

Description

The invention relates to a diffuser for supplying conditioned air to a space and including a plurality of discharges, pivotable means movable by thermally responsive actuator means about a fixed pivot between a first position blocking one of said discharges and a second position blocking another of said discharges, with a third discharge always remaining open, said actuator means comprising an actuator support means, a phase transformation means fixed to said support means, return spring means having first and second ends and providing a return bias to said phase transformation means, and link means having first and second ends, said first end of said link means being connected to said phase transformation means, said link means further being connected to said pivotable means, whereby when said phase transformation means is below a phase transformation temperature said return spring means provides a bias for positioning said pivotable means in one of said first and second positions, and when said phase transformation means is above a phase transformation temperature said pivotable means is moved against the bias of said return spring means into the other of said first and second positions. A diffuser of this type is disclosed in EP-A-0,165,200.

For selectively distributing either warm or cool air, it is common practice to use a diffuser of the above type having different discharges for the warm and cool air. In perimeter zones in particular, it is desirable to have heat discharged towards the outside wall while cool air is directed into the space to cool the occupants. Thermoactuators, which are thermostatic devices containing a material which undergoes a reversible phase change with an associated expansion/contraction, are often used to achieve changeover. A typical phase changing material would be a wax-like material which is solid at the supply temperature of the cool air and is liquid at the supply temperature of the warm air. The expansion of the phase changing material in going from the solid to the liquid state provides the mechanical power to achieve changeover, and reset by spring bias upon a reverse phase change.

In EP-A-0,165,200 referred to a thermally responsive ceiling diffuser is described having a thermally responsive actuator for controlling the air distribution depending upon whether it is distributing warm or cool air. The diffuser provides a two-way discharge, as is desirable for the cooling function, and a one-way discharge having the same total discharge area located so as to direct all of the heating air towards the outside wall. This is achieved by providing a diffuser having two discharges directed toward the outside wall and one directed towards the interior of the conditioned

space. One of the two discharges directed toward the outside wall is always open while one of the other two discharges is open and the other closed depending upon the character of the air being discharged. Since the two discharges subject to being opened and closed face in opposite directions and are of equal discharge area, the result is a two-way discharge for cooling and a one-way discharge for heating having the same discharge area. The one-way blow towards the outside wall on heating is the most effective in maintaining room comfort while an equal heating and cooling discharge area is required for heating with low temperature air such as plenum air. While the heating and cooling air volumes are not conventionally the same, the use of low temperature air for heating in this manner with a higher heating volume has been found to provide favorable room comfort and lower heat energy cost. Changeover from one discharge pattern to the other is achieved by converting linear forces produced due to a liquid solid state phase change actuator into rotary movement of a swing baffle through a linkage connecting the actuator and the baffle.

Reference is also made to US-A-4,497,241 wherein a shape memory alloy helical tension or compression spring is used to angularly position a louver controlling the direction of the air flowing through a single discharge. A bias spring acts against the louver to pivot it in one direction and the shape memory alloy spring acts against the force applied by the bias spring to the louver.

The object of the invention is to provide a diffuser of the recited type having improved means to achieve changeover between the first and second positions of the pivotable means.

According to the invention, to achieve this the diffuser is characterized in that the phase transformation means comprises a first helical torsion spring of shape memory alloy disposed in said discharge which always remains open, said first helical torsion spring having first and second ends, said first end being fixedly connected to said one end of said link means and said second end being fixedly secured to a first attachment portion of said actuator support means, that said link means has a plurality of legs connected by bends, with at least one bend defining an acute angle, the second end of said link means being connected to said pivotable means, that said return spring means is a tension spring means, one end of said tension spring means being connected to said link means at said at least one bend defining an acute angle and the other end of said tension spring means being fixedly connected to a second attachment portion of said actuator support means, said first and second ends of the first helical torsion spring extending in a generally parallel direction when the

shape memory alloy is below the crystalline phase transformation temperature, and the first end of the first helical torsion spring moving away from the fixedly secured second end thereof when the shape memory alloy is above the crystalline phase transformation temperature.

