

DESCRIPTION

MODIFIER FOR THERMOPLASTIC RESIN AND THERMOPLASTIC RESIN
COMPOSITION USING THE SAME

5

TECHNICAL FIELD

The present invention relates to a modifier for thermoplastic resin, comprising polytetrafluoroethylene (A) and an alkyl (meth)acrylate-based polymer (B); and a
10 thermoplastic resin composition comprising this modifier and a thermoplastic resin (C), further, if necessary, a flame retardant (D) and a filler (E) are compounded therein.

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BACKGROUND ART

Polytetrafluoroethylene, due to high crystallinity and low intermolecular force, has a nature of fiberization by a slight stress, and when compounded in a thermoplastic resin, shows improvements in molding processability, mechanical properties and the like. Because
20 of this, polytetrafluoroethylene is conventionally utilized also as an additive to a thermoplastic resin. For example, JP-A No. 9-25420 discloses a method of using polytetrafluoroethylene capsulated by a styrene/acrylonitrile copolymer, for improving the melting
25 speeds of various resins typically including a polyvinyl chloride resin.

When polytetrafluoroethylene is used in a flame-proofing resin composition, it is generally known that fiberization thereof in a resin performs an effect of suppressing fire spreading by dropping of flame drops in combustion. Particularly, there is recently an increased requirement for flame-proofing of resin materials, and regarding housing materials of OA instruments such as computers, printers and the like, and domestic electric appliances such as televisions, audio instruments and the like, there is a strong desire for flame-proofing to decrease combustion damages. Further, the decrease in weight, decrease in thickness and complication of form of instruments cause a requirement for higher flame retardancy of resin materials.

When polytetrafluoroethylene is used in a thermoplastic resin composition, it is known that fiberization thereof in a resin performs effects of enhancing the melt tension of a resin, preventing draw down in blow molding, preventing jetting in injection molding, decreasing specific gravity in foaming molding, improving appearance in extrusion molding, and promoting the dispersibility of a filler in a resin composition containing the filler.

However, polytetrafluoroethylene has poor compatibility with most of thermoplastic resins, and it is difficult to uniformly disperse polytetrafluoroethylene and an aggregate tends to be formed, only by adding

polytetrafluoroethylene to a resin composition and simply blending this. The aggregate of polytetrafluoroethylene causes the poor appearance of a molded article, further, increases the addition amount necessary for
5 manifestation of flame retardancy and tends to invite decrease in mechanical properties such as impact resistance and the like. Because of such a reason, there is a strong desire for a technology by which the uniform dispersion of polytetrafluoroethylene in a thermoplastic
10 resin composition can be conducted easily, and flame retardancy can be improved by adding a small amount of it.

There are conventionally trials in which by using a mixture of polytetrafluoroethylene with an organic polymer, polytetrafluoroethylene is dispersed successfully
15 and the flame retardancy of a thermoplastic resin composition is improved. For example, Japanese Patent Application Publication (JP-B) No. 5-8749 describes that flame retardancy is improved if a powder obtained by mixing a polytetrafluoroethylene dispersion and an aromatic vinyl-based polymer dispersion and co-coagulating
20 the mixture is used and this powder is added. However, in the case of co-coagulation with a polytetrafluoroethylene dispersion using an aromatic vinyl-based polymer dispersion, when temperature in co-coagulation is
25 too low, coating of polytetrafluoroethylene with an aromatic vinyl-based polymer becomes difficult, a mixture of fine particles of an aromatic vinyl-based polymer

single body with a self adhered substance of mutual
polytetrafluoroethylenes is formed, and the resulted
powder mixture shows poor handling and flowability, and
dispersibility in the thermoplastic resin of the powders
5 becomes insufficient. By this, there is a possibility
of occurrence of variation in property of manifesting
prevention of dropping of flame drips in combustion and
there occurs also a possibility of decrease in the sur-
face appearance of a molded article due to poor dis-
10 persibility.

Thus, in the case of obtaining a powder by mixing a
polytetrafluoroethylene dispersion and an aromatic vi-
nyl-based polymer dispersion and co-coagulating the mix-
ture, temperature in co-coagulation should be as near
15 the boiling point of water as possible, therefore, work-
ing safety and productivity are not practical.

Further, Japanese Patent Application Laid-Open (JP-
A) No. 9-95583 describes that a powder obtained by po-
lymerizing an organic monomer in the presence of a
20 polytetrafluoroethylene dispersion is excellent in han-
dling. However, the particle size of an organic polymer
obtained by polymerization in the presence of a
polytetrafluoroethylene dispersion is not described
here. Actually, with the technology described specifi-
25 cally here, a tendency is manifested in which when the
content of polytetrafluoroethylene is higher, the re-
sulted powder gets larger particle size, and the flow-

ability of the powder decreases. Namely, this powder shows a tendency of decrease in handling with increase in the content of polytetrafluoroethylene. When such a powder is mixed with a thermoplastic resin, there is a possibility that poor dispersion in a thermoplastic resin composition is caused, exerting a reverse influence on the surface appearance of a molded article. In completion of polymerization of an acrylonitrile-styrene-based polymer, disposal of remaining acrylonitrile monomer and styrene monomer needs enormous cost, and in burning thereof, there occurs also a possibility of generation of a toxic hydrogen cyanide gas from the acrylonitrile-styrene-based polymer.

Japanese Patent No. 2942888 describes a method of obtaining a powder showing excellent dispersibility of polytetrafluoroethylene, by polymerizing a vinyl-based monomer in a dispersion obtained by mixing an organic polymer particle dispersion composed of an alkyl (meth)acrylate having 5 to 30 carbon atoms with a polytetrafluoroethylene particle dispersion. However, in this method, an alkyl (meth)acrylate-based polymer obtained from an alkyl (meth)acrylate having 5 to 30 carbon atoms is used for the purpose of improving the dispersibility of polytetrafluoroethylene in a polyolefin resin, and use in resins other than polyolefin resins, particularly use in engineering plastics is not considered. Also in dispersibility thereof and storage

stability for a long period of time of a powder, there is the room of improvement.

JP-A No. 2000-63652 describes that an alkyl (meth)acrylate-based polymer and polytetrafluoroethylene show improvements in the draw down resistance and flame retardancy of a thermoplastic resin composition. However, in this method, individual powders of an alkyl (meth)acrylate-based polymer and polytetrafluoroethylene are mixed with a thermoplastic resin, before melting and kneading thereof, and there is a possibility that dispersion of polytetrafluoroethylene becomes poor and no good appearance of a molded article is invited.

DISCLOSURE OF THE INVENTION

The present invention has been investigated for solving the problems of the above-mentioned conventional technologies, and the object thereof is to provide a modifier for thermoplastic resin which provides, in addition to a thermoplastic resin, high dispersibility of polytetrafluoroethylene and can improve various physical properties such as excellent mechanical properties and flame retardancy and the like by addition thereof in small amount, and a thermoplastic resin composition obtained by using this.

The present inventors have intensively studied to attain the above-mentioned object, and resultantly found that a polytetrafluoroethylene-containing modifier ob-

tained by using an alkyl (meth)acrylate-based polymer containing 70% by weight or more of a constituent unit composed of an alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms performs a very excellent effect, leading to completion of the invention.

Namely, the present invention relates to a modifier for thermoplastic resin, comprising polytetrafluoroethylene (A), and an alkyl (meth)acrylate-based polymer (B) containing 70% by weight or more of a constituent unit composed of an alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms.

Further, the present invention relates to a thermoplastic resin composition obtained by adding the above-mentioned modifier to a thermoplastic resin (C) so that the content of the polytetrafluoroethylene (A) is 0.001 to 20 parts by weight based on 100 parts by weight of the thermoplastic resin (C); and a thermoplastic resin composition comprising the above-mentioned modifier, thermoplastic resin (C) and a flame retardant (D), or the above-mentioned modifier, thermoplastic resin (C) and a filler (E).

In the present invention, "(meth)acryl" means acryl and/or methacryl.

BEST MODES FOR CARRYING OUT THE INVENTION

The polytetrafluoroethylene (A) used in the modifier of the present invention is obtained by polymeriz-

ing monomers containing tetrafluoroethylene as the main component. The polytetrafluoroethylene may be copolymerized with other monomer in an amount not deteriorating the desired properties. As the copolymerization component, for example, fluorine-containing olefins such as hexafluoropropylene, chlorotrifluoroethylene, fluoroalkylethylene, perfluoroalkyl vinyl ether and the like; fluorine-containing alkyl (meth)acrylates such as perfluoroalkyl (meth)acrylate and the like; etc. are listed. The amount of the copolymerization components is preferably 10% by weight or less in 100% by weight of the total amount of tetrafluoroethylene and copolymerization components.

The polytetrafluoroethylene (A) is preferably not an aggregate but a particle having an average particle size of 10 μm or less.

The alkyl (meth)acrylate-based polymer (B) used in the modifier of the present invention is a polymer containing 70% by weight or more of a constituent unit composed of an alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms. The alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms can be polymerized by radical polymerization, ion polymerization and the like. In the present invention, since the alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms is used, the dispersibility of polytetrafluoroethylene in various thermoplastic resins

and thermoplastic elastomers is more excellent as compared with conventional polytetrafluoroethylene-containing modifiers. Further, the alkyl (meth)acrylate-based polymer manifests no possibility of generation of a toxic gas in combustion, additionally, shows a significantly smaller amount of monomers remaining in completion of polymerization, and provides low load on environments, as compared with conventional acrylonitrile-styrene-based polymers.

Specific examples of the alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms include methyl (meth)acrylate, ethyl (meth)acrylate, butyl (meth)acrylate and the like. The alkyl group may be linear or branched. These can be used alone or in combination of two or more. Particularly, polymers containing a constituent unit composed of methyl methacrylate in an amount of 50% by weight or more, more preferably 70% by weight or more are preferable since a powder excellent in handling and storage stability is obtained.

In preparing the alkyl (meth)acrylate-based polymer (B), other monomers copolymerizable with the alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms can be used in an amount of 30% by weight or less. Examples of other monomers include vinyl ether-based monomers such as vinyl methyl ether, vinyl ethyl ether and the like; vinyl carboxylate-based mono-

mers such as vinyl acetate, vinyl butyrate and the like; olefin-based monomers such as ethylene, propylene, isobutylene and the like; diene-based monomers such as butadiene, isoprene, dimethylbutadiene and the like; and
5 other monomers.

Particularly, it is preferable to use an alkyl (meth)acrylate-based polymer (B) containing an alkyl methacrylate carrying an alkyl group having 1 to 4 carbon atoms and an alkyl acrylate carrying an alkyl group
10 having 1 to 4 carbon atoms in a total amount thereof of 70% by weight or more. When an alkyl methacrylate is singly used, Tg is higher, a fine powder is generated in large amount in recovering a powder, and powder handling tends to lower, while when an alkyl acrylate is con-
15 tained, Tg lowers, and powder property is improved. In this case, it is preferable that the content of the alkyl methacrylate is 50 to 90% by weight and the content of the alkyl acrylate is 10 to 50% by weight, and powder property is best with such a composition.

20 The weigh-average molecular weight (Mw) of the alkyl (meth)acrylate-based polymer (B) is preferably from 20,000 to 4,000,000, more preferably from 20,000 to 100,000. When Mw is 100,000 or less, there is a tendency that flowability is not deteriorated in adding a
25 modifier to a thermoplastic resin. Particularly from the standpoint of physical property balance, Mw is further preferably from 20,000 to 50,000. This Mw is a

value measured by gel permeation chromatography.

The modifier of the present invention comprises the above-mentioned polytetrafluoroethylene (A) and alkyl (meth)acrylate-based polymer (B) as the main component.

5 Regarding the ratio thereof, it is preferable that the proportion of the polytetrafluoroethylene (A) is from 0.01 to 70 parts by weight based on 100 parts by weight of the total amount of them. In the modifier of the present invention, the content of the polytetrafluoro-
10 ethylene (A) is preferably from 20 to 70% by weight, more preferably from 40 to 70% by weight. When this content is 40% by weight or more, the addition efficiency of the modifier is improved, and when 70% by weight or less, there occurs a tendency that dispersi-
15 bility and processability are not deteriorated.

For example the modifier of the present invention is obtained by a method [first production method] in which monomers containing 70% by weight or more of an alkyl (meth)acrylate carrying an alkyl group having 1 to
20 4 carbon atoms are polymerized in a dispersion wherein the polytetrafluoroethylene (A) particles having an average particle size of 0.05 to 1.0 μm are dispersed, to form an alkyl (meth)acrylate-based polymer (B), then, solid components in the resulted dispersion are coagu-
25 lated or spray-dried.

For further example, the modifier of the present invention is obtained by a method [second production

method] in which a dispersion wherein the polytetrafluoroethylene (A) particles having an average particle size of 0.05 to 1.0 μm are dispersed is mixed with a dispersion wherein the alkyl (meth)acrylate-based polymer (B) particles containing 70% by weight or more of a constituent unit composed of an alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms are dispersed, then, solid components in the mixed dispersion are coagulated or spray-dried.

10 Coagulation of solid components in the dispersion according to the first production method and the second production method can be conducted, for example, by putting them into hot water containing a dissolved metal salt such as calcium chloride, magnesium sulfate and the like and salting them out. Spray drying can be conducted, for example, by spraying the aqueous solution itself.

