

Method of and arrangement for electrochemical machining

The invention relates to a method, an arrangement and a power supply for a process of electrochemically machining an electrically conductive workpiece by applying electrical machining pulses between the workpiece and an electrically conductive electrode while electrolyte is supplied between the workpiece and the
5 electrode.

Electrochemical machining is a process in which an electrically conductive workpiece is dissolved at the location of an electrode while electrolyte and electric current is supplied. For this purpose, the electrode is brought in the proximity of the workpiece and, while electrolyte is fed into the gap between the workpiece and the
10 electrode a powerful current is passed through the workpiece and the electrode via the electrolyte, the workpiece being positive with respect to the electrode. The current is applied in the form of machining pulses having a given amplitude and duration. In the intervals between the machining pulses the electrolyte is renewed. During the application of the machining pulses the electrode and the workpiece are moved towards
15 one another with a given feed rate, as a result of which the electrode forms a cavity or eventually a hole in the surface of the workpiece, the shape of this cavity or hole having a shape corresponding to the shape of the electrode. This process can be used, for example, for making intricate cavities or holes in or for shaping hard metals or alloys.

The copying precision with which the shape of the cavity or the hole in
20 the workpiece follows the shape of the electrode is important for the quality of the result. Meanwhile, many publications in the form of articles in periodicals and patent documents have appeared in which proposals have been made to improve the copying precision of electrochemical machining.

Therefore, it is an object of the present invention to provide an
25 electrochemical machining method and arrangement with a good copying precision. To this end, the method of the type defined in the opening paragraph is characterized in that the machining pulses alternate with electrical passivation pulses of the same polarity

as the machining pulses, the voltage of the passivation pulses having an amplitude which is inadequate to dissolve the workpiece and a passivation film on the workpiece.

In the intervals between the machining pulses, during renewal of the electrolyte, passivation pulses are applied deliberately with such an amplitude that a
5 passivation layer of metal oxides is formed around the electrode on the workpiece. During the next machining pulse this layer is removed selectively at the end face of the electrode. In this way the machining pulse is given a higher effectiveness in the feed direction. This improves the copying precision because comparatively more material of the workpiece is dissolved at the end face of the electrode and in the cavity to be
10 machined in the workpiece smaller radii are formed at the edges and slopes of the lateral surface of the cavity. An additional advantages to be mentioned is that the energy consumption of the process is smaller and that the dissolution rate of the workpiece in the feed direction is higher. This is because, owing to the local passivation layers, the energy of the machining pulses is no longer used for the undesired removal of material
15 from the lateral surfaces of the cavity in the workpiece.

Preferably, a distance between the workpiece and the electrode is maintained, which is smaller during the machining pulses than during the passivation pulses. By increasing the distance between the workpiece and the electrode during the passivation pulses it is achieved that owing to the greater distance the electric field of
20 the passivation pulses has less effect at the end face of the electrode than at the lateral walls of the cavity in the workpiece. Thus, it is achieved with greater accuracy that opposite the end face of the electrode, i.e. at the bottom of the cavity in the workpiece, a thinner passivation layer, or even no passivation layer at all, is formed than elsewhere in the cavity to be machined. The amplitude, duration and waveform of the machining
25 pulses are selected in such a manner that activation of the surface to be machined occurs only in the case of the smaller distance during the machining pulses. In that case anode dissolution during the application of machining pulses occurs only at those locations of the workpiece where the gap is smaller than the critical distance. The remainder of the workpiece is protected by a passivation layer and is not dissolved. This results in a very
30 high copying precision. In a variant of the method in accordance with the invention the workpiece and the electrode perform an oscillating movement relative to one another, the distance between the workpiece and the electrode reaching a minimum during the machining pulses.

The amplitude of the voltage of the passivation pulses plays an important part. Too low a voltage has no or little effect because the passivation layers are too thin. Conversely, too high a voltage causes the previously formed passivation layers to disappear at the lateral surfaces of the cavity and causes the copying precision to deteriorate. An even higher voltage will ultimately yield the same effect as the normal machining pulses and will cause the workpiece to dissolve at various undesired locations in the cavity to be machined. To optimize the amplitude of the passivation pulses a variant of the method in accordance with the invention is characterized in that the amplitude of the voltage of the passivation pulses is adjusted at least once during electrochemical machining, the amplitude of the passivation pulses in a series of successive passivation pulses being changed until the resistance value measured between the workpiece and the electrode has reached a maximum, after which electrochemical machining is continued with an amplitude of the passivation pulse which corresponds to the maximum of the resistance value.

During a series of successive passivation pulses the amplitude of the voltage of the passivation pulses is changed gradually, for example increased from zero to a given maximum value at which the workpiece begins to dissolve. In each subsequent passivation pulse a slightly higher voltage is applied and the resistance of the gap is measured and stored. From the measured resistance values the highest value is chosen and the corresponding amplitude of the voltage is fixed and sustained for some time during the subsequent machining of the workpiece. The amplitude of the voltage of the passivation pulses is thus optimized for a maximal gap resistance. This implies that the formation of passivation layers on the lateral surfaces is also maximal and the copying precision is optimum.

