

TUNER FOR A RECEIVER

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1 The present invention relates to a tuner for a receiver and
concerns a termination arrangement for a mixer of the tuner.

5 An illustrative example of the invention comprises a doubly
balanced mixer to which reference is made hereinafter by way of example.

10 It is desirable to use a doubly-balanced mixer in a tele-
vision tuner because of its properties of inhibiting the input signals
from reaching the output and of inhibiting the generation of unwanted
frequency components. These properties are due to the balanced con-
figuration of a doubly-balanced mixer.

15 When receiving single ended input signals (i.e., input signals
which are referenced to signal ground), a balun for converting a
single ended signal to a double ended or differential input signal
is provided for each input signal. The output signal of the mixer is
usually taken from one of the two baluns. It is desirable to
20 terminate the output of the mixer with the characteristic
impedance of the balun in the frequency range of the
output signal of the mixer to prevent impedance mismatches
which would tend to produce distortion causing unwanted
frequency components. More specifically, since the output
signal of a mixer contains both sum and difference
25 frequency components, it is desirable to provide a
termination network which exhibits the characteristic
impedance of the balun for both the sum and difference
frequency components. Generally, this requires a
relatively complex and therefore expensive network.

30 It is herein recognized that for use in a tuner
of a television receiver, in which the sum and difference
frequency components are very far apart in frequency and
the local oscillator is tuned to provide a difference
frequency component which is the same for each channel,
i.e., always in the nominal IF frequency range, the
termination network for a doubly-balanced mixer can have a
very simple configuration. Specifically, in accordance
35 with the invention, the termination network simply
includes a capacitor and a resistance element having a
value substantially equal to the characteristic impedance
of the mixer connected in series between the output of the

mixer and signal ground for the sum frequency component and an inductor, capacitor and a resistance element having a value substantially equal to the characteristic impedance of the mixer connected in series between the output of the mixer and signal ground for the difference frequency component.

The invention will be described in greater detail with reference to the accompanying Drawing in which:

FIGURE 1 shows the schematic of a preferred embodiment of the present invention; and

FIGURES 1a and 1b show graphical representations of impedance characteristics useful in understanding the embodiment shown in FIGURE 1.

In FIGURE 1 there is shown a television tuner for tuning VHF broadcast and cable channels and UHF broadcast channels. By way of example, for use in the United States, the tuner is capable of tuning channels for which the RF picture carrier and local oscillator frequencies are specified in the following table.

<u>BAND</u>	<u>RF RANGE (MHz)</u>	<u>LO RANGE (MHz)</u>
B1	55.25 - 83.25	101-129
B2	91.25 - 151.25	137-197
B3	157.25 - 265.25	203-311
B4	271.25 - 463.25	317-509
B5	471.25 - 801.25	517-847

It will be appreciated that: band B1 corresponds to channels of the low VHF broadcast band (i.e., channels 2-6); band B2 corresponds to channels in a lower portion of the midband cable band; band B3 corresponds to channels in the remaining portion of the midband cable band, channels in the high VHF broadcast band (i.e., channels 7-13) and channels in the lower portion of the superband cable band; band B4 corresponds to channels in the remaining portion of the superband cable band and channels in the hyperband cable band; and band B5 corresponds to channels in the UHF broadcast band (i.e., channels 14-69).

The RF signals received at respective VHF and UHF inputs are coupled to an RF section 100 where the RF signal corresponding to the selected channel is selected and coupled to a mixer. A local oscillator signal having a frequency corresponding to the selected channel produced by a local oscillator section 300 is also coupled to mixer 200. Mixer 200 combines the selected RF signal and the local oscillator signal to produce an output signal having sum and difference frequency components. The output signal of mixer 200 is coupled to an IF section 400. The frequency of the local oscillator signal for each channel is controlled so that the difference frequency component is in the passband of IF section 400 which, for example, in the United States is approximately between 41 and 46 MHz and has sound and picture carrier frequencies at 41.25 MHz and 45.75 MHz, respectively. The conventional tuning control portion of the tuner for controlling the tuning of RF section 100 and local oscillator section 300 in the various bands is not shown.