Accordingly, torsional forces at one location (helical torsion spring) are converted, through a linkage, into rotary motion at a second location (pivotal means) separated from the first location.

For a fuller understanding of the present invention, reference should now be made to the following detailed description thereof taken in conjunction with the accompanying drawings, wherein:

Figure 1 is a sectional view of an air terminal employing the improved thermally responsive actuator;

Figure 2 is a sectional view of a diffuser employing a first embodiment of the thermally responsive actuator;

Figure 3 is a perspective view of the thermal actuator of Figure 2;

Figure 4 is a sectional view of a diffuser employing a second embodiment of the thermally responsive actuator;

Figure 5 is a top view of the thermal actuator of Figure 4; and

Figure 6 is a perspective view of the thermal actuator of Figure 4.

In figure 1, the numeral 10 generally designates an air terminal which is mounted in ceiling 100 and receives conditioned air via duct 12. The conditioned air supplied via duct 12 is delivered to plenum 14 which contains the actuator structure generally designated 40 and which is in fluid communication with the diffuser assembly 20. The diffuser assembly 20 includes a swing baffle or director 22 and three horizontal discharges 26, 27 and 28, respectively. The director 22 is illustrated in a position blocking discharge 27 whereby the conditioned air flows from discharges 26 and 28 which are in opposite directions. Director 22 is shown in phantom blocking discharge 26 whereby the conditioned air flows from discharges 27 and 28 which are in the same directions. The reason that different distribution patterns are desirable for heating and cooling is that the heating load is always located at the outside wall and the cooling load is produced both at the outside wall and in the exterior spaces by the occupants, light and machinery which are supplemental heat sources in the heating mode but additional loads in the cooling mode. Therefore, in the heating mode it is only necessary to overcome the external heating load and conditioned air is only directed towards the outside wall. In the cooling mode, however, in addition to directing the conditioned air towards the outside wall to overcome the external cooling load,

it is also desirable to direct conditioned air inwardly to overcome the cooling load supplied by the occupants, machinery and lights.

Referring now to Figures 2 and 3, the swing baffle or director 22 has a vertical arm 23 and a horizontal arm 24 which serve as valves. The horizontal arm 24 is connected to the actuator structure 40 by U-clip 42. Specifically, U-clip 42 pivotably connects horizontal arm 24 to link 44. Link 44 is made up of a plurality of straight portions, or legs, 44a-d which are connected by bends. Leg 44a is attached by crimping or any other suitable means to end 50a of helical torsion spring 50 which is made of a nickel-titanium or brass shape memory alloy and is inserted therein. Legs 44b and c form an acute angle defining a notch for receiving one end of return spring 60. Leg 44d is pivotably received in U-clip 42. Ends 50a and b of helical torsion spring 50 extend tangentially from the coils defining helical torsion spring 50 and are parallel to each other. End 50b is received in opening 54a and thereby secured to actuator support 54 which is secured to side diffuser 36 by rivets 55. Actuator support 54 can be of metal or molded plastic, and further includes opening 54b for receiving one end of spring 60.

Helical torsion spring 50 thus has one end 50b secured to side diffuser 36 while link 44 has end 44a secured to end 50a of spring 50 and end 44d pivotably secured to swing baffle 22 by U-clip 42. Tension spring 60 is secured in opening 54b of actuator support 54 and at the bend connecting legs 44b and c to normally position the members defining actuator 40 as illustrated in Figure 3. Helical torsion spring 50 will ordinarily be made from a shape memory alloy chosen to have a crystalline phase transformation in the 21-27°C (70°F to 80°F) range. At the transition temperature of the crystalline phase transformation, there is a sudden dimensional change and if ends 50a and b are considered to be two arms connected by a curved member, as in a Bourdon tube, the movement of the ends is towards a straightening when the temperature is raised to the transition temperature and towards a bending when the temperature is lowered. Compared to phase change materials such as waxes, the mass of the shape memory alloy to be heated/cooled is small, and there is a reduction in the amount of additional force produced after transition due to thermal expansion/contraction. The straightening movement of end 50a due to heating moves link 44 against the bias of spring 60 and movement of leg 44d of link 44 produces rotary motion of swing baffle or director 22 causing arm 23 to serve as a valve by blocking flow through discharge 26 while arm 24 is moved from blocking flow in discharge 27. The reverse happens upon cooling. However, this configuration permits the

usage of a thermally responsive actuator while minimizing the interference with the air flow.

