

Description

This invention relates generally to an improved electron gun system for television receiver cathode ray tubes that provides at least partial dynamic beam convergence substantially independently of any beam-focus-related adjustments in the main focusing field, and without introducing significant beam distortion. The invention has applicability to all types of color picture tubes and to all types of beam convergence systems including those dependent on the self-converging yoke and the uniform field yoke. With regard to gun systems, the invention has application to the many types used in home-entertainment television systems and computer display monitors. It also may be advantageously applied to systems that utilize an extended field main focus lens. The dynamically converging gun system according to the invention is particularly useful in improving the image resolution of flat-faced cathode ray tubes which utilize the tension foil mask, and in which degradation of screen corner resolution and edge resolution is particularly troublesome.

Desired picture tube performance characteristics of color television receiver systems include high resolution, picture brightness, and color purity. Resolution is largely a function of the size and symmetry of the beam spots projected by the electron guns of the picture tube. Beam spots are desirably small, round, and uniform in size at all points on the picture screen. Achievement of these ideals is difficult because of the many factors which exert an influence on the configuration of beam spots. As a result of such factors, a beam spot that is small and symmetrical at the center point of the picture imaging field can become enlarged and distorted at the periphery of the field, for reasons which will be described.

Key factors which influence beam spot size, uniformity and symmetry in picture tubes having three-beam electron guns include the following:

- (a) electron gun design;
- (b) cathode ray tube screen potential;
- (c) magnitude of beam current;
- (d) the "throw" distance from the electron gun to the screen; and,
- (e) the convergence system.

The ability of an electron gun to form small, symmetrical beam spots is a major factor in achieving optimum resolution. The task of designing guns with this capability has become more challenging because of reduction in diameter in the CRT neck. This physical constraint has been largely overcome by new, more effective gun designs, such as the gun having an extended field main focus lens described and claimed in U.S. Patent No. 3,995,194.

Convergence of the three beams of an in-line electron gun is provided in present-day television systems primarily by the self-converging yoke. This type of yoke is a hybrid having toroidal-type vertical deflection coils and saddle-type horizontal deflection coils. The yoke contains windings which produce an astigmatic field component that has the effect of maintaining the beams in convergence as they are swept across the screen. An example of a beam-deflecting yoke that provides for self-converging of multiple beams is disclosed in U.S. Patent No. 3,643,102 to Chiodi. This concept has found wide application in cathode ray display tubes intended for consumer products.

The converging effect is shown highly schematically in Figure 1, in which an electron gun 10 is depicted graphically as emitting three beams 12, 13 and 14 which diverge from a common plane 16 to impinge on a curved screen 18. The three beams are shown as being converged at the center point 20 of the screen 18. Due to the effect of the self-converging yoke, the three beams are also caused to be in convergence at the side of the screen 18, as indicated by point 22, even though the distance that beams must travel from the plane of deflection 16 to point 22 is greater than from the plane of deflection 16 to center point 20 of the screen.

The convergence achieved is not without cost, however, as the beam spots are subject to distortion in the peripheral areas of the screen, as will be shown with reference to Figure 3. The distortion is acceptable in tubes in which lower resolution is acceptable as the benefits and costs savings implicit in the self-converging yoke outweigh its liabilities.

However, when the screen is flat, as indicated by screen 24 in Figure 2, the conventional self-converging yoke is unable to maintain beam convergence, as indicated by the spread of the beam spots 28 at the sides 26 of screen 24. In addition to the spread, the spots 28 will be noted as being elongated. This elongation is due primarily to the self-converging feature of the yoke.

The astigmatic field component, while self-converging the beams, undesirably introduces an astigmatic deflection defocusing of the beams when the beams are deflected away from the screen center point.

This effect is indicated diagrammatically in Figure 3 by beam spots 34. The elongation of the beam spots at the peripheries of the faceplate, and the relative increase in spot size, is indicated in greater detail in the inset figure, Figure 3A. The beam spots 34 will be seen as comprising a bright core 34A, and

transverse to the core, a dim "halo," 34B. The center beam spot 36C is shown to illustrate the magnitude of the spot size increase and distortion at the screen corner. Attempts to focus such beams are largely ineffectual due to the astigmatic effect--focusing merely results in what appears to be a "rotation" of the spot in that the core becomes the halo and the halo becomes the core.

As has been noted, the effect is tolerable in conventional tubes where the screen is curved, as shown by Figure 1, and it is acceptably within the capability of the self-converging yoke to converge the beams without undue distortion. However, when the screen is flat, as indicated by Figure 2, the astigmatic effect of the self-converging yoke is no longer tolerable, especially in high-resolution cathode ray tubes. Any attempt to further modify the configuration of the self-converging yoke field to adapt it to a flat screen will inevitably increase distortion outside the limits of acceptability. The self-converging ability of the yoke was already stretched to its limit in its use with the curved screen before the advent of the flat tension mask tube.

Prior art structures for converging electron beams have relied upon a variety of techniques such as the use of magnetic influence within and/or without the tube envelope, and the use of electrostatically charged plates. Also, the prior art shows many examples of inducing beam divergence or convergence by inducing an asymmetry in an electrostatic field formed at the interface of the two spaced electrodes. An example of this approach is found in U.S. Patent No. 4,058,753, where there is disclosed a three-beam electron gun for color cathode ray tube having an extended field main focus lens. The focus lens means has for each beam at least three electrodes including a focus electrode for receiving a variable potential for electrically adjusting the focus of the beam. In succession down-beam, there are at least two associated electrodes having potentials thereon which form in the gaps between adjacent electrodes significant main focus field components. To adjust beam focus, the strength of a first of these components is controlled by adjustment of the voltage received by the focus electrode. The strength of the second of the field components is relatively less than that of the first component. Each of the lens means is characterized by having addressing faces of the associated electrodes which define the second field component being so structured and disposed as to cause the second field component to be asymmetrical and effective to significantly divert the beam from its path in convergence of the beams without any significant distortion of the beam and substantially independently of any beam-focusing adjustments of the first field component. Electrode structures defined for producing asymmetric field components include a gap angled forwardly and outwardly, a wedge-shaped gap, and radially offset apertures.

Beam convergence in delta guns can also be obtained by means of electromagnets positioned 120 degrees apart azimuthally around the tube neck near the beam-emission points of the guns. The fields of the electromagnets are designed to aid or oppose the fields of associated permanent magnet pole pieces used for positioning the beams during set up. The beams can be dynamically converged by the application of voltages to the electromagnets which are modulated at the scanning rates. An example of such convergence means is disclosed in U.S. Patent No. 3,379,923.

