

SPECIFICATION

METHOD AND APPARATUS FOR GLOBAL WARMING PREVENTION

TECHNICAL FIELD

This invention relates to a method for treating a gas causing global warming and an apparatus therefor. More particularly, it relates to a method for preventing global warming by exothermally decomposing nitrous oxide (N_2O), which causes global warming, into nitrogen (N_2), oxygen (O_2) and optionally nitrogen oxides (NO , NO_2 , etc.) and an apparatus therefor.

10 BACKGROUND ART

In the process of producing adipic acid, nitric acid is used as an oxidizing agent. It has been an accepted practice to release into the atmosphere nitrous oxide formed as a by-product in the formation of adipic acid from the oxidation of cyclohexanone and/or cyclohexanol with nitric acid.

However, nitrous oxide has recently attracted public attention as one of the gases causing global warming, though it is not as well known as carbon dioxide which is a typical gas causing global warming.

Nitrous oxide evolves mostly from natural soil or farmlands. Thus, the chemical industry causes only a small part of the nitrous oxide evolving on the earth. However, it is considered that the amount of nitrous oxide formed by chemical processes such as the adipic acid production process, which are artificial N_2O sources, can be controlled. Therefore, attempts have been made in recent years to reduce, first of all, nitrous oxide generated from these chemical processes.

There have been proposed various methods for reducing nitrous oxide generated from chemical processes. Many of these proposals relate to methods for decomposing nitrous oxide (N_2O) into nitrogen (N_2) and oxygen (O_2) and optionally nitrogen oxides (NO , NO_2). These methods involve two main types for decomposing N_2O , namely, thermal decomposition methods wherein decomposition is carried out by heating without using any catalyst and catalytic decomposition methods wherein decomposition is carried out by using a catalyst. Now, each type of these methods will be described.

Known examples of the thermal decomposition methods without using any catalyst include those proposed in, for example, U.S. Patent 2,974,019, JP-A-61-257940, JP-A-5-339003 and JP-W-A-9-508346 (the term "JP-A" as used herein means an "unexamined published Japanese patent application" and the term "JP-W-A" as used herein means an "international

patent application published in the Japanese national proceeding"). However, these proposals each suffers from unsolved problems as will be described hereinafter. That is, no satisfactory method for thermally decomposing nitrous oxide has been proposed hitherto.

That is, U.S. Patent 2,974,019 proposes an apparatus by which N_2O is thermally decomposed at a high temperature under elevated pressure (to $1692^{\circ}C$, to 25.5 atm) to give NO_2 . However, a highly reliable material for this apparatus used to resist the high temperature and elevated pressure is not readily available and makes the apparatus highly expensive. Therefore, this method is used very little in practice.

JP-A-61-257940, which has been applied by the same applicant as in the present invention, discloses that when a discharged gas containing N_2O is preheated and then heated, the thermal decomposition of N_2O starts at about $900^{\circ}C$ and N_2O can be thermally decomposed at $1000^{\circ}C$ or above. In the method of the thermal decomposition of N_2O proposed in this document, it is necessary to control the total content of NO and NO_2 to be 10% or less in the N_2O -containing gas to be treated. Thus, there arises a problem that an additional step is needed for controlling the discharged gas composition.

JP-A-5-339003 proposes an improved method over the above-mentioned JP-A-61-257940 for thermochemically

decomposing N_2O with a flame treatment in the thermal decomposition method. In this method, N_2O is thermochemically decomposed in the presence of flame by the combustion heat of the flame. Therefore, it is feared that the thermochemical reaction in this method should be performed at a considerably higher temperature due to the combustion heat of the flame coupled with the decomposition heat of N_2O . In this method wherein the flame is continuously employed in the thermochemical decomposition of N_2O , it is unavoidable to use a considerably large amount of fuel for the generation of the flame. As a result, a large amount of a combustion gas is formed and, therefore, the NO and NO_2 concentrations in the thermochemically decomposed gas are lowered, which brings about another fear that a large-scaled device (for example, an absorption tower) should be used to recover the NO and NO_2 .

JP-W-A-9-508346 proposes a method wherein the method of the thermal decomposition of N_2O as disclosed in the above-described JP-A-61-257940 is improved in the preheating portion to thereby produce NO from N_2O . That is, this document proposes a method for producing NO from N_2O by heating an N_2O -containing gas to about 400 to 700°C by using a heat exchanger, then heating the gas to about 850°C without a heat exchanger and using the combustion heat of a combustible gas, etc., thermally decomposing N_2O in the gas

at 1000°C or above, and then quickly cooling the gas thus formed to thereby recover NO. In the case of this method, however, it is needed to heat the whole N₂O-containing gas to be treated to 850°C by using the combustion of a combustible gas, etc. It is therefore unavoidable to use a large amount of the combustible gas. Accordingly, this method suffers from the same problem as in the method proposed by JP-A-5-339003 described above. In this method, furthermore, it is feared that the temperature in the reaction chamber is elevated to a considerably high level, since a large amount of decomposition heat is generated in the reaction chamber from the N₂O holding the combustion heat as described above. Regarding this point, it is described in the specification of this application that the temperature in the reaction chamber might be elevated to 1500°C.

In the thermal decomposition reaction of N₂O, the reaction by which N₂O is decomposed into N₂ and O₂ is an exothermic reaction. Accordingly, there arises a problem that the temperature in the reaction system, where N₂O is thermally decomposed, is remarkably elevated due to the decomposition heat generated in a large amount. As the temperature in the reaction system is elevated, more expensive heat-resistant materials should be employed in the reactor and various devices for treating the gas discharged from the reactor (for example, a heat exchanger, a device

for absorbing the thus formed gas, pipes connecting these devices, etc.). In addition, it is also feared that the maintenance of the equipment becomes more difficult thereby.

In the conventional proposals as described above, however,
5 no consideration has been given with respect to these problems accompanying the decomposition heat of N_2O .

That is to say, no satisfactory method for thermally decomposing nitrous oxide has been proposed hitherto.

As examples of the catalytic decomposition methods
10 with the use of a catalyst, proposals have been made by JP-A-5-4027, JP-A-6-277453, etc. However, these proposals each suffer from unsolved problems as will be described hereinafter. That is, no satisfactory method for catalytically decomposing nitrous oxide has been proposed
15 hitherto similar to the case of the thermal decomposition methods.

For example, JP-A-5-4027, which has been applied by the same applicant as in the present invention, proposes a method for catalytically decomposing an N_2O -containing
20 discharged gas into N_2 and O_2 in the presence of a copper(II) oxide catalyst. This document discloses that the reaction temperature preferably ranges from 400 to 600°C; that it is desirable in case of an adiabatic reaction to supply the gas while diluted with air, etc. into the reactor, since the
25 temperature in the outlet side of the reactor is elevated

due to the large reaction heat of the catalytic decomposition; and that the reaction heat of the catalytic decomposition is recovered from the gas as steam after the completion of the catalytic decomposition by using a heat exchanger or the heat is eliminated by diluting the gas with air, etc. after the completion of the catalytic decomposition. However, the treatment of the reaction heat with the use of a heat exchanger or a diluent gas, as proposed by this document, is accompanied by a problem, since the catalytic decomposition heat of N_2O amounts to 19.5 kcal/mol. In case of, for example, catalytically decomposing an N_2O -containing gas with an N_2O concentration of 34%, a large amount of decomposition heat is generated so that the temperature is elevated by about 600°C after the completion of the catalytic decomposition reaction. To eliminate this heat by the method as proposed above, it is necessary to use a large amount of a diluent gas or a large-scaled heat exchanger, which brings about a fear of a greater cost for the heat elimination.

JP-A-6-277453 proposes an improved process for the catalytic decomposition of N_2O . It is disclosed in this document that the outflow gas at the outlet of the decomposition zone is cooled and a portion of the thus cooled gas stream is refluxed into the decomposition zone so as to maintain the whole N_2O decomposition zone at a

temperature not higher than the maximum allowable temperature T_{max} . However, this proposal also suffers from the problem caused by the reaction heat generated in a large amount in association with the decomposition N_2O , similar to
5 the case of JP-A-5-4027 as described above.

That is to say, no satisfactory method for catalytically decomposing nitrous oxide has been proposed hitherto.

The invention provides a method for decomposing N_2O by
10 which the unsolved problems encountering in the conventionally proposed methods for decomposing N_2O , which have been discussed above in detail, can be solved to thereby prevent global warming through the decomposition of N_2O .

15 Accordingly, the object of the invention is to provide a practically useful method and an apparatus for preventing global warming by decomposing N_2O , by which N_2O contained in an N_2O -containing gas to be treated can be efficiently decomposed at a low temperature while efficiently
20 controlling the N_2O decomposition heat thus generated, and NO and NO_2 can be recovered, if necessary, and which apply only a small heat load to a device for decomposing N_2O and to other instruments, and need only an extremely small amount of heat energy supplied externally, and require only a low
25 equipment cost and a low driving cost.

DISCLOSURE OF THE INVENTION

The inventors have conducted intensive studies on a method for decomposing N_2O , in particular, a method by which the above-described problems in association with the N_2O decomposition heat can be solved. As a result, the inventors have found out a method for exothermally decomposing N_2O which is completely different from the conventional methods for decomposing N_2O as described above and made it possible to solve the above-mentioned object of the invention, thereby completing the invention.

Accordingly, the present invention provides:

1. A method for preventing global warming comprising, a process of thermally or catalytically decomposing N_2O in an N_2O -containing gas to be treated, by dividing the N_2O -containing gas stream to be treated in portions, preheating a portion thereof so as to exothermally decompose N_2O in said gas stream to form a hot gas stream, and supplying the remainder of the divided gas stream to be treated into said hot gas stream to thereby continuously decompose N_2O , so that global warming is prevented.

2. The method for preventing global warming according to the above item 1, wherein said exothermic decomposition of N_2O is performed by thermal decomposition without using any catalyst.

3. The method for preventing global warming according to the above item 2, wherein the remainder of said divided gas to be treated is supplied into plural positions in the flow direction of said hot gas stream.

5 4. The method for preventing global warming according to the above item 2 or 3, wherein said decomposition of N_2O in the gas to be treated is performed in a state of a substantially plug flow.

5. The method for preventing global warming according
10 to the above item 2 or 3, wherein said preheating is performed by a direct heating system utilizing an oxidative exothermic reaction of a fuel.

6. The method for preventing global warming according to the above item 5, wherein said fuel is hydrogen or
15 methanol.

7. The method for preventing global warming according to the above item 1, wherein said exothermic decomposition of N_2O is performed by catalytic decomposition.

8. The method for preventing global warming according
20 to the above item 7, wherein the remainder of said divided gas to be treated is supplied into plural positions in the flow direction of said hot gas stream and each brought into contact with a catalytic bed respectively.

9. The method for preventing global warming according
25 to the above item 7 or 8, wherein the gas stream,

immediately before contacting the catalytic bed, is a mixture with a diluent gas.