As is best shown in Figure 2, discharge 26 is defined between side diffuser 30 and center diffuser 32. Discharge 27 is defined between center diffuser 32 and center divider diffuser 34 while discharge 28 is defined between center divider diffuser 34 and side diffuser 36. A diffuser spacer 37, grommet 38 and bolts 39a and b are located at each end of the diffuser assembly 20 and secure the side diffusers 30 and 36, center diffuser 32 and center divider diffuser 34 in place.

In operation, the conditioned air is always flowing over the helical torsion spring 50 of shape memory alloy which is located in discharge 28. Whenever the conditioned air is at a temperature less than that of the crystalline phase transformation, swing baffle or director 22 is in the solid line position of Figure 1 and the position of Figure 3 whereby arm 24 blocks discharge 27. In this position, cool air passes through discharge 28 towards the outside wall 102 and through discharge 26 towards the interior of the conditioned space where the occupants, machinery and lights provide a cooling load. If the conditioned air is switched over to heating, the conditioned air temperature will be above the temperature of the crystalline phase transformation of shape memory alloy of the spring 50. When spring 50 has been sufficiently heated, the crystalline phase transformation takes place which tends to straighten ends 50a and b with respect to each other against the bias of spring 60 and causes spring 50 to move to the solid line position of Figure 2. The movement of spring 50 results in movement of link 44 which in turn causes the rotation of swing baffle or director 22 from the solid line position of Figure 1 to the solid line position of Figure 2, whereby arm 23 blocks discharge 26. In this position, warm air passes through discharges 27 and 28 so that all of the warm air is directed towards the outer wall 102, the only heating load.

In the movement of the actuator 40 and swing baffle 22 from the Figure 1 to the Figure 2 position, it will be noted that a linkage is established with the two fixed points being the point of attachment of end 50b of spring 50 and the pivot point of swing baffle 22 with respect to center diffuser 32 with which it forms a ball and socket connection 33. Specifically, as clearly shown in Figure 2, spring 50 is caused to rotate about end 50b as a result of the rotational movement of leg 44b of link 44 due to the forces produced by the movement of end 50a against the bias of spring 60 as ends 50a and b move apart. Since link 44 is a single member, the movement of leg 44b is in concert with the movement of the other legs. Leg 44c is connected to swing baffle 22 by leg 44d which coacts with U-clip

42 to pivotably connect link 44 with respect to swing baffle 22. As motion of swing baffle 22 is limited to rotational movement about the fixedly located ball and socket connection 33, link 44 must also rotate about the pivot defined by U-clip 42. Thus link 44 is acted on at three movable points, its connection to end 50a, its connection to spring 60 and its connection to swing baffle 22. As a result of the forces acting on link 44 its movement is both linear and rotational since none of its points are fixed.