For this purpose, the arrangement in accordance with the invention is characterized in that the arrangement comprises:

- an electrode;
- means for positioning the electrode and the workpiece in a spatial relationship so as to maintain a gap between the electrode and the workpiece;
- means for supplying electrolyte into the gap;
- a first electric power supply source, which is electrically connectable to the electrode and the workpiece to supply machining pulses to the workpiece and the electrode;

- a second electric power supply source of the same polarity as the first power supply source and having an output voltage which is controllable by means of a control signal, which second power supply source is electrically connectable to the electrode and the workpiece to supply passivation pulses to the workpiece and the
5 electrode;
- means for alternately connecting the first and the second power supply source to the workpiece and the electrode;
- means for generating a varying control signal for changing the output voltage of the second power supply source during successive passivation pulses;
- 10 - means for measuring during the successive passivation pulses the electrical resistance of the gap between the workpiece and the electrode at an instant during the passivation pulses and for storing resistance information values which are representative of the resistance of the gap at said instant and for storing corresponding control signal values of the control signal at said instant; and
- 15 - means for calculating a maximum value from the resistance information values, and means for maintaining the control signal for the second power supply source at the control signal value which corresponds to the maximum value.

The second power supply source is controllable and its voltage is gradually raised, the value of the voltage for which the measured gap resistance is
20 maximal being stored.

When a varying gap distance is used any value of the distance between the workpiece and the electrode will correspond to another optimum amplitude of the voltage of the passivation pulses. This is the case particularly when the workpiece and the electrode perform an oscillating movement relative to one another and the distance
25 between them is, in fact, never constant. In order to preclude this problem, a further variant of the method in accordance with the invention is characterized in that the passivation pulses are divided into time slices and for each individual time slice the instantaneous amplitude of the voltage of the passivation pulses is changed until the resistance value measured between the workpiece and the electrode has reached a
30 maximum during the individual time slice, after which electrochemical machining is continued with passivation pulses whose instantaneous amplitude varies in accordance with the amplitude found for each time slice and corresponding to the maximum of the resistance value in said time slice.

The time span of each of the passivation pulses is divided into a plurality of slices and in each slice the amplitude of the voltage during successive passivation pulses is changed until the maximal resistance in said slice is found. The corresponding optimum slice voltage of the passivation pulse in this slice is stored. Upon termination
5 of this adjustment procedure all the stored optimum slice voltages are generated consecutively in the correct sequence within the time span of the passivation pulses, as a result of which the amplitude of the voltage of the passivation pulse has a waveform which is optimized for the variation in the gap distance.

For this purpose, an embodiment of the arrangement in accordance with
10 the invention is characterized in that

- the means for generating the varying control signal include means for changing the output voltage of the second power supply source at different instants within the time span of one passivation pulse;
- the means for measuring and storing are adapted to store resistance
15 information values which are representative of the instantaneous resistance of the gap at the different instants within the passivation pulse and to store corresponding control signal values of the control signal at the different instants;
- means for calculating are adapted to calculate individual maximum values from the resistance information values of corresponding instants within successive
20 passivation pulses and to generate a control signal having an instantaneous value which at the different instants is equal to the control signal values which correspond to the individual maximum values.

The voltage of the second power supply source is thus varied within the time span of a passivation pulse whose waveform matches best with the varying gap
25 size during the passivation pulse.

The aforesaid adjustment procedure of determining and maintaining the optimum amplitude waveform for the voltage of the passivation pulses can be repeated as frequently as is necessary during the further electrochemical machining of the workpiece.

30 A variant of the method in accordance with the invention is characterized in that in the time intervals between the successive machining pulses in addition electrical pulses of opposite polarity are applied between the workpiece and the electrode, which last-mentioned pulses have a voltage whose amplitude does not exceed

the amplitude at which the electrode begins to dissolve in the electrolyte, and/or in the time intervals between the successive machining pulses the passivation pulses alternate with electrical pulses of opposite polarity, which last-mentioned pulses have a voltage whose amplitude does not exceed the amplitude at which the electrode begins to dissolve
5 in the electrolyte.

The process is now supplemented and/or alternates with electric pulses of opposite polarity in the intervals between the machining pulses. The purpose, effect and setting of the amplitude of the voltage of the pulses of opposite polarity are described comprehensively in the International Application WO 97/03781. Said Application
10 describes between what optimum limits the amplitude of the voltage of the pulses of opposite polarity should be adjusted, on the one hand, to prevent that the electrode dissolves and thus reduces the machining accuracy and, on the other hand, to achieve a high machining efficiency in combination with a well-defined surface condition, for example in the form of a certain lustre. When chrome-nickel steel is machined it is
15 found that under these working conditions a reduced concentration of hexavalent toxic chromium is left in the finished electrolyte solution, as a result of which it is easier to comply with requirements as regards environmental pollution.

