

Hydraulic Solenoid Distribution Valve

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The present invention relates to a hydraulic solenoid control valve. In particular, a hydraulic 3/2-solenoid control valve embodied as a double-seated valve in cartridge design is proposed.

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From the state of the art, e.g. 3/2-solenoid control valves including a magnetic actuator are known. This type of hydraulic valves offers two different switching positions for three different connection lines. With the two different switching positions, e.g. a pressure line P is selectively connected to a pressure-less tank line T, or an operating line A is selectively connected to the tank line T.

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It is an object underlying the present invention to provide a hydraulic solenoid control valve which is very compact and operates free of leakage oil even upon high pressures, while being manufactured at low costs.

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This object is solved by the independent claim. The dependent claim comprise preferred further developments of the invention.

Thus, this object is solved by a hydraulic solenoid control valve, in particular a hydraulic 3/2-solenoid control valve, comprising a housing, a solenoid and a valve spindle. A valve chamber is integrated into the housing. This valve chamber comprises a first valve seat bore as a connection to a first line, in particular a pressure line, a second valve seat bore as a connection to a second line, in particular an operating line, and a free aperture to a third line, in particular a tank line. The aperture is referred to as "free", since it connects the valve chamber to the third line in any switching position of the valve. The valve spindle is at least partially arranged within the valve chamber and is linearly moved by the solenoid. Further, the valve spindle comprises, within the valve chamber, a first sealing surface facing the first valve seat bore and a second sealing surface facing the second valve seat bore, such that selectively the first valve seat bore or the second valve seat bore can be closed. In addition, the valve spindle protrudes

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from the valve chamber through the second valve seat bore and through the second line toward the solenoid. Due to the protrusion of the valve spindle from the valve chamber, the valve spindle can be connected to the solenoid or can be partially integrated into the solenoid. In case the second valve seat bore is closed, the valve spindle is pulled into the second valve seat bore by a differential-area-ratio through the pressure of the second line, in particular the operating line. This arrangement including a differential area ratio promotes a sealing of the second valve seat bore free of leakage oil.

This differential-area-ratio is in particular achieved in that a sealing diameter of the valve spindle outside the valve chamber is larger than a diameter of the second valve seat bore. The sealing diameter is defined at a seal between the valve spindle and the solenoid.

Preferably, the differential-area-ratio is obtained by configuring the diameter of the valve spindle outside the valve chamber to be larger than the bore diameter of the second valve seat bore. Therewith, the pressure of the second line in front of the valve chamber can support the force of the pressure spring, when the second valve seat bore is closed, and pull the second sealing surface into the second valve seat bore.

Preferably, the first sealing surface comprises a convex surface, in particular a ball. Further preferably, the second sealing surface comprises a cone surface, in particular a cone ring surface. By linearly displacing or moving the valve spindle, the first valve seat bore is closed by the convex surface or the second valve seat bore is closed by the cone surface, selectively. Therewith, selectively the first line, in particular a pressure line, is connected to the third line, in particular a tank line, or the second line, in particular an operating line, is connected to the third line. A seizure in the switching position under pressure is effectively prevented by the ball valve embodiment including the convex surface.

In a preferred embodiment, a pressure spring is arranged between the first valve seat bore and the valve spindle. In the variant including a ball, the inventive valve may therefore be referred to as a spring-loaded ball-cone-seat valve.

In a further preferred embodiment, it is provided that the second sealing surface, in particular the cone surface, seals the second valve seat bore in a de-energized state of the solenoid, and that the first sealing surface, in particular the convex surface, seals the first valve seat bore in an energized state of the solenoid. The preferably provided
5 pressure spring serves to press the second sealing surface of the valve spindle into the second valve seat bore in a de-energized state.