A second embodiment of the thermally responsive actuator is illustrated in Figures 4-6 where corresponding structure has been labeled 100 higher than the corresponding structure of Figures 1-3. The embodiment of Figures 4-6 differs from that of Figures 1-3 in the use of plural helical torsion springs of shape memory alloy, the guided movement of the link and the location and details of attachment of the link to the swing baffle. Actuator 140 includes shape memory alloy helical torsion springs 150 and 250 having ends 150a and b and 250a and b, respectively, extending tangentially from the coils defining springs 150 and 250, respectively; and parallel to each other. Ends 150b and 250b are received in openings 154a and 254a and are thereby secured to actuator support 154 which is secured to side diffuser 36 by rivets 55. Actuator support further includes opening 154b for receiving one end of tension spring 160 which provides a return bias. Link 144 is made up of a plurality of straight portions, or legs, 144a-e which are connected by bends. Leg 144a is attached by crimping or any other suitable means to end 150a of helical torsion spring 150 which is inserted therein. Legs 144b and c form an acute angle defining a notch for receiving the other end of tension spring 160. Leg 144d is loosely slidably received in a slot 134a so as to be generally limited to a reciprocating movement transverse to the flow of conditioned air while permitting all necessary movement. Slot 134a does permit a degree of lateral movement for which it serves as a pivot point and, if desired or necessary, may be defined by a low friction annular member such as a grommet received in an opening in center divider diffuser 34. Leg 144e is slidably received in slot 143 of slot headed plug 142 which is snap fitted or otherwise suitably secured to vertical arm 23 of swing baffle or director 22 at a point beneath horizontal arm 24. Second helical torsion spring 250 has an end 250a which is received in and attached to leg 244a of link 244 by crimping or any other suitable means. Link 244 includes horizontal leg 244a and vertical leg 244b which are connected by a bend. Leg 244b engages leg 144a on the side of leg 144a closest to side diffuser 36 so that springs 150 and 250 act cumulatively in opposition

to spring 160.

In operation of the embodiment of Figures 4-6, if springs 150 and 250 are heated such that they undergo a crystalline phase transformation movable ends 150a and 250a will tend to separate from fixed ends 150b and 250b, respectively. Movement of end 250b causes leg 244b to push against leg 144a which is also moving due to the movement of end 150b. Movement of ends 150b and 250b is opposed by spring 160 which cannot prevent movement due to the crystalline phase change.

Unlike the embodiment of Figures 1-3, link 144 is located in slot 134a. While slot 134a does permit the necessary degree of vertical and horizontal pivoting motion of link 144 there is primarily a reciprocating motion with respect to slot 134a. As a result, the tipping movement to which spring 50 of the Figure 1 device is subject, is restrained by slots 134a and 143. As link 144 reciprocates with respect to slot 134a, leg 144e coact with slot 143 to cause swing baffle or director 22 to move to the Figure 4 position responsive to the supplying of conditioned air. If cool air is supplied such that the springs 150 and 250 are cooled below the crystalline phase transformation then the movements of ends 150b and 250b in conjunction with spring 160 pivots baffle or director 22 so that discharge 27 is blocked.

From the foregoing it is clear that springs 50, 150, and 250 provide a torsional movement of their ends responsive to the reaching of the crystalline phase transformation point by heating or cooling. Springs 60 and 160 provide a return bias. In the embodiment of Figures 4-6 compounding of shape memory actuators is disclosed so as to permit the increasing of the forces. Where there are high flows, such as 11.3m³/min (400 cfm), or higher, the flow impinging upon legs 23 and 24 may provide a significant force requiring a stronger actuator. Also, the forces tending to return the shape memory alloy to its original shape are not necessarily equal to those tending to change its shape due to the different configuration at the time of each change, and the resultant differences in location and direction of the exerted forces.

Claims

1. Diffuser for supplying conditioned air to a space and including a plurality of discharges (26, 27, 28), pivotable means (22) movable by thermally responsive actuator means (14; 140) about a fixed pivot between a first position blocking one (26) of said discharges and a second position blocking another (27) of said discharges, with a third discharge (28) always remaining open, said actuator means (14; 140) comprising an actuator support means

(54;154), a phase transformation means fixed to said support means (54;154), return spring means (60;160) having first and second ends and providing a return bias to said phase transformation means, and link means (44;144) having first and second ends, said first end of said link means (44;144) being connected to said phase transformation means, said link means (44;144) further being connected to said pivotable means (22), whereby when said phase transformation means is below a phase transformation temperature said return spring means (60;160) provides a bias for positioning said pivotable means (22) in one of said first and second positions, and when said phase transformation means is above a phase transformation temperature said pivotable means (22) is moved against the bias of said return spring means (60;160) into the other of said first and second positions,