Dynamic convergence is obtained in the electron gun disclosed in U.S. Patent No. 3,448,316 by adjustment of field potentials at scanning rates. Three in-line electron beams generated by three cathodes cross over in the electrostatic field of a main lens. The center beam (green) follows a straight-line path, but the two outer red and blue beams exit the lens in divergent paths. The outer beams pass through convergence plates which lie parallel to the gun axis and are suspended from the end of the gun nearest the screen. The potential on two outer plates is adjustable to provide for static convergence of the red and blue beams at the aperture mask. The center beam is unaffected as the potential on two inner plates through which it passes is left unchanged. Dynamic convergence is attained by changing the convergence control voltage on the outer two plates at the horizontal scanning frequency. The waveform of the voltage is in the form of a parabola.

In U.S. Patent No. 4,520,292, von Hekken et al disclose means formed in the screen grid of an electron gun for urging the outer two beams of a three-beam electron gun into convergence with the center beam. The screen grid configuration includes a transversely disposed recessed portion having a substantially rectangular central portion and substantially triangular end parts. The total effect is to tilt the field lines within the recessed portion so that the outer beams converge.

Other representative disclosures having electrode structures that influence beam convergence includes:

U.S. Patent 3,952,224 to Evans

U.S. Patent 3,772,554 to Hughes

U.S. Patent 4,473,774 to Hosokoshi et al

U.S. Patent 4,513,222 to Chen.

As has been noted, convergence of the beams of a multiple-beam electron gun will vary as the beams arcuately scan the substantially planiform faceplate. Beam convergence may be achieved dynamically by slightly varying the relative angles of the beams while scanning. In dynamic convergence by circuit means,

signals to induce dynamic convergence may be derived from the horizontal and vertical circuits of the television receiver system or monitor to provide a dynamic convergence-correction signal having the characteristics of a parabola. The voltage of the convergence-correcting signal is zero at the center of the picture imaging field, and changes towards the sides of the screen to effect convergence. Such dynamic convergence signals may be applied to convergence coils located adjacent to the picture tube neck, or to convergence plates suspended from the end of the gun. Such a dynamic convergence circuit is disclosed by Nelson in U.S. Patent No. 2,834,911 in which parabolic convergence current waves are obtained by integration of pulse and saw tooth voltage waves in resistive and inductive reactive circuits, according to the teachings of Nelson.

U.S. Patent No. 2,957,106 discloses a unified focusing lens structure which creates focusing fields which each encompass all three beams. More specifically, each of the electron beams is directed into a different part of a common focusing field component. The system creates a number of focusing field components, but each one receives in a different part thereof, one of the three beams. Dynamic convergence is achieved in this reference by varying the electric field created between the focus electrode and the beam forming electrode. This is done because in that region of the gun, the beam has not yet been accelerated and is easy to control. Hence, variable convergence voltage in this reference is applied to the first electrode of the main focus lens in order that the field established between that electrode and the up beam electrode forming part of the beam forming means in the gun will vary the convergence of the beams. On the other hand, focus is adjusted in this reference by varying the voltage on the second electrode of the main focus lens. In other words, adjusting the field established between the second electrode of the main focus lens and the down beam accelerating electrode controls the focal length of the beams. Thus, in this reference, convergence is effected in the prefocus region up beam from the main focus lens while adjustment of the focus is accomplished at the down beam end of the electron gun.

It is generally desired to provide an electron gun system providing enhanced performance in color picture tubes while reducing component costs, and, more particularly, to provide an electron gun system that enhances resolution and color purity in color picture tubes, especially in peripheral areas of the screen.

The present invention therefore provides an electron gun system for a color cathode ray tube including beam-forming means including prefocus lens means and cathode means for developing an electron beam, main focus lens means for receiving said electron beam and forming a focused electron beam spot at the screen of the tube, said main focus lens means having, in a down beam direction, at least first focus electrode means for receiving a variable focus adjustment potential for controlling the focal distance of said beam, and second and third convergence-associated electrode means, and means for developing and applying to said electrode means potentials effective to form main focusing field components between said electrode means, said second and third electrode means being so structured and arranged as to cause to be formed therebetween a focusing field component which is asymmetrical and effective to significantly divert a passed beam from a straight-line path through a predetermined angle, characterized in that said system includes means for developing and applying a varying voltage to at least one of said second and third electrode means to cause the strength of said asymmetric field component, and thus said angle by which said beam is diverted, to vary in response to said varying voltage.

One of the specific features of the invention is to provide an electron gun system that makes possible dynamic convergence of the electron beams and that wholly or partially dispenses with the need of a self-converging yoke, and in which a uniform field yoke may be used in lieu of the self-converging yoke in many applications.

Another specific feature of the invention is to provide an electron gun system with particular capability for dynamically converging the beams on the screen of a color cathode ray tube having a planar shadow mask and a substantially flat faceplate.

Another feature of the invention is to provide an electron gun system that makes possible reduction in material and manufacturing costs through less stringent requirements for yoke installation, system set up, lighthouse optics, and mask grading.

Further features and advantages of the present invention may best be understood by reference to the following description of preferred embodiments of the invention taken in conjunction with the drawings, in the several figures of which like reference numerals identify like elements, and in which:

Figure 1 is a schematic representation of a desired effect of beam convergence on a curved screen due to the astigmatic convergence field components of the self-converging yoke;

Figure 2 depicts schematically the undesired effect of the self-converging yoke on beam in peripheral areas of the screen of a cathode ray tube having a flat faceplate;

Figure 3 is a schematic representation of undesired beam spot configuration in corner areas of the screen attributable to the self-converging yoke; Figure 3A is an enlarged view of the undesired beam

spot configuration in the screen periphery indicated by Figure 3;

Figure 4 is a view in perspective and partly in section of line screen cathode ray tube having a curved faceplate as used in a television or display system, with the system concept according to the invention represented schematically by the enclosing dashed line;

Figure 5 is an enlarged detail view of a section of the faceplate-shadow mask assembly of the tube shown by Figure 4;

Figure 6 is a view in perspective and partially in section of a cathode ray tube having a planar mask and associated faceplate, with the television or display system represented schematically by the enclosing dashed line, in which the dynamically converging gun system according to the invention can be utilized;

Figure 7 is a schematized top view of a dynamically converging gun system according to the invention, one that has a three-element extended field main focus lens; the system aspect is indicated by the enclosing dashed line; Figure 7A depicts another embodiment of the main focus lens shown by Figure 7; Figure 8 is a view similar to Figure 7, except that there is depicted an electron gun having a four-element extended field main focus lens; and

Figure 9 is schematic diagram of circuit means for forming a variable dynamic convergence signal.