When monomers containing 70% by weight or more of an alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms are polymerized in a dispersion wherein the polytetrafluoroethylene (A) particles are dispersed, to form the alkyl (meth)acrylate-based polymer (B), then, solid components in the dispersion are coagulated or spray-dried, to obtain the modifier of the present invention, or when monomers containing 70% by weight or more of an alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms are polymerized

to obtain a dispersion of alkyl (meth)acrylate-based polymer (B) particles, then, this dispersion is mixed with a dispersion wherein the polytetrafluoroethylene (A) particles are dispersed, and solid components in the
5 resulted dispersion are coagulated or spray-dried, to obtain the modifier of the present invention, it is preferable to conduct polymerization so that the average particle size of the alkyl (meth)acrylate-based polymer (B) is 0.05 to 0.15 μm (more preferably 0.05 to 0.1 μm).
10 In the alkyl (meth)acrylate-based polymer (B), when the content of an alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms is 70% by weight or less, particularly when the content of methyl methacrylate is 70% by weight or less, handling and storage sta-
15 bility for a long period of time of the resulting powder lower, undesirably.

The dispersion of polytetrafluoroethylene (A) particles can be obtained by emulsion-polymerizing monomers containing tetrafluoroethylene as the main component.
20 Further, as the commercially available product (trade name) of the aqueous dispersion of polytetrafluoroethylene (A) particles, Fluone AD-1, AD-936 manufactured by Asahi Fluoro Polymers K.K.; Polyfrone D-1, D-2 manufactured by Daikin Industries, Ltd.; Teflon 30J manufac-
25 tured by Mitsui Dupont Fluoro Chemical K.K., and the like are listed.

The dispersion of alkyl (meth)acrylate-based poly-

mer (B) particles containing 70% by weight or more of a constituent unit composed of an alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms is obtained by emulsion polymerization, mini emulsion polymerization and the like of monomers containing 70% by weight or more of an alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms. The emulsifier which can be used in these polymerizations is not particularly restricted, and conventionally known various emulsifiers can be used. For example, anionic surfactants such as fatty acid salts, alkyl sulfate salts, alkylbenzenesulfonate salts, alkylphosphate salts, dialkylsulfosuccinate salts and the like; nonionic surfactants such as polyoxyethylene alkyl ether, polyoxyethylene fatty esters, sorbitan fatty esters, glycerin fatty esters and the like; cationic surfactants such as alkylamine salts and the like, can be used. These emulsifiers can be used alone or in combination.

When pH of the polymerization system shift to the alkaline side depending on the kind of the emulsifier used, a suitable pH controlling agent can be used for preventing hydrolysis of an alkyl (meth)acrylate. Examples of the pH controlling agent include boric acid-potassium chloride-potassium hydroxide, potassium dihydrogen phosphate-disodium hydrogen phosphate, boric acid-potassium chloride-potassium carbonate, citric acid-potassium hydrogen citrate, potassium dihydrogen

phosphate-boric acid, disodium hydrogen phosphate-citric acid and the like are listed.

As the polymerization initiator used in polymerization of an alkyl (meth)acrylate, for example, single
5 component systems of water-soluble initiators or oil-soluble initiators, or initiators of redox system, are listed. As the specific examples of the water-soluble initiators, inorganic initiators such as a persulfate and the like are listed. As the specific examples of
10 the oil-soluble initiators, organic peroxides such as t-butyl hydroperoxide, cumene hydroperoxide, benzoyl peroxide, lauroyl peroxide and the like; azo compounds, and the like are listed. Specific examples of the redox type initiators include, but not limited to, initiators
15 obtained by combining the above-mentioned inorganic initiators with a sulfite, hydrogensulfite, thiosulfite and the like, initiators obtained by combining the above-mentioned organic peroxides and azo compounds with sodium formaldehyde sulfoxylate and the like, and the
20 like.

One of the thermoplastic resin compositions of the present invention is that obtained by adding the modifier of the present invention so that the content of the polytetrafluoroethylene (A) is from 0.001 to 20 parts by
25 weight based on 100 parts by weight of the thermoplastic resin (C). When the modifier of the present invention is used in an amount within this range, a polytetra-

fluoroethylene component is uniformly dispersed in the thermoplastic resin (C), giving excellent mechanical property and flame retardancy.

As thermoplastic resin (C), conventionally known various thermoplastic resins are listed. The term "thermoplastic resin" referred to in the present invention is intended to include also thermoplastic elastomers. Specific examples thereof include engineering plastics such as styrene-based resins (St-based resins) such as polystyrene (PS), high impact polystyrene (HIPS), (meth)acrylate-styrene copolymer (MS), acrylonitrile-styrene copolymer (SAN), styrene-maleic anhydride copolymer (SMA), ABS, ASA, AES and the like, acrylic resins (Ac-based resins) such as polymethyl methacrylate (PMMA) and the like, polycarbonate-based resins (PC-based resins), polyamide-based resins (PA-based resins), polyester-based resins (PEs-based resins) such as polyethylene terephthalate (PET), polybutylene terephthalate (PBT) and the like, (modified) polyphenylene ether-based resins (PPE-based resins), polyoxymethylene-based resins (POM-based resins), polysulfone-based resins (PSO-based resins), polyarylate-based resins (PAr-based resins), polyphenylene sulfide-based resins (PPS-based resins), thermoplastic polyurethane-based resins (PU-based resins) and the like; polymer alloys such as PC-based resin/St-based resin alloys such as PC/ABS resins and the like, PA-based resin/St-based resin alloys such as

PA/ABS resins and the like, PA-based resin/polyolefin-based resin alloys such as PA/PP and the like, PC-based resin/PES-based resin alloys such as PC/PBT and the like, alloys of mutual polyolefin-based resins such as PP/PE and the like, PPE-based resin alloys such as PPE/HIPS, PPE/PBT, PPE/PA and the like; polyolefin-based resins such as poly- α -olefins such as polyethylene, (ultra) low density polyethylene, polypropylene, polybutene, poly-4-methylpentene and the like, copolymers of mutual α -olefins such as ethylene propylene rubber, ethylene butene copolymer, ethylene butene terpolymer and the like, copolymers of α -olefins with various monomers such as an ethylene vinyl acetate copolymer, ethylene/ethyl acrylate copolymer, ethylene methyl methacrylate copolymer, ethylene/maleic anhydride copolymer, ethylene/acrylic acid copolymer, ethylene/glycidyl methacrylate copolymer and the like; and thermoplastic elastomers such as polylactic acid, polycaprolactone, aliphatic polyester resins essentially consisting of an aliphatic glycol and an aliphatic dicarboxylic acid or derivative thereof, bio-degradable cellulose esters, polypeptides, polyvinyl alcohol, starch, carageenan, chitin·chitosan, bio-degradable resins such as natural linear polyester-based resins and the like, styrene-based elastomers, urethane-based elastomers, polyester-based elastomers, polyamide-based elastomers, fluorine-based elastomers, 1,2-polybutadiene, trans-1,4-

polyisoprene, acrylic elastomers and the like. However, the thermoplastic resin (C) is not limited to these examples, and general thermoplastic resins other than these examples can be used. These may be used alone or
5 in combination of two or more.

To the thermoplastic resin composition of the present invention, various additives such as a flame retardant, plasticizer, stabilizer, filler, impact resistance improving agent, lubricant, processing aid, foaming
10 agent, pigment, de-fogging agent, anti-bacterial agent, antistatic agent, conductivity imparting agent, surfactant, crystal nucleating agent, heat resistance improving agent and the like can be added depending on the object, providing the properties of the composition are
15 not deteriorated.

Examples of the flame retardant (D) include phosphates such as tricresyl phosphate, triallyl phosphate, triphenyl phosphate, cresyl diphenyl phosphate, tri(chloroethyl) phosphate, tris(dichloropropyl) phosphate, tris(2,3-dibromopropyl) phosphate and the like;
20 condensed phosphates such as phenylenebis(phenylglycidyl phosphate) and the like; phosphorus-based compounds such as red phosphorus, polyammonium phosphate/pentaerythritol complex system and the like; poly-
25 ols such as phosphate-type polyols, halogen-containing polyols, phosphorus-containing polyols and the like; aromatic halogen compounds such as hexabromobenzene, de-

cabromodiphenyl oxide and the like; halogenated epoxy resins such as brominated bisphenol-based epoxy resins and the like; halogenated polycarbonate resins; brominated polystyrene resins; brominated bisphenol cyanurate resins; brominated polyphenylene oxides; decabromodiphenyl oxide bisphenol condensate; metal hydroxides such as aluminum hydroxide, magnesium hydroxide, calcium hydroxide, calcium aluminate, hydrotalcite and the like; antimony compounds such as antimony trioxide, antimony pentoxide and the like; triazine compounds such as melamine, cyanuric acid, melamine cyanurate and the like; additionally, kaolin clay, dorsonite, calcium carbonate zinc borate, molybdenum compounds, ferrocene, tin compounds, inorganic complex salts and the like. Particularly, phosphates containing no halogen such as tricresyl phosphate, triallyl phosphate, triphenyl phosphate, cresyl diphenyl phosphate and the like and condensed phosphates such as phenylenebis(phenylglydicyl phosphate) and the like, are preferably used.

As the filler (E), metal powders, oxides, hydroxides, silic acid or silicates, carbonates, silicon carbonate, vegetable fiber, animal fiber, synthetic fiber and the like are listed. Specific typical examples thereof include an aluminum powder, copper powder, iron powder, alumina, natural woods, paper, calcium carbonate, talc, magnesium carbonate, mica, kaolin, calcium sulfate, barium sulfate, aluminum hydroxide, magnesium

hydroxide, silica, clay, zeolite, talc, wollastonite, acetate powder, silk powder, aramide fiber, glass fiber, carbon fiber, metal fiber, carbon black, graphite, glass beads, reproduced filler materials and the like.

5 As the reproduced filler material used in the filler (E), agricultural wastes such as hull, bran, rice polishings, corn waste, potato shell, de-fatted soy bean, walnut shell, coconut shell, bagasse and the like; brewing lees such as distillation lees of distilled al-
10 cohol such as shochu and the like, beer malt lees, wine grape lees, sake-cake, soy bean lees and the like; various sediments such as tea sediment, coffee sediment, citrus squeezed sediment and the like; food processing wastes such as okara (bean curd waste), chlorella and
15 the like; fishery wastes such as shells such as oyster shell and the like, mail of shrimp and crab and the like; wood wastes such as sawdust, scrapped wood (haiho-daki), bark, cut bamboo, waste wood generated by wood cutting in a lumber mill, demolition of wood houses and
20 the like; wastes such as waste pulp, paper piece and the like generating in paper regeneration and paper making businesses, are listed. These can be used alone or in admixture of two or more.

25 The form and size of the filler (E) are not particularly restricted, and in the case of particular shape, when particle size is larger, and in the case of fiber shape, when fiber is too long, the dispersibility

of the filler (E) lowers and the product appearance deteriorates, therefore, ground fillers are preferably used, and those are preferably 10 mesh pass or smaller, more preferably 100 mesh pass or smaller. From the
5 standpoint of handling of a ground article, those are preferably 10000 mesh pass or larger.

Though the water content of the filler (E) is not particularly restricted, since the filler (E) often contains water in large proportion, it is preferable to dry
10 the filler (E) by an oven or heat stirring treatment and the like until the water content reaches 20% by weight or less due to handling as a powder. Further, even if the water content is 20% by weight or less, when abnormal foaming and the like occur on a molded article, it
15 is preferable to further dry the filler by an oven or heat stirring treatment and the like, and it is particularly preferable to dry the filler until the water content reaches 1% by weight or less.

For improving dispersibility into the thermoplastic
20 resin (C), it is possible to use fillers previously surface-treated with fine particles of polybasic acid anhydrides such as maleic anhydride and the like, organic peroxide such as dicumyl peroxide and the like, polyolefins modified with an acid, polyester-based waxes, fatty
25 acid metal salts such as zinc stearate and the like, metal oxides such as titanium oxide, calcium oxide and the like.

The fillers (E) can be used alone or in admixture of two or more. The compounding amount of the filler (E) is preferably from 0 to 2000 parts by weight based on 100 parts by weight of the thermoplastic resin (C).

5 It is preferable from the standpoint of appearance that this compounding amount is 2000 parts by weight or less.

As the typical examples of the foaming agent (F), inorganic foaming agents, volatile foaming agents, decomposing type foaming agents and the like are listed.

10 As the inorganic foaming agent, for example, carbon dioxide, air, nitrogen and the like are listed. Examples of the volatile foaming agent include aliphatic hydrocarbons such as propane, n-butane, isobutene, pentane, hexane and the like, halogenated hydrocarbons such as
15 trichlorofluoromethane, dichlorofluoromethane, dichlorotetrafluoroethane, methyl chloride, ethyl chloride, methylene chloride and the like. As the decomposing type foaming agent, for example, azodicarbonamide, dinitrosopentamethylenetetramine, azobisisobutyronitrile, sodium bicarbonate and the like are listed. These foaming
20 agents may be appropriately used in admixture.

When the foaming agent (F) is used, it may also be permissible to further add a bubble controlling agent into a melt kneaded substance of a thermoplastic resin
25 composition. As the bubble controlling agent, for example, inorganic powders such as talc, silica and the like, reaction mixtures of an acidic salt of a poly-

valent carboxylic acid, a poly-valent carboxylic acid and sodium carbonate or sodium bicarbonate, citric acid and the like are listed.