In a further preferred embodiment, the valve spindle consists of at least two parts. For this purpose, the valve spindle comprises a first part and a second part, wherein the first
10 part is guided to be linearly movable in the solenoid and the second part is screwed into the first part. Consequently, the second part is fixedly connected to the first part and is linearly movable together with the first part. In particular for providing the differential-area-ratio, this two-part form of the valve spindle is especially easy to assemble. Therewith, in particular the sealing diameter can be configured to be larger than the
15 bore diameter of the second valve seat bore.

In addition, it is preferably provided that a seal, in particular a groove ring seal, is arranged between the valve spindle and an armature space of the solenoid. Said seal is disposed at the already discussed sealing diameter between the valve spindle and the
20 solenoid. Particularly preferred, the armature space is always freely connected to the third line, in particular the tank line, via a connection channel extending through the valve spindle. Therewith, a pressure generation in the armature space upon a possible leakage of the groove ring seal is prevented. The connection channel within the valve spindle extends from the armature space through the valve spindle into the valve
25 chamber. As already described, the valve chamber is always freely connected to the third line, in particular the tank line.

Further, the invention preferably comprises a filter, in particular in the first line. Particularly preferred, the filter is arranged outside the valve chamber directly in front of
30 the inlet into the first valve seat bore. The filter prevents pollution of the oil and in particular a pollution of the two valve seats.

In a further preferred embodiment, the first valve seat bore is disposed directly opposite to the second valve set bore.

In a preferred embodiment, the solenoid comprises a coil, an armature, a pole core as well as a gap between the pole core and the armature. The pole core comprises a borehole along the longitudinal axis of the valve spindle and therefore provides an accommodation and a linear guidance for the valve spindle. Further preferably, the inventive solenoid valves comprise a control unit for the solenoid. By means of said control unit, the solenoid can be switched between energized and de-energized.

Further, the invention comprises a hydraulic cartridge solenoid control valve, in particular a hydraulic cartridge 3/-solenoid control valve, comprising an afore-described hydraulic solenoid valve, wherein the housing is configured to be at least partially inserted into a valve adapter. Said valve adapter is located in a component which integrally accommodates the cartridge 3/2-solenoid control valve. Particularly preferred, the first line, in particular the pressure line, and the second line, in particular the operating line, are directed radially or vertically outwardly with respect to the longitudinal axis of the valve spindle. In addition, O-ring seals are preferably arranged laterally of the outwardly directed first and second lines on the surface of the valve housing, such that these lines can be connected pressure-tight by inserting the cartridge housing. Particularly preferred, the valve housing comprises circumferentially extending ring channels for this purpose. Starting at these ring channels, a plurality of radially directed channels for the first line and/or a plurality of radially directed channels for the second line may preferably lead to the valve chamber.

Further, it is preferred that the hydraulic cartridge solenoid control valve comprises a volume compensation unit including a tank compartment. This volume compensation unit including a tank compartment is integrated into the valve housing or connected to the valve housing by a flange. The tank compartment is preferably connected to the third line. The valve is preferably structured along the longitudinal axis of the valve spindle as follows: The valve chamber including the valve spindle is arranged in the center. On one side of the chamber, the volume compensation unit including the tank compartment is integrated or connected by a flange. On the other side of the valve chamber, the solenoid is mounted. Therewith, the hydraulic cartridge solenoid control valve can be inserted into a component with the volume compensation unit to the fore. The solenoid and in particular a plug at the solenoid preferably protrude from the

component. In a preferred embodiment, the tank compartment of the volume compensation unit is slightly pressure-loaded by a volume compensation piston and a compensation spring/pressure spring.

5 In the following, the invention is explained in more detail on the basis of the accompanying drawing, in which:

Fig. 1 shows the switching symbol for the inventive hydraulic 3/2-solenoid control valve according to the embodiment in a de-energized position;

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Fig. 2 shows the switching symbol for the inventive hydraulic 3/2-solenoid control valve according to the embodiment in an energized state,

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Fig. 3 shows the inventive hydraulic 3/2-solenoid control valve according to the embodiment in a de-energized position,

Fig. 4 shows the inventive hydraulic 3/2-solenoid control valve according to the embodiment in an energized position, and

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Fig. 5 shows a detail of Fig. 4.