characterized in that the phase transformation means comprises a first helical torsion spring (50;150) of shape memory alloy disposed in said discharge (28) which always remains open, said first helical torsion spring (50;150) having first and second ends (50a,50b;150a,150b), said first end (50a;150a) being fixedly connected to said one end of said link means (44;144) and said second end (50b;150b) being fixedly secured to a first attachment portion (54a;154a) of said actuator support means (54;154), that said link means (44;144) has a plurality of legs (44a-44d; 144a-144e) connected by bends, with at least one bend defining an acute angle, the second end of said link means (44;144) being connected to said pivotable means (22), that said return spring means (60;160) is a tension spring means, one end of said tension spring means (60;160) being connected to said link means (44;144) at said at least one bend defining an acute angle and the other end of said tension spring means (60;160) being fixedly connected to a second attachment portion (54b;154b) of said actuator support means (54;154), said first and second ends (50a,50b;150a,150b) of the first helical torsion spring (50;150) extending in a generally parallel direction when the shape memory alloy is below the crystalline phase transformation temperature, and the first end (50a;150a) of the first helical torsion spring (50;150) moving away from the fixedly secured second end (50b;150b) thereof when the shape memory alloy is above the crystalline phase transformation temperature.

2. Diffuser according to claim 1, characterized in that said second end of said link means (44) is



to spring 160.

In operation of the embodiment of Figures 4-6, if springs 150 and 250 are heated such that they undergo a crystalline phase transformation movable ends 150a and 250a will tend to separate from fixed ends 150b and 250b, respectively. Movement of end 250b causes leg 244b to push against leg 144a which is also moving due to the movement of end 150b. Movement of ends 150b and 250b is opposed by spring 160 which cannot prevent movement due to the crystalline phase change.

Unlike the embodiment of Figures 1-3, link 144 is located in slot 134a. While slot 134a does permit the necessary degree of vertical and horizontal pivoting motion of link 144 there is primarily a reciprocating motion with respect to slot 134a. As a result, the tipping movement to which spring 50 of the Figure 1 device is subject, is restrained by slots 134a and 143. As link 144 reciprocates with respect to slot 134a, leg 144e coact with slot 143 to cause swing baffle or director 22 to move to the Figure 4 position responsive to the supplying of conditioned air. If cool air is supplied such that the springs 150 and 250 are cooled below the crystalline phase transformation then the movements of ends 150b and 250b in conjunction with spring 160 pivots baffle or director 22 so that discharge 27 is blocked.

From the foregoing it is clear that springs 50, 150, and 250 provide a torsional movement of their ends responsive to the reaching of the crystalline phase transformation point by heating or cooling. Springs 60 and 160 provide a return bias. In the embodiment of Figures 4-6 compounding of shape memory actuators is disclosed so as to permit the increasing of the forces. Where there are high flows, such as 11.3m³/min (400 cfm), or higher, the flow impinging upon legs 23 and 24 may provide a significant force requiring a stronger actuator. Also, the forces tending to return the shape memory alloy to its original shape are not necessarily equal to those tending to change its shape due to the different configuration at the time of each change, and the resultant differences in location and direction of the exerted forces.

Claims

1. Diffuser for supplying conditioned air to a space and including a plurality of discharges (26, 27, 28), pivotable means (22) movable by thermally responsive actuator means (14; 140) about a fixed pivot between a first position blocking one (26) of said discharges and a second position blocking another (27) of said discharges, with a third discharge (28) always remaining open, said actuator means (14; 140) comprising an actuator support means

(54;154), a phase transformation means fixed to said support means (54;154), return spring means (60;160) having first and second ends and providing a return bias to said phase transformation means, and link means (44;144) having first and second ends, said first end of said link means (44;144) being connected to said phase transformation means, said link means (44;144) further being connected to said pivotable means (22), whereby when said phase transformation means is below a phase transformation temperature said return spring means (60;160) provides a bias for positioning said pivotable means (22) in one of said first and second positions, and when said phase transformation means is above a phase transformation temperature said pivotable means (22) is moved against the bias of said return spring means (60;160) into the other of said first and second positions,