The present invention can be embodied in electron guns of several different types both unitized and non-unitized. However, the illustrated embodiments according to the invention are in-line unitized guns as these types are in more general use in color cathode ray tubes.

In the context of the multi-beam color cathode ray tube, this invention may be employed to dynamically converge the off-axis beams all over the screen in common conjunction with the center beam. The convergence means according to the invention is applicable to both the conventional curved faceplate color television display tube depicted schematically in Figure 4 and to a tube having a planar shadow mask and faceplate, as shown in Figure 6.

Figure 4 depicts a television receiver or monitor system 38 indicated highly schematically by the enclosing dashed line, in which the dynamically converging electron gun system according to the invention may be advantageously employed. System 38 has a multi-color television line screen cathode ray picture tube 40 of the conventional type. Tube 40 comprises an evacuated envelope including a curved imaging faceplate 42 having deposits of multi-color emitting phosphors thereon, a funnel 44, a neck 46, and a base 48 through which protrude a plurality of electrical connectors 50 for making connection to components located within the sealed envelope of tube 40. An anode button 51 provides for the introduction of high voltage into the tube envelope for tube and gun operation. An electron gun 52, indicated by the bracket, is enclosed in neck 46. Electron gun 52 is represented as being an in-line gun generating three electron beams 53R, 53G and 53B which are focused by a main focus lens 54 of gun 52 onto a phosphor screen deposited on the inner surface of imaging faceplate 42; the boundaries of the screen 55 are indicated by dash line 56. (Please refer also to Figure 5 which comprises a detailed view of a section of the screen 55 of faceplate 42 of Figure 4).

Multi-color phosphor targets in the form of stripes of luminescing materials that emit light when excited by an electron beam comprise a red-light emitting phosphor stripe 58R, a green-light-emitting phosphor stripe 58G, and a blue-light-emitting phosphor stripe 58B, shown as being deposited on the screen 55 of faceplate 42. The targets are arranged in triads each associated with ones of the apertures 59 of adjacently located color selection shadow mask 62, the apertures being in registration with their respective targets. The targets are separated by intervening strips of a light-absorptive "black surround" 63. The phosphor targets comprising stripes 58R, 58G and 58B are excited to luminescence by electron beams 53R, 53G and 53B, respectively; the electron beams are caused to scan the screen 55 of faceplate 42 to selectively excite the aforesaid red-light-emitting and green-light-emitting targets through the color selection mask 62. Electron beams 53R, 53G and 53B are caused to scan screen 55 by the horizontal and vertical scansion circuit means coupled to yoke 61 which engirds tube 40 in the area of the junction of funnel 44 and neck 46.

The picture or display tube shown by Figure 4 is the type having a line screen. The invention can also be advantageously employed in the type of picture tube wherein the imaging screen is comprised of a pattern of triads of phosphor dots, the dots of each triad emitting red, green and blue light. As described infra, an adjacent color selection shadow mask has round apertures in registration with the phosphor targets. The electron gun could as well comprise a gun of delta configuration. As with the striped-screen tube, the phosphor dot targets are selectively excited by three scanning beams through the interceding aperture mask.

System 38 includes electrical circuits indicated schematically by the block 64, for supplying potentials for operation of the tube 40 and the included electron gun 52. The electrical circuits provide potentials which form electrical field components in the gaps between the adjacent electrodes as well as dynamically varying potentials for the horizontal and vertical scansion of the electron beams 53R, 53G and 53B; and for

luminance control. These circuits also provide potentials for operation of the dynamically converging gun system according to the invention, as will be described. The potentials are introduced into the tube envelope through ones of the conductive pins 50 that pass through the base 48 of tube 40.

A color cathode ray tube having a planar shadow mask and flat faceplate, to which the present invention is also applicable, is depicted in Figure 6. A television or monitor system 67 is depicted as having a cathode ray tube 68 with a flat glass faceplate 70. A shadow mask support frame 72 is represented as being secured to faceplate 70 for supporting a shadow mask 73. Faceplate 70 in turn is depicted as being joined to a rear envelope section, here shown as a funnel 74 which tapers down to a narrow neck 76.

Neck 76 is shown as enclosing an electron gun 78 which is indicated as projecting three electron beams 80R, 80G and 80B on the inner surface 71 of faceplate 70 on which is deposited the screen 82. Screen 82 has a pattern of three compositions of phosphors thereon which emit red, green and blue light when excited by the respective electron beams 80R, 80G and 80B. An anode button 84 provides for the entrance of a high electrical potential for tube operation. Relatively lower electrical potentials for operation of the electron gun 78 are conducted through the base 86 by means of a plurality of conductive pins 88. A yoke 90 provides for the scanning of the electron beams 80R, 80G and 80B across the screen 82 to selectively excite the phosphors deposited there through the medium of the shadow mask 73.

The three electron beams of tubes 40 and 68 shown respectively by Figures 4 and 6 are caused to scan a raster on the respective screens 55 and 82. The beams are modulated; that is, the beam current is varied to form the picture display. Beam scanning is a product of horizontal and vertical scanning circuits by which scanning signals are applied to the yoke of the tube, all as is well known in the art. The luminance signal by which the beams are modulated is developed by the television system luminance channel which produces the luminance signals by amplifying the luminance portion of the video signal. The luminance signals control image brightness by controlling the current of the respective electron beams.

The circuits which provide potentials for beam scanning, beam luminance, and which form field components in the gaps between adjacent electrodes, are indicated schematically by block 92. As has been noted, the potentials are applied to the gun components by way of ones of the conductive pins 88. The circuits also provide a variable dynamic convergence signal for operation of a dynamically converging gun system according to the invention, as will be described.

A dynamically converging electron gun system 94 according to the invention for use in a color cathode ray tube is depicted in Figure 7. The gun utilizes the principles of the extended field lens. The gun system 94 can find beneficial application in home entertainment television receiver systems and in monitors that utilize the high-resolution planar foil mask tube, both of which are described heretofore. The gun system 94 comprises basically an electron gun 96, and means for developing and applying the electrical potentials effective to form field components in the gaps between adjacent ones of the electrodes. The means are indicated schematically by the block 98. Also supplied are potentials necessary for tube operation such as filament voltages to energize the cathodes.