In the following, an embodiment of the invention is described in more detail with reference to Figs. 1 to 5.

25 Fig. 1 shows the switching symbol for a hydraulic 3/2-solenoid control valve 1 in a de-energized position. The pressure line P is connected to the tank line T. The operating line A is blocked. Fig. 2 shows the switching symbol of the hydraulic 3/2-solenoid control valve 1 in an energized state. The pressure line P is blocked. The operating line A is connected to the tank line T.

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In the following, the switching position of Fig. 1 is shown with reference to Fig. 3. Figs. 4 and 5 show the switching position of Fig. 2.

Fig. 3 shows a sectional view of the hydraulic 3/2-solenoid control valve in a de-energized state. The hydraulic 3/2-solenoid control valve 1 comprises a housing 2, a valve chamber 3 integrated into the housing 2, a solenoid 4 and a valve spindle 5. The valve spindle 5 moves in a longitudinal direction along a valve axis 38.

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The valve chamber 3 comprises a first valve seat bore 6 as a connection from the pressure line P to the valve chamber 3 and a second valve seat bore 7 as a connection from the operating line A to the valve chamber 3. Further, a free aperture 8 to the tank line T is formed at the valve chamber 3. The first valve seat bore 6 is located directly opposite to the second valve seat bore 7. The free aperture 8 is also formed as a borehole, wherein the borehole of the free aperture 8 is arranged vertically with respect to the first valve seat bore 6 and the second valve seat bore 7. In addition, a diameter of the first valve seat bore 6 is considerably smaller than a diameter of the second valve seat bore 7.

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The valve spindle 5 has a split structure and comprises a first part 12 and a second part 13 being screwed into the first part 12 and thus fixedly connected to the first part 12. The second part 13 extends from the interior of the valve chamber 3 through the second valve seat bore 7 toward the solenoid 4. The first part 12 is disposed completely outside the valve chamber 3.

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The second part 13 of the valve spindle 5 comprises a first sealing surface, embodied as a convex surface 9 (see in particular Fig. 5) on a side thereof facing the valve seat bore 6. Said convex surface 9 is formed by a ball 10. The ball 10 in turn is embedded into a face side recess of the valve spindle 5, in particular of the second part 13. In addition, a shoulder is formed at the valve spindle 5, in particular at the second part 13. A valve pressure spring 14 is supported on said shoulder. The convex surface 9 is arranged within said valve pressure spring 14. The valve pressure spring 14 is further supported at the front face of the first valve seat bore 6. Said front face can also be referred to as sealing surface or lateral surface of the first valve seat bore 6. Due to this arrangement of the valve pressure spring 14, the valve spindle 5 is loaded toward the solenoid 4. In a de-energized state, this results in an opening of the first valve seat bore 6.

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At the second valve seat bore 7, the valve spindle 5, in particular the second part 13, comprises a second sealing surface, embodied as a cone ring surface 11, within the valve chamber 3. Said cone ring surface 11 is formed about the complete circumference of the valve spindle 5. In a de-energized state of the solenoid 4, said cone ring surface 11 is pushed onto the second valve seat bore 7 and therewith seals the operating line A with respect to the valve chamber 3.

The solenoid 4 comprises a coil 16, an armature 17 and a pole core 18. The coil 16 is wound about the armature 17 and the pole core 18. The armature 17 and the pole core 18 are arranged in series along the longitudinal valve axis 38. In the pole core 18, a borehole is formed along the longitudinal valve axis 38. Said borehole forms a linear guide 19 for at least a portion of the valve spindle 5, in particular a portion of the first part 12 of the valve spindle 5. In an energized state, a gap 20 being as small as possible exists between the pole core 18 and the armature 17. In the de-energized state, said gap 20 is larger. The solenoid 4 further comprises a connecting line or voltage supply 21 for connecting a control unit to the hydraulic 3/2-solenoid valve 1. The armature 17 and the pole core 18 are embedded into a sleeve 23. Further, an insulation 24 exists between the sleeve 23 and the coil 16.

