

Description

The invention relates to a dry-shaving apparatus comprising a housing having a holder for a shear plate with hair-entry apertures and a cutter which is rotatable about an axis of rotation, which cutter comprises a carrier with cutting elements which are movable relative to the carrier in substantially radial directions and which comprise cutting edges at their radial ends, the shear plate comprising a central portion which is shaped as a part of a cylindrical surface and which is formed with the hair-entry apertures, which central portion partly surrounds the cutter, the cutting edges of the cutting elements of the cutter, as it rotates, following, as part of a revolution, a constrained path defined by the shear plate and a free path where the cutting edges are disengaged from the shear plate, the shear plate comprising peripheral portions which adjoin the central portion of the shear plate and by which the shear plate is secured to the holder, said shear plate having a first shear-plate transition between a first peripheral portion and the central portion of the shear plate, in the vicinity of which first shear-plate transition a cutting edge of a cutting element changes from the free path to the constrained path, and having a second shear-plate transition between a second peripheral portion and the central portion, in the vicinity of which second shear-plate transition a cutting edge of a cutting element changes from the constrained path to the free path.

Such a dry-shaving apparatus is disclosed in, for example, US-A 3 710 442. At the transition where the ends of the cutting elements in this known apparatus change over from the free path to the constrained path the sudden contact between the cutting elements and the shear plate will give rise to undesired vibrations in the cutter, which may lead to damage to this cutter, the shear plate and other parts of the apparatus.

It is the object of the invention to mitigate this drawback and to this end the invention is characterized in that the axis of rotation of the cutter is situated closer to the second shear-plate transition than to the first shear-plate transition.

A special embodiment is defined in the appended Claim 2.

An embodiment of the invention will now be described in more detail, by way of example, with reference to the accompanying drawings.

Fig. 1 is a schematic longitudinal sectional view of a dry-shaving apparatus in accordance with the invention.

Fig. 2 is a sectional view taken on the line II-II in Fig. 1.

Fig. 3 is an enlarged-scaled simplified sectional view similar to that of Fig. 2.

The dry-shaving apparatus shown in Figs. 1 and 2 comprises a housing 1 with a holder 2 for a shear plate 3 and a cutter 4 which is rotatable relative to the shear plate.

The shear plate 3 comprises a central portion 5 with hair-entry apertures 6 and also a first peripheral portion 7 and a second peripheral portion 8 by which the shear plate is secured to the holder 2.

5 The cutter 4 comprises cutting elements 9 with cutting edges 11 at their radial ends 10. The cutter 4 is journaled in the holder 2 so as to be rotatable about the axis of rotation 12 and is partly surrounded by the central portion 5 of the shear plate 3. Hairs which project inwards from the hair-entry apertures 6 can be cut by cooperation of the portion 5 of the shear plate 3 with the ends 10 of the cutting elements 9 which slide along the inner side of the portion 5.

10 The cutter 4 comprises a carrier 13 for the cutting elements 9, which carrier comprises a hub 14 and a cylindrical portion 15 with slots 16. The cutting elements 9 are disposed partly inside the slots 16 and are movable over a limited distance in a radial direction relative to the carrier. The hook-shaped ends 17 of the cutting elements are situated between the hub 14 and the cylindrical portion 15 and ensure that the cutting elements 9 cannot fall out of the carrier 13. Pressure springs are arranged between the hub 14 and the cutting elements 9 to exert outwardly directed radial forces on the cutting elements 9.

15 The hub 14 is mounted on a spindle 19 which is journaled in the holder 2 so as to be rotatable about the axis of rotation 12. The housing 1 accommodates an electric motor 20 for driving the cutter 4, for example in a direction of rotation as indicated by the arrow P (Fig. 2). The rotation of the motor 20 is transmitted to the cutter 4 by means of pulleys 21 and 22, mounted on the spindle 19 and the motor shaft 23 respectively, and the drive belt 24.