Mixer 200 is a doubly-balanced mixer including a diode bridge 210 as the mixing element and baluns 220 and 230 for converting the single ended RF and local oscillator signals to respective pairs of differential signals for application to respective pairs of opposite corners of diode bridge 210. Each of baluns 220 and 230 includes two pairs of bifilar wires (221 and 222 and 231 and 232, respectively) wound around a ferrite core and connected in conventional fashion as shown to provide a $1/4$ impedance transformation between the unbalanced (single ended) input and the balanced (double ended) output. RF section 100 is AC coupled to balun 220 through a capacitor 240. Local oscillator section 300 is AC coupled to balun 230 through capacitor 250. The output signal of mixer 200 is coupled from balun 230 to IF section 400 through termination network 500, to be described in greater detail below.

Bias current for diodes 211a and 213a of diode bridge 210 is provided from a source of positive voltage +VB through a resistor 215a. The return for the bias

current is provided by balun 220. Bias current for diodes 211b and 213b of diode bridge 210 is provided through resistor 215b in corresponding fashion. It has been found desirable to bias the diodes in or near saturation for more linear mixer operation.

DC blocking capacitors 217a and 217b, which have negligible impedance in the frequency range of mixer 210, are coupled between diodes 211a and 213b and diodes 211b and 213a, respectively, to DC isolate the two bias current paths. More specifically, capacitor 217a prevents the bias current of diodes 211a and 213a from influencing the bias current of diodes 211b and 213b and also prevents the DC voltage developed at the junction of resistor 215b and diode 213b from being "shorted" to ground through the relatively low DC impedance of winding 222 of balun 220. Capacitor 217b serves in a corresponding manner to capacitor 217a. DC blocking capacitors 219a and 219b, also with negligible impedance in the frequency range of mixer 200, prevent the DC voltages at the junction of diodes 211a and 213a and at the junction of diodes 211b and 213b from being "shorted" to ground through the windings of balun 230.

For optimum operation of doubly-balanced mixer 200 to provide an output signal substantially free of unwanted frequency components, it is desirable that baluns 220 and 230 be terminated in impedances matching those presented by the balun at its inputs and outputs. Thus, if baluns 220 and 230 have a given characteristic impedance for the unbalanced configuration, e.g., 50 ohms, it is desirable that RF section 100 and local oscillator section 300 connected to the unbalanced inputs of baluns 220 and 230, respectively, exhibit output impedances substantially equal to the unbalanced characteristic impedance, e.g., 50 ohms, and that diode bridge 210 connected to the balanced output of baluns 220 and 230 exhibit an input impedance substantially equal to four times the unbalanced characteristic impedance, e.g., 200 ohms. The latter is achievable to a good approximation since a typical diode

bridge exhibits an input impedance of approximately 200 ohms. For the same reasons as stated above, since the output of mixer 200 is unbalanced, it is desirable that it be terminated in an impedance substantially equal to the unbalanced characteristic impedance of balun 230 throughout the frequency range of the output signal of mixer 200 for both the sum and difference frequency components. This is the purpose of termination network 500.

Termination network 500 includes a difference frequency termination portion 510, coupled between the output of mixer 200 and IF section 400 and a sum signal termination portion 520.

Since the difference frequency component of the output signal of mixer 200 is the same for each channel, i.e., it is always within the passband of IF section 400 due to the tuning of local oscillator section 300, difference frequency component termination portion 510 simply includes a series tuned circuit, consisting of an inductor 511 and a capacitor 513 resonant at a frequency substantially equal to the center frequency, e.g., 44 MHz, of the passband of IF section 400, and a resistor 515 having a resistance (R_0) substantially equal to the unbalanced characteristic impedance of balun 230 connected in series between the output of mixer 200 and signal ground. The input of IF section 400 is connected to the junction of the tuned circuit and resistor 515. This arrangement exhibits the impedance characteristic shown in FIGURE 1a. It is noted that resistor 515 may comprise the input impedance of IF section 400. The series tuned circuit not only establishes (together with resistor 515) the desired termination for the difference frequency component, but also prevents the sum and other unwanted frequency components from reaching IF section 400.

