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TABLE-TOP ELID PROCESSING APPARATUS

BACKGROUND OF THE INVENTION

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Technical field of the invention

The present invention relates to a table-top ELID processing apparatus for efficiently and accurately grinding a small workpiece and processing it to a mirror
10 surface.

Prior art

Table-top lathes, table-top milling machines, etc. are widely being used in homes and laboratories for
15 machining small workpieces. These table-top machining apparatuses process easily machinable materials such as copper, aluminum, wood, and plastics. However, for tough materials, e.g., fine ceramics, optical glasses, semiconductor single crystals, and other hard brittle
20 materials and cemented carbides, a general-purposed large machine must conventionally be used, even if the workpiece is small. Therefore, it has been demanded to develop a table-top machining apparatus that can be used like a table-top lathe etc. and can process even a hard brittle
25 material and cemented carbide with high accuracy and efficiency.

However, there were the following problems in developing the aforementioned table-top machining apparatus.

(1) A hard brittle material and cemented carbide may most appropriately be machined by grinding using a grindstone. But, the resistance of a material to grinding is greater than to normal cutting, and the resistance of the linear guide that guides a workpiece is also normally larger. Consequently, the motor etc. required for machining becomes larger and more powerful to drive the equipment. Normally, the above-mentioned processing machine is driven by a three-phase power supply higher than 200V AC. As a result, even if the equipment is made smaller for household or laboratory use, it is difficult to modify the equipment to a compact, low-power system that can be driven by a low voltage (single-phase 100V) and can be used on a table-top.

(2) A grindstone used for grinding normally becomes loaded with cut chips and debris within a short time, so it cannot be operated at a high efficiency. Although the inventors of the present invention, et al. are developing an electrolytic in-process dressing grinding (refer to ELID grinding), a predetermined pulse power supply is indispensable to utilize the grinding system. However, this pulse power supply must provide a rather high voltage (for instance, 60V to 150V) even for a small workpiece, together with a pulse current of about 1A to 3A, therefore, the power supply becomes large. In addition, an ELID grinding system should unavoidably use a conductive processing fluid whose viscosity may often increase processing resistance, so power consumption becomes still

greater. In addition, if this processing fluid enter into the linear guide, the life of the guide becomes shorter and its sliding resistance fluctuates. If a seal etc. is installed to prevent the fluid from ingress, processing resistance increases, and the life of the seal is reduced by the processing fluid.

SUMMARY OF THE INVENTION

Example embodiments have been accomplished to solve these problems. That is, for example, to provide a table-top ELID processing apparatus that can process even a hard brittle material and cemented carbide, whereby both driving and pulse power supplies can be compact, and the equipment can be operated at a low voltage (single-phase 100V) and can be so small that it can be used on the top of a table.

In accordance with a first aspect of the present invention, there is provided a table-top ELID processing apparatus comprising a conductive grindstone for processing a workpiece, an electrode installed with a predetermined spacing from a working surface of the conductive grindstone, a processing fluid supplying device for supplying a conductive processing fluid between the grindstone and the electrode, and a power supply for applying a voltage between the grindstone and the electrode, wherein the power supply comprises a DC power supply and an RC circuit which generates pulse-like voltages, and can be applied to both electrolytic dressing and discharge truing, the RC circuit comprising a variable resistance R connected between input and output terminals at the positive side and a variable capacitor C connected between the positive and negative lines of output terminals; and the apparatus also

comprises a work driving device for driving a table with a workpiece mounted thereon in horizontally orthogonal directions X and Y, a tool-driving device which while rotating the conductive grindstone around the vertical shaft Z thereof, drives the grindstone in the vertical direction thereof in relation to the workpiece, and a numeric control device for numerically controlling the work driving device and the tool-driving device.

In the example embodiments,, because the power supply is comprised with a DC power supply and an RC circuit which generate pulse-like voltages and can supply power for both electrolytic dressing and discharge truing, the power supply may be used for both ELID processing and discharge truing, whenever required. In addition, because of the simplicity of the circuit, the power supply may be made considerably smaller than a conventional pulse power supply, which generates an identical current pulse. Furthermore, a simple numeric control system may be achieved and a workpiece may be processed to a high accuracy by installing work driving device and tool-driving device, and controlling these devices using a numeric control device (for instance, a personal computer).