The potentials are conducted to the electrodes of gun 96 through selected ones of the electrically conductive pins 100 that pass in vacuum-tight seal through electrically insulative base 102 of tube 96. In this diagram, however, the potentials are indicated for illustrative purpose as being conducted from means 98 directly to the electrodes. The very high potential (e.g., 20-30kV) applied to the final, or "anode" electrode, is typically routed through the anode button in the tube envelope (see Ref. No. 84 in Figure 6) to the conductive coating on the inner surface of the funnel, from whence it is conducted to the final, anode electrode of the gun through a convergence cup 101 by way of a plurality of gun-centering springs 103 extending from the front of the gun 96.

In a preferred embodiment of the invention, electron gun 96 comprises means 104 including cathode means 106 for developing three in-line electron beams 108R, 108G and 108B. The means 104 for developing the beams is commonly termed the "prefocusing section," which includes in this embodiment of the invention, the cathode means 106, and electrode means 109, 110, 112 and 114. The three electron sources for the beams are generated by thermionic emission of the cathode means 106 as is well known in the art.

Three main focus lens means 116 receive the three in-line beams 108R, 108G and 108b for focusing and converging the beams at the screen of the tube. The main focus lens means 116 each has a like plurality of main focus electrode means spaced along a lens axis parallel to the other lens axes and parallel to a gun center axis 118. Center beam 118G is noted as being in alignment with the gun center axis 118. Please note that the term "main focus lens means" refers to the focus lens structure employed to focus all the beams. The term "main focus electrode means" refers to a discrete individual focus electrode for a single beam, or an allotted portion of a unitized electrode common to others of the beams. The main focus lens means depicted is an extended field lens, the principles of which are described and fully claimed in

U.S. Patent No. 3,995,194.

At least two of the lens axes, shown in Figure 7 as being two axes--lens axis 120 and lens axis 122--are "off-axis" with respect to the gun center axis 118. Each focus lens means is shown as including a focus electrode means 124, an anode electrode means 126, and at least one intermediate electrode means (shown as being one intermediate electrode means 128, in this example) situated between the focus electrode 124 and the anode electrode 126.

The mains 98 for developing the potentials which form field components in the gaps between adjacent electrodes, indicated by the block, provide for applying the following typical potentials to the electrodes. Circuit means 98A, indicated as supplying potentials to the prefocus section 104, may provide these typical potentials--

<u>Ref. No.</u>	<u>Voltage</u>
109	0
110	725
112	7,000
114	725

It is to be noted that the inventive concept does not depend solely on the use of the four-electrode quadrapotential prefocusing section 104 shown; other prefocusing sections known in the art can as well be used. The potential on focusing electrode 124, indicated as being supplied by circuit section 98B, typically may comprise a potential of about 7,000V. This potential is made, by way of example, manually variable about ± 400 volts e.g. for the set-up focusing of the three beams 108R, 108G and 108B at the center of the screen, a practice well-known in the art.

The potential applied to the anode electrode 126 is typically 25 kilovolts; this is a fixed potential as supplied by circuit section 98C. The potentials supplied by circuit section 98D to intermediate electrode 128 comprised both a static potential and according to the invention, a dynamic convergence signal 130, as will be described.

Addressing faces on at least two adjacent electrodes of the off-axis lens means, which are depicted as lying on axes 120 and 122, are so structured and arranged according to the invention as to cause the associated ones of the field components to be asymmetrical and effective to significantly converge the off-axis beams 108R and 108B from a straight-line path through a predetermined convergence angle. In the example a gun 96, the addressing faces of electrodes 124 and 128, and 126 and 128, are shown by way of example as being so structured and arranged as cause the field components therebetween to be asymmetrical. It is to be noted that with respect to the center beam 108G, the addressing faces of the electrodes are parallel, so no asymmetry, and hence no divergence, is introduced in the beam path.

The addressing faces of the intermediate electrode means 128 and adjacent electrodes 124 and 126 are depicted as being parallel and angled relative to center axis 118 so as to create the associated asymmetry. The preferred angle for the main focus lens shown is about 5 degrees. The greater the angle, the greater the effect on field asymmetry and hence convergence.

The asymmetry could as well be introduced by the angling of the addressing faces of just two of the electrodes such as between electrodes 128 and 126. Alternately only one of the addressing faces of an electrode need be at an angle, with the addressing face of the adjacent electrode perpendicular to gun center axis 118.

Another embodiment of the invention is depicted in Figure 7A, wherein there is indicated schematically a three-element main focus lens means 116A. The addressing faces of the intermediate electrode means 128A of each of the off-axis lens means will be seen to be so structured and arranged as to cause the associated field components on both sides of electrode means 128A to be asymmetric and effective to significantly converge the off-axis beams 108R and 108B through a predetermined convergence angle.

Another means of introducing field component asymmetry between adjacent electrodes to cause convergence is to radially offset the apertures of one off-axis electrode means with respect to the apertures of the adjacent electrode. These means for introducing field component asymmetry between adjacent electrodes are fully described and claimed in U.S. Patent No. 4,058,753 to Blacker et al.

NOTE: The "asymmetry" introduced by either tilting the electrode face(s), or by offsetting the apertures, has very little effect on the symmetry per se of the beam passing therethrough. The effect of

field asymmetry of the context of this invention is to cause the off-axis beam to diverge or converge in a desired direction from the axis of the gun producing the beam.

The all-over screen convergence provided by the dynamically converging gun system according to the invention is in consequence of the aforescribed structure and the development and application of a dynamic convergence signal 130 to the intermediate electrode 128. The means for developing the dynamic convergence signal is indicated as originating in circuit section 98D, as depicted diagrammatically in Figure 7. The dynamic convergence signal 130 is adapted to be correlated with scan of the beams across the screen of the tube. The signal according to the invention causes the strength of the asymmetric field components and thus beam convergence to vary in correspondence with beam deflection.

Figure 8 depicts a dynamically converging gun system 132 according to the invention that utilizes the principles of the extended field lens gun described and claimed in referent U.S. Patents Nos. 3,995, 194 and 4,058,753 both to Blacker et al. As with the guns described heretofore, the gun 134 depicted can find useful application in both home entertainment television receiver systems and in monitors, and in tension mask cathode ray tubes. The dynamically converging gun system 132 is similar to the gun system 94 described heretofore; to avoid needless repetition, only the salient differences in the gun system 132 according to the invention will be described.