The resistance of the gap can be calculated by measuring the current through and the voltage across the gap between the electrode and the workpiece and
20 storing the measurement data in a memory. The current and the voltage are preferably measured by means of analog-to-digital converters coupled to a computer in which the measurement data is stored. The computer calculates the maximum gap resistance by analyzing the measurement data. The computer further generates the control signal for controlling the output voltage of the second power supply source. During the adjustment
25 procedure the output voltage of the second power supply source is gradually changed under command of the control signal from the computer. After the computer has found the maximum resistance value the corresponding control signal is continuously generated by the computer during a given time.

30 These and other aspects of the invention will be described in more detail with reference to the accompanying drawings, in which:

Figure 1 diagrammatically shows an embodiment of an arrangement for carrying out the method in accordance with the invention;

Figure 2 shows waveforms of signals which appear in a variant of the method in accordance with the invention;

Figure 3 shows the change in condition of the electrolyte between the electrode and the workpiece when a variant of the method in accordance with the
5 invention is carried out;

Figure 4 shows a waveform of a signal which occurs in a variant of the method in accordance with the invention;

Figure 5 shows a waveform of an alternative current pulse train for carrying out the method in accordance with the invention;

10 Figure 6 shows an electrical block diagram of an embodiment of an arrangement for carrying out the method in accordance with the invention;

Figure 7 illustrates the formation of passivation layers in the machining cavity of the workpiece when a variant of the method in accordance with the invention is carried out;

15 Figure 8 shows waveforms of the voltage across and the resistance between the electrode and the workpiece when a variant of the method in accordance with the invention is carried out;

Figure 9A and Figure 9B are flow charts of process steps of variant of the method in accordance with the invention;

20 Figure 10 shows waveforms of additional signals which occur in a variant of the method in accordance with the invention; and

Figure 11 shows waveforms of additional signals which occur in another variant of the method in accordance with the invention.

In these Figures parts having a like function or purpose bear the same
25 reference symbols.

Figure 1 shows an arrangement for the electrochemical machining of a workpiece 2. The workpiece 2 is arranged on a table 4 which is moved at a feed rate V_k towards an electrode 6 which performs an oscillating movement with respect to the
30 workpiece 2, which is effected by means of a crankshaft 8 which is driven by a motor 10. The workpiece is made of, for example, a kind of steel containing chromium. An electrolyte, for example an aqueous solution of nitrates of alkali metals, flows in the gap 5 between the workpiece 2 and the electrode 6 and is circulated at a pressure P_1

from a reservoir 3. The workpiece 2, the table 4 and the electrode 6 are electrically conductive. The electrode 6 and the table 4 are connected to an electric power supply source 12 which supplies electric pulses to the electrode 6 and the table 4. The electric pulses include machining pulses having a polarity for which the table 4 and,

- 5 consequently, the workpiece 2 are positive with respect to the electrode 6, which pulses alternate with passivation pulses having the same polarity but having a voltage and waveform to be described hereinafter. During the machining pulses the metal of the workpiece 2 enters into anode dissolution in the electrolyte. During the passivation pulses the surface of the workpiece 2 is passivated locally.

- 10 A curve I in Figure 2 represents the variation of the size $S(t)$ of the gap 5 between the electrode 6 and the workpiece 2. A curve II in Figure 2 represents the variation of the voltage U across the gap 5 during an adjustment procedure to be described hereinafter, and a curve III represents the voltage variation across the gap 5 during the subsequent machining period. The machining pulses MP are applied in a time
15 interval t_i , indicated in the a curve IV of Figure 2, in which the electrode 6 is nearest the workpiece 2. During these machining pulses the voltage across the gap 5 has a waveform with a global minimum, as indicated in the curve II of Figure 2. The machining pulses alternate with passivation pulses PP in a time interval t_u , indicated in a curve V in Figure 2. It is to be noted that the shown waveforms of the voltage U
20 across the gap 5 are merely an approximation of the actual voltage waveforms.

- Figure 3 gives an impression of the processes which occur in the gap 5. In the initial stage of the approach of the electrode 6 to the workpiece 2 in the case of a comparatively large gap S_{max} the flow of the electrolyte is of a turbulent nature and the electrolyte contains vapor and gas bubbles. In this stage the space between the electrode
25 6 and the workpiece 2 has a comparatively high electrical resistance, which is apparent from the first maximum in the voltage U in the curve II of Figure 2. As the electrode 6 approaches, the pressure in the electrolyte increases and the vapor and gas bubbles dissolve, as a result of which the electrolyte is homogeneous and uniform in the gap and a high current density is attainable with a small gap size. As a result of this, the
30 electrical resistance decreases, which is apparent from the occurrence of a global minimum in the voltage U in the curve II of Figure 2. As a result of the increase of the distance between the electrode 6 and the workpiece 2 and the resumed generation of vapor and gas bubbles the electrical resistance increases again to a second maximum as

shown in the curve II of Figure 2. The supply of electric power can be so large that the electrolyte begins to boil violently and consequently cavitation is produced in the gap. The cavitation gives rise to a temporary increase in the electrical resistance of the electrolyte, which manifests itself as a local maximum in the voltage variation U between the electrode and the workpiece during the machining pulses. Figure 4 shows in greater detail the variation of the voltage U with the local maximum U_{3max} which occurs therein after the global minimum U_{min} .