The pole core 18 and the armature 17 are arranged in a so-called armature space 22. Said armature space 22 is located within the sleeve 23. The operating line A is sealed with respect to said armature space 22 by a specific seal, in particular a groove ring seal 25. Said groove ring seal 25 is arranged between the valve spindle 5, in particular the first part 12, and the pole core 18. A connection channel 15 is extending within the valve spindle 5. Said connection channel 15 connects the armature space 22 to the valve chamber 3. Since the valve chamber 3 is always freely connected to the tank line T, also the armature space 22 is always pressureless. The connection channel 15 is formed by a longitudinal borehole along the longitudinal valve axis 38 in the valve spindle 5 as well as by boreholes being vertical with respect to the longitudinal valve axis 38 from the surface of the valve spindle 5 to the longitudinally extending borehole. Due to the split structure of the valve spindle 5, in particular, the longitudinal borehole can be formed along the longitudinal valve axis 38 inside the valve spindle 5.

The housing 2 comprises a base housing component 26, a first valve chamber insert 27 and a second valve chamber insert 28. The first valve chamber insert 27 and the second valve chamber insert 28 together form the valve chamber 3. The hydraulic 3/2-solenoid control valve 1 is structured and assembled as follows: An annular extension 29 is disposed at the solenoid 4. A part of the second valve chamber insert 28 is embedded into said extension 29. The second valve chamber insert 28 in turn accommodates the first valve chamber insert 27. The already mentioned sleeve 23 of the solenoid 4 extends to the second valve chamber insert 28 and is connected thereto. The complete unit consisting of solenoid 4, second valve chamber insert 28 and first valve chamber insert 27 is screwed into the base housing component 26. For this purpose, an internal thread is formed at the base housing component 26, and a corresponding external thread is formed at the extension 29 of the solenoid 4. The individual housing components are sealed against each other.

In addition, the housing 2 comprises a cap 30. The cap 30 encases the solenoid 4 and sits on the base housing component 26.

A drilled insert 35 is formed inside the first valve chamber insert 27. The first valve seat bore 6 is formed in said drilled insert 35. In addition, a filter 36 is arranged in the first valve chamber insert 27. Said filter 36 is disposed outside the valve chamber 3 and in the pressure line P.

In addition, a volume compensation unit 37 including the tank compartment 31 is integrated inside the base housing component 26. Said volume compensation unit 37 including the tank compartment 31 comprises a volume compensation piston 32, a compensation spring/length compensation spring 33 and a bearing 35 for the compensation spring 33. The tank compartment 31 is connected to the tank line T. The volume compensation piston 32 defines a wall of the tank compartment 31. The piston 32 is slightly spring-loaded by the compensation spring 33. The compensation spring 33 is supported against the volume compensation piston 32 on one side thereof and against the spring bearing 34 on the other side thereof. The front face of the spring bearing 34 is screwed into the base housing component 26.

The hydraulic 3/2-solenoid control valve 1 is constructed substantially rotation-symmetrically with respect to the longitudinal valve axis 38. The pressure lines P, the operating lines A and the tank lines T obviously deviate from said rotation symmetry. The pressure line P and the operating line A end at respectively at least one position on the circumferential surface of the base housing component 26. At this position, ring channels 39 are formed. Said ring channels 39 are sealed with O-ring seals 40, when the 3/2-solenoid control valve 1, embodied as a cartridge valve, is inserted into a corresponding receptacle.