Gun system 132 basically comprises a seven-element extended field electron gun 134 and means (indicated by the block 136) for the supplying of necessary voltages for gun operation as well as a dynamic beam convergence voltage, as will be described. Gun 134 consists essentially of means comprising a prefocusing section 138 for developing three electron beams 140R, 140G and 140B; prefocusing section 138 is shown as including three discrete cathodes 142 for beam generation and a control grid 144. Gun 134 also includes four integrated (unitized) extended field main focus lens means 148, indicated by the bracket, for focusing and converging the three beams 140 R, 140G and 140B. The four electrodes of main focus lens means 148 are depicted as comprising a first focusing electrode means 150 for receiving a focusing voltage, and in succession downbeam, a second electrode means 152, and a third electrode means 154 followed by an anode electrode means 156.

Means 136 for supplying operating voltages include section 136A for supplying the prefocusing section 138. Sections 136B-136E provide for developing and applying to the electrode means of each of the focus lens means 150, 152, 154 and 156 potentials which form field components in the gaps between adjacent electrodes. Section 136E is represented schematically as supplying an operating potential to the anode electrode 156 through centering spring 158 which is attached to convergence cup 160, attached physically and electrically to anode electrode 156.

The axes of the off-axis lens means of the main focus lens 148 are indicated by reference numbers 162 and 164. The addressing faces of these off-axis lenses on the third electrode 154 and on adjacent anode electrode 156 are shown as being parallel and angled relative to the central axis 166 of gun 134 so as to create asymmetries in the field components between the electrodes effective to significantly converge the off-axis beams 140R and 140B from a straight line path through a predetermined convergence angle.

Section 136D of the means 136 for developing and applying focus lens potentials provides, in addition to the potential which form field components in the gaps, a variable dynamic convergence signal 168 to third electrode 154 of each off-axis focus electrode means. The signal 168, indicated highly schematically by the parabolic waveform, is adapted to be correlated with the scan of the beams across the screen of the tube. Signal 168 according to the invention causes the strength of the asymmetrical field components to vary and thus the convergence angle and beam convergence to vary in correspondence with beam deflection.

The potentials, both fixed and varying, supplied by the means 136 to the unitized electrodes of the main focus lens 148 may be as follows, by way of example:

<u>Voltage Supply Section</u>	<u>Supplied to</u>	<u>Voltages Supplied</u>
136B	first electrode 150	12kVs fixed
136C	second electrode 152	7kV fixed*
136D	third electrode 154	12kV fixed plus a variable dynamic con- vergence signal ($\approx$ 2kV p-p)
136E	anode electrode 156	27kV, fixed

*May include a dynamic focus voltage waveform ($\approx$ 300V p-p)

In company with other standard circuits for reproducing television signals, the application and operation of which are well known in the art, the dynamically converging gun system according to the invention has means for developing horizontal and vertical scansion circuits, and deriving a variable dynamic convergence signal from them.

Television receiver systems in which the inventive concept can be advantageously employed comprise well-known types; as a result, details as to the best mode of implementation of the invention can be devoted to a simplified description of suitable circuit means for developing and supplying a dynamic convergence signal in conjunction with widely used television circuits and stages. Although similar in function, details of the types of components used, the specific circuit values, and the operating values of input and output signal voltages thereof will differ significantly among the many brands of television receiver systems currently available. So a description of a basic functional circuit is supplied, the details of which can be readily provided and implemented by one skilled in the art in adapting basic television and monitor circuits to specific receiver systems.

The dynamic convergence signal is essentially a combination of the parabolic waveforms developed by the horizontal and vertical sweep circuits of the television receiver or monitor system. With reference to Figure 9, which shows schematically a waveform-combining circuit means, there is depicted a fast horizontal sweep waveform 170. This waveform can be taken by sampling the output of the "S" (sweep) capacitor 172 common to most television and monitor sweep circuits. Waveform 170 is in the form of a parabola; the frequency is typically 15kHz in television receivers, and in the range of 30 to 60 kHz or higher in monitor circuits. Amplifier stage 174 provides for amplification of the sweep waveform to a high voltage. The output waveform 176, shown as being an inverted parabola, has an amplitude of 2,000 volts, by way of example.

The parabola 178 represents the vertical sweep waveform and is taken from a suitable point in the vertical sweep circuits. It is, typically, a "slow" parabolic waveform having a frequency of 60 Hz, or higher. The signals are amplified in amplifier 180 to about 2,000 volts. The output of both amplifiers is AC-coupled through capacitor 181 to the output as indicated, and is combined at point 182. Resistor 183 provides for isolation. The composite signal waveform 184 provides for a dynamic convergence according to the invention by application of the signal to a specified electrode of the main focus lens, as has been described. The voltage level is controlled by a resistive network 186, indicated highly schematically.

The dynamic electrostatic convergence voltage may be generated either by analog or digital electronics. Parabolic waveshapes from analog circuitry has been described. Digitally, based correction voltages may be generated based on a ROM (read-only memory) mapping of the correction voltages needed for discrete, small areas, and covering the entire tube face. The use of ROM mapping to generate correction voltages eliminates the need for symmetry in the correction "waveforms." The principle of ROM correction voltage is that for each position of the scanning beam, there is an index number which prompts the ROM to

generate an electrostatic convergence correction voltage appropriate to that beam position. Ideally, this approach, in conjunction with the present invention, can provide a perfectly converged tube. A system for providing suitable correction voltages as described in set forth in U.S. Patent No. 4,386, 368 to Banks.

There are many benefits to be gained by the implementation of the inventive means. For example, a homogenous "uniform-field" yoke can be utilized in lieu of the self-converging yoke. Not only is there a direct cost saving, but also the saving in manufacturing costs as well. Magnets for adjustment of purity and convergence can be made weaker and thus are lower in cost; also, less adjustment time is required and the beams are less subject to distortion. Relatively little time and effort is required for installation of the uniform field yoke--the purity and raster orientation can be done quickly, and without time-consuming tilting of the yoke. No special yoke adjusting machines ("YAM") are required. With regard to performance, less inherent astigmatism is introduced by the uniform field yoke. Most important, the size of deflected beam spots is dramatically reduced.