Examples of the plasticizer include phthalate-based plasticizers such as dimethyl phthalate, diethyl phthalate, dibutyl phthalate, dihexyl phthalate, di-n-octyl phthalate, 2-ethylhexyl phthalate, diisooctyl phthalate, dicapryl phthalate, dinonyl phthalate, diisononyl phthalate, didecyl phthalate, diisodecyl phthalate, diundecyl phthalate, dilauryl phthalate, ditridecyl phthalate, dibenzyl phthalate, dicyclohexyl phthalate, butylbenzyl phthalate, octyldecyl phthalate, butyloctyl phthalate, octylbenzyl phthalate, n-hexyl-n-decyl phthalate, n-octyl-n-decyl phthalate and the like; phosphate-based plasticizers such as tricresyl phosphate, tri-2-ethylhexyl phosphate, triphenyl phosphate, 2-ethylhexyl diphenyl phosphate, cresyl diphenyl phosphate and the like; adipate-based plasticizers such as di-2-ethylhexyl adipate, diisodecyl adipate, n-octyl-n-decyl adipate, n-heptyl-n-nonyl adipate, diisooctyl adipate, diiso-n-octyl adipate, di-n-octyl adipate, didecyl adipate and the like; sebacate-based plasticizers such as dibutyl sebacate, di-2-ethylhexyl sebacate, diisooctyl sebacate, butylbenzyl sebacate and the like; azelate-based plasticizers such as di-2-ethylhexyl azelate, dihexyl azelate, diisooctyl azelate and the like; citrate-based plasticizers such as triethyl citrate, triethyl acetylcitrate,

tributyl citrate, tributyl acetylcitrate, tri-2-ethylhexyl acetylcitrate and the like; glycolate-based plasticizers such as methylphthalylethyl glycolate, ethylphthalylethyl glycolate, butylphthalylbutyl glycolate and the like; trimellitate-based plasticizers such as tributyl trimellitate, tri-n-hexyl trimellitate, tri-2-ethylhexyl trimellitate, tri-n-octyl trimellitate, tri-isooctyl trimellitate, tri-isodecyl trimellitate and the like; phthalic acid isomer ester-based plasticizers such as di-2-ethylhexyl isophthalate, di-2-ethylhexyl terephthalate and the like; ricinolate-based plasticizers such as methylacetyl ricinolate, butylacetyl ricinolate and the like; polyester-based plasticizers such as polypropylene adipate, polypropylene sabacate, modified polyesters thereof, and the like; epoxy-based plasticizers such as epoxidized soy bean oil, epoxybutyl stearate, epoxy(2-ethylhexyl) stearate, epoxidized linseed oil and the like. These can be used alone or in combination of two or more.

Examples of the stabilizer include lead-based stabilizers such as tri-basic lead sulfate, dibasic lead phosphite, basic lead sulfite, lead silicate and the like; metal soap-based stabilizers derived from metals such as potassium, magnesium, barium, zinc, cadmium, lead and the like and fatty acids such as 2-ethylhexanoic acid, lauric acid, myristic acid, palmitic

acid, stearic acid, isostearic acid, hydroxystearic acid, oleic acid, ricinoleic acid, behenic acid and the like; organic tin-based stabilizers derived from an alkyl group, ester group, and fatty acid salt, maleate, sulfur-containing compound; complex metal soap-based stabilizers such as Ba-Zn-based, Ca-Zn-based, Ba-Ca-based, Ca-Mg-Sn-based, Ca-Zn-Sn-based, Pb-Sn-based, Pb-Ba-Ca-based stabilizers and the like; metal salt-based stabilizers derived from metals such as barium, zinc and the like, and usually two or more organic acids such as branched fatty acids such as 2-ethylhexanoic acid, isodecanoic acid, trialkylacetic acid and the like, unsaturated fatty acids such as oleic acid, ricinoleic acid, linoleic acid and the like, alicyclic acids such as naphthenic acid and the like, aromatic acids such as phenol, benzoic acid, salicylic acid, and substituted derivatives thereof; metal-based stabilizers such as metal salt liquid stabilizers obtained by dissolving the above-mentioned stabilizers in an organic solvent such as petroleum-based hydrocarbons, alcohols, glycerin-derivatives and the like, and further compounding a stabilizing aid such as phosphites, epoxy compounds, coloration preventing agents, transparency improving agents, light stabilizers, antioxidants, lubricants and the like; and non-metal-based stabilizers such as epoxy compounds such as epoxy resins, epoxidized soy bean oil, epoxidized vegetable oil, epoxidized fatty alkyl esters

and the like, organic phosphites in which phosphorus is substituted by an alkyl group, aryl group, cycloalkyl group, alkoxyl group and the like and which has a dihydric alcohol such as propylene glycol and the like, an aromatic compound such as hydroquinone, bisphenol A and the like, hindered phenols such as bisphenol dimerized via BHT, sulfur, methylene group and the like, ultraviolet absorbers such as salicylates, benzophenone, benzotriazole and the like, light stabilizers such as hindered amine or nickel complex salt, ultraviolet shielding agents such as carbon black, rutile type titanium oxide and the like, poly-hydric alcohols such as trimethylolpropane, pentaerythritol, sorbitol, mannitol and the like, nitrogen-containing compounds such as β -aminocrotonate, 2-phenylindole, diphenylthiourea, dicyanedi-
15 amide and the like, sulfur-containing compounds such as dialkylthiodipropionates and the like, keto compounds such as acetoacetates, dehydro acetic acid, β -diketone and the like, organic silicon compounds, borates and the like. These can be used alone or in combination of two or more.

Examples of the impact resistance improving agent include polybutadiene, polyisoprene, polychloroprene, fluorine rubber, styrene-butadiene-based copolymer rubber, methyl methacrylate-butadiene-styrene-based copolymer, methyl methacrylate-butadiene-styrene-based graft copolymer, acrylonitrile-styrene-butadiene-based copoly-

mer rubber, acrylonitrile-styrene-butadiene-based graft
copolymer, styrene-butadiene-styrene block copolymer
rubber, styrene-isoprene-styrene copolymer rubber, sty-
rene-ethylene-butylene-styrene copolymer rubber, ethyl-
5 ene-propylene copolymer rubber, ethylene-propylene-diene
copolymer rubber (EPDM), silicone-containing acrylic
rubber, silicone/acryl complex rubber-based graft co-
polymer, silicone-based rubber and the like. As the di-
ene in ethylene-propylene-diene copolymer rubber (EPDM),
10 1,4-hexanediene, dicyclopentadiene, methylenenorbornene,
ethlidenenorbornene, propenylnorbornene and the like are
listed. These impact resistance improving agents can be
used alone or in combination of two or more.

Examples of the lubricant include pure hydrocarbon-
15 based lubricants such as liquid paraffin, natural paraf-
fin, micro wax, synthetic paraffin, lower molecular
weight polyethylene and the like; halogenated hydrocar-
bon-based lubricants; aliphatic lubricants such as
higher fatty acids, oxy fatty acids and the like; fatty
20 amide-based lubricants such as fatty amides, bisfatty
amides and the like; ester-based lubricants such as
lower alcohol esters of fatty acids, poly-hydric alcohol
esters of fatty acids such as glyceride and the like,
polyglycol esters of fatty acids, fatty alcohol esters
25 of fatty acids (ester waxes) and the like; and lubri-
cants composed of metal soaps, fatty alcohols, polyva-
lent alcohols, polyglycols, polyglycerols, partial es-

ters of fatty acids and poly-hydric alcohols, partial esters of fatty acids, polyglycols and polyglycerols.

Examples of the processing aid include (meth)acrylate-based copolymers, (meth)acrylate-styrene copolymers, (meth)acrylate-styrene- α -methylstyrene copolymers, acrylonitrile-styrene copolymers, acrylonitrile-styrene-(meth)acrylate copolymers, acrylonitrile-styrene- α -styrene copolymers, acrylonitrile-styrene-maleimide copolymers and the like.

10 Compounding of the modifier of the present invention into the thermoplastic resin (C) can be conducted, for example, by melt kneading by conventionally known methods such as extrusion kneading, roll kneading and the like. Further possible is multi-stage mixing in
15 which the modifier of the present invention and a part of the thermoplastic resin (C) are mixed first to provide a master batch, and the remaining part of the thermoplastic resin (C) is further added to and mixed with this.

20 As the method of molding a thermoplastic resin composition containing the modifier of the present invention added, for example, calender molding, heat molding, extrusion blow molding, foaming molding, extrusion molding, injection molding, melt spinning and the like are
25 listed.

As the useful molded articles obtained by using a thermoplastic resin composition containing the modifier

of the present invention added, for example, molded articles in the form of sheet, film or hetero shape obtained by extrusion molding; hollow molded bodies, injection molded bodies and the like obtained by blow

5 molding and injection molding. Specific examples thereof include bumpers, spoilers, side moles of automobiles, ceilings, interiors, housings of OA instruments, construction materials such as window frames, shelf plates, floor materials, wall materials and the like.

10 The present invention will be illustrated further in detail by the following examples below, but the scope of the present invention is not limited to them. In the descriptions, parts and % are all by weight. Measurements of physical properties were carried out by the
15 following methods.

(1) Solid component concentration:

It was determined by drying a particle dispersion at 180°C for 30 minutes.

(2) Particle size measurement:

20 A dispersion of modifier particles was diluted with distilled water and used as a sample, and the particle size thereof was measured using CHDF 2000 type grain size distribution meter manufactured by MATEC, US. The measurement was conducted according to the standard conditions recommended by MATEC. Namely, an exclusive capillary type cartridge for particle separation and approximately neutral carrier liquid were used, and 0.1 ml
25

of a diluted latex sample having a concentration of about 3% was used for measurement, at a flow rate of 1.4 ml/min, a pressure of about 4000 psi (2600 KPa) and a temperature of 35°C. As the standard particle size substances, twelve mono-dispersed polystyrene particles in total, having known particle sizes within the range from 0.02 μm to 0.8 μm , manufactured by DUKE, US were used.

(3) Weigh-average molecular weight measurement:

Measurement was conducted using a column (K-806L, manufactured by Showa Denko K.K.) in gel permeation chromatography (LC-10A system, manufactured by Shimadzu Corp.)

(4) Measurement of flowability of powder:

It was measured using a bulk specific gravity meter (manufactured by Tsutsui Rikagaku Kikai K.K.) according to JIS K6721. In this measurement, a powder was filled in a funnel of the bulk specific gravity meter, then, the powder was flowed for 10 seconds from the funnel, and the powder flown was weighed, and used as an index of flowability of the powder (g/10 sec).

Larger amount of the powder flow during 10 seconds means excellent flowability of the powder. In actual working, a powder showing excellent flowability means excellent handling, too.

(5) Measurement of storage stability of powder

20 g of a powder was filled in an acrylic resin vessel, which was placed in a gear oven (GHPS-222, manu-

factured by Tabai K.K.) having a temperature controlled in the oven of 50°C and left for 6 hours while placing a weight of 5 kg on the vessel, then, removed and cooled to room temperature, to produce a block of the powder.

- 5 This powder was placed on a sieve having an opening of 12 mesh, and crushed by a vibration sieving machine (micro form magnetic vibration sieving machine M-2, manufactured by Tsutsui Rikagaku Kikai K.K.), and time when the crushed amount reached 60% was used measured and
10 used to indicate the storage stability of the powder.

When the time when this crushed amount reaches 60% is shorter, the powder is not easily solidified during actual storage of the powder, and even if solidified, the block of the powder can be easily broken.

- 15 (6) Combustibility test:

Vertical combustibility test was carried out according to UL 94 standard. A specimen having a thickness of 1.6 mm was used.

- (7) Izod impact strength test:

- 20 It was measured using a notched specimen having a thickness of 3.2 mm at 23°C according to ASTM D256.

- (8) Tensile test:

The tensile strength and tensile elongation were measured according to ASTM D638.

- 25 (9) Surface appearance:

The surface appearance of a specimen injection-molded was visually observed and judged according to the

following standards.

○: Neither fish eye nor steak is observed on the surface.

×: Fish eye and steak are observed on the surface.

5 However, only in evaluations shown in Table 2, presence or absence of an aggregate in specimen was visually observed in addition to the surface appearance.

○: No fish eye is observed on the surface and no aggregate is observed in a specimen.

10 ×: Fish eye is observed on the surface and aggregate is observed in a specimen.

<Production Example 1: modifier for thermoplastic resin (A-1)>

15 To 83.3 parts of a polytetrafluoroethylene particle dispersion (manufactured by Asahi Fluoro Polymers K.K., Fluone AD936, solid concentration: 63.0%, containing a polyoxyethylene alkyl phenyl ether in a proportion of 5% based on polytetrafluoroethylene) was added 116.7 parts of distilled water, to obtain a polytetrafluoroethylene
20 particle dispersion (A-1-1) having a solid content of 26.2%. This dispersion (A-1-1) contains 25% of polytetrafluoroethylene particles and 1.2% of a polyoxyethylene alkyl phenyl ether.

25 165 parts of distilled water and 2.0 parts of dipotassium alkenylsuccinate were charged into a reaction vessel equipped with a stirrer, condenser, thermocouple and nitrogen introduction port, then, 80 parts of the

polytetrafluoroethylene dispersion (A-1-1) (20 parts by weight of polytetrafluoroethylene) was charged into the reaction vessel using a rotary pump (manufactured by Johnson Pump, IC30S-D), then, the atmosphere in the reaction vessel was purged with nitrogen by passing a nitrogen flow through the vessel. Then, the temperature in the system was raised to 55°C, and when the liquid temperature inside reached 55°C, a mixture composed of 0.1 part of potassium persulfate and 5 parts of distilled water was added, further, to this was dropped 64 parts of methyl methacrylate and 16 parts of n-butyl methacrylate over 90 minutes, and these were polymerized. After completion of dropping, the reaction mixture was kept for about 45 minutes, to complete the polymerization. Throughout a series of operations, no separation of solid was observed, and a uniform particle dispersion was obtained.

On the other hand, 150 parts of an aqueous solution dissolving calcium acetate in a proportion of 7% was heated at 70°C and stirred. Into this aqueous solution was gradually dropped 100 parts of the particle dispersion previously prepared, to precipitate solid. Then, this precipitate was separated, filtrated and dried, to obtain a polytetrafluoroethylene-containing thermoplastic resin modifier (A-1).