10. The method for preventing global warming according to the above item 9, wherein said diluent gas is
5 air and/or the gas, which has been subjected to the catalytic decomposition of N_2O in the gas to be treated.

11. The method for preventing global warming according to the above item 9, wherein the gas having been subjected to the catalytic decomposition of N_2O in the gas to
10 be treated is cooled and then used as the diluent gas.

12. The method for preventing global warming according to the above item 7, 8, 10 or 11, wherein said preheating is performed by mixing the gas to be treated and/or the diluent gas with steam formed by reacting
15 hydrogen and oxygen using a noble metal catalyst.

13. An apparatus for preventing global warming by thermally decomposing N_2O in an N_2O -containing gas, comprising:

(a) an introduction portion for the N_2O -containing gas
20 to be treated;

(b) a preheating portion for the thus introduced gas to be treated;

(c) a thermal decomposition portion adjacent to the preheating portion, said thermal decomposition portion
25 having means for supplying the gas to be treated, said

supplying means being provided at one or more positions in the flow direction of a gas stream; and

(d) a discharging portion for the thermally decomposed gas.

5 14. The apparatus for preventing global warming according to the above item 13, wherein said preheating portion is having means of fuel combustion.

15 15. The apparatus for preventing global warming according to the above item 14, wherein the temperature of the gas stream at the outlet of said discharging portion is controlled to a constant level by controlling the amount of the fuel fed into said fuel-combustion means.

15 16. The apparatus for preventing global warming according to the above item 13, 14 or 15, wherein said thermal decomposition portion has a porous plate and/or a multi-pipe nozzle in front of and/or at the back of at least one means for supplying the gas to be treated.

20 17. The apparatus for preventing global warming according to the above item 13, 14 or 15, wherein said porous plate, multi-pipe nozzle and/or inlet of the gas to be treated are located in such a manner that the gas stream flowing towards the means for supplying the gas to be treated flows as a rotary stream.

25 18. An apparatus for preventing global warming by bringing N_2O in an N_2O -containing gas into contact with a

catalytic bed to thereby catalytically decompose N_2O ,
comprising:

(a) an introduction portion for the gas to be treated
and/or a diluent gas;

5 (b) a mixing portion for the gas to be treated and/or
the diluent gas;

(c) a mixing portion having one or more means for
supplying the gas to be treated and/or the diluent gas at
different positions in the longitudinal direction of the
10 apparatus;

(d) a catalytic decomposition portion having the
catalytic bed; and

(e) a discharging portion for the catalytically
decomposed gas.

15 19. An apparatus for preventing global warming by
catalytic decomposition of N_2O in an N_2O -containing gas,
comprising:

a device which comprises:

(a) an introduction portion for the gas to be treated
20 and/or a diluent gas;

(b) a mixing portion for the gas to be treated and/or
the diluent gas;

(c) a catalytic decomposition portion having a
catalytic bed; and

(d) a discharging portion for the catalytically decomposed gas; and

one or more devices each of which comprises:

(e) an introduction portion for the discharged gas
5 having been catalytically decomposed, the gas to be treated
and/or a diluent gas;

(f) a mixing portion for the discharged gas having
been catalytically decomposed, the gas to be treated and/or
the diluent gas;

10 (g) a catalytic decomposition portion having a
catalytic bed; and

(h) a discharging portion for the catalytically
decomposed gas.

20. The apparatus for preventing global warming
15 according to the above item 18 or 19, wherein said mixing
portion for the gas to be treated and/or the diluent gas
involves a preheating portion for the gas to be treated
and/or the diluent gas.

21. A process for producing adipic acid with reduced
20 release of N_2O that causes global warming, comprising:

(1) a nitric acid-oxidation step in which cyclohexanol
and/or cyclohexanone are oxidized with nitric acid to form
adipic acid;

(2) a nitric acid recovery step in which HNO_3 is recovered from an N_2O -containing gas caused in the nitric acid-oxidation step;

(3) a N_2O decomposition step in which the remaining
5 N_2O -containing gas stream to be treated, from which HNO_3 has been recovered, is divided, a portion thereof is preheated to exothermally decompose N_2O in the gas stream to form a hot gas stream, and the remainder of the divided gas stream to be treated is supplied into said hot gas stream to thereby
10 continuously decompose N_2O ; and

(4) a N_2O decomposition heat recovery step in which the N_2O decomposition heat emitted from the N_2O decomposition step is recovered.

BRIEF DESCRIPTION OF THE DRAWINGS

15 Fig. 1 is a schematic view of an apparatus for thermally decomposing N_2O according to the invention.

Fig. 2 is a schematic view of a thermal decomposition apparatus used in Example 1.

Fig. 3 is a schematic view of a thermal decomposition
20 apparatus used in Example 7.

Fig. 4 is a model view of an apparatus for catalytically decomposing N_2O provided with plural catalytic beds according to the invention.

Fig. 5 is a model view of an apparatus for catalytically decomposing N_2O provided with plural catalytic beds independent from each other according to the invention.

In these figures, each numerical symbol has the

5 following meaning:

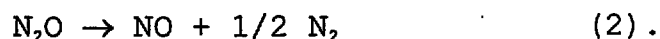
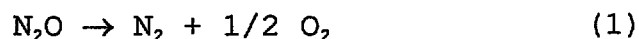
- 1: an introduction portion for an N_2O -containing gas;
- 2: a preheating portion;
- 3: a preheated gas-receiving portion;
- 4: a supplying portion for the N_2O -containing gas;
- 10 5: an N_2O thermal decomposition portion;
- 6: a discharging portion for the thermally decomposed gas;
- 7: a wall of a thermal decomposition portion;
- 8: a thermal decomposition portion;
- 15 9: a porous plate;
- 10: a preheating portion;
- 11: a baffle plate;
- 12: a supplying portion for the N_2O -containing gas;
- 13: a thermal decomposition portion;
- 20 14: a porous plate;
- 15: a preheating portion;
- 16: a supplying portion for the N_2O -containing gas;
- 17: an introduction portion for the gas to be treated;
- 18: an introduction portion for a diluent gas;
- 25 19: a preheating portion;

- 20: a preheated gas-receiving portion;
21: a space;
22: a catalytic decomposition portion;
23: a mixing portion;
5 24: a supplying portion for the gas to be treated;
25: a supplying portion for the diluent gas;
26: a discharging portion for the catalytically
decomposed gas; and
27: a wall of the catalytic decomposition portion.

10 BEST MODE FOR CARRYING OUT THE INVENTION

Now, the invention will be described in detail.

The invention aims at preventing global warming by exothermally decomposing N_2O in an N_2O -containing gas and thus considerably reducing the release of N_2O gas, which
15 causes global warming, into the atmosphere. With respect to the decomposition of N_2O , there have been known reactions represented by the following formulae (1) and (2).



20 The reaction of the above formula (1) is an exothermic reaction by which 19.5 kcal/mol of heat is generated, while the reaction represented by the above formula (2) is an endothermic reaction consuming 1.96 kcal/mol of heat. In the case where the heat generated by the reaction of the

formula (1) exceeds the heat absorbed in the reaction of the formula (2), then the whole reaction of the decomposition of N_2O is an exothermic decomposition. The term "decomposition of N_2O " as used herein means this exothermic decomposition of
5 N_2O .

According to the invention, in a process of decomposing N_2O by thermally decomposing or catalytically decomposing N_2O in an N_2O -containing gas to be treated, the N_2O -containing gas stream to be treated is divided in
10 portions. Then a portion thereof is preheated to thereby exothermally decompose N_2O in the gas stream thereby giving a hot gas stream. Next, the remainder of the divided gas stream to be treated is supplied into the hot gas stream, and thus N_2O is continuously decomposed.

15 It is preferable in the invention that the N_2O -containing gas to be treated is a feedstock gas from the process for producing adipic acid by the nitric acid-oxidation method, though the invention is not restricted thereto. Moreover, it may contain, in addition to N_2O , air,
20 nitrogen, oxygen, moisture, carbon dioxide, carbon monoxide, nitrogen monoxide, nitrogen dioxide, hydrocarbons and the like.

The term "thermal decomposition of N_2O " as used herein means conversion of N_2O into N_2 , O_2 , NO , NO_2 , etc. by
25 exothermally decomposing N_2O in an N_2O -containing gas without

using any catalyst. In the invention, the N_2O -containing gas stream (i.e., the gas to be treated) is divided into plural gas streams and a portion thereof is preheated.

In this step, it is preferable that the preheating is
5 performed at such a temperature as to substantially allow the initiation of the thermal decomposition of N_2O . In the invention, the preferred preheating temperature is from about 750°C to about 950°C , inclusive. When the preheating temperature is lower than about 750°C , it is feared that N_2O
10 cannot be thermally decomposed at a practical reaction speed when the preheated gas stream is supplied into the N_2O thermal decomposition zone. When the preheating temperature exceeds about 950°C , on the other hand, the substantial thermal decomposition of N_2O starts and thus the advantage of
15 the invention of preheating cannot be achieved. Depending on this preheating temperature, the retention time of the gas to be treated, which is introduced into the thermal decomposition zone close to the preheating zone can be appropriately determined.

20 A portion of the preheated gas stream to be treated as described above is introduced into the N_2O thermal decomposition zone adjacent to the preheating zone. In this thermal decomposition zone, the self-thermal decomposition of N_2O exothermally starts and thus N_2O is thermally
25 decomposed. Due to the decomposition heat of N_2O , the

temperature of the gas stream is further elevated in the flow direction of the supplied gas stream, thereby forming a hot gas stream at a high temperature.

In the invention, the remainder of the divided gas stream to be treated is supplied into this hot gas stream. Thus, the temperature of the remainder of the gas to be treated is elevated to the thermal decomposition temperature of N_2O or above and the N_2O contained in the gas to be treated, which has been supplied into the hot gas stream, is continuously thermally decomposed.

It is still preferable to supply the remainder of the divided gas stream to be treated into plural positions (preferably two to five positions) in the flow direction of the above-described hot gas stream. According to the invention, the decomposition heat generated by the self-thermal decomposition of N_2O in the gas stream to be treated, which has been formerly supplied, can be successively and efficiently utilized in elevating the temperature of the gas stream to be treated which is supplied later. It is also possible to control the temperature of the atmosphere in the N_2O thermal decomposition system to an optimum level ranging from a relatively low temperature zone (about $1000^{\circ}C$) to a moderate temperature zone (about $1300^{\circ}C$). With an increase in the number of the divided gas streams to be treated, the amount of the fuel to be fed thereinto can be lessened and,

in its turn, the energy cost required in maintaining the N_2O decomposition reaction at a definite temperature can be reduced.