Further with respect to benefits of the invention--with regard to screening of the faceplate using the photoscreening device known as a "lighthouse", the optics can be made simpler. A spherical correction lens can be used, for example, in lieu of the more complex aspheric lens, which may require segmented elements. Also, there is less need to "grade" the mask, and any grading can be simpler with a reduced need of alteration of the pitch, size and shape of the apertures to compensate for deficiencies in beam convergence. Further, a systematic and simpler radial distribution of the mask apertures makes for less mask heating and consequent less mask aperture displacement relative to the pattern of phosphor deposits on the screen.

Claims

1. An electron gun system (78) for a color cathode ray tube (68) including beam-forming means including prefocus lens means (104) and cathode means (106) for developing an electron beam (80R, 80G, 80B), main focus lens means (116) for receiving said electron beam and forming a focused electron beam spot at the screen (82) of the tube (68), said main focus lens means (116) having, in a down beam direction, at least first focus electrode means (124) for receiving a variable focus adjustment potential for controlling the focal distance of said beam, and second and third convergence-associated electrode means (126, 128), and means (98) for developing and applying to said electrode means potentials effective to form main focusing field components between said electrode means (124, 126, 128), said second and third electrode means (120, 128) being so structured and arranged as to cause to be formed therebetween a focusing field component which is asymmetrical and effective to significantly divert a passed beam from a straight-line path through a predetermined angle, characterized in that said system (78) includes means (98D) for developing and applying a varying voltage (130) to at least one of said second and third electrode means (128, 120) to cause the strength of said asymmetric field component, and thus said angle by which said beam is diverted, to vary in response to said varying voltage.
2. The electron gun system of claim 1, wherein the beam-forming means also include cathode means (106) for developing three in-line electron beams, a central beam (108G) and two off-axis beams (108B, 108R), the main focus lens means (116) is one of three main focus lens means for receiving said electron beams and forming three focused electron beam spots at a common location on the screen (82) of the tube (68), the potential developing and applying means comprising power supply means (98) for applying to said electrode means (124, 126, 128) of each of said main focus lens means (116) potentials effective for maintaining the focusing field components between said electrode means (124, 126, 128), said main focus lens means (116) and power supply (98) potentials being such that said field components are discrete and independent for each of said three beams (108G, 108B, 108R), said second and third electrode means (126, 128) for each of said main focus lens means (116) being so structured and arranged as to cause to be formed therebetween a focusing field component which is asymmetrical and effective to converge said off-axis beams (108B, 108R), and characterized in that the dynamic convergence voltage developing and applying means (98D) provides a varying dynamic convergence voltage having amplitude variations correlated with a scan of the beams (108G, 108B, 108R) across the screen (82) to at least one of said second and third electrode means (126, 128) of each of said off-axis focus lens means (116) for said off-axis beams (108B, 108R) to cause the strength of said asymmetric field component, and thus said convergence of said off-axis beams (108B, 108R), to vary in response to said varying voltage.

generate an electrostatic convergence correction voltage appropriate to that beam position. Ideally, this approach, in conjunction with the present invention, can provide a perfectly converged tube. A system for providing suitable correction voltages as described in set forth in U.S. Patent No. 4,386, 368 to Banks.

There are many benefits to be gained by the implementation of the inventive means. For example, a homogenous "uniform-field" yoke can be utilized in lieu of the self-converging yoke. Not only is there a direct cost saving, but also the saving in manufacturing costs as well. Magnets for adjustment of purity and convergence can be made weaker and thus are lower in cost; also, less adjustment time is required and the beams are less subject to distortion. Relatively little time and effort is required for installation of the uniform field yoke--the purity and raster orientation can be done quickly, and without time-consuming tilting of the yoke. No special yoke adjusting machines ("YAM") are required. With regard to performance, less inherent astigmatism is introduced by the uniform field yoke. Most important, the size of deflected beam spots is dramatically reduced.

Further with respect to benefits of the invention--with regard to screening of the faceplate using the photSCREENING device known as a "lighthouse", the optics can be made simpler. A spherical correction lens can be used, for example, in lieu of the more complex aspheric lens, which may require segmented elements. Also, there is less need to "grade" the mask, and any grading can be simpler with a reduced need of alteration of the pitch, size and shape of the apertures to compensate for deficiencies in beam convergence. Further, a systematic and simpler radial distribution of the mask apertures makes for less mask heating and consequent less mask aperture displacement relative to the pattern of phosphor deposits on the screen.

Claims

1. An electron gun system (78) for a color cathode ray tube (68) including beam-forming means including prefocus lens means (104) and cathode means (106) for developing an electron beam (80R, 80G, 80B), main focus lens means (116) for receiving said electron beam and forming a focused electron beam spot at the screen (82) of the tube (68), said main focus lens means (116) having, in a down beam direction, at least first focus electrode means (124) for receiving a variable focus adjustment potential for controlling the focal distance of said beam, and second and third convergence-associated electrode means (126, 128), and means (98) for developing and applying to said electrode means potentials effective to form main focusing field components between said electrode means (124, 126, 128), said second and third electrode means (120, 128) being so structured and arranged as to cause to be formed therebetween a focusing field component which is asymmetrical and effective to significantly divert a passed beam from a straight-line path through a predetermined angle, characterized in that said system (78) includes means (98D) for developing and applying a varying voltage (130) to at least one of said second and third electrode means (128, 120) to cause the strength of said asymmetric field component, and thus said angle by which said beam is diverted, to vary in response to said varying voltage.
2. The electron gun system of claim 1, wherein the beam-forming means also include cathode means (106) for developing three in-line electron beams, a central beam (108G) and two off-axis beams (108B, 108R), the main focus lens means (116) is one of three main focus lens means for receiving said electron beams and forming three focused electron beam spots at a common location on the screen (82) of the tube (68), the potential developing and applying means comprising power supply means (98) for applying to said electrode means (124, 126, 128) of each of said main focus lens means (116) potentials effective for maintaining the focusing field components between said electrode means (124, 126, 128), said main focus lens means (116) and power supply (98) potentials being such that said field components are discrete and independent for each of said three beams (108G, 108B, 108R), said second and third electrode means (126, 128) for each of said main focus lens means (116) being so structured and arranged as to cause to be formed therebetween a focusing field component which is asymmetrical and effective to converge said off-axis beams (108B, 108R), and characterized in that the dynamic convergence voltage developing and applying means (98D) provides a varying dynamic convergence voltage having amplitude variations correlated with a scan of the beams (108G, 108B, 108R) across the screen (82) to at least one of said second and third electrode means (126, 128) of each of said off-axis focus lens means (116) for said off-axis beams (108B, 108R) to cause the strength of said asymmetric field component, and thus said convergence of said off-axis beams (108B, 108R), to vary in response to said varying voltage.