characterized in that the phase transformation means comprises a first helical torsion spring (50;150) of shape memory alloy disposed in said discharge (28) which always remains open, said first helical torsion spring (50;150) having first and second ends (50a,50b;150a,150b), said first end (50a;150a) being fixedly connected to said one end of said link means (44;144) and said second end (50b;150b) being fixedly secured to a first attachment portion (54a;154a) of said actuator support means (54;154), that said link means (44;144) has a plurality of legs (44a-44d; 144a-144e) connected by bends, with at least one bend defining an acute angle, the second end of said link means (44;144) being connected to said pivotable means (22), that said return spring means (60;160) is a tension spring means, one end of said tension spring means (60;160) being connected to said link means (44;144) at said at least one bend defining an acute angle and the other end of said tension spring means (60;160) being fixedly connected to a second attachment portion (54b;154b) of said actuator support means (54;154), said first and second ends (50a,50b;150a,150b) of the first helical torsion spring (50;150) extending in a generally parallel direction when the shape memory alloy is below the crystalline phase transformation temperature, and the first end (50a;150a) of the first helical torsion spring (50;150) moving away from the fixedly secured second end (50b;150b) thereof when the shape memory alloy is above the crystalline phase transformation temperature.

2. Diffuser according to claim 1, characterized in that said second end of said link means (44) is



connected to said pivotable means (22) by means (42) defining a pivotal connection.

3. Diffuser according to claim 1, characterized by including means (134a) for generally limiting motion of said link means (144) to reciprocating motion with respect to said pivotable means (22) and said second end of said link means (144) is connected to said pivotable means (22) by means defining a slidable connection (142). 5
4. Diffuser according to claim 1, characterized by said actuator support means (154) including a third attachment portion (254a) and by further including a second helical torsion spring (250) of shape memory alloy having first and second ends (250a,250b) with said first end (250a) of said second helical torsion spring (250) coaxing with said link means (144) cumulatively with said first helical torsion spring (150) and said second end (250b) of said second helical torsion spring (250) being fixedly secured to said third attachment portion (254a). 10 15 20 25

Revendications

1. Diffuseur pour fournir de l'air conditionné dans un espace, comportant une pluralité d'orifices de décharge (26,27,28.), un moyen pouvant pivoter (22), pouvant être déplacé par un actionneur thermosensible (14,140), autour d'un pivot fixe, entre une première position dans laquelle il obture l'un des orifices de décharge (26) et une seconde position dans laquelle il obture un autre (27) des orifices de décharge, un troisième orifice de décharge (20) demeurant toujours ouvert, l'actionneur (14,140) comprenant un support d'actionneur (54,154), un moyen à transformation de phase fixé au support (54,154), un ressort de rappel (60,160) ayant des première et seconde extrémités et produisant une sollicitation de rappel s'exerçant sur le moyen à transformation de phase, et un moyen de liaison (44,144) ayant des première et seconde extrémités, la première extrémité du moyen de liaison (44,144) étant reliée au moyen à transformation de phase, ce moyen de liaison (44,144) étant en outre relié au moyen pouvant pivoter (22), si bien que, lorsque le moyen à transformation de phase se trouve endessous d'une température de transformation de phase, le ressort de rappel (60,160) exerce une sollicitation pour placer le moyen pouvant pivoter (22) dans l'une des première et seconde positions, et que, lorsque le moyen à transformation de phase se trouve au-dessus d'une température de transformation 30 35 40 45 50 55