Since the lowest sum frequency component of the output signal of mixer 200 is approximately 155 MHz, i.e., the sum of the frequency of the lowest sideband component of the RF picture carrier and the frequency of the local

oscillator signal for channel 2, and that is more than 99 MHz from the highest sideband component of the IF picture carrier, sum frequency component termination portion 520 simply includes a capacitor 521 and a resistor 523 having
5 a resistance (R_0) substantially equal to the unbalanced characteristic impedance of balun 230 connected in series between the output of mixer 200 and signal ground.

Capacitor 521 is selected to isolate resistance 523 from difference frequency component termination portion 510 for
10 frequencies below the lowest sum frequency and to have insignificant impedance at frequencies above the lowest sum frequency so as to provide the impedance characteristic shown in FIGURE 1b.

It will be appreciated that modifications can be
15 made to the preferred embodiment. For example, the order of resistor 521 and capacitor 523 in sum frequency component termination portion 520 may be interchanged.

Furthermore, if the input impedance of IF section 400 is very high, the input of IF section 400 may be directly
20 coupled to the output of mixer 200 instead of the junction of the tuned circuit and resistor 515 of difference frequency component termination portion 510. In the latter case the order of the elements in difference frequency component termination portion 510 is not
25 important, however, the filtering provided by the tuned circuit in the configuration shown no longer exists.

Furthermore, if the use of a single resistive termination element is desired, resistor 523 may be eliminated and capacitor 521 may then be connected in parallel with the
30 series connection of inductor 511 and capacitor 513.

These and other modifications are contemplated to be within the scope of the present invention defined by the following claims.

1 Claims:

1. A tuner for a receiver comprising:
an input for receiving RF signals corresponding
5 to various channels;

RF means for selecting the RF signal
corresponding to a selected channel;

local oscillator means for generating a local
oscillator signal having a frequency corresponding to the
10 selected channel;

mixer means for combining said selected RF
signal and said local oscillator signal to produce an
output signal at an output having sum and difference
frequency components;

15 IF means having an input coupled to the output
of said mixer means and having a predetermined passband;

said local oscillator signal being controlled so
that said difference frequency component is within said
passband;

20 sum frequency component termination means
coupled to said output of said mixer means for terminating
said output of said mixer substantially in its
characteristic impedance including a capacitor and a
resistance element connected in series between said output
25 of said mixer and a point of reference potential, said
resistance element having a resistance value substantially
equal to that of said characteristic impedance of said
mixer, said capacitance having a value such that it has a
negligible impedance in the frequency range between the
30 highest frequency of said difference frequency component
and the lowest frequency of said sum frequency component;
and

35 difference frequency component termination means
for terminating said output of said mixer substantially in
its characteristic impedance including an inductor and a
capacitor and a resistance element coupled in series
between said output of said mixer and said point of
reference potential, said resistance element having a
resistance value substantially equal to that of said



characteristic impedance of said mixer, said inductor, capacitor and resistance element forming a tuned circuit having a resonance at a frequency within said passband of said IF means.

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2. The tuner recited in Claim 1, wherein:
said RF means, said local oscillator means and said IF means are adapted for tuning television signals.

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3. The tuner recited in Claim 1
said inductor and said capacitor of said difference frequency component terminating means are connected in series between said output of said mixer means and said input of said IF means.

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4. The tuner recited in Claim 1, 2 or 3 wherein:
said capacitor of said sum frequency component terminating means has a value such that it exhibits negligible impedance for frequencies above the lowest
20 frequency of said sum frequency component.

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5. The tuner recited in any preceding claim, wherein the said resistance element is common to both the sum and difference frequency component termination means.

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6. The tuner recited in Claim 3, wherein:
said resistance element of said difference frequency component terminating means comprises the input impedance of said IF means.

wherein:

7. The tuner recited in any preceding claim,
said mixer is a doubly-balanced mixer.

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8. A tuner for a receiver substantially as hereinbefore described with reference to Figure 1.



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