The average particle size of the alkyl (meth)acrylate-based polymer in this particle dispersion

was 0.80 μm . The weigh-average molecular weight (M_w) of the alkyl (meth)acrylate-based polymer measured by gel permeation chromatography was 2,600,000.

<Production Example 2: modifier for thermoplastic resin
5 (A-2)>

A polytetrafluoroethylene particle dispersion (A-2-1) having a solid content of 26.2% was obtained in the same manner as in Production Example 1. 200 parts of this dispersion (A-2-1) (50 parts of polytetrafluoro-
10 ethylene) was charged into a reaction vessel equipped with a stirrer, condenser, thermocouple and nitrogen introduction port by using a rotary pump (IC30S-D), then, 35 parts of distilled water, 3.0 parts of dipotassium alkenylsuccinate, 40 parts by methyl methacrylate, 10
15 parts of n-butyl acrylate, 0.2 parts of t-butyl hydroperoxide and 0.5 parts of n-octylmercaptane as a chain transfer agent were charged, and the atmosphere in the reaction vessel was purged with nitrogen by passing a nitrogen flow through the vessel. Then, the temperature
20 in the system was raised to 60°C, and when the liquid temperature inside reached 60°C, a mixture composed of 0.0005 parts of iron sulfate (II), 0.0015 parts of disodium ethylenediaminetetraacetate, 0.3 parts of rongalite salt and 5 parts of distilled water was added, to initi-
25 ated radical polymerization. This condition was kept for 90 minutes, to complete the polymerization. Through a series of operations, no separation of solid was ob-

served, and a uniform particle dispersion was obtained. Thereafter, precipitation, separation, filtration and drying were conducted in the same manner as in Production Example 1, to obtain a polytetrafluoroethylene-
5 containing thermoplastic resin modifier (A-2).

The average particle size of the alkyl (meth)acrylate-based polymer in this particle dispersion was 0.07 μm . The Mw of the alkyl (meth)acrylate-based polymer was 47,000.

10 <Production Example 3: modifier for thermoplastic resin (A-3)>

A polytetrafluoroethylene particle dispersion (A-3-1) having a solid content of 26.2% was obtained in the same manner as in Production Example 1.

15 On the other hand, into a reaction vessel equipped with a stirrer, condenser, thermocouple and nitrogen introduction port was charged 225 parts by distilled water, 80 parts of methyl methacrylate, 20 parts of n-butyl acrylate, 0.2 parts of n-octylmercaptane and 2.5
20 parts of sodium dodecylbenzenesulfonate, and the atmosphere in the reaction vessel was purged with nitrogen by passing a nitrogen flow through the vessel. Then, the temperature in the system was raised to 60°C, and when the liquid temperature inside reached 60°C, a mixture
25 composed of 0.0005 parts of iron sulfate (II), 0.0015 parts of disodium ethylenediaminetetraacetate, 0.3 parts of rongalite salt and 5 parts of distilled water was

added, to initiated radical polymerization. The liquid temperature was raised up to 95°C by the initiation of polymerization. Thereafter, when the liquid temperature lowered to 80°C, this condition was kept for 90 minutes, to complete the polymerization, to obtain a (meth)acrylate-based polymer particle aqueous dispersion (A-3-2). This particle aqueous dispersion (A-3-2) had a solid content of 30.4%. The average particle size of the alkyl (meth)acrylate-based polymer in this particle dispersion (A-3-2) was 0.08 μm . The Mw of the alkyl (meth)acrylate-based polymer was 50,000.

200 parts of the polytetrafluoroethylene particle dispersion (A-3-1) (50 parts of polytetrafluoroethylene) previously prepared was charged into a reaction vessel equipped with a stirrer, condenser, thermocouple and nitrogen introduction port by using a rotary pump (IC30S-D), then, 164.5 parts of the (meth)acrylate-based polymer particle aqueous dispersion (A-3-2) (50 parts of (meth)acrylate-based polymer) was charged, and the liquid inside was heated and stirred until the temperature reached 80°C. When the liquid temperature inside reached 80°C, stirring was continued for 1 hour, to obtain a mixture of both dispersions. Thereafter, precipitation, separation, filtration and drying were conducted in the same manner as in Production Example 1, to obtain a polytetrafluoroethylene-containing thermoplastic resin modifier (A-3).

<Production Example 4: modifier for thermoplastic resin (A-4)>

A polytetrafluoroethylene particle dispersion having a solid content of 26.2% (A-4-1) was obtained in the same manner as in Production Example 1.

280 parts of this dispersion (A-4-1) (70 parts of polytetrafluoroethylene) was charged into a reaction vessel equipped with a stirrer, condenser, thermocouple and nitrogen introduction port by using a rotary pump (IC30S-D), then, the atmosphere in the reaction vessel was purged with nitrogen by passing a nitrogen flow through the vessel. Then, 4.0 parts of dipotassium alkenylsuccinate and 5 parts of distilled water were charged, and the temperature in the system was raised to 55°C and when the liquid temperature inside reached 55°C, a mixture composed of 0.1 part of potassium persulfate and 5 parts of distilled water was added, further, 24 parts of methyl methacrylate, 6 parts of n-butyl methacrylate, 0.3 parts of n-octylmercaptane were dropped over 90 minutes, and they were polymerized. After completion of dropping, the mixture was kept for about 45 minutes to complete polymerization. Throughout a series of operations, no separation of solid was observed, and a uniform particle dispersion was obtained.

On the other hand, 150 parts of an aqueous solution dissolving calcium acetate in a proportion of 7% was heated at 70°C and stirred. Into this aqueous solution

was gradually dropped 100 parts of the particle dispersion previously prepared, to precipitate solid. Then, this precipitate was separated, filtrated and dried, to obtain a polytetrafluoroethylene-containing thermoplastic resin modifier (A-4).

The average particle size of the alkyl (meth)acrylate-based polymer in this particle dispersion was 0.07 μm . The weigh-average molecular weight (Mw) of the alkyl (meth)acrylate-based polymer measured by gel permeation chromatography was 20,000.

<Production Example 5: modifier for thermoplastic resin (A-5)>

A polytetrafluoroethylene particle dispersion having a solid content of 26.2% (A-5-1) was obtained in the same manner as in Production Example 1.

Into a mixture of 35 parts of methyl methacrylate and 65 parts of dodecyl methacrylate was dissolved 0.1 part of azobisdimethylvaleronitrile. To this was added a mixture of 2.0 parts of sodium dodecylbenzenesulfonate and 225 parts of distilled water, and the mixture was stirred for 4 minutes by a homo-mixer at 10,000 rpm, then, passed twice at a pressure of 30 MPa through a homogenizer, to obtain a stable methyl methacrylate/dodecyl methacrylate previous dispersion. This was charged into a reaction vessel equipped with a stirred, condenser, thermocouple and nitrogen introduction port, and the liquid temperature inside was raised to 80°C un-

der a nitrogen flow and stirred for 3 hours to complete radical polymerization, to obtain a (meth)acrylate-based polymer particle aqueous dispersion (A-5-2). This particle aqueous dispersion (A-5-2) had a content of 30.4%.

5 The average particle size of the alkyl (meth)acrylate-based polymer in this particle dispersion (A-5-2) was 0.20 μm . The Mw of the alkyl (meth)acrylate-based polymer was 100000.

Into a reaction vessel equipped with a stirrer,
10 condenser, thermocouple and nitrogen introduction port was charged 80 parts of the polytetrafluoroethylene particle dispersion (A-3-1) (20 parts of polytetrafluoroethylene) previously prepared, by using a rotary pump (IC30S-D), then, 263.2 parts of the (meth)acrylate-based
15 polymer particle aqueous dispersion (A-5-2) (80 parts of (meth)acrylate-based polymer) was charged, and the liquid inside was heated and stirred until the temperature reached 80°C. When the liquid temperature inside reached 80°C, stirring was continued for 1 hour, to obtain a mixture
20 of both dispersions. Thereafter, precipitation, separation, filtration and drying were conducted in the same manner as in Production Example 1, to obtain a polytetrafluoroethylene-containing thermoplastic resin modifier (A-5).

25 <Production Example 6: modifier for thermoplastic resin (A-6)>

A polytetrafluoroethylene particle dispersion (A-6-

1) having a solid content of 26.2% was obtained in the same manner as in Production Example 1. 165 parts of distilled water and 1.5 parts of dipotassium alkenylsuccinate were charged into a reaction vessel equipped with a stirrer, condenser, thermocouple and nitrogen introduction port, then, 200 parts of the polytetrafluoroethylene dispersion (A-6-1) (50 parts by weight of polytetrafluoroethylene) was charged into the reaction vessel using a rotary pump (IC30S-D), then, the atmosphere in the reaction vessel was purged with nitrogen by passing a nitrogen flow through the vessel. Then, the temperature in the system was raised to 55°C, and when the liquid temperature inside reached 55°C, a mixture composed of 0.1 part of potassium persulfate and 5 parts of distilled water was added, further, to this was dropped 10 parts of acrylonitrile and 40 parts of styrene over 90 minutes, and these were polymerized. After completion of dropping, the reaction mixture was kept for about 45 minutes, to complete the polymerization. Throughout a series of operations, no separation of solid was observed, and a uniform particle dispersion was obtained.

On the other hand, 150 parts of an aqueous solution dissolving calcium acetate in a proportion of 7% was heated at 98°C and stirred. Into this aqueous solution was gradually dropped 100 parts of the particle dispersion previously prepared, to precipitate solid. Then,

this precipitate was separated, filtrated and dried, to obtain a polytetrafluoroethylene-containing thermoplastic resin modifier (A-6).

The average particle size of the alkyl
5 (meth)acrylate-based polymer in this particle dispersion was 0.10 μm . The weigh-average molecular weight (M_w) of the alkyl (meth)acrylate-based polymer measured by gel permeation chromatography was 49,000.

<Production Example 7: modifier for thermoplastic resin
10 (A-7)>

230 parts of distilled water and 2.0 parts of dipotassium alkenylsuccinate were charged into a reaction vessel equipped with a stirrer, condenser, thermocouple and nitrogen introduction port, further, 80 parts of
15 methyl methacrylate and 20 parts of n-butyl methacrylate were charged, then, the atmosphere in the reaction vessel was purged with nitrogen by passing a nitrogen flow through the vessel. Then, the temperature in the system was raised to 55°C, and when the liquid temperature inside reached 55°C, a mixture composed of 0.1 part of potassium persulfate and 5 parts of distilled water was
20 added, the reaction mixture was kept for about 45 minutes, to complete the polymerization, to obtain an aqueous dispersion of a (meth)acrylate-based polymer.

25 In the same manner as in Example 1, a (meth)acrylate-based polymer was recovered from the aqueous dispersion of a (meth)acrylate-based polymer, to

obtain a thermoplastic resin modifier (A-7). The resulted (meth)acrylate-based polymer had a Mw of 2,400,000.

<Examples 1 to 4, Comparative Examples 1 to 3>

- 5 The evaluation results of the flowability and storage stability of the powder bodies are shown in Table 1. As the PTFE powder in the table, Aflon PTFE CD-1 (trade name: manufactured by Asahi Glass Co., Ltd.) was used.

Table 1

	Ex. 1	Ex. 2	Ex. 3	Ex. 4	Comp. Ex. 1	Comp. Ex. 2	Comp. Ex. 3
PTFE-containing modifier A-1	100						
PTFE-containing modifier A-2		100					
PTFE-containing modifier A-3			100				
PTFE-containing modifier A-4				100			
PTFE powder-1					100		
PTFE-containing modifier A-5						100	
PTFE-containing modifier A-6							100
Flowability of powder (g/10 sec)	35.2	32.6	31.8	25.8	4.5	21.0	No flow
Storage stability (sec)	2	3	2	15	>4000	3600	1500

<Examples 5 to 8, Comparative Examples 4 to 7>

The components shown in table 2 were mixed at respective proportions (ratio by weight), and the mixture was shaped by a co-direction twin-screw extruder (PCM-30) set at a cylinder temperature of 260°C, to produced a pellet. Then, using this pellet, injection molding was conducted by an injection molding machine (SAV-60) set at a cylinder temperature of 260°C and a mold temperature of 80°C for combustibility test, and an injection molding machine (M-100AII-DM) set at a cylinder temperature of 260°C and a mold temperature of 80°C for physical property evaluation, to obtain respective specimens.

<Examples 9 to 11, Comparative Examples 8 to 11>

The components shown in table 3 were mixed at respective proportions (ratio by weight), and the mixture was shaped by a co-direction twin-screw extruder (PCM-30) set at a cylinder temperature of 260°C, to produced a pellet. Then, using this pellet, injection molding was conducted by an injection molding machine (SAV-60) set at a cylinder temperature of 260°C and a mold temperature of 80°C for combustibility test, and an injection molding machine (M-100AII-DM) set at a cylinder temperature of 260°C and a mold temperature of 80°C for physical property evaluation, to obtain respective specimens.

<Examples 13 to 16, Comparative Examples 12 to 15>

The components shown in table 4 were mixed at respective proportions (ratio by weight), and the mixture was shaped by a co-direction twin-screw extruder (PCM-30) set at a cylinder temperature of 260°C, to produced a pellet. Then, using this pellet, injection molding was conducted by an injection molding machine (SAV-60) set at a cylinder temperature of 260°C and a mold temperature of 60°C for combustibility test, and an injection molding machine (M-100AII-DM) set at a cylinder temperature of 260°C and a mold temperature of 60°C for physical property evaluation, to obtain respective specimens.