In the thermal decomposition of N_2O in the N_2O -
5 containing gas according to the invention, it is preferable that the gas stream to be introduced into the N_2O thermal decomposition zone is in a plug flow state. Thus, the decomposition heat generated by the thermal decomposition of N_2O in the gas stream to be treated can be more efficiently
10 utilized in elevating the temperature of the gas stream to be treated supplied into the N_2O thermal decomposition zone later. When the gas stream is in the plug flow state, the temperature of the hot gas stream in the N_2O thermal decomposition zone can be more exactly controlled and,
15 therefore, the remainder of the divided gas stream to be treated can be supplied to desired positions of the hot gas stream in the desired temperature zone.

When the gas stream to be treated is divided and a portion of the thus obtained gas stream is preheated in the
20 invention, the preheating method is not particularly restricted and any well-known method for heating a gas is usable therefor. For example, use may be made of the indirect heating systems such as the pipe heating wherein a pipe which the gas stream to be treated flow through and is
25 externally heated, the gas heat medium heating method

wherein the gas stream to be treated is fed into a combustion gas and is heated, the direct heating systems such as the partial combustion heating method wherein a fuel and/or a portion of the gas stream to be treated is

5 subjected to combustion and the gas stream to be treated is heated by the thus generated heat, the heating system with the use of an electric furnace, the microwave heating system, and the like.

Among the preheating methods as cited above, it is
10 particularly preferred in the invention to employ the direct heating system, since the gas stream can be easily and economically heated to a desired temperature thereby, as compared to other heating systems.

Now, the direct heating system will be described more
15 particularly. The partial combustion heating method can be performed by, for example, by reacting N_2O in the gas stream to be treated directly with a fuel and the gas stream to be treated is heated by the reaction heat thus generated. The gas heat medium heating method can be performed by, for
20 example, mixing a hot gas formed by the combustion of a fuel with the gas stream to be treated.

The above-described fuel in the invention means a substance undergoing combustion in the presence of a combustion-supporting gas. Use may be widely made therefor
25 of gas fuels, liquid fuels and solid fuels. Examples of the

gas fuels include natural gas, hydrocarbon gas (methane, propane, butane, etc.), hydrogen gas, ammonia and hydrazine. Examples of the liquid fuels include hydrocarbons (gasoline, kerosine, light oil, etc.) and alcohols (methanol, ethanol, etc.). Among gas fuels, it is particularly preferred to use hydrogen gas, since it is superior to other fuels in being free from the generation of carbon dioxide and little affecting the environment. Among the liquid fuels, it is particularly preferred in the invention to use methanol which is inexpensive and easy to handle. Examples of the combustion-supporting gas include air, oxygen and nitrous oxide.

Next, the apparatus of the invention for preventing global warming by thermally decomposing N_2O is now illustrated.

The apparatus of the invention for preventing global warming through the thermal decomposition of N_2O , That is, the N_2O thermal decomposition apparatus comprising:

(a) an introduction portion for the N_2O -containing gas to be treated;

(b) a preheating portion for the thus introduced gas to be treated;

(c) a thermal decomposition portion adjacent to the preheating portion, said thermal decomposition portion having means for supplying the gas to be treated, said

supplying means being provided at one or more positions in the flow direction of a gas stream; and

(d) a discharging portion for the thermally decomposed gas.

5 The thermal decomposition portion is a zone wherein N_2O is thermally decomposed.

Fig. 1 is a schematic view illustrating the N_2O thermal decomposition apparatus according to the invention. In Fig. 1, 1 stands for an introduction portion for the N_2O -
10 containing gas; 2 stands for a preheating portion for the thus introduced gas; 3 stands for a preheated gas-receiving portion; 4 stands for a supplying portion for the N_2O -containing gas; 5 stands for a N_2O thermal decomposition portion wherein the reaction of thermally decomposing N_2O is
15 carried out; 6 stands for a discharging portion for the thermally decomposed gas; and 7 stands for the wall of the thermal decomposition reactor (furnace).

A portion of the gas stream to be treated is supplied from the gas introduction portion 1 to the preheating
20 portion 2 where it is uniformly heated to a temperature at which the thermal decomposition of N_2O can start. When the preheating is performed by the direct heating system as described above, the preheating portion may be provided with a portion of introducing a fuel and a combustion-supporting
25 gas (not shown). In this case, it is favorable that the

preheating portion is provided therein with a fuel combustion means such as a combustion burner.

The thus preheated N_2O -containing gas is introduced from the preheated gas reception portion 3 into the thermal decomposition portion 5. This thermal decomposition portion 5 is located adjacent to the preheating portion 2 or connected thereto via a preheated gas reception portion 3. In the thermal decomposition portion 5, N_2O is thermally decomposed at the N_2O thermal decomposition temperature or above and a hot gas stream is formed due to the N_2O decomposition heat thus generated.

In the thermal decomposition portion 5, the hot gas stream thus formed is mixed with the remainder of the divided gas stream to be treated, which is supplied from the gas-supplying portion 4. In the case of Fig. 1, three portions 4 are provided for supplying the N_2O -containing gas. It is particularly preferable in the invention that there are two to five supplying portions (i.e., the number of stages supplying the gas stream to be treated) in the portion 5 for thermally decomposing the N_2O -containing gas.

It is preferable that the portion 4 for supplying the N_2O -containing gas is provided with a means for supplying the gas by which the flow condition of the hot gas stream in the thermal decomposition portion 5 can be controlled. For example, one or more of the gas-supplying portions

comprising one or more nozzles by which the flow direction and speed of the gas stream to be treated can be controlled. By providing such a means, the gas stream to be treated, the flow direction and speed of which have been appropriately
5 controlled, can be introduced into the thermal decomposition portion and thus flow conditions of the hot gas stream in the thermal decomposition zone can be controlled.

The above-described hot gas stream is combined and mixed with the gas supplied from a first gas-supplying
10 portion 4. Thus, the temperature thereof is temporarily lowered. The temperature of the combined gas stream is elevated as the thermal decomposition of N_2O proceeds and thus a hot gas stream is formed again. This hot gas stream is combined and mixed with the gas stream to be treated
15 supplied from a second gas-supplying portion 4. Thus, N_2O contained in the gas stream to be treated supplied from the gas-supplying portions 4 is thermally decomposed successively. After the completion of the thermal decomposition at a high conversion ratio, the gas is
20 discharged from the thermal decomposition reaction apparatus via the thermally decomposed gas-discharging portion 6.

It is preferable in the invention that the thermal decomposition of N_2O stably proceeds as a chain reaction. To achieve this object, it is preferable that the gas stream in
25 the thermal decomposition portion 5 is substantially in the

form of a plug flow. If necessary, the thermal decomposition portion may be provided with a means for controlling the gas stream such as a barrier, a baffle plate, a porous plate, a packing, etc. It is preferable in the invention that the thermal decomposition portion 5 is provided with a porous plate and/or a multi-pipe nozzle (not shown) in front of and/or at the back of the gas-supplying portion 4 so as to make the gas stream into a plug flow.

It is also preferable in the invention that the gas stream is controlled so that the hot gas stream flowing toward the means for supplying the N_2O -containing gas flows as a rotary stream. To make the hot gas stream into a rotary stream, the thermal decomposition portion 5 may be provided with a means for controlling the gas stream such as a barrier, a baffle plate, a porous plate, a packing, etc. To control the hot gas stream thereby giving a rotary stream, it is preferable that the gas-supplying portion 4 is provided with a gas-supplying means comprising one or more nozzles by which the flow direction and speed of the gas stream to be treated can be controlled.

In the invention, it is preferable that the temperature of the gas stream at the outlet of the thermal decomposition apparatus (the outlet of the portion 6 for discharging the thermally decomposed gas) is controlled at a definite level. Thus, the instruments can be continuously

operated over a long period of time. The outlet temperature varies depending on the temperature of the supplied gas to be treated, the N_2O concentration in the gas stream to be treated, the speed of supplying the gas stream to be treated, 5 the amount of the fuel fed into the preheating portion, etc. To maintain the gas stream at a constant temperature at the outlet of the thermal decomposition apparatus, it is therefore needed to control these factors. In the invention, it is preferable to maintain the gas stream at the outlet of 10 the thermal decomposition apparatus at a constant temperature by regulating the amount of the fuel fed into the preheating portion. Thus, the decomposition temperature can be maintained in a more stable state.

It is preferable in the invention to maintain the 15 supplying temperature of the gas stream to be treated at less than about $750^\circ C$. The temperature of the gas flowing out from the thermal decomposition apparatus after the completion of the reaction is not particularly restricted but can be controlled within a wide temperature range from a 20 relatively low temperature region (about $1000^\circ C$) to a moderate temperature region (about $1300^\circ C$). If necessary, use may be made of a temperature of $1500^\circ C$ or higher.

The term "catalytic decomposition of N_2O " as used herein means that N_2O in an N_2O -containing gas is 25 exothermally decomposed with the use of a catalyst (by

bringing into contact with a catalyst) into N_2 and O_2 . The invention provides a method for preventing global warming by catalytically decomposing N_2O and an apparatus therefor. Compared with the thermal decomposition method as described
5 above, the catalytic decomposition is performed at a relatively low temperature in this method. Thus, little, if any, NO and NO_2 are generated thereby.

As described above, the N_2O -containing gas to be treated in the invention may contain, in addition to N_2O , air,
10 nitrogen, oxygen, moisture, carbon dioxide, carbon monoxide, nitrogen monoxide, nitrogen dioxide, hydrocarbons and the like. In the case where it is feared that the catalyst might be poisoned by some components contained in the gas to be treated under certain temperature conditions or in the
15 case where it is feared that some unfavorable reaction might occur, it is preferable in the catalytic decomposition method to preliminarily eliminate these components before supplying into the catalytic bed. When the N_2O -containing gas also contains nitrogen monoxide and nitrogen dioxide
20 poisoning a palladium catalyst, etc., for example, it is preferable that these components are preliminarily oxidized and absorbed in an absorption column and the mist moisture is eliminated before using as the gas to be treated in the invention. Therefore, the gas to be treated in the
25 invention may be a gas from which other components have been



eliminated before supplying into the N_2O decomposition apparatus or a gas which has been mixed with other gases, etc.

The present invention is not restricted by the kind of the catalyst for decomposing N_2O . To achieve the objects of the invention, however, it is preferable to use those containing copper, nickel, iron, cobalt, palladium, or oxides or complex oxides of these metals. It is preferable that the catalyst is carried on a carrier. As the carrier, those having appropriate pores and showing a high heat stability may be selected. Preferred examples of the catalyst carrier to be used in the invention include oxides and complex oxides of aluminum, silica, titanium, magnesium and zirconium. As aluminum oxides among these carriers, it is still preferable to use α -alumina, β -alumina or γ -alumina. As the silica/alumina complex oxides, it is still preferable to use zeolite such as ZSM5. As the titanium oxides, it is still preferable to use those of the anatase and rutile types. It is also preferable to use zirconia which has a high heat resistance. Furthermore, it is preferable to use a carrier obtained by mixing these carriers as cited above. In the invention, the catalyst may be carried on the carrier by a well-known method. For example, the carrier is impregnated with an aqueous solution of a water-soluble salt of a metal catalyst and then baked.