Fig. 4 shows the hydraulic 3/2-solenoid control valve 1 according to the embodiment in the energized state. Herein, it is clearly visible that the valve spindle 5 was moved to the left compared to the illustration of Fig. 3. Consequently, the operating line A is directly connected to the valve chamber 3 and thus with the tank line T and the tank compartment 31 via the second valve seat bore 7. The pressure line P is blocked by the seating of the ball 10 in the first valve seat bore 6 and is therefore not connected to the valve chamber 3.

Fig. 5 shows a detail of Fig. 4. Based on this illustration, particularly the differential-area-ratio can be explained. It shall be noted that said differential-area-ratio is used upon a closed second valve seat bore 7 and thus in the de-energized valve position shown in Figs. 1 and 3. As shown in Fig. 5, the valve spindle 5 comprises a sealing diameter D1 at the groove ring seal 25. The second valve seat bore 7 has an inner diameter D2. In a region between the groove ring seal 25 and the second valve seat bore 7, the valve spindle 5 has a smallest diameter D3. When the second valve seat bore 7 is closed, the pressure in the operating line A acts on the following surfaces of the valve spindle 5: The first surface is calculated by $(D2^2/4 * \pi) - (D3^2/4 * \pi)$. The second surface is calculated by $(D1^2/4 * \pi) - (D3^2/4 * \pi)$. Due to the fact that the first surface is smaller than the second surface, the operating pressure acts to the right in the shown illustration, when the second valve seat bore 7 is closed. Therewith, the valve pressure spring 14 is supported and the cone surface 11 is pulled into the second valve seat bore 7.

Based on the shown embodiment, it was explained how a hydraulic 3/2-solenoid control valve 1, in particular with a cartridge design, can be formed for an operation free of

leakage oil. In the de-energized switching position, shown in Fig. 3, the side of the valve spindle 5 formed as the cone surface 11 is pushed into the second valve seat bore 7 of the operating line by the pressure spring 14 and therewith blocks the connection of said line with respect to the tank in an oil-tight manner. On the magnet side, the valve spindle 5 is radially formed with a groove ring seal 25 with respect to the armature space 22. The sealing diameter D1 of the valve spindle 5 toward the armature space 22 is larger than the second valve seat bore 7. Therewith, there results a defined area ratio between the cone seat and the sealing diameter D1 of the armature space 22. If the operating line A is pressurized, a differential force is generated through the area ratio between the operating line and the sealed armature space 22, which force pulls the valve spindle 5 toward the solenoid 4 and acts in addition to the elastic force against the second valve seat bore 7. The sealing effect increases with increasing pressure in the operating line A. The solenoid 4 is preferably configured such that a switching against the elastic force plus differential force is prevented. In this position, the pressure line P and the tank line T are connected to each other.

In the energized switching position according to Fig. 4, the operating line A is pressureless, wherein the valve spindle 5 seals, with its ball 10, the pressure line P in an oil-tight manner against the elastic force. A consumer connected through the pressure line P, can now be effectively sealed until the rated operating pressure is reached. Said operating pressure is dependent on the magnetic force. In this switching position, the operating line A is connected to the tank line T without pressure. Therewith, no pressure or only a small dynamic pressure can build up in the operating line A.

The embodiments of the proposed 3/2-solenoid control valve are applicable according to the invention also for other valve designs, independent from the cartridge design and independent of the number of lines and/or switching positions. In particular a combination of ball seat and cone seat in a valve, in particular on a valve spindle, and/or the differential-area-ratio are applicable for other valves according to the invention.

List of Reference Numerals

	1	3/2-solenoid control valve
	2	valve housing
5	3	valve chamber
	4	solenoid
	5	valve spindle
	6, 7	valve seat bores
	8	free aperture
10	9	convex surface
	10	ball
	11	cone ring surface
	12	first part
	13	second part
15	14	valve pressure spring
	15	connection channel
	16	coil
	17	armature
	18	pole core
20	19	linear guide
	20	gap
	21	connecting line
	22	armature space
	23	sleeve
25	24	insulation
	25	groove ring seal
	26	base housing component
	27	first valve chamber insert
	28	second valve chamber insert
30	29	extension
	30	cap
	31	tank compartment
	32	volume compensation piston
	33	compensation spring