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25 Fig. 3 is an enlarged-scaled simplified sectional view similar to that shown in Fig. 2. The shear plate 3 comprises a central portion 5 which is shaped as a part of a cylindrical surface represented by an arc of circle 25' which forms part of a circle 25 having a centre M_1 and a radius R_1 . At the shear-plate transitions 26 and 27 the arc of circle 25' is contiguous with the peripheral portions 7 and 8 respectively of the shear plate 3. These peripheral portions 7 and 8 extend for example in directions defined by tangent planes to the central portion 5 at the location of the shear-plate transitions 26 and 27. The arc of circle 25' corresponds to a central angle $\alpha = 150^\circ$.

30 If the cutting elements 9 of the cutter 4 are subjected only to the forces exerted by the pressure springs 18, the gravitational force being ignored, the cutting elements 9 will be urged outwards as far as possible relative to the carrier 13 by the pressure springs 18, causing the hook-shaped ends 17 to engage against the cylindrical portion 15 (Fig. 1). When the cutter 4 is rotated about the axis of rotation 12 the free path followed in this situation by the cutting edges 11 at the ends 10 of the cutting elements may be represented as a cylindrical surface whose cross-section is given by a circle having a centre M_2 , as is shown in Fig. 3. If the radius R_2 of this circle is equal to the radius R_1 of the circle 25 and the centre M_2 coincides with the centre M_1 , this free path of the cutting edges 11 in Fig. 3 consequently coincides with the circle 25. Theoretically, there will be no pressure between an end 10 of a cutting element 9 and the shear plate 3 in this situation.

For effectively cutting a hair by the cooperation of a cutting element with the shear plate, however, a pressure is required between these two parts. Moreover, in practice the holder 2, the shear plate 3 and parts of the cutter 4 are subject to manufacturing tolerances, i.e. dimensional errors as a result of manufacturing inaccuracies are accepted within specified limits. During assembly of the shaving apparatus parts with dimensional errors may be combined in such a way that in the situation in which M_1 coincides with M_2 the ends 10 remain clear of the shear plate 3 during a revolution which effect, referred to as a cutting gap, has an even more unfavourable influence on the shaving action than the absence of a pressure force.

In order to preclude the occurrence of cutting gaps as a result of an unfavourable accumulation of dimensional errors and in order to ensure that pressure forces act between the cutting elements and the shear plate, the cutter 4 may be displaced relative to the shear plate 3. If an axis from M_1 through the middle 28 of the arc of circle 25' is defined as the positive y-axis the cutter may be shifted along this positive y-axis, for example until the axis of rotation 12 coincides with the centre M'_2 . The free path of the cutting edges 11 may then be represented by an arc of circle 29' which forms part of a circle 29 having a radius R_2 and a centre M'_2 on the positive y-axis. This circle 29 intersects the shear plate at the location of a first path-transition 30 which is situated near the first shear-plate transition 26 where the central portion 5 adjoins the first peripheral portion 7. For the direction of rotation of the cutter 4 indicated by the arrow P in Fig. 3 an end 10 of a cutting edge 10 which follows the free path 29' will come into contact with the shear plate 3 at the first path-transition 30. As the movement proceeds the end will slide along the shear plate and the cutting edge will follow a constrained path defined by the shear plate.

The circle 29 also intersects the shear plate 3 at the location of the second path-transition 31 near the second shear-plate transition 27, where the central portion 5 adjoins the second peripheral portion 8. At the second path-transition 31 the ends 10 become disengaged from the shear plate 3 after which the cutting edges 11 again follow the free path 29'.

For the direction of rotation P the constrained path defined by the shear plate 3 extends from the first path-transition 30 to the second path-transition 31 and is situated within the circle 29 defining the free path. The ordinate Y'_2 of the centre M'_2 is selected so as to preclude the occurrence of cutting gaps as a result of dimensional errors and, moreover, in such a way that in the constrained path the cutting elements 9 are urged slightly inwards by the shear plate 3 against the action of the pressure springs 18. As a result of this, the springs 18 will exert a radial pressure K on the cutting elements 9 and the cutting elements will engage against the shear plate with a similar force K acting in a radial direction.