Hence, an electrolytic in-process dressing grinding (ELID grinding) method may be configured using a small, simple power supply, whereby the grindstone is dressed to greatly reduce cutting resistance, the necessary power can be decreased, and a hard brittle material and cemented carbide can be processed at a high efficiency and a high accuracy.

According to an example embodiment, the aforementioned work driving device is guided by a hard porous carbon material whose dynamic friction coefficient and static friction coefficient are substantially the same no matter whether it is unlubricated or it is in water. Using

the above-mentioned hard porous carbon material (for example, RB ceramics) as a guide at a sliding portion, even if processing fluid enters the linear guide, the coefficient of friction does not alter. Therefore, positioning accuracy which is numerically controlled, can be maintained high. Because the coefficient of friction does not vary and the carbon material is not attacked by the processing fluid, no seal is required, and the sliding resistance can be kept at a low value.

Other objects and advantages of the present invention are revealed by the following paragraphs referring to the attached drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a general perspective view of a table-top ELID processing apparatus according to the present invention.

Fig. 2 shows a circuit of the power supply for both electrolytic dressing and discharge truing.

Fig. 3 is a load characteristic diagram of the power supply in Fig. 2.

5 Figs. 4A to 4C show examples of pulse-like voltages with the power supply in Fig. 2.

Fig. 5 is a structural view of a guide portion of the work driving device.

10 Fig. 6 shows the relationship between baking temperatures and friction coefficients of a hard porous carbon material.

DESCRIPTION OF PREFERRED EMBODIMENTS

15 Embodiments of the present invention are described below referring to the drawings. In each figure, common portions are identically numbered, and no duplicate description is given here.

20 Fig. 1 is a general perspective view of a table-top ELID processing apparatus according to the present invention. In Fig. 1, table-top ELID processing apparatus 10 according to the present invention is provided with a conductive grindstone 2, an electrode 4, a processing fluid supplying device 6, and a power supply 8 which applies a
25 voltage between grindstone 2 and electrode 4. In addition, table-top ELID processing apparatus 10 is also provided with a work driving device 12 which drives a table 11 with a workpiece 1 mounted thereon in horizontally orthogonal

directions X and Y, a tool-driving device 14 which drives
conductive grindstone 2 in the vertical direction, while
rotating the grindstone around vertical shaft Z with
respect to workpiece 1, and a numeric control device 16
5 which numerically controls work driving device 12 and tool-
driving device 14.

In this embodiment, workpiece 1 is fixed directly on
top of table 11, whose upper surface is to be processed.
However, the present invention is not limited only to this
10 configuration. For example, another table for fixing
workpiece 1 on table 11 is installed, and workpiece 1 can
be rotated around an axis (X, Y, Z, etc.) using this table.

Conductive grindstone 2 is a cylindrical or cup
grindstone which rotates around the vertical Z shaft and
15 whose lower surface processes workpiece 1. Conductive
grindstone 2 may also preferably be a metal bond grindstone
using fine diamond grains. However, conductive grindstone
2 is not limited only to these examples. Instead, various
types suitable for ELID processing can also be used freely.

20 Electrode 4 can be installed with a predetermined
spacing from a surface of the workpiece of conductive
grindstone 2. This electrode 4 is preferably
electrolytically dressed during ELID processing, as
installed away from the working surface of conductive
25 grindstone 2. The working surface of conductive grindstone
2 can also be electrolytically dressed or discharge trued
by installing the electrode on a table separate from the
workpiece.

Processing fluid supplying device 6 supplies a
conductive processing fluid between grindstone 2 and
electrode 4. In Fig. 1, numeral 13 represents a tank of
processing fluid in which processing fluid is stored and
5 fed between the working surface of grindstone 2 and
electrode 4 using a pump (not illustrated). The processing
fluid should preferably be an electrolyte suitable for ELID
processing. The electric conductivity of the fluid may
also be adjusted according to discharge truing intended.
10 Moreover, a surfactant etc. may preferably be added to
reduce surface tension while reducing processing resistance
due to the processing fluid.