A catalytic system which is particularly preferred in the invention is one having an N_2O catalytic decomposition temperature of from 200 to 800°C, still more preferably from 300 to 700°C.

5 In a catalytic system having a catalytic decomposition temperature higher than the temperature as specified above, the decomposition heat generated in association with the catalytic decomposition of N_2O can be more efficiently utilized in the subsequent N_2O catalytic decomposition by
10 applying the method of catalytically decomposing N_2O according to the invention.

 In the invention, the gas to be treated is divided into gas streams. Then, a portion of the divided gas streams (i.e., one of plural gas streams) is preheated and
15 introduced into an N_2O catalytic decomposition zone wherein N_2O in the gas to be treated is catalytically decomposed to form a hot gas stream. Next, the remainder of the divided gas to be treated is supplied into this hot gas stream.
 Thus, the temperature of the remainder of the gas streams to
20 be treated can be elevated to a temperature higher than the temperature at which the catalytic decomposition reaction of N_2O starts. Then the gas stream is passed through a catalytic bed so as to catalytically decompose N_2O in the gas to be treated continuously. The catalytic bed serves as the
25 catalytic decomposition zone of N_2O .

It is preferable that the remainder of the divided gas to be treated is supplied to plural positions in the flow direction of the above-described hot gas stream. The thus supplied gas to be treated is mixed with the above-described hot gas stream at each of the plural positions as described above and then brought into contact with the catalytic bed located at the back of each supplying position. According to the invention, therefore, N_2O in the gas to be treated, which has been formerly supplied, is catalytically decomposed and the decomposition heat thus generated can be efficiently and successively utilized in elevating the temperature of the gas stream to be treated, which is supplied thereafter. It is particularly preferred that two to four positions for supplying the divided gas stream to be treated as described above are formed. With an increase in the number of the divided gas streams to be treated, the amount of the diluent gas to be employed can be lessened and, in its turn, the energy cost required in maintaining the N_2O decomposition reaction at a definite temperature can be reduced.

In the invention, the gas stream to be treated is divided and introduced into the catalytic decomposition apparatus via plural inlets as described above. In this step, the division ratio of the gas to be treated may be appropriately determined by taking into consideration the N_2O

concentration in the gas to be treated, the N_2O decomposition temperature of the catalyst system employed and the treating capability of the catalytic bed employed. To improve the effect achieved by supplying the gas to be treated in portions, it is still preferable that, when $Q \text{ Nm}^3/\text{H}$ of the gas to be treated is introduced into the anterior catalytic bed, then the amount of the gas to be introduced into the posterior catalytic bed adjacent thereto is controlled to 1.1 to $3.0Q \text{ Nm}^3/\text{H}$, still preferably 1.2 to $2.7Q \text{ Nm}^3/\text{H}$. With respect to the catalytic bed volume, similarly, when catalytic beds have the same catalytic system and the same inlet and outlet temperatures and the volume of the anterior catalytic bed is $V \text{ m}^3$, then it is preferable that the volume of the posterior catalytic bed is controlled to 1.1 to $3.0 V \text{ m}^3$, still preferably form 1.2 to $2.7 V \text{ m}^3$.

As described above, the gas to be treated is divided and a portion thereof is preheated in the invention. The preheating method is not particularly restricted in the catalytic decomposition method too but any well-known method for heating a gas is usable therefor. For example, use may be made of the indirect heating systems such as the pipe heating wherein a pipe through which the gas stream to be treated flow is externally heated, the gas heat medium heating method wherein the gas stream to be treated is fed into a combustion gas and heated, the direct heating systems

such as the partial combustion heating method wherein a fuel and/or a portion of the gas stream to be treated is subjected to combustion and the gas stream to be treated is heated by the thus generated heat, the heating system with the use of an electric furnace, the microwave heating system, and the like. It is also possible to use a preheating method wherein a combustible gas (for example, hydrogen gas) is reacted with an oxidative gas (for example, oxygen gas) by using a catalyst and the obtained reaction mixture is mixed with the gas to be treated. Among the preheating methods as cited above, it is particularly preferred in the invention to employ the method wherein hydrogen gas is reacted with oxygen in the air with the use of a noble metal catalyst and then the steam thus generated is used as a preheat source, since preheating can be started from a low temperature and the preheating temperature can be controlled over a broad scope in this method.

In the method of catalytically decomposing N_2O according to the invention, a diluent gas can be used if needed. This diluent gas may be used in the catalytic decomposition system without being restricted to any definite position. It may be used in the case where the temperature of the gas stream is to be controlled at a definite level. That is to say, when the gas to be treated contains N_2O only at a low concentration and thus there is no

fear of an unnecessary increase in the temperature due to the generation of the decomposition heat, for example, then no diluent gas is needed. When N_2O is contained at a high concentration, on the contrary, or the catalytic system

5 employed is available within only a specific narrow reaction temperature range, then it is preferable to use a diluent gas so as to prevent an increase in the temperature of the gas stream after the decomposition or to control the temperature of the gas stream within the specific range.

10 When a diluent gas is employed in the invention, it is preferable that the diluent gas is supplied from the same position from which the gas to be treated is supplied. The diluent gas may be selected from those which are free from catalyst-poisoning substances or N_2O decomposition reaction
15 inhibitors. Particularly preferred examples of the diluent gas to be used in the invention include air and/or the N_2O -containing gas after the catalytic decomposition of N_2O , since these gases are inexpensive, readily available and easy to handle.

20 The catalytic decomposition of N_2O , which is the subject of the invention, is an irreversible reaction by which nitrogen and oxygen are generated and thus the gas volume is increased. It is therefore considered advantageous to elevate the operation pressure of the
25 catalytic bed so as to increase the amount of the gas to be

treated and reduce the scale of the equipment. However, it is said that pure N_2O gas would undergo an explosive reaction under elevated pressure. Therefore, the inventors consider that N_2O might undergo an explosive reaction under an
5 excessively elevated pressure even in a mixed gas system. Accordingly, it is preferable in the invention to control the operation pressure of the catalytic bed to from atmospheric pressure to 0.5 MPa, still more preferably from atmospheric pressure to 0.3 MPa. The same applies to the
10 pressure in the thermal decomposition method as described above.

Either the thermal decomposition method or the catalytic decomposition method according to the invention is more appropriately applicable to an N_2O -containing gas having
15 an N_2O concentration of 60% by volume or less. It is still more preferable that the N_2O concentration in the gas to be treated ranges from 2 to 50% by volume. When the N_2O concentration in the gas to be treated exceeds 60% by volume, there arises a fear of the explosive decomposition behavior
20 sown by pure N_2O gas.

In the invention, the N_2O concentration of the gas stream at the inlet of each catalytic bed may be appropriately determined so as to successfully achieve the objects of the invention. The N_2O concentration preferably
25 ranges from 2 to 20% by volume, still more preferably from 5

to 15% by volume. When the N_2O concentration of the gas at the inlet of the catalytic bed is less than 2% by volume, the heat generated by the catalytic decomposition can result in only a small increase in the temperature at the outlet of
5 the catalytic bed. In this case, it is feared that the obtained gas stream cannot be efficiently and successively utilized in elevating the temperature of the gas stream to be treated, which is supplied thereafter. When the N_2O concentration of the gas at the inlet of each catalytic bed
10 exceeds 20% by volume, on the other hand, the temperature at the outlet of the catalytic bed is excessively elevated due to the heat generated by the catalytic decomposition. In this case, the thermal deterioration of the catalyst is accelerated and, furthermore, there arise a fear that the
15 equipment will become damaged.

Next, the apparatus of the invention for preventing global warming by catalytically decomposing N_2O , that is, an N_2O catalytic decomposition apparatus will become illustrated.

The N_2O catalytic decomposition apparatus of the
20 invention is an apparatus wherein an N_2O -containing gas to be treated is brought into contact with a catalytic bed to thereby catalytically decompose N_2O . This apparatus comprising:

(a) a introduction portion for the gas to be treated
25 and/or a diluent gas;

(b) a mixing portion for the gas to be treated and/or the diluent gas;

(c) a mixing portion having one or more means for supplying the gas to be treated and/or the diluent gas at
5 different positions in the longitudinal direction of the apparatus;

(d) a catalytic decomposition portion having the catalytic bed; and

(e) a discharging portion for the catalytically
10 decomposed gas.

In another embodiment, the N_2O catalytic decomposition apparatus of the invention is an apparatus by which N_2O in an N_2O -containing gas is catalytically decomposed. This apparatus comprises:

15 a device which comprises:

(a) a introduction portion for the gas to be treated and/or a diluent gas;

(b) a mixing portion for the gas to be treated and/or the diluent gas;

20 (c) a catalytic decomposition portion having a catalytic bed; and

(d) a discharging portion for the catalytically decomposed gas; and

one or more devices each of which comprises:

(e) an introduction portion for the discharged gas having been catalytically decomposed, the gas to be treated and/or a diluent gas;

(f) a mixing portion for the discharged gas having
5 been catalytically decomposed, the gas to be treated and/or the diluent gas;

(g) a catalytic decomposition portion having a catalytic bed; and

(h) a discharging portion for the catalytically
10 decomposed gas.

In each case, the catalytic bed serves as the above-mentioned N_2O decomposition zone.

In the invention, it is an effective means for regulating the N_2O decomposition reaction, to preheat the gas
15 to be treated and/or the diluent gas. Therefore, it is preferable that the mixing portion for the gas to be treated and/or the diluent gas is also provided with a part in which the gas to be treated and/or the diluent gas are preheated.

Figs. 4 and 5 are schematic views illustrating the N_2O
20 catalytic decomposition apparatus of the invention.

As Fig. 4 shows, the catalytic decomposition apparatus according to the invention may have plural catalytic beds in a single decomposition apparatus. Alternatively, the decomposition apparatus may comprise independent catalytic
25 beds connected to each other, as Fig. 5 shows.

In Figs. 4 and 5, 17 stands for an introduction portion for the gas to be treated; 18 stands for an introduction portion for a diluent gas; 19 stands for a preheating portion for the introduced gas; 20 stands for a preheated gas-receiving portion; 21 stands for a space; 22 stands for a catalytic decomposition portion; 23 stands for a mixing portion; 24 stands for a supplying portion for the gas to be treated; 25 stands for a supplying portion for the diluent gas; 26 stands for a discharging portion for the catalytically decomposed gas; and 27 stand for the wall of the catalytic decomposition reactor.