It is to be noted that such a violent cavitation can be avoided by applying groups of machining pulses, which groups alternate with passivation pulses. Such a pulse train is shown in Figure 5. Thus, the process proceeds more steadily with a more accurate result using the same minimum gap size.

Figure 6 shows the electrical block diagram of an electrochemical machining arrangement in accordance with the invention, which includes an electric power supply source 12 in accordance with the invention. The power supply source 12 comprises a current source 14 for supplying the machining pulses, which current source supplies a current I whose magnitude is controllable by means of a control signal CSI, and a controllable voltage source 16 for supplying the passivation pulses, which voltage source supplies an output voltage U_p which is controllable by means of a control signal CSU. The negative terminal of the current source 14 and the negative terminal of the controllable voltage source 16 are both connected to the electrode 6 via a series resistor 18. The positive terminal of the current source 14 is connected to the workpiece 2 via a switch 20. The switch 20 is closed at time intervals t_i (see Figure 2) under control of a signal S_i , which is supplied by a synchronization unit 22. The positive terminal of the controllable voltage source 16 is connected to the workpiece 2 via a switch 24. The switch 24 is closed at time intervals t_u (see Figure 2) under control of a signal S_u , which is also supplied by the synchronization unit 22, which also synchronizes the motor 10. The analog voltage U between the electrode 6 and the workpiece 2 is measured on the terminals 32 and 34 by means of an analog-to-digital converter 26 and is converted into a digital signal DU, which is stored, analyzed and processed in a computer 28. The current I through the gap is measured by measuring the voltage drop across the series resistor 18 on the terminals 36 and 38 by means of a second analog-to-digital converter 30, which converts the analog voltage drop into a digital signal DI, which is processed by the computer 28 similarly to the digital signal DU. Instead of a

series resistor 18 a current transformer or any other suitable interface may be chosen. The analog-to-digital converter 30 can be dispensed with if at appropriate instants the input terminals of the analog-to-digital converter 26 are switched over from voltage measurement via the terminals 32 and 34 to current measurement via the terminals 36 and 38. The synchronization unit 22, the analog-to-digital converters 26 and 30, and the computer 28 are supplied with clock pulses (not shown in Figure 6) which ensure that the data acquisition and the data processing are in synchronism with the appearance of the alternating machining and passivation pulses and the oscillation of the electrode. The position of the table 4 is monitored by means of a position sensor 40, which supplies a signal DS which is a measure of the displacement of the table 4. The computer 28 generates the control signal CSI for the current source 14 and the control signal CSU for the controllable voltage source 16 via suitable interfaces 42 and 44, which can be constructed, for example, as digital-to-analog converters. The angle of rotation of the crankshaft 8 is measured by means of a sensor 46, which supplies a signal DP to the computer 28, which signal is a measure of the relative distance between the electrode 6 and the workpiece 2.

By controlling the feed rate V_k of the table 4 the gap 5 can be adjusted in such a manner that a local maximum U_{3max} occurs as shown in Figure 4. This local maximum can be detected by analyzing the voltage U by means of the analog-to-digital converter 26 and the computer 28 or by means of an oscilloscope. However, if desired, any other operating point for the size of the gap 5 can be chosen, i.e. also one for which no local maximum U_{3max} occurs in the voltage U .

Figure 7 illustrates the effect of the passivation pulses. The amplitude of the voltage U_p of the controllable voltage source 16 is selected so as to form passivation layers PL in the machining cavity in the workpiece 2. However, the amplitude of the voltage U_p is not so high that the workpiece dissolves and is neither so high that the passivation layers dissolve again. Owing to the oscillating movement the distance d_2 between the end face of the electrode 6 during the machining pulses is smaller than the distance d_1 between the lateral wall of the machining cavity and the electrode 6. In the case of a correct choice of the amplitude and duration of the machining pulses it is achieved that the workpiece 2 dissolves only frontally, i.e. opposite to the end face of the electrode 6 in the feed direction, and not at the location of the passivation layers PL. This results in a very good copying precision, the shape of the cavity in the

workpiece 2 following the shape of the electrode 6 very accurately. Intricate profiles and punched slopes with a precision of 10 minutes of arc are attainable. The locally deposited passivation layers PL provide not only a higher machining precision but also a better energy efficiency and a higher machining speed. This is because no energy is wasted for the undesired removal of material from the lateral walls of the machining cavity.

For an optimum effect it is therefore desirable if the voltage U_p of the passivation pulses has an amplitude which is not so large that the passivation layers PL or even the workpiece 2 dissolve and which is neither so small that not enough or hardly any passivation layers are formed. In both cases the machining pulses will dissolve the workpiece 2 wherever possible and will produce a relatively larger machining cavity in all directions and thereby reduce the copying precision. The optimum amplitude of the passivation pulses is that amplitude for which the resistance of the gap 5 is highest. This is because then the growth of the passivation layers PL, which have a poor electrical conduction, is maximal and the copying precision is also maximal.