3. Use of the electron gun system of claim 2 in a color cathode ray tube system having a screen (82) with multi-color light-emitting phosphor elements thereon having uniform-field yoke means (90), characterized in that the means (98D) for developing and applying a varying dynamic convergence voltage having amplitude variations to at least one of said second and third electrode means (126, 128) of each of said off-axis focus lens means (116) for said off-axis beams (108B, 108R) causes the strength of said asymmetric field component, and thus the convergence of said off-axis beams (108B, 108R), to vary in response to said varying voltage, whereby the use of a uniform field yoke (90) is permitted, with consequent reduced deforming and distortion of the beams (108G, 108R, 108B) at the sides of the screen (82).
4. The use of the electron gun system of claim 3, characterized in that the screen (82) is disposed on a substantially flat faceplate (70) having an associated flat tension shadow mask (73) and whereby the use of an uniform-field yoke (90) is permitted, with consequent reduced deflection, defocusing and distortion of the beams (108G, 108B, 108R) at the sides of the screen (82).

Revendications

1. Un système (78) de canon à électrons destiné à un tube à rayons cathodiques couleur (68) comprenant des moyens (104) de formation de faisceaux incluant un moyen (104) de lentille de focalisation préalable et un moyen de cathode (106) pour développer un faisceau d'électrons (80R, 80G, 80B), un moyen (116) de lentille principale de focalisation pour recevoir ledit faisceau d'électrons et former une tache focalisée de faisceau d'électrons sur l'écran (82) du tube (68), ledit moyen (116) de lentille principale de focalisation comprenant, dans une direction aval du faisceau, au moins un premier moyen (124) d'électrode de focalisation pour recevoir un potentiel d'ajustement variable de focalisation pour commander la distance focale dudit faisceau, et un deuxième et un troisième moyens d'électrodes associées en convergence (126, 128), et un moyen (98) pour développer et appliquer, auxdits moyen d'électrodes, des potentiels susceptibles de former des composantes du champ principal de focalisation entre lesdits moyens d'électrode (124, 126, 128), lesdits deuxième et troisième moyens d'électrodes (126, 128) étant structurés et agencés de manière à provoquer la formation entre eux d'une composante de champ de focalisation qui est asymétrique et apte à dévier de façon significative, d'un angle prédéterminé par rapport à un trajet en ligne droite, un faisceau traversant, caractérisé en ce que ledit système (78) comprend un moyen (98D) pour développer et appliquer une tension variable (130) à au moins l'un desdits deuxième et troisième moyens d'électrode (126, 128) afin d'amener l'intensité de ladite composante asymétrique de champ, et donc ledit angle dont est dévié ledit faisceau, à varier en réponse à ladite tension variable.
2. Le système de canon à électrons selon la revendication 1, dans lequel les moyens de formation de faisceau comprennent aussi un moyen de cathode (106) pour développer trois faisceaux d'électrons en ligne, un faisceau central (8G) et deux faisceaux désaxés (108B, 108R), le moyen (116) de lentille principale de focalisation est un moyen parmi trois moyens principaux de lentille pour recevoir lesdits faisceaux d'électrons et former trois tâches focalisées de faisceau d'électrons à un emplacement commun sur l'écran (82) du tube (68), les moyens de développement et d'application de potentiel comprenant un moyen (98) d'alimentation en énergie pour appliquer, auxdits moyens d'électrode (124, 126, 128) de chacun desdits moyens (116) de lentille principale de focalisation, des potentiels permettant de maintenir les composantes du champ de focalisation entre lesdits moyens d'électrode (124, 126, 128), lesdits moyens (116) de lentille principale de focalisation et les potentiels des moyens (98) d'alimentation étant tels que lesdites composantes de champ sont discrètes et indépendantes pour chacun desdits trois faisceaux (108G, 108B, 108R), lesdits deuxième et troisième moyens d'électrode (126, 128) de chacun desdits moyens (116) de lentille principale de focalisation étant structurés et agencés de manière à amener la formation entre eux d'une composante de champ de focalisation qui est asymétrique et qui est apte à faire converger lesdits faisceaux désaxés (108B, 108R), et caractérisé en ce que le moyen (98D) de développement et d'application de tension dynamique de convergence fournit une tension dynamique de convergence variable dont les variations d'amplitude sont corrélées avec un balayage des faisceaux (108G, 108B, 108R) en travers de l'écran (82) pour au moins l'un desdits deuxième et troisième moyens d'électrode (126, 128) de chacun desdits moyens (116) de lentille de focalisation désaxée pour lesdits faisceaux désaxés (108B, 108R) pour amener l'intensité de ladite composante asymétrique de champ, et donc ladite convergence desdits faisceaux désaxés (108B, 108R) à varier en réponse à ladite tension variable.



3. Utilisation du système de canon à électrons selon la revendication 2 dans un système de tube à rayons cathodiques couleur comportant un écran (82) revêtu d'éléments photoluminescents émetteurs de lumière multicolore comportant un moyen (90) d'armature de champ uniforme, caractérisée en ce que le moyen (98D) de développement et d'application d'une tension dynamique de convergence variable présentant des variations d'amplitude à au moins l'un desdits deuxième et troisième moyens d'électrode (126, 128) de chacun desdits moyens (116) de lentille de focalisation désaxée pour lesdits faisceaux désaxés (108B, 108R) amènent l'intensité de ladite composante asymétrique de champ, et donc la convergence desdits faisceaux désaxés (108B, 108R) à varier en réponse à ladite tension variable, grâce à quoi l'utilisation d'une classe uniforme de champ (88) est permise, ce qui réduit par conséquent la déformation et la distorsion des faisceaux (108G, 108R, 108B) sur les côtés de l'écran (82).
4. L'utilisation du système de canon à électrons selon la revendication 3, caractérisée en ce que l'écran (82) est disposé sur un fond (70) sensiblement plat auquel est associé un masque perforé plat en tension (73) et grâce à quoi l'utilisation d'une culasse à champ uniforme (90) est permise, ce qui réduit par conséquent la déflexion, la défocalisation et la distorsion des faisceaux (108G, 108B, 108R) sur les côtés de l'écran (82).