<Examples 17 to 20, Comparative Examples 16 to 19>

The components shown in table 5 were mixed at respective proportions (ratio by weight), and the mixture was shaped by a co-direction twin-screw extruder (PCM-30) set at a cylinder temperature of 260°C, to produced a pellet. Then, using this pellet, injection molding was conducted by an injection molding machine (SAV-60) set at a cylinder temperature of 260°C and a mold temperature of 60°C for combustibility test, and an injection molding machine (M-100AII-DM) set at a cylinder temperature of 260°C and a mold temperature of 60°C for physical property evaluation, to obtain respective specimens.

<Examples 21 to 24, Comparative Examples 20 to 23>

The components shown in table 6 were mixed at respective proportions (ratio by weight), and the

spective proportions (ratio by weight), and the mixture was shaped by a co-direction twin-screw extruder (PCM-30) set at a cylinder temperature of 250°C, to produced a pellet. Then, using this pellet, injection molding was
5 conducted by an injection molding machine (SAV-60) set at a cylinder temperature of 250°C and a mold temperature of 80°C for combustibility test, and an injection molding machine (M-100AII-DM) set at a cylinder temperature of 250°C and a mold temperature of 80°C for physical prop-
10 erty evaluation, to obtain respective specimens.

<Examples 25 to 28, Comparative Examples 24 to 27>

The components shown in table 7 were mixed at respective proportions (ratio by weight), and the mixture was shaped by a co-direction twin-screw extruder
15 (PCM-30) set at a cylinder temperature of 250°C, to produced a pellet. Then, using this pellet, injection molding was conducted by an injection molding machine (SAV-60) set at a cylinder temperature of 250°C and a mold temperature of 80°C for combustibility test, and an
20 injection molding machine (M-100AII-DM) set at a cylinder temperature of 250°C and a mold temperature of 80°C for physical property evaluation, to obtain respective specimens.

<Examples 29 to 32, Comparative Examples 28 to 31>

25 The components shown in table 8 were mixed at respective proportions (ratio by weight), and the mixture was shaped by a co-direction twin-screw extruder (PCM-30) set at a cylinder temperature of 250°C, to

30) set at a cylinder temperature of 250°C, to produced a pellet. Then, using this pellet, injection molding was conducted by an injection molding machine (SAV-60) set at a cylinder temperature of 250°C and a mold temperature of 80°C for combustibility test, and an injection molding machine (M-100AII-DM) set at a cylinder temperature of 250°C and a mold temperature of 80°C for physical property evaluation, to obtain respective specimens.

<Examples 33 to 36, Comparative Examples 32 to 35>

10 The components shown in table 9 were mixed at respective proportions (ratio by weight), and the mixture was shaped by a co-direction twin-screw extruder (PCM-30) set at a cylinder temperature of 250°C, to produced a pellet. Then, using this pellet, injection molding was conducted by an injection molding machine (SAV-60) set at a cylinder temperature of 250°C and a mold temperature of 80°C for combustibility test, and an injection molding machine (M-100AII-DM) set at a cylinder temperature of 250°C and a mold temperature of 80°C, for physical property evaluation, to obtain respective specimens.

<Examples 37 to 40, Comparative Examples 36 to 39>

25 The components shown in table 10 were mixed at respective proportions (ratio by weight), and the mixture was shaped by a co-direction twin-screw extruder (PCM-30) set at a cylinder temperature of 250°C, to produced a pellet. Then, using this pellet, injection molding was conducted by an injection molding machine

conducted by an injection molding machine (SAV-60) set at a cylinder temperature of 250°C and a mold temperature of 80°C for combustibility test, and an injection molding machine (M-100AII-DM) set at a cylinder temperature of 250°C and a mold temperature of 80°C, for physical property evaluation to obtain respective specimens.

<Examples 41 to 44, Comparative Examples 40 to 43>

The components shown in table 11 were mixed at respective proportions (ratio by weight), and the mixture was shaped by a co-direction twin-screw extruder (PCM-30) set at a cylinder temperature of 220°C, to produced a pellet. Then, using this pellet, injection molding was conducted by an injection molding machine (SAV-60) set at a cylinder temperature of 220°C and a mold temperature of 60°C for combustibility test, and an injection molding machine (M-100AII-DM) set at a cylinder temperature of 220°C and a mold temperature of 60°C for physical property evaluation, to obtain respective specimens.

<Examples 45 to 48, Comparative Examples 44 to 47>

The components shown in table 12 were mixed at respective proportions (ratio by weight), and the mixture was shaped by a co-direction twin-screw extruder (PCM-30) set at a cylinder temperature of 280°C, to produced a pellet. Then, using this pellet, injection molding was conducted by an injection molding machine (SAV-60) set at a cylinder temperature of 280°C and a mold temperature of 80°C for combustibility test, and an

of 80°C for combustibility test, and an injection molding machine (M-100AII-DM) set at a cylinder temperature of 280°C and a mold temperature of 80°C for physical property evaluation, to obtain respective specimens.

5 <Examples 49 to 52, Comparative Examples 48 to 51>

The components shown in table 13 were mixed at respective proportions (ratio by weight), and the mixture was shaped by a co-direction twin-screw extruder (PCM-30) set at a cylinder temperature of 240°C, to
10 produced a pellet. Then, using this pellet, injection molding was conducted by an injection molding machine (SAV-60) set at a cylinder temperature of 230°C and a mold temperature of 80°C for combustibility test, and an injection molding machine (M-100AII-DM) set at a
15 cylinder temperature of 230°C and a mold temperature of 80°C for physical property evaluation, to obtain respective specimens.

<Examples 53 to 56, Comparative Examples 52 to 55>

The components shown in table 14 were mixed at
20 respective proportions (ratio by weight), and the mixture was shaped by a co-direction twin-screw extruder (PCM-30) set at a cylinder temperature of 240°C, to produced a pellet. Then, using this pellet, injection molding was conducted by an injection molding machine
25 (SAV-60) set at a cylinder temperature of 230°C and a mold temperature of 80°C for combustibility test, and an injection molding machine (M-100AII-DM) set at a cylinder temperature of 230°C and a mold temperature of

230°C and a mold temperature of 80°C for physical property evaluation, to obtain respective specimens.

<Examples 57 to 60, Comparative Examples 56 to 59>

The components shown in table 15 were mixed at
5 respective proportions (ratio by weight), and the
mixture was shaped by a co-direction twin-screw extruder
(PCM-30) set at a cylinder temperature of 240°C, to
produced a pellet. Then, using this pellet, injection
molding was conducted by an injection molding machine
10 (SAV-60) set at a cylinder temperature of 240°C and a
mold temperature of 60°C for combustibility test, and an
injection molding machine (M-100AII-DM) set at a
cylinder temperature of 240°C and a mold temperature of
60°C for physical property evaluation, to obtain
15 respective specimens.

<Examples 61 to 64, Comparative Examples 60 to 63>

The components shown in table 16 were mixed at
respective proportions (ratio by weight), and the
mixture was shaped by a co-direction twin-screw extruder
20 (PCM-30) set at a cylinder temperature of 230°C, to
produced a pellet. Then, using this pellet, injection
molding was conducted by an injection molding machine
(SAV-60) set at a cylinder temperature of 230°C and a
mold temperature of 60°C for combustibility test, and an
25 injection molding machine (M-100AII-DM) set at a
cylinder temperature of 230°C and a mold temperature of
60°C for physical property evaluation, to obtain
respective specimens.

<Examples 65 to 68, Comparative Examples 64 to 67>

The components shown in table 17 were mixed at respective proportions (ratio by weight), and the mixture was shaped by a co-direction twin-screw extruder (PCM-30) set at a cylinder temperature of 230°C, to produced a pellet. Then, using this pellet, injection molding was conducted by an injection molding machine (SAV-60) set at a cylinder temperature of 230°C and a mold temperature of 60°C for combustibility test, and an injection molding machine (M-100AII-DM) set at a cylinder temperature of 230°C and a mold temperature of 60°C for physical property evaluation, to obtain respective specimens.

Regarding the resulted specimens, the vertical combustion test, Izod impact strength, tensile strength and tensile elongation were measured according to UL-94 standard, and the results are shown in Tables 2 to 17.

Table 2

Composition	Ex. 5	Ex. 6	Ex. 7	Ex. 8	Comp. Ex. 4	Comp. Ex. 5	Comp. Ex. 6	Comp. Ex. 7
PC resin	100	100	100	100	100	100	100	100
PTFE-containing modifier A-1 (PTFE content in 100 parts of resin)	1.5 (0.3)							
PTFE-containing modifier A-2 (PTFE content in 100 parts of resin)		0.4 (0.2)	0.4 (0.2)					
PTFE-containing modifier A-3 (PTFE content in 100 parts of resin)				0.29 (0.2)				
PTFE-containing modifier A-4 (PTFE content in 100 parts of resin)						1.0 (0.2)	0.4 (0.2)	0.2
PTFE-containing modifier A-5 (PTFE content in 100 parts of resin)								8
PTFE-containing modifier A-6 (PTFE content in 100 parts of resin)								
PTFE powder-1	8	8	8	8				
Flame retardant 1								
Combustion test								
UL-94V	V-0 5/0	V-0 5/0	V-0 5/0	V-0 5/0	V-2 5/5	V-2 5/4	V-1 5/1	V-0 5/0
Proportion of drip								
Izod impact strength (J/m)	835	840	840	850	840	840	850	843
Tensile yield strength (MPa)	59	58	59	59	59	59	58	57
Tensile elongation (%)	96	99	100	98	107	98	91	90
Surface appearance	○	○	○	○	○	×	×	×
Aggregate in specimen	○	○	○	○	○	○	×	×

Table 3

Composition	Ex. 9	Ex. 10	Ex. 11	Ex. 12	Comp. Ex. 8	Comp. Ex. 9	Comp. Ex. 10	Comp. Ex. 11
PC resin	100	100	100	100	100	100	100	100
PTFE-containing modifier A-1 (PTFE content in 100 parts of resin)	1.5 (0.3)							
PTFE-containing modifier A-2 (PTFE content in 100 parts of resin)		0.4 (0.2)						
PTFE-containing modifier A-3 (PTFE content in 100 parts of resin)			0.4 (0.2)					
PTFE-containing modifier A-4 (PTFE content in 100 parts of resin)				0.29 (0.2)				
PTFE-containing modifier A-5 (PTFE content in 100 parts of resin)					1.0 (0.2)		0.4 (0.2)	0.2
PTFE-containing modifier A-6 (PTFE content in 100 parts of resin)								12
PTFE powder-1								6
Flame retardant 2	12	12	12	12		12	12	12
Flame retardant aid 1	6	6	6	6		6	6	6
Combustion test UL-94V Proportion of drip	V-0 5/0	V-0 5/0	V-0 5/0	V-0 5/0	V-2 5/5	V-2 5/2	V-1 5/1	V-0 5/0
Izod impact strength (J/m)	845	841	843	849	840	830	845	840
Tensile yield strength (MPa)	59	58	60	58	59	56	58	57
Tensile elongation (%)	92	91	95	93	107	98	91	90
Surface appearance	○	○	○	○	○	×	×	×

Table 4

Composition	Ex.13	Ex.14	Ex.15	Ex.16	Comp. Ex.12	Comp. Ex.13	Comp. Ex.14	Comp. Ex.15
PC resin	80	80	80	80	80	80	80	80
Graft copolymer 1 (ABS)	10	10		10	10		10	10
Graft copolymer 2 (AAS)			10			10		
Vinyl-based copolymer (SAN)	10	10	10	10	10	10	10	10
PTFE-containing modifier A-1	1.5							
(PTFE content in 100 parts of resin)	(0.3)							
PTFE-containing modifier A-2		0.4						
(PTFE content in 100 parts of resin)		(0.2)						
PTFE-containing modifier A-3			0.4					
(PTFE content in 100 parts of resin)			(0.2)					
PTFE-containing modifier A-4				0.4				
(PTFE content in 100 parts of resin)				(0.2)				
PTFE-containing modifier A-5						1.5		
(PTFE content in 100 parts of resin)						(0.3)		
PTFE-containing modifier A-6							0.4	
(PTFE content in 100 parts of resin)							(0.2)	
PTFE powder-1	10	10	10	10	10	10	10	0.3
Flame retardant 1								10
Combustion test								
UL-94V					Not			
Proportion of drip	V-0	V-0	V-0	V-0	passed	V-2	V-1	V-0
	5/0	5/0	5/0	5/0	5/5	5/4	5/0	5/0
Izod impact strength (J/m)	720	750	750	760	740	750	792	750
Tensile yield strength (MPa)	56	55	57	55	58	57	55	54
Tensile elongation (%)	65	62	64	62	68	66	63	68
Surface appearance	○	○	○	○	○	×	×	×

Table 5

Composition	Ex. 17	Ex. 18	Ex. 19	Ex. 20	Comp. Ex. 16	Comp. Ex. 17	Comp. Ex. 18	Comp. Ex. 19
PC resin	80	80	80	80	80	80	80	80
Graft copolymer 1 (ABS)	10	10		10	10		10	10
Graft copolymer 2 (AAS)			10			10		
Vinyl-based copolymer (SAN)	10	10	10	10	10	10	10	10
PTFE-containing modifier A-1	1.5							
(PTFE content in 100 parts of resin)	(0.3)							
PTFE-containing modifier A-2		0.4						
(PTFE content in 100 parts of resin)		(0.2)						
PTFE-containing modifier A-3			0.4					
(PTFE content in 100 parts of resin)			(0.2)					
PTFE-containing modifier A-4				0.4				
(PTFE content in 100 parts of resin)				(0.2)				
PTFE-containing modifier A-5						1.5		
(PTFE content in 100 parts of resin)						(0.3)		
PTFE-containing modifier A-6							0.4	
(PTFE content in 100 parts of resin)							(0.2)	
PTFE powder-1	13	13	13	13	13	13	13	0.3
Flame retardant 2	6.5	6.5	6.5	6.5	6.5	6.5	6.5	13
Flame retardant aid 2								6.5
Combustion test								
UL-94V	V-0	V-0	V-0	V-0	Not passed	V-2	V-1	V-0
Proportion of drip	5/0	5/0	5/0	5/0	5/5	5/5	5/0	5/0
Izod impact strength (J/m)	700	720	720	720	738	715	730	710
Tensile yield strength (MPa)	50	50	51	50	48	45	52	50
Tensile elongation (%)	61	61	62	63	60	64	59	60
Surface appearance	○	○	○	○	○	×	×	×