During rotation of the cutter 4, the cutting elements 9 are subjected to a frictional force W

caused by the force K. In order to minimise frictional losses between the ends 10 of the cutting elements 9 and the shear plate 3 the length of the constrained path should be as small as possible. In order to achieve this a value of 150° or smaller is generally selected for the central angle α , as shown in Fig. 3 and associated with the arc of circle 25' of the central portion 5.

By shifting the axis of rotation 12 and hence shifting the centre M_2 to M'_2 the circle 29 will intersect the shear plate at the location of the peripheral portions 7 and 8. This means that after the free path the ends 10 of the cutting elements 9 come into contact with the first peripheral portion 7 at the first path-transition 30. This sudden contact may be regarded as a collision between a cutting element and the shear plate, which may give rise to vibrations in the apparatus which may impair the shaving action of the apparatus and may even lead to damage. These collisions may also result in substantial forces acting between the shear plate and the cutting elements, which may also give rise to damage. These forces may occur, in particular, if the cutting elements 9 are mounted in the carrier 13 so as to obtain a self-biasing or self-locking effect, which are commonly used techniques in shaving apparatuses.

For a uniform transition from the free path to the constrained path, which is required in order to minimise the above collision effects and the undesirable consequences thereof, it is found to be essential that the first path-transition is situated on the arc of circle 25' between the first and second shear-plate transitions 26 and 27 respectively. This is achieved if the axis of rotation 12 of the cutter 4 is situated closer to the second shear-plate transition 27 than to the first shear-plate transition 26.

If in the cross-sectional view of Fig. 3 the positive x-axis is defined as an axis perpendicular to the y-axis from M_1 to the side of the second shear-plate transition 27, the location of the axis of rotation 12, which is represented by M'_2 , is preferably situated in the quadrant defined by the positive x-axis and y-axis with positive coordinates x'_2 and y'_2 . For simplicity y'_2 is assumed to be equal to y'_2 . An arc of circle 32', which is part of a circle 32 having a centre M'_2 and a radius $R_2 = R_1$, represents the free path which extends from the second path-transition 34 to the first path-transition 33 in the direction of rotation P. As can be seen in Fig. 3, the first path-transition 33 is situated on the arc of circle 25', i.e. after the cutting edges 11 have traversed the free path the cutting elements come directly into contact with the central portion 5 of the shear plate which is curved as a cylindrical surface. The constrained path consequently extends in the direction of rotation P from the first path-transition 33 along the arc of circle 25' and partly along the peripheral portion 8 to the second path-transition 34. The fact that the second path-transition is situated on the peripheral portion 8 has no adverse effect, because at this location the constrained path changes into the free path 32' and this is not attended by collision effects.

In Fig. 3 the shear plate is represented by a few lines as a foil without any thickness. In fact, the

lines 7, 8 and 25' represent the inner side of the shear plate. Further, it is assumed that as the cutter rotates the cutting edges 11 of the cutting elements 9 always come into contact with the inner side of the shear plate, so that the cutting edges follow the constrained path as defined above.

Instead of coupling the cutter to the motor by means of a belt transmission this is also possible by means of, for example, a gearwheel transmission. The biasing force for the cutting elements may also be provided by magnetic or centrifugal forces instead of spring forces.

The transition of a cutting edge from the free path to the constrained path will be smoother as the angle between the tangent line to the free path and the tangent line to the shear plate at the location of the first path-transition decreases. For the first path-transition 33 this angle corresponds to the angle β between the radii from M_1 and M'_2 to point 33. For the first path-transition 30 this angle corresponds to the angle γ between the radius from M_1 to the first shear-plate transition 26 and the radius from M'_2 to the first path-transition 30. Since these radii intersect one another within the circle 29, the angle γ is larger than the angle β . In Fig. 3 the angle γ is approximately twice as large as the angle β . Thus, by shifting the axis of rotation 12 towards the second shear-plate transition 27 it is simply possible to obtain a substantial improvement with respect to a smooth engagement of the cutting elements with the shear plate.