de phase, le moyen pouvant pivoter (22) est déplacé, à l'encontre de la sollicitation exercée par le ressort de rappel (60,160), vers et dans l'autre des première et seconde positions, caractérisé en ce que le moyen à transformation de phase est constitué par un premier ressort de torsion hélicoïdal (50,150) en alliage à mémoire de forme, disposé dans l'orifice de décharge (28) qui demeure toujours ouvert, ce premier ressort de torsion hélicoïdal (50,150) ayant des première et seconde extrémités (50a,50b;150a,150b), sa première extrémité (50a;150a) étant reliée fixement à une extrémité du moyen de liaison (44,144) tandis que sa seconde extrémité (50b;150b) est fixée fermement à une première portion d'attache (54a;154a) du support d'actionneur (54,154), en ce que le moyen de liaison (44,144) comporte une pluralité de branches (44a-44d;144a-144e) reliées par des coudes, au moins un coude définissant un angle aigu, la seconde extrémité du moyen de liaison (44,144) étant reliée au moyen pouvant pivoter (22), en ce que le ressort de rappel (60,160) est un ressort de traction, une extrémité de ce ressort de traction (60,160) étant reliée au moyen de liaison (44,144), à l'endroit du coude définissant un angle aigu tandis que l'autre extrémité du ressort de traction (60,160) est reliée fixement à une seconde portion d'attache (54b,154b) du support d'actionneur (54,154), les première et seconde extrémités (50a,50b;150a,150b) du premier ressort de torsion hélicoïdal (50,150) s'étendant dans une direction généralement parallèle lorsque l'alliage à mémoire de forme se trouve en dessous de la température de transformation de phase cristalline, et la première extrémité (50a,150a) du premier ressort de torsion hélicoïdal (50,150) s'écartant de sa seconde extrémité montée fixe (50b,150b), lorsque l'alliage à mémoire de forme se trouve au-dessus de la température de transformation de phase cristalline.

2. Diffuseur suivant la revendication 1 caractérisé en ce que la seconde extrémité du moyen de liaison (44) est reliée au moyen pouvant pivoter (22) par l'intermédiaire d'un moyen (42) définissant une liaison à pivotement.
3. Diffuseur suivant la revendication 1 caractérisé en ce qu'il comporte un moyen (134a) pour limiter, d'une manière générale, le mouvement du moyen de liaison (144) à un mouvement alternatif par rapport au moyen pouvant pivoter (22), et la seconde extrémité du moyen de liaison (144) est reliée au moyen pouvant pivoter (22) par l'intermédiaire d'un moyen définis-



sant une liaison à coulissement (142).

4. Diffuseur suivant la revendication 1 caractérisé en ce que le support d'actionneur (154) comporte une troisième portion d'attache (254a) et le diffuseur comprend en outre un second ressort de torsion hélicoïdal (250), en alliage à mémoire de forme, ayant des première et seconde extrémités (250a, 250b), la première extrémité (250a) du second ressort de torsion hélicoïdal (250) coopérant avec le moyen de liaison (144) d'une manière cumulative avec le premier ressort de torsion hélicoïdal (150), et la seconde extrémité (250b) du second ressort de torsion hélicoïdal (250) étant fixée à la troisième portion d'attache (254a).