Table 6

Composition	Ex. 21	Ex. 22	Ex. 23	Ex. 24	Comp. Ex. 20	Comp. Ex. 21	Comp. Ex. 22	Comp. Ex. 23
PC resin	65	65	65	65	65	65	65	65
PBT resin	25	25	25	25	25	25	25	25
Graft copolymer (SAS)	15	15	15	15	15	15	15	15
PTFE-containing modifier A-1 (PTFE content in 100 parts of resin)	2.5 (0.5)	0.8 (0.4)	0.8 (0.4)	0.57 (0.4)		2.5 (0.5)	0.8 (0.4)	0.4
PTFE-containing modifier A-2 (PTFE content in 100 parts of resin)								16
PTFE-containing modifier A-3 (PTFE content in 100 parts of resin)								8
PTFE-containing modifier A-4 (PTFE content in 100 parts of resin)								
PTFE-containing modifier A-5 (PTFE content in 100 parts of resin)								
PTFE-containing modifier A-6 (PTFE content in 100 parts of resin)								
PTFE powder-1	16	16	16	16	16	16	16	16
Flame retardant 2	8	8	8	8	8	8	8	8
Flame retardant aid 2								
Combustion test								
UL-94V	V-0	V-0	V-0	V-0	Not passed	Not passed	V-1	V-2
Proportion of drip	5/0	5/0	5/0	5/0	5/5	5/5	5/1	5/5
Izod impact strength (J/m)	205	212	205	210	200	211	210	210
Tensile yield strength (MPa)	46	46	48	49	49	45	49	48
Tensile elongation (%)	92	93	95	93	100	90	90	91
Surface appearance	○	○	○	○	○	×	×	×

Table 7

Composition	Ex.25	Ex.26	Ex.27	Ex.28	Comp. Ex.24	Comp. Ex.25	Comp. Ex.26	Comp. Ex.27
PC resin	65	65	65	65	65	65	65	65
PBT resin	25	25	25	25	25	25	25	25
Graft copolymer (SAS)	15	15	15	15	15	15	15	15
PTFE-containing modifier A-1	2.5							
(PTFE content in 100 parts of resin)	(0.5)							
PTFE-containing modifier A-2		0.8						
(PTFE content in 100 parts of resin)		(0.4)						
PTFE-containing modifier A-3			0.8					
(PTFE content in 100 parts of resin)			(0.4)					
PTFE-containing modifier A-4				0.57				
(PTFE content in 100 parts of resin)				(0.4)				
PTFE-containing modifier A-5						2.5		
(PTFE content in 100 parts of resin)						(0.5)		
PTFE-containing modifier A-6							0.8	
(PTFE content in 100 parts of resin)							(0.4)	
PTFE powder-1								0.5
Flame retardant 3	2	2	2	2	2	2	2	2
Combustion test								
UL-94V	V-0	V-0	V-0	V-0	Not passed	V-2	V-1	V-2
Proportion of drip	5/0	5/0	5/0	5/0	5/5	5/5	5/1	5/5
Izod impact strength (J/m)	210	205	220	220	208	211	216	200
Tensile yield strength (MPa)	47	45	42	49	50	45	54	45
Tensile elongation (%)	90	94	98	100	100	91	90	93
Surface appearance	○	○	○	○	○	×	×	×

Table 8

Composition	Ex. 29	Ex. 30	Ex. 31	Ex. 32	Comp. Ex. 28	Comp. Ex. 29	Comp. Ex. 30	Comp. Ex. 31
PBT resin	70	70	70	70	70	70	70	70
Graft copolymer 1 (ABS)	30	30	30	30	30	30	30	30
PTFE-containing modifier A-1	2.5							
(PTFE content in 100 parts of resin)	(0.5)							
PTFE-containing modifier A-2		0.8						
(PTFE content in 100 parts of resin)		(0.4)						
PTFE-containing modifier A-3			0.8					
(PTFE content in 100 parts of resin)			(0.4)					
PTFE-containing modifier A-4				0.57				
(PTFE content in 100 parts of resin)				(0.4)				
PTFE-containing modifier A-5						2.5		
(PTFE content in 100 parts of resin)						(0.5)		
PTFE-containing modifier A-6							0.8	
(PTFE content in 100 parts of resin)							(0.4)	
PTFE powder-1								0.4
Flame retardant 2	16	16	16	16	16	16	16	16
Flame retardant aid	8	8	8	8	8	8	8	8
Combustion test								
UL-94V						Not passed		
Proportion of drip	V-0	V-0	V-0	V-0	Not passed	Not passed	V-1	V-2
	5/0	5/0	5/0	5/0	5/5	5/5	5/3	5/5
Izod impact strength (J/m)	205	210	213	210	196	195	210	210
Tensile yield strength (MPa)	39	39	39	38	39	38	40	39
Tensile elongation (%)	38	38	38	38	40	36	38	42
Surface appearance	○	○	○	○	○	×	×	×

Table 9

Composition	Ex. 33	Ex. 34	Ex. 35	Ex. 36	Comp. Ex. 32	Comp. Ex. 33	Comp. Ex. 34	Comp. Ex. 35
PBT resin	100	100	100	100	100	100	100	100
PTFE-containing modifier A-1 (PTFE content in 100 parts of resin)	2.5 (0.5)							
PTFE-containing modifier A-2 (PTFE content in 100 parts of resin)		0.8 (0.4)						
PTFE-containing modifier A-3 (PTFE content in 100 parts of resin)			0.8 (0.4)					
PTFE-containing modifier A-4 (PTFE content in 100 parts of resin)				0.57 (0.4)				
PTFE-containing modifier A-5 (PTFE content in 100 parts of resin)						2.5 (0.5)		
PTFE-containing modifier A-6 (PTFE content in 100 parts of resin)							0.8 (0.4)	
PTFE powder-1								0.4
Flame retardant 3	2	2	2	2	2	2	2	2
Combustion test								
UL-94V	V-0	V-0	V-0	V-0	Not passed	Not passed	V-1	V-2
Proportion of drip	5/0	5/0	5/0	5/0	5/5	5/5	5/3	5/5
Izod impact strength (J/m)	34	35	32	35	40	31	36	33
Tensile yield strength (MPa)	52	53	53	54	56	50	55	54
Tensile elongation (%)	140	141	142	141	160	150	140	143
Surface appearance	○	○	○	○	○	×	×	×

Table 10

Composition	Ex. 37	Ex. 38	Ex. 39	Ex. 40	Comp. Ex. 36	Comp. Ex. 37	Comp. Ex. 38	Comp. Ex. 39
PBT resin	100	100	100	100	100	100	100	100
PTFE-containing modifier A-1 (PTFE content in 100 parts of resin)	2.5 (0.5)							
PTFE-containing modifier A-2 (PTFE content in 100 parts of resin)		0.8 (0.4)						
PTFE-containing modifier A-3 (PTFE content in 100 parts of resin)			0.8 (0.4)					
PTFE-containing modifier A-4 (PTFE content in 100 parts of resin)				0.57 (0.4)				
PTFE-containing modifier A-5 (PTFE content in 100 parts of resin)						2.5 (0.5)		
PTFE-containing modifier A-6 (PTFE content in 100 parts of resin)							0.8 (0.4)	
PTFE powder-1								0.4
Flame retardant 4	14	14	14	14	14	14	14	14
Flame retardant aid	7	7	7	7	7	7	7	7
Combustion test								
UL-94V	V-0	V-0	V-0	V-0	Not passed	Not passed	V-1	V-2
Proportion of drip	5/0	5/0	5/0	5/0	5/5	5/5	5/3	5/5
Izod impact strength (J/m)	39	38	39	39	40	32	40	38
Tensile yield strength (MPa)	60	63	63	64	56	52	65	64
Tensile elongation (%)	120	121	122	120	160	110	120	123
Surface appearance	○	○	○	○	○	×	×	×

Table 11

Composition	Ex. 41	Ex. 42	Ex. 43	Ex. 47	Comp. Ex. 40	Comp. Ex. 41	Comp. Ex. 42	Comp. Ex. 43
Graft copolymer 1 (ABS)	30	30	30	30	30	30	30	30
Vinyl-based copolymer (SAN)	70	70	70	70	70	70	70	70
PTFE-containing modifier A-1	0.5							
(PTFE content in 100 parts of resin)	(0.08)							
PTFE-containing modifier A-2		0.16						
(PTFE content in 100 parts of resin)		(0.08)						
PTFE-containing modifier A-3			0.16					
(PTFE content in 100 parts of resin)			(0.08)					
PTFE-containing modifier A-4				0.11				
(PTFE content in 100 parts of resin)				(0.08)				
PTFE-containing modifier A-5						0.5		
(PTFE content in 100 parts of resin)						(0.08)		
PTFE-containing modifier A-6							0.16	
(PTFE content in 100 parts of resin)							(0.08)	
PTFE powder-2								0.1
Flame retardant 2	24	24	24	24	24	24	24	24
Flame retardant aid	12	12	12	12	12	12	12	12
Combustion test								
UL-94V					Not			
Proportion of drip	V-0	V-0	V-0	V-0	passed	V-1	V-0	V-1
	5/0	5/0	5/0	5/0	5/5	5/3	5/0	5/0
Izod impact strength (J/m)	170	163	163	163	173	181	169	163
Tensile yield strength (MPa)	46	45	46	45	46	46	46	46
Tensile elongation (%)	10	10	9	9	7	10	7	8
Surface appearance	○	○	○	○	○	×	×	×

Table 12

Composition	Ex. 45	Ex. 46	Ex. 47	Ex. 48	Comp. Ex. 44	Comp. Ex. 45	Comp. Ex. 46	Comp. Ex. 47
PPE resin	60	60	60	60	60	60	60	60
PS resin	40	40	40	40	40	40	40	40
PTFE-containing modifier A-1 (PTFE content in 100 parts of resin)	1.5 (0.3)	0.6 (0.3)	0.6 (0.3)	0.43 (0.3)		0.6 (0.3)	0.6 (0.3)	0.3
PTFE-containing modifier A-2 (PTFE content in 100 parts of resin)								
PTFE-containing modifier A-3 (PTFE content in 100 parts of resin)								
PTFE-containing modifier A-4 (PTFE content in 100 parts of resin)								
PTFE-containing modifier A-5 (PTFE content in 100 parts of resin)								
PTFE-containing modifier A-6 (PTFE content in 100 parts of resin)								
PTFE powder-1	10	10	10	10	10	10	10	10
Flame retardant 1								
Combustion test								
UL-94V	V-0	V-0	V-0	V-0	V-2	Not passed	V-1	V-0
Proportion of drip	5/0	5/0	5/0	5/0	5/5	5/5	5/0	5/0
Izod impact strength (J/m)	121	126	125	125	130	114	130	125
Tensile yield strength (MPa)	56	58	58	58	56	55	58	55
Tensile elongation (%)	27	28	28	28	30	24	30	27
Surface appearance	○	○	○	○	○	×	×	×

Table 13

Composition	Ex. 49	Ex. 50	Ex. 51	Ex. 52	Comp. Ex. 48	Comp. Ex. 49	Comp. Ex. 50	Comp. Ex. 51
Ny6 resin	100	100	100	100	100	100	100	100
PTFE-containing modifier A-1 (PTFE content in 100 parts of resin)	2.0							
PTFE-containing modifier A-2 (PTFE content in 100 parts of resin)	(0.4)	0.8 (0.4)						
PTFE-containing modifier A-3 (PTFE content in 100 parts of resin)			0.8 (0.4)					
PTFE-containing modifier A-4 (PTFE content in 100 parts of resin)				0.57 (0.4)		2.0 (0.4)		
PTFE-containing modifier A-5 (PTFE content in 100 parts of resin)							0.8 (0.4)	
PTFE-containing modifier A-6 (PTFE content in 100 parts of resin)								0.4
PTFE powder-1								15
Flame retardant 2	15	15	15	15	15	15	15	15
Flame retardant aid	8.5	8.5	8.5	8.5	8.5	8.5	8.5	8.5
Combustion test								
UL-94V					Not			
Proportion of drip	V-0	V-0	V-0	V-0	Passed	V-1	V-0	V-0
Izod impact strength (J/m)	5/0	5/0	5/0	5/0	5/5	5/0	5/0	5/0
Tensile yield strength (MPa)	235	240	240	240	480	220	240	240
Tensile elongation (%)	38	40	40	40	38	25	45	40
Surface appearance	17	18	17	17	17	13	15	18
	○	○	○	○	○	×	×	×

Table 14

Composition	Ex. 53	Ex. 54	Ex. 55	Ex. 56	Comp. Ex. 52	Comp. Ex. 53	Comp. Ex. 54	Comp. Ex. 55
Ny6 resin	100	100	100	100	100	100	100	100
PTFE-containing modifier A-1 (PTFE content in 100 parts of resin)	2.0 (0.4)							
PTFE-containing modifier A-2 (PTFE content in 100 parts of resin)		0.8 (0.4)						
PTFE-containing modifier A-3 (PTFE content in 100 parts of resin)			0.8 (0.4)					
PTFE-containing modifier A-4 (PTFE content in 100 parts of resin)				0.57 (0.4)				
PTFE-containing modifier A-5 (PTFE content in 100 parts of resin)						2.0 (0.4)		
PTFE-containing modifier A-6 (PTFE content in 100 parts of resin)							0.8 (0.4)	
PTFE powder-1								0.4 5
Flame retardant 3	5	5	5	5	5	5	5	
Combustion test								
UL-94V	V-0 5/0	V-0 5/0	V-0 5/0	V-0 5/0	Not Passed 5/5	V-2 5/5	V-0 5/0	V-0 5/0
Proportion of drip								
Izod impact strength (J/m)	240	240	238	239	480	230	245	235
Tensile yield strength (MPa)	37	39	39	39	38	30	43	41
Tensile elongation (%)	20	19	18	18	18	15	20	18
Surface appearance	○	○	○	○	○	×	×	×