- 34 spring bearing
- 35 drilled insert
- 36 filter
- 37 volume compensation unit
- 5 38 longitudinal valve axis
- 39 ring channels
- 40 O-ring seals
- P first line, in particular pressure line
- A second line, in particular operating line
- 10 T third line, in particular tank line

Patent Claims

- 5 1. A hydraulic solenoid control valve, in particular a hydraulic 3/2-solenoid control valve (1), comprising:

 - a valve housing (2),
 - a valve chamber (3) integrated into the valve housing (2), including a first valve seat bore (6) as a connection to a first line, in particular a pressure line (P), a second valve seat bore (7) as a connection to a second line, in particular an operating line (A), and a free aperture (8) to a third line, in particular a tank line (T),
 - a solenoid (4), and
 - a valve spindle (5) movable by the solenoid (4) and partially arranged in the valve chamber (3),
 - 15 - wherein the valve spindle (5) comprises, within the valve chamber (3) a first sealing surface (9) facing the first valve seat bore (6) and a second sealing surface (11) facing the second valve seat bore (7), such that selectively the first valve seat bore (6) and or the second valve seat bore (7) can be closed,
 - wherein the valve spindle (5) protrudes from the valve chamber (3) through the second valve seat bore (7) toward the solenoid (4), and
 - 20 - wherein, when the second valve seat bore (7) is closed, the valve spindle (5) is pulled into the second valve seat bore (7) by a differential-area-ratio through the pressure in the second line, in particular the operating line (A).
- 25 2. The hydraulic solenoid control valve of claim 1, characterized in that a pressure spring (14) is arranged between the first valve seat bore (6) and the valve spindle (5).
- 30 3. The hydraulic solenoid control valve of one of the preceding claims, characterized in that the second sealing surface (11) seals the second valve seat bore (7) in a de-energized state of the solenoid (4), and that the first sealing surface (9) seals the first valve seat bore (6) in an energized state of the solenoid (4).

4. The hydraulic solenoid control valve of one of the preceding claims, characterized in that the first sealing surface (9) comprises a convex surface, in particular a ball (10).
- 5 5. The hydraulic solenoid control valve of one of the preceding claims, characterized in the second sealing surface (11) comprises a cone surface, in particular a cone ring surface.
- 10 6. The hydraulic solenoid control valve of one of the preceding claims, characterized in that a sealing diameter (D1) of the valve spindle (5) outside the valve chamber (3) is larger than a diameter (D2) of the second valve seat bore (7), such that the differential-area-ratio is generated, wherein the sealing diameter (D1) is defined at a seal (25) between the valve spindle (5) and the solenoid (4).
- 15 7. The hydraulic solenoid control valve of one of the preceding claims, characterized in that the valve spindle (5) comprises a first part (12) and a second part (13), wherein the first part (12) is guided to be linearly movable in the solenoid (4) and the second part (13) is screwed into the first part (12).
- 20 8. The hydraulic solenoid control valve of one of the preceding claims, characterized in that a seal (25), in particular a groove ring seal, is arranged between the valve spindle (5) and an armature space (22) of the solenoid (4), wherein the armature space (22) is freely connected to the third line, in particular the tank line (T), via a connection channel (15) extending through the valve spindle (5).
- 25 9. A hydraulic cartridge solenoid control valve, in particular a hydraulic cartridge 3/2-solenoid control valve, comprising a hydraulic solenoid control valve (1) according to one of the preceding claims, wherein the valve housing (2) is configured to be at least partially inserted into a valve adapter.
- 30 10. The hydraulic cartridge solenoid control valve of claim 9, characterized by a volume compensation unit (37) including a tank compartment (31), wherein the volume compensation unit (37) including the tank compartment (31) is integrated into the valve housing (2) or connected to the valve housing (2) by a flange.