Patentansprüche

1. Diffusor zum Abgeben von konditionierter Luft an einen Raum, mit mehreren Auslässen (26, 27, 28), mit einer schwenkbaren Einrichtung (22), die durch eine wärmeempfindliche Stellantriebseinrichtung (14; 140) um einen festen Drehpunkt zwischen einer ersten Position, in der sie einen (26) der Auslässe blockiert, und einer zweiten Position, in der sie einen anderen (27) Auslaß blockiert, bewegbar ist, wobei ein dritter Auslaß (28) immer offen bleibt, wobei die Stellantriebseinrichtung (14; 140) eine Stellantriebstrageinrichtung (54; 154), eine Phasenumwandlungseinrichtung, die an der Trageinrichtung (54; 154) befestigt ist, eine Rückholfedereinrichtung (60; 160), die ein erstes und ein zweites Ende hat und eine Rückholfedervorspannung auf die Phasenumwandlungseinrichtung ausübt, und ein Verbindungsglied (44; 144) aufweist, das ein erstes und ein zweites Ende hat, wobei das erste Ende der Verbindungsgliedeinrichtung (44; 144) mit der Phasenumwandlungseinrichtung verbunden ist, wobei das Verbindungsglied (44; 144) weiter mit der schwenkbaren Einrichtung (22) verbunden ist, wodurch, wenn die Phasenumwandlungseinrichtung unter einer Phasenumwandlungstemperatur ist, die Rückholfedereinrichtung (60; 160) eine Vorspannung zum Positionieren der schwenkbaren Einrichtung (22) in der ersten oder zweiten Position erzeugt, und, wenn die Phasenumwandlungseinrichtung über einer Phasenumwandlungstemperatur ist, die schwenkbare Einrichtung (22) gegen die Vorspannung der Rückholfedereinrichtung (60; 160) in die andere der beiden Positionen bewegt wird, dadurch gekennzeichnet, daß die Phasenumwandlungseinrichtung eine erste Schraubentorsionsfeder (50; 150) aus einer Formspeicherlegierung aufweist, die in dem Auslaß (28) angeordnet ist, der immer offen bleibt, wobei die erste Schraubentorsionsfeder (50; 150) ein erstes und ein zweites Ende (50a, 50b; 150a, 150b) hat, wobei das erste Ende (50a; 150a) mit dem einen Ende des Verbindungsglieds (44; 144) fest verbunden ist und das zweite Ende (50b; 150b) mit einem ersten Befestigungsteil (54a; 154a) der Stellantriebstrageinrichtung (54; 154) fest verbunden ist, daß das Verbindungsglied (44; 144) mehrere Schenkel (44a-44d; 144a-144e) hat, die durch Biegungen verbunden sind, wobei wenigstens eine Biegung einen spitzen Winkel bildet, wobei das zweite Ende des Verbindungsglieds (44; 144) mit der schwenkbaren Einrichtung (22) verbunden ist, daß die Rückholfedereinrichtung (60; 160) eine Zugfedereinrichtung ist, wobei ein Ende der Zugfedereinrichtung (60; 160) mit dem Verbindungsglied (44; 144) an der wenigstens einen Biegung, die einen spitzen Winkel bildet, verbunden ist und wobei das andere Ende der Zugfedereinrichtung (60; 160) mit einem zweiten Befestigungsteil (54b, 154b) der Stellantriebstrageinrichtung (54; 154) fest verbunden ist, wobei sich das erste und das zweite Ende (50a, 50b; 150a, 150b) der ersten Schraubentorsionsfeder (50; 150) in einer insgesamt parallelen Richtung erstrecken, wenn die Formspeicherlegierung unter der Kristallphasenumwandlungstemperatur ist, und wobei sich das erste Ende (50a; 150a) der ersten Schraubentorsionsfeder (50; 150) von dem fest verbundenen zweiten Ende (50b; 150b) derselben weg bewegt, wenn die Formspeicherlegierung über der Kristallphasenumwandlungstemperatur ist.
2. Diffusor nach Anspruch 1, dadurch gekennzeichnet, daß das zweite Ende des Verbindungsglieds (44) mit der schwenkbaren Einrichtung (22) mittels einer Drehverbindung (42) verbunden ist.
3. Diffusor nach Anspruch 1, dadurch gekennzeichnet, daß eine Einrichtung (134a) vorgesehen ist, um die Bewegung des Verbindungsglieds (144) insgesamt auf eine Hin- und Herbewegung in bezug auf die schwenkbare Einrichtung (22) zu begrenzen und daß das zweite Ende des Verbindungsglieds (144) mit der schwenkbaren Einrichtung (22) mittels einer Schiebeverbindung (142) verbunden ist.
4. Diffusor nach Anspruch 1, dadurch gekennzeichnet, daß die Stellantriebstrageinrichtung (154) einen dritten Befestigungsteil (254a) aufweist und daß eine zweite Schraubentorsions-



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feder (250) aus einer Formspeicherlegierung
vorgesehen ist, die ein erstes und ein zweites
Ende (250a, 250b) hat, wobei das erste Ende
(250a) der zweiten Schraubentorsionsfeder
(250) mit dem Verbindungsglied (144) kumula-
tiv mit der ersten Schraubentorsionsfeder (150)
zusammenwirkt und wobei das zweite Ende
(250b) der zweiten Schraubentorsionsfeder
(250) mit dem dritten Befestigungsteil (254a)
fest verbunden ist.

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