In order achieve an optimum adjustment of the amplitude of the voltage of the passivation pulses the electrochemical machining arrangement (Figure 6) effects an adjustment procedure in which the voltage U_p of the passivation pulses is increased stepwise from zero volts to the voltage U_{ap} , at which the workpiece 2 enters into anode dissolution, during a plurality of successive oscillations of the electrode 6. For this purpose, the computer 28 applies a suitable control signal CSU to the controllable voltage source 16 via the interface 44. After each increase of the voltage U_p the resistance of the gap 5 is measured by means of the analog-to-digital converters 26 and 30. The measured resistance value and the corresponding control signal CSU are stored as numerical values in the main memory of the computer 28. From all the resistance values found the computer determines the largest value and the associated amplitude of the voltage U_p . The adjustment procedure is now finished and the machining process is continued for a given time T_M , using the amplitude of the voltage U_p thus found. As a result of the oscillating movement of the electrode 6 the distance between the workpiece 2 and the electrode 6 in the feed direction changes continually during the passivation pulses. Each value of the distance between the workpiece and the electrode corresponds to another optimum amplitude of the voltage of the passivation pulses. In order to allow

for this, the time span of the passivation pulse is divided into slices. The optimum amplitude for each time slice is now determined, the resistance of the gap being maximal in this time slice. Upon completion of the adjustment procedure the computer 28 supplies such a series of control signals to the controllable voltage source 16 within 5 the time span of each passivation pulse that the amplitude of the passivation pulse is given a variation which is optimized for the varying gap size. An example of such a varying amplitude of the passivation pulses is given in curve III of Figure 2. This elaborate adjustment procedure will now be described in more detail with reference to the diagrams of Figure 8 and a flow chart in Figures 9A and 9B.

10 Figure 8, curve I shows the distance S between the workpiece 2 and the electrode 6. The rotation of the crankshaft 8 produces a sinusoidal variation of the distance S , which reaches a minimum S_{min} during the machining pulses MP. Each revolution of the crankshaft 8 corresponds to an oscillation having a period T . The adjustment procedure covers a group of m oscillations and consequently has a duration 15 mT . The adjustment procedure, i.e. the group of m oscillations, is followed by a machining period T_M , in which the workpiece is further machined by means of machining pulses MP and passivation pulses PP having an amplitude variation determined in the preceding adjustment procedure. The length of the machining period T_M depends on the operating conditions and can be set according to need. Upon 20 completion of the machining period T_M the adjustment procedure, which again covers m oscillations, is repeated. The number of times that the adjustment procedure is repeated also depends on the operating conditions and on the desired result. In the simplest case the adjustment procedure is performed only once and the workpiece is electrochemically machined in one go in the subsequent machining period. Each group 25 has a sequence number i running from 1 to a value determined by the total length of time of the machining process. Each oscillation in the group i has a sequence number j running from 1 to m . Moreover, each oscillation, i.e. also the oscillations in the machining period T_M , is divided into time slices of a length Dt . Each slice has a sequence number k running from 1 to n . In Figure 8 each passivation pulse PP has been 30 divided into 8 slices, i.e. $n = 8$, but obviously a greater or smaller number of slices is also possible. The number of slices required depends on the magnitude and the change in time of the relative movement between the workpiece and the electrode. More slices result in the resolution with which the optimum waveform of the amplitude of the

voltage of the passivation pulses is determined being raised and the copying precision being improved.

The curve II in Figure 8 shows the stepwise increase of the amplitude of the passivation pulses. In oscillation $j = 1$ the first step is applied, starting from zero volts. For all the slices $k = 1$ through $k = n$ the steps are equal. Furthermore, the penultimate oscillation having the sequence number $j = m-1$ and the last oscillation having the sequence number $j = m$ are shown. In the last oscillation having the sequence number $j = m$ the amplitude of the voltage is equal to the voltage U_{ap} at which the workpiece enters into anode dissolution. Upon expiry of each time slice k ($k = 1..n$) the resistance R of the gap is measured and stored in the memory of the computer. Moreover, the corresponding value of the control signal CSU is stored as a numerical value. These n resistance measurements are repeated for each oscillation j ($j = 1..m$) and the result is illustrated in the curve III, in which the resistance values for the individual slices are shown. For each slice the maximum resistance R_{max} in the series of m measurements is determined. It has been assumed, by way of example, that the resistance values per slice measured in the penultimate oscillation having the sequence number $j = m-1$ are also the maximum resistance values $R_{max}(j = m-1, k = 1)$ through $R_{max}(j = m-1, k = n)$ for each slice. However, this is not necessary. The maximum gap resistance for each individual slice k can be found in oscillations having a different sequence number j . The computer knows the value of the corresponding control signal CSU for each value found for the maximum resistance R_{max} . After completion of the adjustment procedure, i.e. in the machining period T_M , the computer generates the corresponding values of the control signal CSU in the correct sequence within the time span of each passivation pulse. The curve IV in Figure 8 gives an example of the variation of the voltage U across the gap in the machining period T_M .