In the embodiment described in the foregoing the central portion of the shear plate is shaped as a part of a circularly cylindrical surface having the same radius as the free path of the cutting edges of the cutting elements. Generally, it will be favourable for the operation of the apparatus if the shape and dimensions of the central portion of the shear plate are thus adapted to the rotating cutter. The advantages of the said shift of the axis of rotation, however, can also be obtained in those cases in which the radius of the central portion deviates from that of the free path or in which the central portion has a shape other than that of a circularly cylindrical surface. By moving the axis of rotation towards the second shear-plate transition it is also possible to ensure that in such cases the first path-transition is situated at the location of the central portion, so that a smooth transition from the free path to the constrained path is obtained and the adverse effects of a collision of the cutting elements with the shear plate are avoided.

Claims

1. A dry-shaving apparatus comprising a housing (1) having a holder (2) for a shear plate (3) with hair-entry apertures (6) and a cutter (4) which is rotatable about an axis of rotation (12), which cutter comprises a carrier (13) with cutting elements (9) which are movable relative to the carrier in substantially radial directions and which comprise cutting edges (11) at their radial ends (10), the shear plate comprising a central portion (5) which is shaped as a part of a cylindrical surface and which is formed with the

hair-entry apertures (6), which central portion (5) partly surrounds the cutter (4), the cutting edges of the cutting elements of the cutter, as it rotates, following, as part of a revolution, a constrained path defined by the shear plate and a free path where the cutting edges are disengaged from the shear plate, the shear plate (3) comprising peripheral portions (7, 8) which adjoin the central portion (5) of the shear plate and by which the shear plate is secured to the holder (2), said shear plate having a first shear-plate transition (26) between a first peripheral portion and the central portion (5) of the shear plate, in the vicinity of which first shear-plate transition a cutting edge (11) of a cutting element (9) changes from the free path to the constrained path, and having a second shear-plate transition (27) between a second peripheral portion and the central portion (5), in the vicinity of which second shear-plate transition a cutting edge (11) of a cutting element (9) changes from the constrained path to the free path, characterized in that the axis of rotation (12) of the cutter (4) is situated closer to the second shear-plate transition (27) than to the first shear-plate transition (26).

2. A shaving-apparatus as claimed in Claim 1, in which the free path followed by the ends of the cutting elements (9) is situated on a cylindrical surface whose central axis is the axis of rotation (12) and the central portion (5) of the shear plate (3) is curved as a circularly cylindrical surface having a central axis through a point M_1 , whilst in a cross-section taken along the axis of rotation a line from M_1 through the centre of the central portion defines a positive y-axis and a line perpendicular to the y-axis from M_1 towards the second shear-plate transition (27) defines a positive x-axis, characterized in that the axis of rotation is situated in the quadrant defined by the positive x-axis and y-axis with positive coordinates x_1 and y_1 .

Patentansprüche

1. Rasiergerät mit einem Gehäuse (1) mit einer Halterung (2) für eine Scherplatte (3) mit Haardurchgangsöffnungen (6) und mit einem um eine Drehungsachse (12) drehend antreibbaren Schneidelement (4), das einen Träger (13) aufweist mit in im wesentlichen radialen Richtungen gegenüber dem Träger verschiebbaren Meißeln (9), die an den radialen Enden (10) mit Schneidkanten (11) versehen sind, wobei die Scherplatte einen Zentralteil (5) aufweist, der als Teil eines Zylindermantels ausgebildet und mit Haardurchgangsöffnungen (6) versehen ist, wobei dieser Zentralteil (5) das Schneidelement (4) teilweise umgibt, wobei die Schneidkanten der Meißel des Schneidelementes bei Drehung desselben als Teil einer Umdrehung einer durch die Scherplatte bestimmten Zwangsbahn folgen, sowie einer freien Bahn, wenn die Schneidkanten nicht mit der Scherplatte zusammenarbeiten, wobei die Scherplatte (3) mit Randteilen (7, 8) versehen ist, die sich an den Zentralteil (5) der Scherplatte anschließen, wobei die Scherplatte mit den Randteilen an der Halterung (2) befestigt ist, wobei die Scherplatte einen ersten Scherplattenübergang (26) zwischen einem

lines 7, 8 and 25' represent the inner side of the shear plate. Further, it is assumed that as the cutter rotates the cutting edges 11 of the cutting elements 9 always come into contact with the inner side of the shear plate, so that the cutting edges follow the constrained path as defined above.