Table 15

Composition	Ex. 57	Ex. 58	Ex. 59	Ex. 60	Comp. Ex. 56	Comp. Ex. 57	Comp. Ex. 58	Comp. Ex. 59
Pst resin	100	100	100	100	100	100	100	100
PTFE-containing modifier A-1 (PTFE content in 100 parts of resin)	2.0 (0.4)							
PTFE-containing modifier A-2 (PTFE content in 100 parts of resin)		0.8 (0.4)						
PTFE-containing modifier A-3 (PTFE content in 100 parts of resin)			0.8 (0.4)					
PTFE-containing modifier A-4 (PTFE content in 100 parts of resin)				0.57 (0.4)		2.0 (0.4)		
PTFE-containing modifier A-5 (PTFE content in 100 parts of resin)							0.8 (0.4)	0.4
PTFE-containing modifier A-6 (PTFE content in 100 parts of resin)								20
PTFE powder-1								10
Flame retardant 2	20	20	20	20	20	20	20	20
Flame retardant aid 1	10	10	10	10	10	10	10	10
Combustion test					Not passed	Not passed		
UL-94V	V-0 5/0	V-0 5/0	V-0 5/0	V-0 5/0	5/5	5/5	V-1 5/0	V-0 5/0
Proportion of drip								
Izod impact strength (J/m)	14	13	13	14	14	9	12	14
Tensile yield strength (MPa)	43	42	43	43	44	38	43	41
Tensile elongation (%)	3	3	3	3	3	3	3	3
Surface appearance	○	○	○	○	○	×	×	×

Table 16

Composition	Ex. 61	Ex. 62	Ex. 63	Ex. 64	Comp. Ex. 60	Comp. Ex. 61	Comp. Ex. 62	Comp. Ex. 63
PP resin	100	100	100	100	100	100	100	100
PTFE-containing modifier A-1 (PTFE content in 100 parts of resin)	2.5 (0.5)							
PTFE-containing modifier A-2 (PTFE content in 100 parts of resin)		1.0 (0.5)						
PTFE-containing modifier A-3 (PTFE content in 100 parts of resin)			1.0 (0.5)					
PTFE-containing modifier A-4 (PTFE content in 100 parts of resin)				0.57 (0.5)		1.0 (0.5)		
PTFE-containing modifier A-5 (PTFE content in 100 parts of resin)							1.0 (0.5)	
PTFE-containing modifier A-6 (PTFE content in 100 parts of resin)								0.5
PTFE powder-1								150
Flame retardant 6	150	150	150	150	150	150	150	150
Combustion test								
UL-94V	V-0 5/0	V-0 5/0	V-0 5/0	V-0 5/0	Not passed 5/5	V-2 5/5	V-2 5/5	V-1 5/3
Proportion of drip	72	75	76	73	74	64	62	70
Izod impact strength (J/m)	20	21	21	21	19	23	17	20
Tensile yield strength (MPa)	7	7	7	8	7	8	6	5
Tensile elongation (%)	0	0	0	0	0	0	0	0
Surface appearance								

Table 17

Composition	Ex. 65	Ex. 66	Ex. 67	Ex. 68	Comp. Ex. 64	Comp. Ex. 65	Comp. Ex. 66	Comp. Ex. 67
PE resin	100	100	100	100	100	100	100	100
PTFE-containing modifier A-1 (PTFE content in 100 parts of resin)	2.5 (0.5)							
PTFE-containing modifier A-2 (PTFE content in 100 parts of resin)		1.0 (0.5)						
PTFE-containing modifier A-3 (PTFE content in 100 parts of resin)			1.0 (0.5)					
PTFE-containing modifier A-4 (PTFE content in 100 parts of resin)				0.57 (0.5)				
PTFE-containing modifier A-5 (PTFE content in 100 parts of resin)						1.0 (0.5)		
PTFE-containing modifier A-6 (PTFE content in 100 parts of resin)							1.0 (0.5)	
PTFE powder-1								0.5
Flame retardant 6	150	150	150	150	150	150	150	150
Combustion test								
UL-94V					Not passed	V-2 5/5	V-2 5/5	V-1 5/3
Proportion of drip	V-0 5/0	V-0 5/0	V-0 5/0	V-0 5/0				
Izod impact strength (J/m)	61	60	62	62	61	54	55	61
Tensile yield strength (MPa)	19	20	19	19	20	17	14	20
Tensile elongation (%)	8	8	8	8	7	8	6	6
Surface appearance	○	○	○	○	○	×	×	×

As the composition components in Tables 2 to 17,
the following components were specifically used.

- 5 • "PC resin" : polycarbonate resin, manufactured by Mit-
subishi Engineering Plastics K.K., trade name: Jupi-
ron S-2000F
- "PBT resin" : polybutylene terephthalate resin, manu-
factured by Mitsubishi Rayon Co., Ltd., trade name:
Tafpet N1000
- 10 • "PPE resin" : polyphenylene ether resin; the used
polyphenylene ether resin is poly(2,6-dimethyl-1,4-
phenylene) ether, had a reduced viscosity measured by
Ubbellohde viscometer in a 0.1% chloroform solution
at 25°C of 0.59
- 15 • "PSt resin" : polystyrene resin, manufactured by Nip-
pon Polystyrene K.K., trade name: G440K
- "Ny6 resin" : polyamide resin, manufactured by Ube In-
dustries. Ltd., trade name: UBE Nylon 1013B
- "PP resin" : polypropylene resin, manufactured by Nip-
pon Polychem K.K., trade name: Novatec PP BC6
- 20 • "PE resin" : polyethylene resin, manufactured by Nip-
pon Polychem K.K., trade name: Novatec LD LC522
- "Graft copolymer 1 (ABS)" : ABS graft copolymer, manu-
factured by Mitsubishi Rayon Co., Ltd., trade name:
R-80
- 25 • "Graft copolymer 2 (AAS)" : Acrylonitrile-butyl acry-
late-styrene graft copolymer, manufactured by Mits-
ubishi Rayon Co., Ltd., trade name: MUX-80

- "Graft copolymer 3 (SAS)" : Acrylonitrile-butyl acrylate-silicone graft copolymer, manufactured by Mitsubishi Rayon Co., Ltd., trade name: RK-200
- 5 · "Vinyl-based copolymer (SAN copolymer)" : Acrylonitrile-styrene copolymer, manufactured by Mitsubishi Rayon Co., Ltd., trade name: AP-20
- "PTFE-containing modifier A-1" : polytetrafluoroethylene-containing modifier (A-1) obtained in Production Example 1
- 10 · "PTFE-containing modifier A-2" : polytetrafluoroethylene-containing modifier (A-2) obtained in Production Example 2
- "PTFE-containing modifier A-3" : polytetrafluoroethylene-containing modifier (A-3) obtained in Production
- 15 Example 3
- "PTFE-containing modifier A-4" : polytetrafluoroethylene-containing modifier (A-4) obtained in Production Example 4
- "PTFE-containing modifier A-5" : polytetrafluoroethylene-containing modifier (A-5) obtained in Production
- 20 Example 5
- "PTFE-containing modifier A-6" : polytetrafluoroethylene-containing modifier (A-6) obtained in Production Example 6
- 25 · "Flame retardant 1" : Triphenyl phosphate, manufactured by Daihachi Kagaku Kogyo K.K., trade name: TTP
- "Flame retardant 2" : halogenated epoxy oligomer,

manufactured by Bromine Compounds Ltd., trade name:
F2400

- "Flame retardant 3" : red phosphorus, manufactured by
Rin Kagaku Kogyo K.K., trade name: Norba Red 120
- 5 · "Flame retardant 4" : tetrabispheol A carbonate oligomer, manufactured by Teijin Chemical K.K., trade name: FG-7500
- "Flame retardant 5" : tetrabispheol A, manufactured by Tosoh Corp., trade name: Flame Cut 120R
- 10 · "Flame retardant 6" : magnesium hydroxide, manufactured by Kyowa Kagaku Kogyo K.K., trade name: Kisma 5A
- "Flame retardant aid 1" : antimony trioxide, manufactured by Nippon Seiko K.K., trade name: Patox M
- 15 · "PTFE powder 1" : polytetrafluoroethylene, manufactured by Asahi Glass Co. Ltd., trade name: Aflon PTFE CD-1
- "PTFE powder 2" : polytetrafluoroethylene, manufactured by Daikin Industries Ltd., trade name: F201L
- 20 <Examples 69 to 73, Comparative Examples 68 to 77>

Compositions to which the modifier for thermoplastic resin of the present invention had been added, and compositions to which a PTFE powder or modifier for thermoplastic resin (A-3) had been added, or no PTFE powder had been added, for comparative, were prepared, and bottle molding was conducted by a blow molding machine having a screw diameter of 40 mm. The evaluation

results are shown in Table 18.

Table 18

	Resin	PTFE-containing modifier (A-3)	PTFE powder	Draw down in molding	Appearance of bottle
Ex. 69	ABS resin	0.6		○	○
Comp. Ex. 68	ABS resin		0.3	×	×
Comp. Ex. 69	ABS resin			×	×
Ex. 70	PC resin	0.6		○	○
Comp. Ex. 70	PC resin		0.3	×	×
Comp. Ex. 71	PC resin			×	×
Ex. 71	PET resin	0.6		○	○
Comp. Ex. 72	PET resin		0.3	×	×
Comp. Ex. 73	PET resin			×	×
Ex. 72	PS resin	0.6		○	○
Comp. Ex. 74	PS resin		0.3	×	×
Comp. Ex. 75	PS resin			×	×
Ex. 73	PE resin	0.6		○	○
Comp. Ex. 76	PE resin		0.3	×	×
Comp. Ex. 77	PE resin			×	×

The resins specifically used as the resins in Table 18, bottle molding conditions, and evaluation methods are shown below.

- "ABS resin" : ABS graft copolymer, manufactured by Mitsubishi Rayon Co., Ltd., trade name: Diapet 3001

Molding conditions: cylinder temperature (C1): 180 °C, (C2): 200°C, (C3): 200°C, head: 200°C, dice: 200°C

- "PC resin" : polycarbonate resin, manufactured by Mitsubishi Engineering Plastics K.K., trade name: Novalex 7022A

Molding conditions: cylinder temperature (C1): 230 °C, (C2): 260°C, (C3): 270°C, head: 270°C, dice: 280°C

- "PET resin" : polyethylene terephthalate resin, manufactured by Mitsubishi Rayon Co., Ltd., trade name: Dianite A-200

Molding conditions: cylinder temperature (C1): 280 °C, (C2): 280°C, (C3): 280°C, head: 260°C, dice: 260°C

- "PS resin" : polystyrene resin, manufactured by Nippon Polystyrene K.K.; trade name: G440K

Molding conditions: cylinder temperature (C1): 160 °C, (C2): 180°C, (C3): 200°C, head: 200°C, dice: 210°C

- "PE resin" : polyethylene resin, manufactured by Mitsui Chemical Co., Ltd.; trade name: Highzex 7000F

Molding conditions: cylinder temperature (C1): 150 °C, (C2): 165°C, (C3): 175°C, head: 175°C, dice: 175°C

- "PTFE-containing modifier A-3" : polytetrafluoroethylene-containing modifier (A-3) obtained in Production

Example 3

- "PTFE powder 1" : polytetrafluoroethylene, manufactured by Asahi Glass Co. Ltd., trade name: Aflon PTFE CD-1

5 (a) "Draw down in molding"

Draw down of parison in molding of was visually judged according to the following criterion.

○: Die swell is large, and no draw down is observed.

10 ×: Die swell is small, and draw down is observed.

(b) "Appearance of bottle"

The appearance of the resulted bottle was visually judged according to the following criterion.

15 ○: Gloss is excellent, and surface roughening is not found.

×: Gloss is poor, and surface roughening is found.

<Examples 74 to 106, Comparative Examples 78 to 92>

The components shown in Tables 19 to 22 were mixed at respective proportions, and the mixtures were subjected to extrusion molding by a 50 mm single screw extruder (manufactured by IKG K.K.) at a cylinder temperature set at 230°C, to obtain sheets made of thermoplastic resin compositions having a width of 80 mm and a thickness of 3 mm. Regarding the resulted sheets, the following items were evaluated. The results are shown in Tables 19 to 22.

- Surface appearance: The resulted sheet was visually ob-

served and judged according to the following criterion.

○: Surface roughening, splinter, generation of fish eyes supposed to be caused by poor dispersion of PTFE, are not observed.

5 ×: Surface roughening, splinter, generation of fish eyes supposed to be caused by poor dispersion of PTFE, are observed.

·Plate out: Pollution on the surface of a roll in molding was observed, using a two-roll mill.