In Fig. 4, a portion of the gas to be treated and the diluent gas are introduced, via the gas introducing portions 17 and 18, into the preheating portion 19 where these gases are uniformly preheated to the initiation temperature of the N_2O catalytic decomposition reaction with the use of the catalyst. The N_2O -containing gas thus preheated is transported to the preheated gas receiving portion 20 and then to the catalytic decomposition portion 22. The catalytic decomposition portion 22 is located adjacent to the preheating portion 19 or connected thereto via the preheated gas-receiving portion 20. In this catalytic decomposition portion 22, N_2O is catalytically decomposed and a hot gas stream is formed by the N_2O decomposition heat thus generated. In the mixing portion 23, the hot gas stream

formed above is mixed with the remainder of the divided gas to be treated, which is supplied from the supplying portion for the gas to be treated, and the diluent gas, which is supplied from the supplying portion for the diluent gas, to
5 thereby attain a definite concentration and a definite temperature. Subsequently, N_2O is catalytically decomposed in the catalytic decomposition portion 22. In the case as shown in Fig. 4, two supplying portions 24 for the gas to be treated are provided. In the invention, it is particularly
10 preferred that the catalytic decomposition portion 22 is provided with two to four portions of supplying the N_2O -containing gas. In the case shown in Fig. 4, similarly, two portions 25 of supplying the diluent gas are provided. In the invention, it is particularly preferred to provide two
15 to four portions of supplying the diluent gas.

Subsequently, N_2O contained in the gas to be treated, which has been supplied from the supplying portion 24 for the gas to be treated, is successively decomposed with the catalyst. Finally, the catalytically decomposed gas is
20 discharged from the catalytic decomposition apparatus via the portion 26 for discharging the catalytically decomposed gas.

Although the above description has been made by reference to Fig. 4, the same applies substantially to the
25 apparatus shown in Fig. 5.

To stably perform the catalytic decomposition reaction of N_2O with the use of the catalyst, it is preferable in the invention that the apparatus is provided with a porous plate and/or a contraction portion (not shown) in front of and/or
5 at the back of the mixing portion 23 so as to give a uniform gas stream after mixing. It is also possible to insert a structure capable of mixing gases (a baffle plate, a packing, etc.) into the mixing portion 23. To make the hot gas stream in the reactor a rotary stream, it is preferable that
10 the portion 24 of supplying the N_2O -containing gas and the portion 25 of supplying the diluent gas are provided each a means of supplying gas comprising one or more nozzles by which the flow direction and speed of the supplied gas can be controlled.

15 The methods for controlling the gas flow and gas temperature to be used in the invention are not particularly restricted. However, it is favorable that the gas to be treated is supplied to each catalytic bed in an amount determined depending on the amount of the catalyst packed
20 into the corresponding bed so that the gas streams have substantially the same N_2O concentration and the same gas temperature at the inlet of the respective catalytic bed. Thus, the inlet and outlet temperatures of each catalytic bed can be controlled to the desired level.

In the invention, the gas to be treated is divided and a portion thereof is supplied into a first catalytic decomposition portion. Thus, the subsequent catalytic decomposition and thereafter (i.e., the catalytic decomposition at the second stage and thereafter) can be performed by heating the gas to be treated up to the reaction initiation temperature, either totally or partly, with the use of the heat obtained by mixing the gas to be treated with the hot gas supplied from the prior catalytic decomposition portion. Accordingly, the size of a heat exchanger of the gas to be treated required in the reaction system can be reduced. According to the invention, the diluent gas may be supplied, preferably in the form of a gas mixture with the gas to be treated, into each of the catalytic decomposition portions to thereby control the temperature over the whole catalytic decomposition zone. Thus, the temperature of each catalytic bed can be easily controlled and the total amount of the diluent gas can be reduced. As a result, a smaller device for feeding the diluent gas can be used and thus the operation cost and the investment in equipment can be remarkably reduced.

From the viewpoint of efficiently utilizing the heat maintained by the decomposed gas stream, it is preferable in the invention that the gas flowing out from the N_2O decomposition apparatus after the completion of the reaction

is introduced into a boiler having a common structure and the reaction heat is recovered as steam. It is also preferable that the gas to be treated is subjected to heat-exchange with the gas after the completion of the reaction, which has been cooled by the boiler, thereby heating the gas to be treated, which is supplied into the reaction apparatus of the invention.

It is also preferable that nitrogen oxides (NO , NO_2) contained in the gas flowing out from the reactor after the completion of the thermal decomposition are brought into contact with water and air to thereby recover NO and NO_2 as an aqueous nitric acid solution. As described above, it is preferable that the gas to be treated in the invention (i.e., the N_2O -containing gas) is a feedstock gas from the process of producing adipic acid by the nitric acid-oxidation method. When nitrous oxide discharged from an adipic acid plant is to be thermally decomposed by the method of the invention, it is preferable that the recovered aqueous nitric acid solution as described above is reused in the production of adipic acid. When it is unnecessary to reuse the NO and NO_2 thus formed, it is preferable that NO and NO_2 contained in the discharged gas flowing out from the above-described boiler or heat exchanger are reduced in the presence of a catalyst. The reduction may be carried out by, for example, reacting the discharged gas containing NO and NO_2 with NH_3 in

the presence of a catalyst to thereby convert NO and NO₂ into N₂ and H₂O. Thus, the gases formed after the completion of the thermal decomposition can be made causing no pollution.

As the above description clearly indicates, the method
5 for preventing global warming and the apparatus therefor according to the invention are preferably applicable to an N₂O-containing gas, in particular, an N₂O-containing gas generated from a chemical plant with the use of nitric acid as an oxidizing agent and an N₂O-containing feedstock gas.
10 The method and apparatus of the invention are preferably usable, in particular, in the process for producing adipic acid.

Accordingly, the invention is particularly preferred to be applicable to a process for producing adipic acid with
15 extremely reduced release of N₂O causing global warming, which process involves:

(1) a nitric acid-oxidation step in which cyclohexanol and/or cyclohexanone are oxidized with nitric acid to form adipic acid;

20 (2) a nitric acid recovery step in which HNO₃ is recovered from an N₂O-containing gas caused in the nitric acid-oxidation step;

(3) an N₂O decomposition step in which the remaining N₂O-containing gas stream to be treated, from which HNO₃ has
25 been recovered, is divided, a portion thereof is preheated

to exothermally decompose N_2O in the gas stream to form a hot gas stream, and the remainder of the divided gas stream to be treated is supplied into said hot gas stream to thereby continuously decompose N_2O ; and

- 5 (4) an N_2O decomposition heat recovery step in which the N_2O decomposition heat emitted from the N_2O decomposition step is recovered.

EXAMPLES

The present invention will be described in greater
10 detail by reference to the following Examples, but the invention should not be construed as being limited thereto.

Example 1

N_2O in an N_2O -containing gas (a feedstock gas) to be treated, which had been discharged from an adipic acid plant
15 and had the composition and flow rate as given in Table 1 was thermally decomposed.

Fig. 2 is a schematic view of the thermal decomposition apparatus.

A thermal decomposition reaction furnace (thermal
20 decomposition portion 8) employed was one made of heat resistant bricks and having a cylindrical shape with 450 mm in inner diameter and 4750 mm in length. The wall thickness thereof was 300 mm. The inside of the furnace was divided in series into four thermal decomposition chambers (N_2O

decomposition zones), having a space of almost the same volume, with porous plates made of heat resistant bricks (thickness: 200 mm). That is, the number of the supplying stage of the gas to be treated was four. The gas to be
5 treated, which had been divided and preheated was fed into the first reaction chamber, while the remainder of the divided gas to be treated was introduced into the second, third and fourth reaction chambers. The second, third and fourth reaction chambers were each provided with an inlet of
10 the gas to be treated immediately after the hot gas stream was fed thereinto. Further, the second, third and fourth chambers are provided each with a baffle plate made of heat resistant bricks (thickness: 200 mm, height: 300 mm) at the back of the above-described inlet of the gas to be treated
15 at a distance of 150 mm from the porous plate from which the hot gas stream was fed. A preheating portion, which was made of heat resistant bricks similar to the thermal decomposition portion, had a cylindrical shape with a space of 200 mm in inner diameter and 500 mm in length. It was
20 provided with an inlet of the gas to be treated at one end while the other end was connected to the thermal decomposition portion. Into this preheating portion, hydrogen corresponding to 12 kcal per 1 Nm³ of the gas to be treated was introduced with air at a rate of 1.3 Nm³/hr.
25 Then it was subjected to combustion in the preheating

portion and uniformly mixed with the gas to be treated introduced into the preheating portion at 17.9 Nm³/hr. The temperature of the gas to be treated was adjusted to 550°C. The temperature of the gas stream introduced from the preheating portion to the first reaction chamber was 830°C. The gas to be treated at 550°C was supplied into the second, third and fourth reaction chambers respectively at flow rates of 34.1 Nm³/hr, 72.6 Nm³/hr and 155.4 Nm³/hr. The mixtures of the hot gas stream with the gas to be treated at the inlets of the second, third and fourth reaction chambers had each a temperature of 830°C. The pressure within the furnace was 1.25 kg/cm² (gauge pressure).

The temperature of the gas stream discharged from the thermal decomposition reaction furnace was 1163°C and N₂O contained in the supplied gas to be treated had been thus thermally decomposed at a ratio of 99% or more.

Example 2

N₂O contained in a gas to be treated discharged from an adipic acid plant was thermally decomposed as in Example 1 but the temperature of the supplied gas to be treated being 300°C; the flow rate of hydrogen supplied into the preheating portion being 7.2 Nm³/hr; and the flow rates of the gas to be treated supplied into the preheating portion and the second, third and fourth reaction chambers being respectively 55.7 Nm³/hr, 60.0 Nm³/hr, 72.9 Nm³/hr and 91.4 Nm³/hr.

The pressure within the furnace was 1.25 kg/cm². The gas stream mixtures in the preheating portion and at the inlets of the second, third and fourth reaction chambers had each a temperature of 830°C. The temperature of the gas stream discharged from the thermal decomposition reaction furnace was 1027°C and N₂O contained in the supplied gas to be treated had been thus thermally decomposed at a ratio of 99% or more.

Example 3

10 N₂O contained in a gas to be treated was thermally decomposed as in Example 1 but the temperature of the supplied gas to be treated being 700°C; the flow rate of hydrogen supplied into the preheating portion being 0.1 Nm³/hr; and the flow rates of the gas to be treated supplied
15 into the preheating portion and the second, third and fourth reaction chambers being respectively 3 Nm³/hr, 12.0 Nm³/hr, 50.6 Nm³/hr and 214.4 Nm³/hr.

The pressure within the furnace was 1.25 kg/cm². The gas stream mixtures in the preheating portion and at the
20 inlets of the second, third and fourth reaction chambers had each a temperature of 830°C. The temperature of the gas stream discharged from the thermal decomposition reaction furnace was 1263°C and N₂O contained in the supplied gas to be treated had been thus thermally decomposed at a ratio of
25 99%.