Instead of coupling the cutter to the motor by means of a belt transmission this is also possible by means of, for example, a gearwheel transmission. The biasing force for the cutting elements may also be provided by magnetic or centrifugal forces instead of spring forces.

The transition of a cutting edge from the free path to the constrained path will be smoother as the angle between the tangent line to the free path and the tangent line to the shear plate at the location of the first path-transition decreases. For the first path-transition 33 this angle corresponds to the angle β between the radii from M_1 and M'_2 to point 33. For the first path-transition 30 this angle corresponds to the angle γ between the radius from M_1 to the first shear-plate transition 26 and the radius from M'_2 to the first path-transition 30. Since these radii intersect one another within the circle 29, the angle γ is larger than the angle β . In Fig. 3 the angle γ is approximately twice as large as the angle β . Thus, by shifting the axis of rotation 12 towards the second shear-plate transition 27 it is simply possible to obtain a substantial improvement with respect to a smooth engagement of the cutting elements with the shear plate.

In the embodiment described in the foregoing the central portion of the shear plate is shaped as a part of a circularly cylindrical surface having the same radius as the free path of the cutting edges of the cutting elements. Generally, it will be favourable for the operation of the apparatus if the shape and dimensions of the central portion of the shear plate are thus adapted to the rotating cutter. The advantages of the said shift of the axis of rotation, however, can also be obtained in those cases in which the radius of the central portion deviates from that of the free path or in which the central portion has a shape other than that of a circularly cylindrical surface. By moving the axis of rotation towards the second shear-plate transition it is also possible to ensure that in such cases the first path-transition is situated at the location of the central portion, so that a smooth transition from the free path to the constrained path is obtained and the adverse effects of a collision of the cutting elements with the shear plate are avoided.

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hair-entry apertures (6), which central portion (5) partly surrounds the cutter (4), the cutting edges of the cutting elements of the cutter, as it rotates, following, as part of a revolution, a constrained path defined by the shear plate and a free path where the cutting edges are disengaged from the shear plate, the shear plate (3) comprising peripheral portions (7, 8) which adjoin the central portion (5) of the shear plate and by which the shear plate is secured to the holder (2), said shear plate having a first shear-plate transition (26) between a first peripheral portion and the central portion (5) of the shear plate, in the vicinity of which first shear-plate transition a cutting edge (11) of a cutting element (9) changes from the free path to the constrained path, and having a second shear-plate transition (27) between a second peripheral portion and the central portion (5), in the vicinity of which second shear-plate transition a cutting edge (11) of a cutting element (9) changes from the constrained path to the free path, characterized in that the axis of rotation (12) of the cutter (4) is situated closer to the second shear-plate transition (27) than to the first shear-plate transition (26).

2. A shaving-apparatus as claimed in Claim 1, in which the free path followed by the ends of the cutting elements (9) is situated on a cylindrical surface whose central axis is the axis of rotation (12) and the central portion (5) of the shear plate (3) is curved as a circularly cylindrical surface having a central axis through a point M_1 , whilst in a cross-section taken along the axis of rotation a line from M_1 through the centre of the central portion defines a positive y-axis and a line perpendicular to the y-axis from M_1 towards the second shear-plate transition (27) defines a positive x-axis, characterized in that the axis of rotation is situated in the quadrant defined by the positive x-axis and y-axis with positive coordinates x_1 and y_1 .

