least 50% of the fibers in the composite article have a length of 5 mm or more;
 - (iii) the composite article contains less than 10% by weight binder;
 - (iv) the composite article exhibits a total weight loss in thermogravimetric analysis (TGA) when being heated in a nitrogen atmosphere from 30°C to 1100°C with a temperature increase of 10 °C/min of less than 35% by weight;
 - (v) the weight ratio of the one or more aerogels to the one or more fibers (aerogel/fiber) in the composite article is 1:8 or higher;
 - (vi) the composite article has a burn-through time of 60 minutes or more, wherein the burn-through resistance is determined using the composite article in the form of a DIN A4 sheet with a thickness of 1 to 3 mm and treating the composite article at the centre of its first major surface with a flame having a temperature of 1400°C, using a soldering torch, wherein the burn-through time is the duration from start of the flame treatment until the centre of the second major surface reaches a temperature of 1000°C.
51. The composite article according to item 50, further comprising inorganic opacifiers and/or mineral fillers.

52. The composite article according to item 50 or 51, wherein the composite article contains less than 15% by weight organic compounds, preferably less than 10% by weight organic compounds, more preferably less than 5% by weight organic compounds, wherein the term organic compound relates to any compounds containing at least one carbon-hydrogen bond.
53. The composite article according to any one of items 50 to 52, wherein at least 50% of the fibers in the composite article have a length of 5 mm or more, preferably wherein at least 50% of the fibers in the composite article have a length of 10 mm or more, more preferably wherein at least 75% of the fibers in the composite article have a length of 5 mm or more, even more preferably wherein at least 75% of the fibers in the composite article have a length of 10 mm or more, still more preferably wherein at least 75% of the fibers in the composite article have a length of 15 mm or more, most preferably wherein at least 75% of the fibers in the composite article have a length of 20 mm or more.
54. The composite article according to any one of items 50 to 53, wherein the composite article contains less than 10% by weight binder, preferably less than 5% by weight binder, more preferably less than 2% by weight binder, even more preferably less than 1% by weight binder, still more preferably less than 0.5% by weight binder, most preferably less than 0.1% by weight binder.
55. The composite article according to any one of items 50 to 54, wherein the composite article exhibits a total weight loss in thermogravimetric analysis (TGA) when being heated in a nitrogen atmosphere from 30°C to 1100°C with temperature increase of 10 °C/min of less than 35% by weight, preferably less than 30% by weight, more preferably less than 25% by weight, even more preferably less than 20% by weight, still more preferably less than 15% by weight, most preferably less than 10% by weight.
56. The composite article according to any one of items 50 to 55, wherein the weight ratio of the one or more aerogels to the one or more fibers (aerogel/fiber) in the composite article is higher than 1:8, preferably 1:4 or higher, more preferably 1:2 or higher, even

more preferably 1:1 or higher.

57. The composite article according to any one of items 50 to 56, wherein the composite article contains 15 to 70 wt.-%, preferably 25 to 60 wt%, more preferably 35 to 50 wt% aerogel based on the total weight of the composite article.
58. The composite article according to any one of items 50 to 57, wherein the composite article has a thickness in the range of less than 3 mm, preferably in the range of 0.001 to less than 3 mm, more preferably in the range of 0.01 to 2.5 mm, even more preferably in the range of 0.01 to 2 mm.
59. The composite article according to any one of items 50 to 58, wherein the composite article has a burn-through time of 60 minutes or more, preferably 120 minutes or more, even more preferably 180 minutes or more, still more preferably 240 minutes or more.
60. The composite article according to any one of items 50 to 60, wherein, when the width of the composite article is W, the length of the composite article is L and the thickness of the composite article is T, the following requirement is fulfilled:

$$R = \frac{W \times L}{T^2}$$

wherein R is 100 or more, preferably 1000 or more, more preferably 10000 or more,

wherein W/L is preferably in a range of 1000/1 to 1/1000,

wherein W/T is preferably 10 or more, and

wherein L/T is preferably 10 or more.

The present application claims the priority of EP21161398, filed on 09 March 2021 at the European Patent Office with the title composite article comprising aerogel particles and ceramic fibers, the contents of which (in particular the experimental examples) are incorporated herein by reference.

EXAMPLES

Example 1

Materials

Aerogel powder (JIOS AeroVa Aerogel Powder, D20 Grade)

2-Propanol (technical grade)

Ceramic fiber paper A (Insulfrax Paper supplied by Unifrax, contains 55-72 wt. % silica and 28-45 wt. % alkaline earth metal oxide, paper density of 150 kg/m³, with a raw paper thickness of 1 mm)

Ceramic fiber paper B (Insulfrax Paper supplied by Unifrax, contains 55-72 wt. % silica and 28-45 wt. % alkaline earth metal oxide, paper density of 150 kg/m³, with a raw paper thickness of 2 mm)

Ceramic fiber paper C (Insulfrax Paper supplied by Unifrax, contains 55-72 wt. % silica and 28-45 wt. % alkaline earth metal oxide paper density of 150 kg/m³, with a raw paper thickness of 3 mm)

Soldering torch (Rotenberger Industrial, Type ROFIRE Piezo 1950, 35429) equipped with a gas cartridge (Rotenberger Industrial, 30% Propane/70% Butane)

Experimental

The aerogel was dispersed using a standard lab mixing equipment, more specifically a propeller mixer (Heidolph overhead stirrer RZR2020) in 2-propanol to reach a solid content of 11 wt-%.