Example 4

N_2O contained in a gas to be treated was thermally decomposed as in Example 1 but the flow rate of hydrogen supplied into the preheating portion being $1.2 \text{ Nm}^3/\text{hr}$; and
5 the flow rates of the gas to be treated supplied into the preheating portion and the second, third and fourth reaction chambers being respectively $19.7 \text{ Nm}^3/\text{hr}$, $36.1 \text{ Nm}^3/\text{hr}$, $73.4 \text{ Nm}^3/\text{hr}$ and $150.8 \text{ Nm}^3/\text{hr}$.

The pressure within the furnace was 1.25 kg/cm^2 . The
10 gas stream mixtures in the preheating portion and at the inlets of the second, third and fourth reaction chambers had each a temperature of 800°C . The temperature of the gas stream discharged from the thermal decomposition reaction furnace was 1131°C and N_2O contained in the supplied gas to
15 be treated had been thus thermally decomposed at a ratio of 99% or more.

Example 5

The inside of the thermal decomposition reaction furnace as in Example 1 was divided in series into first,
20 second and third chambers, having a space of almost the same volume, with porous plates made of heat resistant bricks (thickness: 200 mm). The inlets of the gas to be treated and the baffle plates were arranged as in Example 1. The preheating portion had the same volume as in Example 1.

25 N_2O contained in a gas to be treated was thermally

decomposed as in Example 1 but the flow rate of hydrogen supplied into the preheating portion being 2.9 Nm³/hr; and the flow rates of the gas to be treated supplied into the preheating portion and the second and third reaction chambers being respectively 40.4 Nm³/hr, 76.5 Nm³/hr and 163.1 Nm³/hr.

The pressure within the furnace was 1.25 kg/cm². The temperature of the gas stream discharged from the thermal decomposition reaction furnace was 1173°C and N₂O contained in the supplied gas to be treated had been thus thermally decomposed at a ratio of 99% or more.

Example 6

The inside of the thermal decomposition reaction furnace as in Example 1 was divided in series into first and second chambers, having a space of almost the same volume, with a porous plate made of heat resistant bricks (thickness: 200 mm). The inlets of the gas to be treated and the baffle plates were arranged as in Example 1. The preheating portion had the same volume as in Example 1. N₂O contained in a gas to be treated was thermally decomposed as in Example 1 but the flow rate of hydrogen supplied into the preheating portion being 6.9 Nm³/hr; and the flow rates of the gas to be treated supplied into the preheating portion and the second reaction chamber being respectively 96.6 Nm³/hr and 183.4 Nm³/hr.



The pressure within the furnace was 1.25 kg/cm². The gas stream mixtures in the preheating portion and at the inlet of the second reaction chamber had each a temperature of 830°C. The temperature of the gas stream discharged from the thermal decomposition reaction furnace was 1200°C and N₂O contained in the supplied gas to be treated had been thus thermally decomposed at a ratio of 99% or more.

Example 7

N₂O in an N₂O-containing gas to be treated, which had been discharged from an adipic acid plant and had the composition and flow rate as given in Table 1 was thermally decomposed.

Fig. 3 is a schematic view of the thermal decomposition apparatus.

A thermal decomposition reaction furnace (thermal decomposition portion) employed was one made of heat resistant bricks and having a cylindrical shape with 400 mm in inner diameter and 4300 mm in length. The wall thickness thereof was 300 mm. The inside of the furnace was divided in series into four thermal decomposition chambers (N₂O decomposition zones), having a space of almost the same volume, with porous plates made of heat resistant bricks (thickness: 200 mm). The gas to be treated, which had been divided and preheated was fed into the first reaction chamber, while the remainder of the divided gas to be

treated was introduced into the second, third and fourth reaction chambers. The second, third and fourth reaction chambers were each provided with inlets of the gas to be treated immediately after the hot gas stream was fed thereinto. These inlets of the gas to be treated were formed at two positions in opposition to each other on planes vertical to the major axis of the thermal decomposition reaction furnace in such a manner that the blow direction of the gas to be treated and the major axis did not intersect each other. A preheating portion, which was made of heat resistant bricks similar to the thermal decomposition portion, had a cylindrical shape with a space of 200 mm in inner diameter and 500 mm in length. It was provided with an inlet of the gas to be treated at one end while the other end was connected to the thermal decomposition portion. Into this preheating portion, methanol corresponding to 13 kcal per 1 Nm³ of the gas to be treated was introduced with air at a rate of 0.0231 kmol/hr. Then it was subjected to combustion in the preheating portion and uniformly mixed with the gas to be treated introduced into the preheating portion at 17.8 Nm³/hr. The temperature of the gas to be treated was adjusted to 550°C. The temperature of the gas stream introduced from the preheating portion to the first reaction chamber was 830°C. The gas to be treated at 550°C was supplied into the second,

third and fourth reaction chambers respectively at flow rates of 34.3 Nm³/hr, 72.7 Nm³/hr and 155.2 Nm³/hr. The mixtures of the hot gas stream with the gas to be treated at the inlets of the second, third and fourth reaction chambers
5 had each a temperature of 830°C. The pressure within the furnace was 1.25 kg/cm² (gauge pressure).

The temperature of the gas stream discharged from the thermal decomposition reaction furnace was 1162°C and N₂O contained in the supplied gas to be treated had been thus
10 thermally decomposed at a ratio of 99% or more.

Example 8

The inside of the thermal decomposition reaction furnace as in Example 7 was divided in series into first, second and third chambers, having a space of almost the same
15 volume, with porous plates made of heat resistant bricks (thickness: 200 mm). The inlets of the gas to be treated were arranged as in Example 7. The preheating portion had the same volume as in Example 7. N₂O in the gas to be treated was thermally decomposed as in Example 7 but the
20 flow rate of methanol supplied into the preheating portion being 0.0520 kmol/hr; and the flow rates of the gas to be treated supplied into the preheating portion and the second and third chambers being respectively 39.9 Nm³/hr, 77.0 Nm³/hr and 163.1 Nm³/hr.

The pressure within the furnace was 1.25 kg/cm².

The temperatures of the gas stream mixtures in the preheating portion and at the inlets of the second and third chambers were each 830°C. The temperature of the gas stream
5 discharged from the thermal decomposition reaction furnace was 1172°C and N₂O contained in the supplied gas to be treated had been thus thermally decomposed at a ratio of 99% or more.

Table 2 summarizes the conditions of the thermal
10 decomposition of N₂O and the results in the above Examples 1 to 8.

Comparative Example 1

The thermal decomposition reaction furnace as in Example 1 was provided with neither porous plate made of
15 heat resistant bricks nor baffle plate. That is, the inside of the furnace was made a single reaction chamber and the N₂O-containing gas to be treated was supplied as a whole (i.e., not divided) exclusively into the preheating portion. Then N₂O contained in the gas to be treated was thermally
20 decomposed as in Example 1 but the flow rates of hydrogen and the gas to be treated supplied into the preheating portion being respectively 19.9 Nm³/hr and 280 Nm³/hr.

The pressure within the furnace was 1.25 kg/cm². The temperature of the gas stream mixture at the inlet of the
25 thermal decomposition portion was 830°C. The temperature of

the gas stream discharged from the thermal decomposition reaction furnace was 1283°C and N₂O contained in the supplied gas to be treated had been thermally decomposed at a ratio of 99% or more.

5 As described above, the temperature of the gas stream at the outlet of the thermal decomposition furnace was 1283°C in Comparative Example 1, while the corresponding temperature in the above Example 2 was 1027°C, i.e., much lower (by 256°C). In Comparative Example 1, 19.9 Nm³/hr of
10 hydrogen was employed to thermally decompose 280 Nm³/hr of the gas to be treated. In, for example, Example 3 according to the invention, in contrast thereto, only 0.1 Nm³/hr of hydrogen was supplied to thermally decompose the same amount (i.e., 280 Nm³/hr) of the gas to be treated as in Comparative
15 Example 1. N₂O in the gas to be treated was thermally decomposed at a ratio of 99% or more in both of these Examples, which indicates that, in the invention, the heat generated in association with the decomposition of N₂O in the thermal decomposition furnace can be very efficiently
20 utilized by supplying the gas to be treated in portions.

 Since the gas to be treated is preheated in the invention, only a small amount of a fuel is needed, as described above. In case where NO formed by the thermal decomposition of N₂O is recovered if necessary, the NO
25 product is diluted with the gas generated only at an

extremely low dilution ratio and thus NO can be recovered at a high concentration.

Comparative Example 2

N₂O in a gas to be treated was thermally decomposed
5 without dividing the gas to be treated as in Comparative
Example 1 but the flow rate of hydrogen supplied into the
preheating portion being 2.9 Nm³/hr.

The pressure within the furnace was 1.25 kg/cm². The
temperatures of the gas stream mixture at the inlet of the
10 thermal decomposition portion was 598°C. The temperature of
the gas stream discharged from the thermal decomposition
furnace was 601°C and N₂O contained in the supplied gas to be
treated had not been thermally decomposed.

As described above, hydrogen was supplied at a flow
15 rate of 2.9 Nm³/hr in Comparative Example 2. However, N₂O in
280 Nm³/hr of the gas to be treated could not be thermally
decomposed by using hydrogen in such a small amount. In,
for example, Example 1 of the invention as described above,
N₂O in 280 Nm³/hr of the gas to be treated could be thermally
20 decomposed at a ratio of 99% or more by using only 1.3 Nm³/hr
of hydrogen.

Table 3 summarizes the conditions of the thermal
decomposition of N₂O and the results in the above Comparative
Examples 1 and 2.

25 Example 9

N₂O contained in a gas to be treated at 200°C, which had a composition of N₂O (15.0% by mol), O₂ (13.5% by mol), N₂ (70.2% by mol), CO₂ (1.1% by mol), NO (0.1% by mol) and NO₂ (0.1% by mol) and was supplied at a flow rate of 130.6 m³/H, was catalytically decomposed by using a catalyst.

The catalyst employed was a copper oxide/alumina catalyst. That is, use was made of a catalyst carrying 3.7% of copper oxide and having a surface area of 145 m²/g and a packing density of 758 kg/m³ prepared by impregnating γ-alumina with a copper nitrate solution, drying under a hot air stream at 120°C for 6 hours and then baking at 500°C for 3 hours.

The catalytic decomposition reactor employed was a cylindrical container of 2700 mm in inner diameter and 5000 mm in length. The inside of the reactor was divided into five catalytic decomposition reaction chambers (N₂O decomposition zones) in opposition to the flow direction of the hot gas stream (i.e., in opposition to the longitudinal direction of the reactor). Mixing chambers partitioned with porous plates were located in front and at the back of each reaction chamber. The first, second, third, fourth and fifth reaction chambers had respectively 0.25 m³, 0.14 m³, 0.63 m³, 2.27 m³ and 6.61 m³ of the catalyst.

130.6 Nm³/H of the gas to be treated was divided into five gas streams. The preheated gas to be treated was fed

into the first reaction chamber and formed a hot gas stream at the outlet of the first reaction chamber. Into the mixing chambers in front of the second, third, fourth and fifth reaction chambers, the remainder of the divided gas to
5 be treated was respectively introduced each from two directions perpendicular to the hot gas stream flow direction in such a manner as to form a rotary stream.