The machining process and the adjustment procedure proceed as shown in the flow charts of Figures 9A and 9B. The blocks in these Figures have the following inscriptions:

- 30 B0: begin
- B1: $i = 1$
- B2: $U_k^* = 0, k = 1..n$
- B3: $R_k^* = 0, k = 1..n$

B4: $U_{k11} = 0, k = 1..n$
 B5: $j = 1$
 B6: check DP
 switch 20 ON; switch 22 OFF
 5 generate machining pulse
 B7: $k = 1$
 B8: $U_{kji} = (U_{kji} + dU) < U_{ap}$
 switch 20 OFF; switch 22 ON
 B9: wait Dt
 10 B10: measure I_{kji}
 B11: $R_{kji} = U_{kji} / I_{kji}$
 B12: $R_{kji} > R_k^*$?
 B13: $R_k^* = R_{kji}$
 B14: $U_k^* = U_{kji}$
 15 B15: $k = k+1$
 B16: $k > n$?
 B17: $j = j+1$
 B18: $j > m$?
 B19: ECM (U_k^* , TM)
 20 B20: $i = i+1$
 B21: stop ECM ?
 B22: End

In the block B1 the sequence number i of the group is set to the starting
 25 value 1. In the block B2 all the individual optimum voltages U^* for all the slices k are
 set to the starting value zero. In the block B3 all the individual maximum resistance
 values R^* for all the slices k are set to the starting value zero. In the block B4 the initial
 values of the passivation pulse amplitudes to be incremented for all the slices k are set
 to zero. In the block B5 the counter j which keeps score of the number of oscillations
 30 which have elapsed is set to the starting value 1.

After this initialization the machining process is started. In the block B6
 the signal DP which indicates the electrode position is checked. In the case of the
 correct position the current source 14 is connected by opening the switch 20 and the

controllable voltage source 16 is disconnected by opening the switch 24. Subsequently, a machining pulse is applied. This machining pulse has a given duration, which is also determined by the computer. After the machining pulse has finished the slice counter k is set to the value 1 in the block B7.

- 5 In the block B8 the amplitude U_{kji} in the k^{th} slice of the j^{th} oscillation of the i^{th} group of the passivation pulse is incremented by a step value dU . The resulting amplitude should not exceed the voltage U_{ap} . Moreover, the current source 14 is disconnected by opening the switch 20 and the controllable voltage source is connected by closing the switch 24. Subsequently, a waiting time of one slice period Dt is
- 10 observed in the block B9. After this, in the block B10 the instantaneous value of the current I_{kji} in the k^{th} slice of the j^{th} oscillation of the i^{th} group is measured and stored. In the block B11 the instantaneous resistance value R_{kji} is calculated by dividing the instantaneous voltage U_{kji} by the instantaneous current I_{kji} .

- In the block B12 it is checked whether the instantaneous resistance value
- 15 R_{kji} thus found is greater than the individual maximum resistance value R_k^* of the slice. If this is not the case, a jump to the block B15 is performed. If said value is greater, the individual maximum resistance value R_k^* is made equal to the instantaneous resistance value R_{kji} , which is effected in the block B13. Moreover, in the block B14 the corresponding individual optimum voltage U^* for said slice is made equal to the
- 20 instantaneous value U_{kji} . In the block B15 it is examined whether the slice count k is greater than n . If this is not the case, all the slices have not yet been traversed and the program returns to the block B8, the voltage for the next slice is incremented by one step, the current is measured, the resistance is calculated and the maximum resistance value with the associated instantaneous voltage value are stored. This continues until all
- 25 the slices have been traversed.

- Once all the slices have been completed the oscillation count j is incremented by one in the block B17 and is compared with the value m in the block B18. If the number of oscillations which have lapsed is smaller than or equal to m the program returns to the block B6 and a following machining pulse is applied and in the
- 30 subsequent passivation pulse the voltage is incremented by one step. This continues for m oscillations. Subsequently, in the block B20 the electrochemical machining process is continued with the individual optimum slice voltages U_k^* ($k = 1..n$) during the period TM . After this, in the block B20 the group counter i is incremented by 1. In the block

B21 it is decided whether the machining process has lasted long enough. If the machining process is to be continued for a longer time the group counter i should be incremented before the decision to stop is taken. A criterion for stopping the machining process can be, for example, the displacement of the table 4 by means of the signal DS
5 of the position sensor 40 or the elapsed process time. If the machining process is not yet completed a return to the block B2 follows and a new adjustment procedure is started, followed by another machining period TM. When the final value is reached the machining process is terminated in the block B22.

The method and arrangement described above were used for machining a
10 test sample. The material of the sample and of the electrode was steel 40X13 in an annealed condition, the machining area was 2 cm^2 and the electrolyte was 8% NaNO_3 . In the machining process the voltage of the machining pulses was 7 V, the duration of the machining pulses was 2 ms, the pressure of the electrolyte near the inlet to the gap was 350 kPa, the temperature of the electrolyte was $18\text{ }^\circ\text{C}$, the frequency of the
15 oscillations of the electrode was 47 Hz, the amplitude of the oscillations was 0.2 mm. The voltage of the passivation pulses was +2.8 V in the case of a minimal gap and +3.8 V in the case of a maximal gap +3.8 V.