Patentansprüche

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ersten Randteil und dem Zentralteil (5) der Scherplatte aufweist, wobei in der Nähe des ersten Scherplattenüberganges eine Schneidkante (11) eines Meißels (9) von der freien Bahn in die Zwangsbahn übergeht und wobei die Scherplatte einen zweiten Scherplattenübergang (27) zwischen einem zweiten Randteil und dem Zentralteil (5) aufweist, wobei in der Nähe des zweiten Scherplattenüberganges eine Schneidkante (11) eines Meißels (9) von der Zwangsbahn in die freie Bahn übergeht, dadurch gekennzeichnet, daß die Drehungsachse (12) des Meißels (4) näher bei dem zweiten Scherplattenübergang (27) liegt als bei dem ersten Scherplattenübergang (26).

2. Rasiergerät nach Anspruch 1, wobei die freie Bahn, der die Enden der Meißel (9) folgen, auf einer Zylindermantelfläche liegt, deren Zentralachse die Drehungsachse (12) ist und wobei der Zentralteil (5) der Scherplatte (3) wie eine Kreiszyylinderfläche gekrümmt ist mit einer Zentralachse durch einen Punkt M_1 , während in einem Schnitt längs der Drehungsachse eine Linie von M_1 durch die Mitte des Zentralteils eine positive y-Achse und eine Linie senkrecht zu der y-Achse von M_1 zu dem zweiten Scherplattenübergang (27) eine positive x-Achse definiert, dadurch gekennzeichnet, daß die Drehungsachse in dem Quadranten liegt, der durch die positive x-Achse und y-Achse mit positiven Koordinaten x_1 und y_1 definiert ist.

Revendications

1. Rasoir à sec comportant un boîtier (1) muni d'un support (2) pour un peigne (3) présentant des ouvertures d'entrée de poil (6) et d'un organe de coupe (4) pouvant tourner autour d'un axe de rotation (12) et comportant un support (13) muni d'éléments de coupe (9) qui peuvent être déplacés par rapport à celui-ci dans des directions sensiblement radiales et qui présentent des tranchants (11) à leurs extrémités radiales (10), peigne comportant une partie centrale (5) réalisée sous la forme d'une partie d'une surface cylindrique et dans laquelle sont pratiquées les ouvertures d'entrée de poil (6), ladite partie centrale (5) entourant partiellement l'organe de coupe (4), rasoir dans lequel, lors de la rotation de l'organe de coupe, les tranchants des éléments de celui-ci suivent, comme partie d'un tour, un trajet forcé défini par le peigne et un trajet libre dans lequel les tranchants sont dégagés du peigne, le peigne (3) présentant des parties périphériques (7, 8) contiguës à la partie centrale (5) du peigne et par lesquelles le peigne est fixé au support (2), ledit peigne présentant en outre, d'une part, une première transition de peigne (26) formée entre une première partie périphérique et la partie centrale (5) du peigne et à proximité de laquelle un tranchant (11) d'un élément de coupe (9) passe du trajet libre au trajet forcé et, d'autre part, une deuxième transition de peigne (27) formée entre une deuxième partie périphérique et la partie centrale (5) et à proximité de laquelle un tranchant (11) d'un élément de coupe (9) passe du trajet forcé au trajet libre, caractérisé en ce que l'axe de rotation (12) de l'organe de coupe (4)

est plus rapproché de la deuxième transition de peigne (27) que de la première transition de peigne (26).

2. Rasoir à sec selon la revendication 1, dans lequel le trajet libre suivi par les extrémités des éléments de coupe (9) est situé sur une surface cylindrique ayant l'axe de rotation (12) comme axe central et la partie centrale (5) du peigne (3) est courbée suivant une surface cylindrique circulaire ayant un axe central traversant un point M_1 , alors que, dans une coupe transversale suivant l'axe de rotation, une ligne partant de M_1 et traversant le centre de la partie centrale définit un axe y positif et une ligne perpendiculaire à l'axe y s'étendant à partir de M_1 en direction de la deuxième transition de peigne (27) définit un axe x positif, caractérisé en ce que l'axe de rotation est situé dans le quadrant défini par l'axe x et l'axe y positifs avec des coordonnées positives x_1 et y_1 .

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