Patentansprüche

1. Elektronenstrahlerzeugungssystem (78) für eine Farb-Kathodenstrahlröhre (68), mit einer Strahlerzeugungseinrichtung, die eine Vorfokussierlinseneinrichtung (104) und eine Kathodeneinrichtung (106) zum Erzeugen eines Elektronenstrahls (80R, 80G, 80B) besitzt; ferner mit einer Hauptfokussierlinseneinrichtung (116) zum Empfang des Elektronenstrahls und zum Erzeugen eines fokussierten Elektronenstrahlflecks auf dem Leuchtschirm (82) der Röhre (68), wobei die Hauptfokussierlinseneinrichtung (116) in einer Strahlrichtung hintereinander mindestens eine erste Fokussierelektrodeneinrichtung (124) zum Empfang eines veränderbaren Brennweiteinstellpotentials zur Steuerung der Brennweite des Strahls besitzt, sowie zweite und eine dritte Elektrodeneinrichtung (126, 128) zur Steuerung der Konvergenz und eine Einrichtung (98) zum Erzeugen und zum Anlegen von Potentialen an die genannten Elektrodeneinrichtungen zum Erzeugen von Hauptfokussierfeldkomponenten zwischen den Elektrodeneinrichtungen (124, 126, 128), wobei die zweite und die dritte Elektrodeneinrichtung (120, 128) so aufgebaut und angeordnet sind, daß sie bewirken, daß zwischen ihnen eine asymmetrische Fokussierfeldkomponente erzeugt wird, die bewirkt, daß ein hindurchtretender Strahl von einer geradlinigen Bahn um einen vorherbestimmten Winkel abgelenkt wird, dadurch gekennzeichnet, daß das System (78) eine Einrichtung (98D) besitzt, die dazu dient, durch Erzeugen und Anlegen einer variierenden Spannung (130) an die zweite und/oder dritte Elektrodeneinrichtung (128, 120) die Feldstärke der asymmetrischen Feldkomponente und dadurch den Winkel, um den der Strahl abgelenkt wird, in Abhängigkeit von der variierenden Spannung zu verändern.
2. Elektronenstrahlsystem nach Anspruch 1, in dem die Strahlerzeugungseinrichtung ferner eine Kathodeneinrichtung (106) zum Erzeugen von drei in-line-Elektronenstrahlen, und zwar eines zentralen Strahls (108G) und zweier außeraxialer Strahlen (108B, 108R) besitzt, daß die Hauptfokussierlinseneinrichtung (116) eine von drei Hauptfokussierlinseneinrichtungen ist, die dazu dienen, die genannten Elektronenstrahlen zu erzeugen und auf dem Leuchtschirm (82) der Röhre (68) an einer gemeinsamen Stelle drei fokussierte Elektronenstrahlflecken zu erzeugen, die Einrichtung zum Erzeugen und Anlegen des Potentials eine Stromversorgungseinrichtung (98) aufweist, die dazu dient, an die Elektrodeneinrichtungen (124, 126, 128) jeder der Hauptfokussierlinseneinrichtungen (116) Potentiale anzulegen, die die Fokussierfeldkomponenten zwischen den Elektrodeneinrichtungen (124, 126, 128) aufrechterhalten, daß die Potentiale der Hauptfokussierlinseneinrichtungen (116) und der Stromversorgungseinrichtung (98) derart sind, daß die genannten Feldkomponenten für die drei Strahlen (108G, 108B, 108R) diskret und voneinander unabhängig sind, und die zweite und die dritte Elektrodeneinrichtung (126, 128) jeder der Hauptfokussierlinseneinrichtungen (116) so aufgebaut und angeordnet sind, daß sie bewirken, daß zwischen ihnen eine asymmetrische Fokussierfeldkomponente erzeugt wird, die eine Konvergenz der genannten außeraxialen Strahlen (108B, 108R) bewirkt, dadurch gekennzeichnet, daß die Einrichtung (98D) zum Erzeugen und Anlegen der dynamischen Spannung zur Steuerung der Konvergenz eine sich ändernde dynamische Konvergenzsteuerspannung erzeugen, deren Amplitude sich in Korrelation mit einer Abtastbewegung der Strahlen (108G, 108B, 108R) auf dem Leuchtschirm (82) derart ändern, daß die zweite und/oder die dritte Elektrodeneinrichtung (126, 128) jeder der Fokussierlinseneinrichtungen



(116) für die außeraxialen Strahlen (108B, 108R) bewirkt, daß die Feldstärke der asymmetrischen Feldkomponente und damit die Konvergenz der außeraxialen Strahlen (108B, 108R) in Abhängigkeit von der variierenden Spannung verändert werden.

- 5 3. Verwendung des Elektronenstrahlerzeugungssystems nach Anspruch 2 in einem Farb-Kathodenstrahl-
röhrensystem mit einem Leuchtschirm (82), der mit mehrfarbiges Licht emittierenden Leuchtstoffele-
menten versehen ist, und einer ein homogenes Feld erzeugenden Ablenkeinrichtung (90), dadurch
gekennzeichnet, daß die Einrichtung (98D) zum Erzeugen und Anlegen einer variierenden dynamischen
Konvergenzsteuerspannung mit Amplitudenveränderungen an die zweite und/oder die dritte Elektroden-
10 einrichtung (126, 128) jeder der Hauptfokussierlinseneinrichtungen (116) für die außeraxialen Strahlen
die Feldstärke der asymmetrischen Feldkomponente und damit auch die Konvergenz der außeraxialen
Strahlen (108B, 108R) in Abhängigkeit von der variierenden Spannung verändert, so daß die Verwen-
dung einer ein homogenes Feld erzeugenden Ablenkeinrichtung (90) zulässig ist und daher die
Verformung und Verzerrung der Strahlen (108G, 108R, 108B) an den Seiten des Bildschirms (82)
15 vermindert wird.
- 20 4. Verwendung des Elektronenstrahlerzeugungssystems nach Anspruch 3, dadurch gekennzeichnet, daß
der Leuchtschirm (82) auf einer im wesentlichen ebenen Frontscheibe (70) angeordnet ist, der eine im
wesentlichen ebene, unter Zugspannung stehende Schattenmaske (73) zugeordnet ist, so daß die
Verwendung einer ein homogenes Feld erzeugenden Ablenkeinrichtung (90) zulässig ist und daher die
Ablenkung, das Defokussieren und die Verzerrung der Strahlen (108G, 108B, 108R) an den Seiten des
Leuchtschirms (82) vermindert wird.