An analysis of the machining results has shown that as compared with conventional machining methods the use of the electrochemical machining method in
20 accordance with the invention provided an increase in machining productivity by a factor of 1.25 and a reduction of the power consumption by a factor of 1.2. The copying error of the electrode to the surface to be machined was not more than 0.01 mm.

If desired, the passivation pulses shown in the curve III of Figure 2 and in
25 the curve IV of Figure 8 may be supplemented and/or may alternate with electric pulses of opposite polarity. The purpose, effect and setting of the amplitude of the voltage of the pulses of opposite polarity are described comprehensively in the International Application WO 97/03781. Said Application describes between what optimum limits the amplitude of the voltage of the pulses of opposite polarity should be adjusted, on the
30 one hand, to prevent that the electrode dissolves and thus reduces the machining accuracy and, on the other hand, to achieve a high machining efficiency in combination with a well-defined surface condition, for example in the form of a certain lustre. In many respects the arrangement described in said International Application is similar to

the arrangement shown in Figures 1 and 6. However, for the generation of voltage pulses of opposite polarity in the intervals between the machining pulses the polarity of the controllable voltage source 16 (Fig. 6) should be reversed temporarily, or an additional controllable voltage source of opposite polarity should be provided as well as
5 an additional switch comparable to the switch 24.

The curve II in Figure 10 illustrates how the machining pulses alternate with negative voltage pulses. Instead of the positive passivation pulses negative pulses are now applied, which give the workpiece a high lustre. The negative voltage pulses can be applied before, during or after completion of the machining method described
10 hereinbefore.

Figure 11 shows an alternative in which in the intervals between the machining pulses first a negative voltage pulse is applied and subsequently a positive passivation pulse whose waveform and amplitude are determined in accordance with the adjustment procedure described hereinbefore.

15 So far, it has been assumed that the electrode and the workpiece perform an oscillating movement with respect to one another, a machining pulse being applied during the smallest distance between the workpiece and the electrode. Increasing the distance promotes the ease with which the electrolyte can be renewed. However, strictly speaking, such a change of the distance is not necessary if the operating conditions and
20 the desired result permit this.

Instead of a revolving crankshaft it is possible to use other drive mechanisms in order to generate an oscillating or other movement for changing the distance between the electrode 6 and the workpiece 2. For this purpose, an electrically or hydraulically driven construction with a pinion and toothed rack can be used, or an
25 electrically or hydraulically driven lead screw. The electrode 6 can then be made to abut with the workpiece 2, after which the gap size is adjusted. During the machining process the gap size is adapted so as to achieve an on average substantially constant feed rate which is substantially equal to the rate of dissolution of the workpiece 2.

Claim

1. A method of electrochemically machining an electrically conductive workpiece (2) by applying electrical machining pulses between the workpiece (2) and an electrically conductive electrode (6) while electrolyte is supplied between the workpiece
5 (2) and the electrode (6), characterized in that the machining pulses alternate with electrical passivation pulses of the same polarity as the machining pulses, the voltage of the passivation pulses having an amplitude which is inadequate to dissolve the workpiece (2) and a passivation film on the workpiece (2).
- 10 2. A method as claimed in Claim 1, characterized in that the amplitude of the voltage of the passivation pulses is adjusted at least once during electrochemical machining, the amplitude of the passivation pulses in a series of successive passivation pulses being changed until the resistance value measured between the workpiece (2) and the electrode (6) has reached a maximum, after which electrochemical machining is
15 continued with an amplitude of the passivation pulse which corresponds to the maximum of the resistance value.
3. A method as claimed in Claim 2, characterized in that the passivation pulses are divided into time slices and for each individual time slice the instantaneous
20 amplitude of the voltage of the passivation pulses is changed until the resistance value measured between the workpiece (2) and the electrode (6) has reached a maximum during the individual time slice, after which electrochemical machining is continued with passivation pulses whose instantaneous amplitude varies in accordance with the amplitude found for each time slice and corresponding to the maximum of the resistance
25 value in said time slice.
4. A method as claimed in Claim 1, 2 or 3, characterized in that between the workpiece (2) and the electrode (6) distance is kept which is smaller during the machining pulses than during the passivation pulses.
- 30 5. A method as claimed in Claim 4, characterized in that the workpiece (2) and the electrode (6) perform an oscillating movement relative to one another, the



distance between the workpiece (2) and the electrode (6) reaching a minimum during the machining pulses.