Work driving device 12, in this embodiment, is
comprised with a Y-axis table 12a installed on top of the
15 processing fluid tank 13 and an X-axis table 12b installed
thereon. Aforementioned table 11 is fixed on the upper
surface of the X-axis table 12b. The Y-axis table 12a and
the X-axis table 12b are provided with respective linear
guides, driving motors, and position detecting scales, and
20 can be precisely positioned by numeric control.

Numeral 15 in Fig. 1 denotes a cover installed to
enclose the Y-axis table 12b to prevent the processing
fluid from spraying out during processing, although only
the upper front portion 15a is open. Open portion 15a can
25 be closed with a transparent cover so that one can access
the equipment and observe processing conditions.

The tool driving device 14 is configured with a
column 14a and a spindle unit 14b provided thereon.

Spindle unit 14a houses a spindle, which holds and rotates grindstone 2, a motor to drive the spindle, and a Z-axis table for driving the grindstone 2 in the vertical direction Z. The Z-axis table can also be positioned
5 precisely by a numeric control system, because linear guide, driving motor, and position-detecting scale are equipped in the unit, like Y-axis table 12a and X-axis table 12b.

Numeric control device 16 is a personal computer provided with a parallel and/or serial interface (for
10 instance, RS-232C), and drives Y-axis table 12a, X-axis table 12b and the Z-axis table by NC control. However, in place of the personal computer, a custom chip and a micro-servo controller can also be incorporated to make up a small, simple NC control device.

15 Fig. 2 is a circuit diagram of the power supply for both electrolytic dressing and discharge truing. As shown in Fig. 2, power supply 8 applied to table-top ELID processing apparatus 10 according to the present invention has a DC power supply circuit, not illustrated, and an RC
20 circuit connected thereto, and can generate pulse-like voltages. In detail, as shown in Fig. 2, this circuit is provided with a variable resistance R connected between input and output terminals 9a, 9b at the positive side, and a variable capacitor C connected between positive and
25 negative lines of output terminals 9b.

According to the embodiment of the present invention, the DC power supply circuit provides output voltages at DC 30V to 150V using a low voltage power supply of AC single-

phase 100V. In addition, variable resistance R can be varied stepwise or continuous in a range of 50Ω to 500Ω , and variable capacitor C can be changed without or with steps in the $0.01\mu F$ to $10\mu F$ range.

5 Using this configuration, predetermined pulse voltages can be applied between grindstone 2 and electrode 4 by charging capacitor C using a simple circuit when output terminals 9b are open, and discharging capacitor C when the resistance between terminals 9a and 9b decreases.

10 Fig. 3 is a load characteristic diagram of this power supply. As shown in Fig. 3, any voltage in the range with a maximum voltage of about 150V and a maximum current of 1.2A can be generated by adjusting variable resistance R and variable capacitor C .

15 Figs. 4A, 4B, and 4C show examples of pulse-like voltages generated by the power supply in Fig. 2. Figs. 4A, 4B, and 4C relate to $R = 50\Omega$, $R = 100\Omega$, and $R = 200\Omega$, respectively, using capacitor C with $1\mu F$ in all cases.

From these figures, one skilled in the state of the art can understand that pulse-like voltages can be generated by adjusting variable resistance R and variable capacitor C , although the voltages are not complete pulses. In addition, in any of the cases of $R = 50\Omega$, 100Ω , and 200Ω , a

20 capacitance of $C = 10\mu F$ resulted in a pulse drooping at wave front and rear, however, as the capacitance was made small, pulses approached complete ones, and with $C = 0.1$

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and $0.01 \mu\text{F}$, pulses were much better than those in Figs. 4A, 4B, and 4C, according to an experiment carried out. Even when $R = 500\Omega$, a capacitor with $C = 0.01\mu\text{F}$ rendered similar pulse waves to those in Fig. 4A, 4B, and 4C.

5 Referring to the results of Figs. 3, 4A, 4B, and 4C, it was confirmed that the above-mentioned power supply can be applied to both electrolytic dressing and discharge
10 truing whenever required. In power supply 8, output voltage, variable resistance, variable capacitor, etc. can be freely adjusted by controller 8a shown in Fig. 1.