The pressure at the inlet of the reactor was adjusted to 0.21 MPa. 12.5 Nm³/H of the gas to be treated was heated
10 to 430°C by indirect heat-exchange with the outlet gas of the reactor and then supplied into the first reaction chamber. The gas at the outlet of the first reaction chamber was a hot gas at 779°C due to the N₂O decomposition heat. The gas to be treated was supplied at a rate of 10.0 Nm³/H to the
15 mixing chamber in front of the second reaction chamber in such a manner as to give an N₂O concentration of 6.5% by mol after mixing with the above-described hot gas. After mixing, the temperature of the gas attained 528°C. The gas at the outlet of the second reaction chamber was a hot gas at 685°C
20 due to the N₂O decomposition heat. The gas to be treated was supplied at a rate of 18.1 Nm³/H to the mixing chamber in front of the third reaction chamber. After mixing, the gas showed an N₂O concentration of 6.5% by mol and a temperature of 473°C. The gas at the outlet of the third reaction
25 chamber was a hot gas at 632°C due to the N₂O decomposition

heat. The gas to be treated was supplied at a rate of 32.6 Nm³/H to the mixing chamber in front of the fourth reaction chamber. After mixing, the gas showed an N₂O concentration of 6.5% by mol and a temperature of 443°C. The gas at the
5 outlet of the fourth reaction chamber was a hot gas at 603°C due to the N₂O decomposition heat. The gas to be treated was supplied at a rate of 57.4 Nm³/H to the mixing chamber in front of the fifth reaction chamber. After mixing, the gas showed an N₂O concentration of 6.5% by mol and a temperature
10 of 426°C. The temperature of the decomposed gas at the outlet of the fifth reaction chamber was 587°C. Thus, N₂O contained in the supplied gas to be treated had been catalytically decomposed at a ratio of 99% or more.

The total amount of the gas to be treated in this
15 Example amounts to 130.6 m³/H. Since the gas to be treated is supplied in portions, a 12.5 m³/H portion alone in 130.6 m³/H is preheated to the initiation temperature of the reaction of 430°C before supplying. Thus, the heat load on the heat exchanger required for preheating is 908 kcal/h.
20 The remainder of the divided gas to be treated can be supplied without preheating. Although the remainder of the gas to be treated is supplied without preheating, the outlet temperature of each catalytic bed can be maintained at 430°C (i.e., the initiation temperature of the reaction) or higher

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and N_2O can be catalytically decomposed continuously, as this Example clearly shows.

Example 10

N_2O contained in a gas to be treated discharged from an
5 adipic acid plant having the composition and flow rate as
given in Table 4 was catalytically decomposed by using a
catalyst. The same catalyst as that of Example 9 was
employed.

The catalytic decomposition reactor employed was a
10 cylindrical container of 2700 mm in inner diameter and 5000
mm in length. The inside of the reactor was divided into
two catalytic decomposition reaction chambers in opposition
to the flow direction of the hot gas stream. A mixing
chamber partitioned with porous plates was located between
15 these reaction chambers. The first and second reaction
chambers had respectively 3.90 m^3 and 6.04 m^3 of the catalyst.

The preheated gas to be treated was fed into the first
reaction chamber, while the remainder of the divided gas to
be treated was introduced into the mixing chamber in front
20 of the second reaction chamber from two positions
perpendicular to the hot gas stream flow direction in such a
manner as to form a rotary stream.

The pressure at the inlet of the reactor was adjusted
to 0.21 MPa. $114.8 \text{ Nm}^3/\text{H}$ of the gas to be treated at 30°C
25 and $406.7 \text{ Nm}^3/\text{H}$ of a diluent gas at 230°C were mixed together



in the first reaction chamber to thereby give an N_2O concentration of 7.5% by mol. Further, the gas mixture was subjected to indirect heat-exchange with the outlet gas of the reactor to attain a temperature of 500°C.

5 The above-described diluent gas was one obtained by heat-recovery with the use of a boiler from the reaction mixture after catalytically decomposing N_2O in the gas to be treated.

 The gas stream at the outlet of the first reaction
10 chamber was a hot gas at 680°C heated by the N_2O decomposition heat.

 165.2 Nm^3/H of the gas to be treated and 44.1 Nm^3/H of the diluent gas were mixed together in the mixing chamber in front of the second reaction chamber to thereby give an N_2O
15 concentration of 7.5% by mol and a gas temperature of 500°C. The temperature of the decomposed gas at the outlet was 680°C. Thus, N_2O contained in the supplied gas to be treated had been catalytically decomposed at a ratio of 99% or more. The ratio of the total amount of the diluent gas employed to
20 the supplied gas to be treated was 1.61.

Example 11

 The same catalyst as employed in Example 9 was used. The catalytic decomposition reactor employed was a cylindrical container of 2700 mm in inner diameter and 5000
25 mm in length. The inside of the reactor was divided into

three catalytic decomposition reaction chambers in opposition to the flow direction of the hot gas stream. Mixing chamber partitioned with porous plates were located in front of each reaction chamber. The first, second and 5 third reaction chambers had respectively 2.07 m³, 3.08 m³ and 4.70 m³ of the catalyst.

The preheated gas mixture of the gas to be treated with the diluent gas was fed into the first reaction chamber, while the remainder of the divided gas to be treated and the 10 diluent gas were introduced into the mixing chambers in front of the second and third reaction chambers each from two positions perpendicular to the hot gas stream flow direction (i.e., the longitudinal direction of the reactor) in such a manner as to form a rotary stream.

15 The pressure at the inlet of the reactor was adjusted to 0.21 MPa. 62.0 Nm³/H of the gas to be treated at 30°C and 219.2 Nm³/H of a diluent gas at 230°C were mixed together in the first reaction chamber to thereby give an N₂O concentration of 7.5% by mol. Further, the gas mixture was 20 subjected to indirect heat-exchange with the outlet gas of the reactor to attain a temperature of 500°C.

The above-described diluent gas was one obtained by heat-recovery with the use of a boiler from the reaction mixture after catalytically decomposing N₂O in the gas to be 25 treated.

The gas stream at the outlet of the first reaction chamber was a hot gas at 680°C heated by the N₂O decomposition heat. 89.3 Nm³/H of the gas to be treated and 23.8 Nm³/H of a diluent gas were supplied into the mixing chamber in front of the second reaction chamber. After mixing, the gas showed an N₂O concentration of 7.5% by mol and a temperature of 500°C. The gas stream at the outlet of the second reaction chamber was a hot gas at 680°C heated by the N₂O decomposition heat. 128.7 Nm³/H of the gas to be treated and 34.2 Nm³/H of a diluent gas were supplied into the mixing chamber in front of the third reaction chamber. After mixing, the gas showed an N₂O concentration of 7.5% by mol and a temperature of 500°C. The gas stream at the outlet was a hot gas at 680°C. Thus, N₂O contained in the supplied gas to be treated had been catalytically decomposed at a ratio of 99% or more. The ratio of the total amount of the diluent gas employed to the supplied gas to be treated was 0.99.

20 Example 12

The same catalyst as employed in Example 9 was used. The catalytic decomposition reactor employed was a cylindrical container having an inner diameter of 2700 mm and a length of 5000 mm. The inside of the reactor was divided into four catalytic decomposition reaction chambers

in opposition to the flow direction of the hot gas stream. Mixing chamber partitioned with porous plates were located in front of each reaction chamber. The first, second, third and fourth reaction chambers had respectively 1.24 m³, 1.81
5 m³, 2.69 m³ and 4.07 m³ of the catalyst.

The preheated gas mixture of the gas to be treated with the diluent gas was fed into the first reaction chamber, while the remainder of the divided gas to be treated and the diluent gas were introduced into the mixing chambers in
10 front of the second, third and fourth reaction chambers each from two positions perpendicular to the hot gas stream flow direction (i.e., the longitudinal direction of the reactor) in such a manner as to form a rotary stream.

The pressure at the inlet of the reactor was adjusted
15 to 0.21 MPa. 37.4 Nm³/H of the gas to be treated at 30°C and 131.6 Nm³/H of a diluent gas at 230°C were mixed together in the first reaction chamber to thereby give an N₂O concentration of 7.5% by mol. Further, the gas mixture was subjected to indirect heat-exchange with the outlet gas of
20 the reactor to attain a temperature of 500°C.

The above-described diluent gas was one obtained by heat-recovery with the use of a boiler from the reaction mixture after catalytically decomposing N₂O in the gas to be treated.

The gas stream at the outlet of the first reaction chamber was a hot gas at 680°C heated by the N_2O decomposition heat. 53.8 Nm^3/H of the gas to be treated and 14.3 Nm^3/H of a diluent gas were supplied into the mixing chamber in front of the second reaction chamber. After mixing, the gas showed an N_2O concentration of 7.5% by mol and a temperature of 500°C. The gas stream at the outlet of the second reaction chamber was a hot gas at 680°C heated by the N_2O decomposition heat. 77.4 Nm^3/H of the gas to be treated and 20.5 Nm^3/H of a diluent gas were supplied into the mixing chamber in front of the third reaction chamber. After mixing, the gas showed an N_2O concentration of 7.5% by mol and a temperature of 500°C. The gas stream at the outlet of the third reaction chamber was a hot gas at 680°C heated by the N_2O decomposition heat. 111.4 Nm^3/H of the gas to be treated and 29.6 Nm^3/H of a diluent gas were supplied into the mixing chamber in front of the fourth reaction chamber. After mixing, the gas showed an N_2O concentration of 7.5% by mol and a temperature of 500°C. The gas stream at the outlet was a hot gas at 680°C. Thus, N_2O contained in the supplied gas to be treated had been catalytically decomposed at a ratio of 99% or more. The ratio of the total amount of the diluent gas employed to the supplied gas to be treated was 0.70.

25 Example 13

The same catalyst as employed in Example 9 was used. The catalytic decomposition reactor employed was a cylindrical container of 2700 mm in inner diameter and 5000 mm in length. The inside of the reactor was divided into five catalytic decomposition reaction chambers in opposition to the flow direction of the hot gas stream. Mixing chamber partitioned with porous plates were located in front of each reaction chamber. The first, second, third, fourth and fifth reaction chambers had respectively 0.78 m³, 1.14 m³, 1.67 m³, 2.48 m³ and 3.73 m³ of the catalyst.

The preheated gas mixture of the gas to be treated with the diluent gas was fed into the first reaction chamber, while the remainder of the divided gas to be treated and the diluent gas were introduced into the mixing chambers in front of the second, third, fourth and fifth reaction chambers each from two positions perpendicular to the hot gas stream flow direction (i.e., the longitudinal direction of the reactor) in such a manner as to form a rotary stream.