10 ○: No pollution on the surface of a roll

△: Slight pollution on the surface of a roll

×: Heavy pollution on the surface of a roll

Table 19

Example	74	75	76	77	78	79	80	81	82	83	84	85	86
PP resin 1	100	100	100	100									
PP resin 2					100	100	100						
PE resin 1								100	100	100			
PE resin 2											100	100	100
PTFE-containing modifier A-3 (PTFE content in 100 parts of resin)	10	10	10	10	10	10	10	10	10	10	10	10	10
Talc	200	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)
Wood powder		200			200	200		200	200		200	200	
Kenaf ground product			200				200						
Water paper				200						200			200
Appearance of molded article	○	○	○	○	○	○	○	○	○	○	○	○	○
Plate out	○	○	○	○	○	○	○	○	○	○	○	○	○

Table 20

Comparative Example	78	79	80	81	82	83	84
PP resin 1	100	100	100	100			
PP resin 2					100	100	
PE resin 1							
PE resin 2							100
Thermoplastic resin modifier A-7		5	5	5		5	5
PTFE powder-1			5	5	5		
Talc	200	200	200		200	200	
Wood powder							
Water paper				200			200
Appearance of molded article	x	x	△	x	x	x	x
Plate out	x	x	x	x	x	x	x

Table 21

Example	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106
PS resin	100	100	100																	
ABS resin				100	100	100														
PET resin							100	100	100											
Biodegradable resin										100	100	100								
Recycled PP resin													100	100	100	100				
Bumper ground product																	100			
Recycled PET resin																		100	100	100
PTFE-containing modifier A-3																				
(PTFE content in 100 parts of resin)	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
Talc	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)
Wood powder	200	200	200	200	200	200	200	200	200	200	200	200	200	200	200	200	200	200	200	200
Kenaf ground product																				
Waste paper			200			200			200			200			200	200	200			200
Appearance of molded article	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○
Plate out	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○

Table 22

Comparative Example	85	86	87	88	89	90	91	92
PS resin	100	100						
ABS resin			100	100				
PET resin					100			
Biodegradable resin								
Recycled PP resin						100		
Bumper ground product							100	100
Recycled PET resin								5
Thermoplastic resin modified A-7		5	5		5			
PTFE powder-1			5	5				
Talc				200				
Wood powder	200	200	200			200	200	
Kenaf ground product								
Waste paper					200			200
Appearance of molded article	X	X	△	X	X	X	X	X
Plate out	X	X	X	X	X	X	X	X

As the composition components in Tables 19 to 22, the following components were specifically used.

- 5 • "PP resin 1" : polypropylene resin, manufactured by
Nippon Polychem K.K., trade name: Novatec PP BC06C,
molding temperature: 230°C
- "PP resin 2" : polypropylene resin, manufactured by
Nippon Polychem K.K., trade name: Novatec PP FY-6C,
molding temperature: 230°C
- 10 • "PE resin 1" : polyethylene resin, manufactured by
Nippon Polychem K.K., trade name: Novatec HD HY540,
molding temperature: 210°C
- "PE resin 2" : polyethylene resin, manufactured by
Nippon Polychem K.K., trade name: Novatec LD LJ801N,
molding temperature: 210°C
- 15 • "PS resin" : polystyrene resin, manufactured by Nippon
Polystyrene K.K.; trade name: G440K, molding tempera-
ture: 230°C
- 20 • "ABS resin" : acrylonitrile/styrene copolymer rein-
forced by rubber, manufactured by Mitsubishi Rayon
Co., Ltd., trade name: Diapet, molding temperature:
200°C
- "PET resin" : polyethylene terephthalate resin, manu-
factured by Mitsubishi Rayon Co., Ltd., trade name:
Dianite PA-200, molding temperature: 250°C
- 25 • "Biodegradable resin" : polylactic acid-based resin,
manufactured by Shimadzu Corp., trade name: Lacty
9400, molding temperature: 220°C

- "Recycled PP resin" : That obtained by two cycles of extrusion, shaping and grinding of PP resin 1 was used. Molding temperature: 230°C
- "Bumper ground product" : An automobile bumper essentially composed of a PP resin was ground into pellets. In the present invention, TSOP was used as a specific example. Molding temperature: 240°C
- "Recycled PET resin" : Materials other than PET were removed from fractioned and collected PET bottles used for beverage and the like, then, washed with a weak alkaline aqueous solution and water, then, wet-ground, then, resins other than the PET resin and, metal pieces were separated by utilizing specific gravity difference, to obtain ground products of PET bottles. Molding temperature: 250°C
- "PTFE-containing modifier A-3" : polytetrafluoroethylene-containing modifier (A-3) obtained in Production Example 3
- "Thermoplastic resin modifier A-7" : A (meth)acrylate-based polymer (A-7) obtained in Production Example 7
- "PTFE powder 1" : polytetrafluoroethylene, manufactured by Asahi Glass Co. Ltd., trade name: Aflon PTFE CD-1

<Examples 107 to 123, Comparative Examples 93 to 101>

The components shown in Tables 23 to 24 were mixed at respective proportions, and the mixtures were subjected to extrusion foaming molding by a 50 mm single

screw extruder (manufactured by IKG K.K.), to obtain foamed sheets having a width of 80 mm and a thickness of 5 mm. Regarding the resulted foamed sheets, the following items were evaluated. The results are shown in Tables 23 to 24.

• Foamed cell condition in molded article: The section of a foamed sheet was observed and judged according to the following criterion.

○: Ratio of cell size near surface to cell size at center part is not over 2-fold.

×: Ratio of cell size near surface to cell size at center part is over 2-fold.

• Surface appearance of molded article: The surface of a foamed sheet was visually observed, and judged according to the following criterion.

○: No trace of foam breaking is found on the surface of a sheet, and the sheet is smooth.

×: Trace of foam breaking is found on the surface of a sheet, and the sheet reveals unevenness on the surface.

Table 23

	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123
PP resin	100	100	100														
Recycled PP resin				100													
PE resin 1					100	100	100										
PE resin 2								100	100	100							
PE resin 3											100	100	100				
PET resin														100			
Recycled PET resin															100		
PS resin																	100
ABS resin																	
PTFE-containing modified A-4	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
(PTFE content in 100 parts of resin)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)	(5)
ADCA	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5
Butane		5															
Sodium bicarbonate		2					2			2			2	2	2	2	2
Foamed body density	0.12	0.11	0.31	0.12	0.11	0.11	0.31	0.1	0.11	0.35	0.11	0.11	0.41	0.43	0.33	0.33	0.37
Foamed cell condition	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○
Foamed body appearance	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○

Table 24

Comparative Example	93	94	95	96	97	98	99	100	101	102
PP resin	100	100								
Recycled PP resin			100							
PE resin 1				100						
PE resin 2					100					
PE resin 3						100				
PET resin							100			
Recycled PET resin								100		
PS resin									100	
ABS resin										100
Thermoplastic resin modifier A-7					5	5	5	5		
PTFE powder-1		5	5	5		5			5	5
Sodium bicarbonate	2	2	2	2	2	2	2	2	2	2
Foamed body density	0.60	0.62	0.64	0.49	0.45	0.46	0.61	0.62	0.52	0.48
Foamed cell condition	X	X	X	△	X	X	X	X	X	X
Foamed body appearance	X	X	X	△	X	X	X	X	X	X

As the composition components in Tables 23 to 24, the following components were specifically used.

- "PP resin" : polypropylene resin, manufactured by Nippon Polychem K.K., trade name: Novatec PP FY-6C,
5 molding temperature: 230°C
- "PE resin 1" : polyethylene resin, manufactured by Nippon Polychem K.K., trade name: Novatec HD HJ580,
molding temperature: 210°C
- "PE resin 2" : polyethylene resin, manufactured by
10 Nippon Polychem K.K., trade name: Novatec LD LC720,
molding temperature: 210°C
- "PE resin 3" : polyethylene resin, manufactured by Nippon Polychem K.K., trade name: Novatec LL UJ370,
molding temperature: 210°C
- 15 • "PET resin" : polyethylene terephthalate resin, manufactured by Mitsubishi Rayon Co., Ltd., trade name: Dianite KR-560, molding temperature: 250°C
- "Recycled PP resin" : That obtained by two cycles of extrusion, shaping and grinding of PP resin 1 was
20 used. Molding temperature: 230°C
- "Recycled PET resin" : materials other than PET were removed from fractioned and collected PET bottles used for beverage and the like, then, washed with a weak alkaline aqueous solution and water, then, wet-
25 ground, then, resins other than the PET resin and, metal pieces were separated by utilizing specific gravity difference, to obtain ground products of PET

bottles. Molding temperature: 250°C

- "PS resin" : polystyrene resin, manufactured by Nippon Polystyrene K.K.; trade name: G440K, molding temperature: 230°C
- 5 • "ABS resin" : acrylonitrile/styrene copolymer reinforced by rubber, manufactured by Mitsubishi Rayon Co., Ltd., trade name: Diapet 3001, molding temperature: 200°C
- 10 • "PTFE-containing modifier A-4" : polytetrafluoroethylene-containing modifier (A-4) obtained in Production Example 4
- "Thermoplastic resin modifier A-7" : A (meth)acrylate-based polymer (A-7) obtained in Production Example 7
- 15 • "PTFE powder 1" : polytetrafluoroethylene, manufactured by Asahi Glass Co. Ltd., trade name: Aflon PTFE CD-1

As described above, when the thermoplastic resin modifier of the present invention is used, the dispersibility of polytetrafluoroethylene is high in adding to
20 the thermoplastic resin, and various physical properties such as flame retardancy, mechanical properties and the like are improved by addition in small amount, and the dispersibility of fillers is improved, further, a foamed body of excellent appearance having uniform foamed cells
25 is obtained.

CLAIMS

1. A modifier for thermoplastic resin, comprising 40 to 70% by weight of polytetrafluoroethylene (A), and an alkyl (meth)acrylate-based polymer (B) containing an alkyl methacrylate carrying an alkyl group having 1 to 4 carbon atoms and an alkyl acrylate carrying an alkyl group having 1 to 4 carbon atoms and in which the total content of these constituent units is 70% by weight or more.

2. The modifier for thermoplastic resin according to Claim 1 wherein the weight-average molecular weight of the alkyl (meth)acrylate-based polymer (B) is from 20,000 to 100,000.

3. The modifier for thermoplastic resin according to Claim 2 wherein the weight-average molecular weight of the alkyl (meth)acrylate-based polymer (B) is from 20,000 to 50,000.

4. The modifier for thermoplastic resin according to Claim 1 wherein the alkyl (meth)acrylate-based polymer (B) is a copolymer composed of 50 to 90% by weight of an alkyl methacrylate carrying an alkyl group having 1 to 4 carbon atoms and 10 to 50% by weight of an alkyl acrylate carrying an alkyl group having 1 to 4 carbon atoms.

5. The modifier for thermoplastic resin according to Claim 1, obtained by polymerizing monomers containing 70% by weight or more of an alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms in the

dispersion wherein polytetrafluoroethylene (A) particles having an average particle size of 0.05 to 1.0 μm are dispersed, to form the alkyl (meth)acrylate-based polymer (B), then coagulating or spray-drying solid components in the resulted dispersion.

6. The modifier for thermoplastic resin according to Claim 1, obtained by polymerizing monomers containing 70% by weight or more of an alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms in the dispersion wherein polytetrafluoroethylene (A) particles are dispersed, to form the alkyl (meth)acrylate-based polymer (B) particles having an average particle size of 0.05 to 0.15 μm , then coagulating or spray-drying solid components in the resulted dispersion.

7. The modifier for thermoplastic resin according to Claim 1, obtained by polymerizing monomers containing 70% by weight or more of an alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms in a dispersion wherein polytetrafluoroethylene (A) particles are dispersed, to form an alkyl (meth)acrylate-based polymer (B) having a weight-average molecular weight measured by gel permeation chromatography of 20,000 to 5,000,000, then coagulating or spray-drying solid components in the resulted dispersion.

8. The modifier for thermoplastic resin according to Claim 1, obtained by mixing a dispersion wherein the alkyl (meth)acrylate-based polymer (B) particles are

dispersed, which was prepared by polymerizing monomers containing 70% by weight or more of an alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms, with a dispersion wherein the polytetrafluoroethylene (A) particles having an average particle size of 0.05 to 1.0 μm , and coagulating or spray-drying solid components in the mixed dispersion.

9. The modifier for thermoplastic resin according to Claim 1, obtained by mixing a dispersion wherein the alkyl (meth)acrylate-based polymer (B) particles having an average particle size of 0.05 to 0.15 μm , which was prepared by polymerizing monomers containing 70% by weight or more of an alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms, with a dispersion wherein the polytetrafluoroethylene (A) particles, and coagulating or spray-drying solid components in the mixed dispersion.

10. The modifier for thermoplastic resin according to Claim 1, obtained by mixing a dispersion wherein the alkyl (meth)acrylate-based polymer (B) particles having a weight-average molecular weight measured by gel permeation chromatography of 20,000 to 5,000,000, which was prepared by polymerizing monomers containing 70% by weight or more of an alkyl (meth)acrylate carrying an alkyl group having 1 to 4 carbon atoms, with a dispersion wherein the polytetrafluoroethylene (A) particles having an average particle size of 0.05 to 1.0 μm , and coagulating or spray-drying solid components in the mixed dispersion.

11. A thermoplastic resin composition obtained by adding the modifier according to Claim 1 to a thermoplastic resin (C) so that the content of the polytetrafluoroethylene (A) is 0.001 to 20 parts by weight based on 100 parts by weight of the thermoplastic resin (C).

12. A thermoplastic resin composition comprising the modifier according to Claim 1, a thermoplastic resin (C) and a flame retardant (D).

13. A thermoplastic resin composition comprising the modifier according to Claim 1, a thermoplastic resin (C) and a filler (E).

14. A molded article obtained by injection molding, extrusion molding or extrusion blow molding of the thermoplastic resin composition according to Claim 11.

15. A molded article obtained by injection foaming molding or extrusion forming molding of the thermoplastic resin composition according to Claim 11.