6. A method as claimed in Claim 1, 2, 3, 4 or 5, characterized in that in
5 time intervals between the successive machining pulses in addition electrical pulses of opposite polarity are applied between the workpiece (2) and the electrode (6), which last-mentioned pulses have a voltage whose amplitude does not exceed the amplitude at which the electrode (6) begins to dissolve in the electrolyte.
- 10 7. A method as claimed in Claim 1, 2, 3, 4 or 5, characterized in that in time intervals between the successive machining pulses the passivation pulses alternate with electrical pulses of opposite polarity, which last-mentioned pulses have a voltage whose amplitude does not exceed the amplitude at which the electrode (6) begins to dissolve in the electrolyte.
- 15 8. An arrangement for electrochemically machining an electrically conductive workpiece (2) by applying electrical machining pulses between the workpiece (2) and an electrically conductive electrode (6) while electrolyte is supplied between the workpiece (2) and the electrode (6), characterized in that the arrangement comprises:
- an electrode (6);
 - 20 - means (4, 40) for positioning the electrode (6) and the workpiece (2) in a spatial relationship so as to maintain a gap (5) between the electrode (6) and the workpiece (2);
 - means (3) for supplying electrolyte into the gap (5);
 - a first electric power supply source (14), which is electrically connectable
25 to the electrode (6) and the workpiece (2) to supply machining pulses to the workpiece (2) and the electrode (6);
 - a second electric power supply source (16) of the same polarity as the first power supply source (14) and having an output voltage which is controllable by means of a control signal (CSU), which second power supply source (16) is electrically
30 connectable to the electrode (6) and the workpiece (2) to supply passivation pulses to the workpiece (2) and the electrode (6);
 - means (20, 24) for alternately connecting the first (14) and the second (16) power supply source to the workpiece (2) and the electrode (6);



- means (28, 44) for generating a varying control signal for changing the output voltage of the second power supply source (16) during successive passivation pulses;
 - means (18, 30, 26, 28) for measuring during the successive passivation pulses the electrical resistance of the gap (5) between the workpiece (2) and the electrode (6) at an instant during the passivation pulses and for storing resistance information values which are representative of the resistance of the gap (5) at said instant and for storing corresponding control signal values of the control signal (CSU) at said instant; and
 - 10 - means (28) for calculating a maximum value from the resistance information values, and means (28, 44) for maintaining the control signal (CSU) for the second power supply source (16) at the control signal value which corresponds to the maximum value.
- 15 9. An arrangement as claimed in Claim 8, characterized in that
- the means (28, 44) for generating the varying control signal include means for changing the output voltage of the second power supply source (16) at different instants within the time span of one passivation pulse;
 - the means (18, 30, 26, 28) for measuring and storing are adapted to store
 - 20 resistance information values which are representative of the instantaneous resistance of the gap (5) at the different instants within the passivation pulse and to store corresponding control signal values of the control signal at the different instants;
 - means (28) for calculating are adapted to calculate individual maximum values from the resistance information values of corresponding instants within
 - 25 successive passivation pulses and to generate a control signal having an instantaneous value which at the different instants is equal to the control signal values which correspond to the individual maximum values.
10. An arrangement as claimed in Claim 9, characterized in that the
- 30 arrangement further includes means (8, 10) for changing the distance between the electrode (6) and the workpiece (2), which distance is smaller during the supply of the machining pulses than during the supply of the passivation pulses.



11. An arrangement as claimed in Claim 10, characterized in that the arrangement includes means (8, 10) for producing an oscillating movement between the workpiece (2) and the electrode (6), and means (22) for synchronizing the means (20, 24) for alternately connecting the first (14) and the second (16) power supply source
5 with the oscillating movement of the workpiece (2).

12. An electrical power supply source for use in a method of electrochemically machining an electrically conductive workpiece (2) by applying electrical machining pulses between the workpiece (2) and an electrically conductive
10 electrode (6) while electrolyte is supplied between the workpiece (2) and the electrode (6), characterized in that the electrical power supply source comprises:

- a first electric power supply source (14), which is electrically connectable to the electrode (6) and the workpiece (2) to supply machining pulses to the workpiece (2) and the electrode (6);
- 15 - a second electric power supply source (16) of the same polarity as the first power supply source (14) and having an output voltage which is controllable by means of a control signal (CSU), which second power supply source (16) is electrically connectable to the electrode (6) and the workpiece (2) to supply passivation pulses to the workpiece (2) and the electrode (6);
- 20 - means (20, 24) for alternately connecting the first and the second power supply source to the workpiece (2) and the electrode (6);
- means (28, 44) for generating a varying control signal (CSU) for changing the output voltage of the second power supply source (16) during successive passivation pulses;
- 25 - means (18, 26, 28, 30) for measuring during the successive passivation pulses the electrical resistance of the gap (5) between the workpiece (2) and the electrode (6) at an instant during the passivation pulses and for storing resistance information values which are representative of the resistance of the gap (5) at said instant and for storing corresponding control signal values of the control signal at said
30 instant; and
- means (28) for calculating a maximum value from the resistance information values, and means (28, 44) for maintaining the control signal (CSU) for the



second power supply source (16) at the control signal value which corresponds to the maximum value.

13. An electrical power supply as claimed in Claim 12, characterized in that
- 5 - the means (28, 44) for generating the varying control signal include means for changing the output voltage of the second power supply source (16) at different instants within the time span of one passivation pulse;
- the means (18, 30, 26, 28) for measuring and storing are adapted to store resistance information values which are representative of the instantaneous resistance of
- 10 the gap (5) at the different instants within the passivation pulse and to store corresponding control signal values of the control signal at the different instants;
- means (28) for calculating are adapted to calculate individual maximum values from the resistance information values of corresponding instants within successive passivation pulses and to generate a control signal having an instantaneous
- 15 value which at the different instants is equal to the control signal values which correspond to the individual maximum values.