Fig.5 shows the structure of a guide unit of the work driving device. In Fig.5, numeral 17 represents a guide rail at the fixed side, 18 represents a guide block at the driven side, and 19 represents sliding materials located
15 between both sides. These sliding materials 19 should preferably be made of a hard porous carbon material whose dynamic and static friction coefficients without lubricating are substantially the same as those in water. These hard porous carbon materials include RB ceramics
20 manufactured by mixing a phenol resin into degreasing rice bran, forming and processing the mix, and carbonizing it in a nitrogen gas atmosphere.

Fig.6 shows the relationship between baking temperatures and friction coefficients of the
25 aforementioned hard porous carbon material. In Fig.6, a baking temperature of 500°C or more drastically reduces the coefficient of friction to an essentially constant value of

0.13 to 0.17. This hard porous carbon material gives, even in water, a low coefficient of friction that is substantially identical to that in air. In addition, even in a wide pressure range, static and dynamic friction coefficients of the material are approximately the same. Consequently, when such a hard porous carbon material as that described above (for instance, RB ceramics) is used as a guide at the sliding unit, even if processing fluid intrudes to the linear guide, friction coefficients do not fluctuate, therefore, positioning accuracy can be maintained high by numeric control. Because friction coefficients do not vary and the carbon material is not attacked by a processing fluid, no seal is required, so sliding resistance can be kept low.

According to the aforementioned configuration of the present invention, power supply 8 is comprised with the DC power supply and the RC circuit, which generate pulse-like voltages; and can be applied to both electrolytic dressing and discharge truing. Therefore, using this power supply, both ELID processing and discharge truing can be actuated when required. In addition, because the circuit is simple, the size thereof can be made much smaller than conventional pulse power supply circuits, provided the same pulse current is generated. In addition, Work driving device 12 and tool-driving device 14 are installed and controlled by numeric control device 16 (personal computer), so a simple numeric control system can be achieved and high-precision processing is enabled.

As a result, electrolytic in-process dressing grinding (ELID grinding) can be established using a small, simple power supply 8, thus cutting resistance can be greatly reduced by dressing the grindstone, while also decreasing power consumption. Therefore, a hard brittle material and cemented carbide can be processed highly efficiently at a high accuracy.

As described above, the table-top ELID processing apparatus according to the present invention can process a hard brittle material and cemented carbide at a high accuracy, and both power supplies for driving power and pulse generation can be made compact. Therefore, the apparatus can be operated with small power at a low voltage (single-phase 100V), and can be small enough to be put on a desk, which are preferred advantages.

Although the present invention has been described using several preferred embodiments, it should be understood that the scope of rights covered by the present invention is not limited only to these embodiments. Conversely, the scope of rights of the present invention includes all amendments, corrections, and equivalent entities belonging to the scope of the attached claims.

Claims:

1. A table-top ELID processing apparatus comprising a conductive grindstone for processing a workpiece, an electrode installed with a predetermined spacing from the working surface of the conductive grindstone, a processing fluid supplying device for supplying a conductive processing fluid between the grindstone and the electrode, and a power supply for applying a voltage between the grindstone and the electrode, wherein

the power supply comprises a DC power supply and an RC circuit, which generates pulse-like voltages, and can be applied to both electrolytic dressing and discharge truing, the RC circuit comprising a variable resistance R connected between input and output terminals at the positive side and a variable capacitor C connected between the positive and negative lines of output terminals; and

the apparatus also comprises a work driving device for driving a table with a workpiece mounted thereon in horizontally orthogonal directions X and Y, a tool-driving device, which while rotating the conductive grindstone around the vertical shaft Z thereof, drives the grindstone in the vertical direction thereof in relation to the workpiece, and a numeric control device for numerically controlling the Work driving device and the tool-driving device.

2. The table-top ELID processing apparatus specified in claim 1, wherein the work driving device is guided by a hard porous carbon material whose dynamic coefficients and static coefficients of friction, without lubricating and in water, are substantially the same.