Preparation of aerogel-incorporated ceramic fiber papers:

1 L of aerogel dispersion (11 wt-% aerogel in 2-propanol as prepared above) were impregnated at room temperature (20°C) into a 21x29.7 cm (DIN A4 size) ceramic fiber paper by means of

soaking the raw paper in the aerogel dispersion. The sample was dried immediately after the impregnation in a hot-air oven at 110°C for 4 h, followed by post-drying at 200°C for 16 h.

Example	Ceramic fiber paper	Paper thickness [mm]	Aerogel content in dried prototype [wt.%]
1-1	A	1	38
1-2	B	2	0
1-3	C	3	33
1-4	B	2	30
1-5	B	2	30
1-6	C	3	24
1-7	C	3	15
1-8	A	1	0
1-9	C	3	0

Examples 1-1, 1-3, 1-4, 1-5, 1-6 and 1-7 are according to the present invention, while Examples 1-2, 1-8 and 1-9 are reference examples.

Results and evaluation

Homogeneous aerogel-incorporated ceramic fiber papers were obtained, as shown in Figures 1 and 2. The papers showed low dust release by shaking. There is no pocketing or delamination within the papers observed.

In order to investigate the thermal insulation capability and the resistance to high temperature, the aerogel-incorporated ceramic fiber papers as well as blank ceramic fiber papers were exposed to a soldering torch flame, as shown in Figure 3. The soldering torches had a flame temperature of around 1400°C. The temperature increase on the back side (non-flamed side) of the papers was recorded by thermal couples.

Although the blank ceramic fiber papers used in Examples 1-2, 1-8 and 1-9 are designed for high temperature applications and are nominally resistant to temperature up to 1200°C, the flamed sites on them melted quickly and completely burnt through after 10 sec, 20 sec and 8

min for the blank ceramic fiber paper of Example 1-8, 1-2, and 1-9, respectively, as shown in Figures 4, 8 and 9.

In contrast to the blank ceramic fiber papers, the aerogel-incorporated ceramic fiber papers showed much better resistance to the torch flame. As shown in Figures 5, 6 and 10, the aerogel-incorporated ceramic fiber papers (Examples 1-1, 1-3 and 1-4) remained almost undamaged after being flamed for 60 min. The colour change of the flamed sites was attributed to the decomposition and evaporation of sizing agents, which originate from the manufacturing process of the raw ceramic fiber papers.

A cross-sectional analysis of the flamed area showed that only the very first surface (thinner than 0.5 mm) of the ceramic fiber paper became rigid but the paper as a whole remained flexible. The back side of the flamed area maintained the same colour as before the test.

A comparison of the temperature increase of the back side middle part among the blank ceramic fiber paper (Example 1-2, raw paper thickness 2 mm) and the two aerogel-incorporated ceramic fiber papers (Examples 1-1 and 1-3) is shown in Figure 7.

The blank ceramic fiber paper (raw paper thickness 2 mm) showed a sharp temperature increase to 1350°C, because the paper was burnt through after only 20 sec of flaming.

In contrast, the aerogel-incorporated ceramic fiber papers (Examples 1-1 and 1-3) showed much better thermal insulation capability and resistance to high temperature. The temperature of the back side middle part was measured as 820°C and 540°C for the aerogel-incorporated ceramic fiber paper with raw paper thickness of 1 and 3 mm, respectively. The aerogel-incorporated ceramic fiber papers withstood the torch flame for much longer exposure period.

Comparisons of the temperature increase on the non-exposed side between the blank ceramic fiber papers and aerogel-incorporated ceramic fiber papers are shown in Figures 11, 12 and 13 (relating to comparisons of Examples 1-8 vs. 1-1, Examples 1-2 vs. 1-4 and Examples 1-9 vs. 1-3). The blank ceramic fiber papers (raw paper thickness 1 and 2 mm) showed a sharp temperature increase to 1350°C, because the papers were burnt through after only 10 and 20

sec of flaming, respectively. The blank ceramic fiber paper (raw paper thickness 3 mm) was burnt-through after 8 min of flaming.

In contrast, the aerogel-incorporated ceramic fiber papers showed much better thermal insulation capability and resistance to high temperature. The temperature on the non-exposed side was measured as 820°C, 800°C and 540°C for the aerogel-incorporated ceramic fiber paper with raw paper thickness of 1, 2 and 3 mm, respectively. The aerogel-incorporated ceramic fiber papers withstood the torch flame for much longer exposure period.

The comparison between the prototypes of aerogel-incorporated ceramic fiber papers and the blank ceramic fiber paper suggests that the incorporation of aerogel powder in the ceramic fiber papers induces a synergy between the two components, which significantly improves the thermal insulation capability and the resistance to very high temperatures.

Fire resistance test

In order to study the fire resistance performance, soldering torch test was conducted for both blank ceramic papers and aerogel-incorporated ceramic papers. The specimens were cut into a dimension A4 and were exposed to a soldering torch (Rotenberger Industrial, Type ROFIRE Piezo 1950, 35429) equipped with a gas cartridge (Rotenberger Industrial, 30% Propane/70% Butane), whose flame temperature is in the range of 1300 – 1400°C. On the back side (non-flamed side) of the specimen, thermal couples (type K) were installed in the middle location to record the temperature increase.