The pressure at the inlet of the reactor was adjusted to 0.21 MPa. 23.7 Nm³/H of the gas to be treated at 30°C and 83.8 Nm³/H of a diluent gas at 230°C were mixed together in the first reaction chamber to thereby give an N₂O concentration of 7.5% by mol. Further, the gas mixture was subjected to indirect heat-exchange with the outlet gas of the reactor to attain a temperature of 500°C.

The above-described diluent gas was one obtained by heat-recovery with the use of a boiler from the reaction mixture after catalytically decomposing N_2O in the gas to be treated.

5 The gas stream at the outlet of the first reaction chamber was a hot gas at 680°C heated by the N_2O decomposition heat. $34.2 \text{ Nm}^3/\text{H}$ of the gas to be treated and $9.1 \text{ Nm}^3/\text{H}$ of a diluent gas were supplied into the mixing chamber in front of the second reaction chamber. After
10 mixing, the gas showed an N_2O concentration of 7.5% by mol and a temperature of 500°C . The gas stream at the outlet of the second reaction chamber was a hot gas at 680°C heated by the N_2O decomposition heat. $49.2 \text{ Nm}^3/\text{H}$ of the gas to be treated and $13.1 \text{ Nm}^3/\text{H}$ of a diluent gas were supplied into
15 the mixing chamber in front of the third reaction chamber. After mixing, the gas showed an N_2O concentration of 7.5% by mol and a temperature of 500°C . The gas stream at the outlet of the third reaction chamber was a hot gas at 680°C heated by the N_2O decomposition heat. $70.9 \text{ Nm}^3/\text{H}$ of the gas to be
20 treated and $18.9 \text{ Nm}^3/\text{H}$ of a diluent gas were supplied into the mixing chamber in front of the fourth reaction chamber. After mixing, the gas showed an N_2O concentration of 7.5% by mol and a temperature of 500°C . The gas stream at the outlet of the fourth reaction chamber was a hot gas at 680°C heated
25 by the N_2O decomposition heat. $102.0 \text{ Nm}^3/\text{H}$ of the gas to be

treated and 27.2 Nm³/H of a diluent gas were supplied into the mixing chamber in front of the fifth reaction chamber. After mixing, the gas showed an N₂O concentration of 7.5% by mol and a temperature of 500°C. The gas stream at the outlet
5 was a hot gas at 680°C. Thus, N₂O contained in the supplied gas to be treated had been catalytically decomposed at a ratio of 99% or more. The ratio of the total amount of the diluent gas employed to the supplied gas to be treated was 0.54.

10 Table 5 summarizes the conditions of the catalytic decomposition of N₂O and the results in the above Examples 10 to 13.

Comparative Example 3

The same catalyst and gas to be treated as employed in
15 Example 9 were used. The catalytic decomposition reactor employed was a cylindrical container of 2700 mm in inner diameter and 5000 mm in length composed of a single reaction chamber. The reaction chamber had 2.60 m³ of the catalyst.

The preheated gas to be treated was fed into the
20 reaction chamber. The pressure at the inlet of the reactor was adjusted to 0.21 MPa. 130.6 Nm³/H of the gas to be treated was subjected to indirect heat-exchange with the outlet gas of the reactor to attain a temperature of 430°C and then supplied into the reaction chamber. The gas stream
25 at the outlet of the reaction chamber was a hot gas at 779°C

heated by the N_2O decomposition heat. Thus, N_2O contained in the supplied gas to be treated had been catalytically decomposed at a ratio of 99% or more. In this Comparative Example 3, the heat load required in preheating was 9.623
5 kcal/h. Accordingly, use should be made in this case of a large-scaled heat exchanger with which 11 times as much heat can be subjected to heat-exchange as compared to the case of Example 6.

Comparative Example 4

10 The same catalyst and gas to be treated as employed in Example 9 were used. The catalytic decomposition reactor employed was a cylindrical container of 2700 mm in inner diameter and 5000 mm in length composed of a single reaction chamber. The reaction chamber had 10.18 m³ of the catalyst.

15 The preheated mixture of the gas to be treated and the diluent gas was fed into the reaction chamber. The pressure at the inlet of the reactor was adjusted to 0.21 MPa. 280.0 Nm³/H of the gas to be treated at 30°C and 989.8 Nm³/H of the gas to be treated at 230°C were mixed together to give an N_2O
20 concentration of 7.5% by mol. Further, the gas mixture was subjected to indirect heat-exchange with the outlet gas of the reactor to attain a temperature of 500°C followed by supplying.

The above-described diluent gas was one obtained by
25 heat-recovery with the use of a boiler from the reaction



mixture after catalytically decomposing N_2O in the gas to be treated.

The gas stream at the outlet of the reaction chamber was a hot gas at 680°C heated by the N_2O decomposition heat.

5 Thus, N_2O contained in the supplied gas to be treated had been catalytically decomposed at a ratio of 99% or more.

The ratio of the total amount of the diluent gas employed to the supplied gas to be treated was 3.54.

As described above, 3.54 times as much diluent gas was
10 required in catalytically decomposing $280.0 \text{ Nm}^3/\text{H}$ of the gas to be treated by using a catalyst in Comparative Example 4. In contrast thereto, only 0.54 times as much diluent gas was required in Example 13 according to the invention. In Comparative Example 4, furthermore, the sum of the diluent
15 gas and the gas to be treated to be heated at the inlet of the first stage amounted to $1269.8 \text{ Nm}^3/\text{H}$, while the corresponding amount of the gases in Example 12 was as small as $432.1 \text{ Nm}^3/\text{H}$. Since N_2O in the gas to be treated could be decomposed at a ratio of 99% or more in each case, it is
20 obvious that, in the invention, the heat generated in association of the decomposition of N_2O in the catalytic decomposition reactor can be more efficiently utilized by supplying the gas to be treated in portions.

Table 6 summarizes the conditions of the catalytic decomposition of N_2O and the results in the above Comparative Example 4.

- 5 Table 1: Composition of N_2O -containing gas (gas to be treated)

	Discharged gas composition (mol%)	Discharged gas flow rate (Nm^3/H)
N_2O	33.9	94.9
NO	0.3	0.8
NO_2	0.4	1.1
CO_2	2.4	6.7
O_2	4.2	11.8
N_2	58.9	164.9
Total	100.0	280.2

Table 2: Reaction conditions and results

	Ex. 1	Ex. 2	Ex. 3	Ex. 4	Ex. 5	Ex. 6	Ex. 7	Ex. 8
No. of stages supplying gas to be treated	4	4	4	4	3	2	4	3
Supplying temp. (°C)	550	300	700	550	550	550	550	550
Amount of Hydrogen (Nm ³ /hr)	1.3	7.2	0.1	1.2	2.9	6.9	-	-
Amount of Methanol (kmol/hr)	-	-	-	-	-	-	0.0231	0.0520
H ₂ or MeOH (kcal)	12	66	0.9	11	26	63	13	28
(per 1 Nm ³ of gas to be treated)								
Pressure (kg/cm ²)	1.25	1.25	1.25	1.25	1.25	1.25	1.25	1.25
Feed (Nm ³ /H)								
Preheating portion	17.9	55.7	3	19.7	40.4	96.6	17.8	39.9
Chamber 2	34.1	60.0	12.0	36.1	76.5	183.4	34.3	77.0
Chamber 3	72.6	72.9	50.6	73.4	163.1	-	72.7	163.1
Chamber 4	155.4	91.4	214.4	150.8	-	-	155.2	-
Inlet temp. (°C)	830	830	830	800	830	830	830	830
Chamber 2	830	830	830	800	830	830	830	830
Chamber 3	830	830	830	800	830	-	830	830
Chamber 4	830	830	830	800	-	-	830	-
Final outlet temp. (°C)	1163	1027	1263	1131	1173	1200	1162	1172
N ₂ O decomposition ratio (%)	>99	>99	>99	>99	>99	>99	>99	>99

Note: 1. Pressure is expressed in gauge pressure.

2. Preheating portion is referred to as the first stage.

Table 3: Reaction conditions and Results of Comparative Examples 1 and 2

	Compa. Ex. 1	Compa. Ex. 2
No. of stages supplying gas to be treated	1	1
Supplying temp. (°C)	550	550
Amount of Hydrogen (Nm ³ /hr)	19.9	2.9
Ditto (kcal/ Nm ³) - treated gas	182	
Reaction pressure (kg/cm ²)	1.25	1.25
Feed (Nm ³ /H) of gas to be treated	280	280
Initiation temp. (°C)	830	598
Final outlet temp. (°C)	1283	601
Reaction ratio(%)	99	0

Pressure is expressed in gauge pressure.

5 Table 4: Composition and flow rate of N₂O-containing gas to be treated)

	Discharged gas composition (mol%)	Discharged gas flow rate (Nm ³ /H)
N ₂ O	34.1	95.5
NO	0.1	0.3
NO ₂	0.1	0.3
CO ₂	2.4	6.7
O ₂	4.0	11.2
N ₂	59.3	166.0
Total	100.0	280.0

Table 5: Reaction conditions and results

	Ex.10	Ex.11	Ex.12	Ex.13
No. of stages supplying gas to be treated	2	3	4	5
Supplying temp. (°C)	500	35	35	35
Diluent gas temp. (°C)	230	230	230	230
Inlet temp. at each stage (°C)	500	500	500	500
Outlet temp. at each stage (°C)	680	680	680	680
Pressure at reactor inlet (MPa)	0.21	0.21	0.21	0.21
Feed of gas to be treated (Nm ³ /H)				
Stage 1	114.8	62.0	37.4	23.7
Stage 2	165.2	89.3	53.8	34.2
Stage 3	-	128.7	77.4	49.2
Stage 4	-	-	111.4	70.9
Stage 5	-	-	-	102.0
Σ	280.0	280.0	280.0	280.0
Feed of diluent gas (Nm ³ /H)				
Stage 1	406.7	219.2	131.6	83.8
Stage 2	44.1	23.8	14.3	9.1
Stage 3	-	34.2	20.5	13.1
Stage 4	-	-	29.6	18.9
Stage 5	-	-	-	27.2
Σ	450.8	277.2	196.0	152.1
Σ Diluent gas/Σ gas to be treated (molar ratio)	1.61	0.99	0.70	0.54
Catalytic bed volume (m ³)				
Stage 1	3.90	2.07	1.24	0.78
Stage 2	6.04	3.08	1.81	1.14
Stage 3	-	4.70	2.69	1.67
Stage 4	-	-	4.07	2.48
Stage 5	-	-	-	3.73
Σ	9.93	9.85	9.82	9.80
N ₂ O conversion (%)	>99	>99	>99	>99

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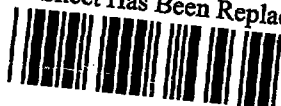


Table 6: Reaction conditions and results of Comparative Example 4

	Compara. Example. 4
Discharged gas: Feed Stage number	1
Ditto : Feed temp. (°C)	35
Diluent gas temp. (°C)	230
Inlet temp. (°C)	500
Outlet temp. (°C)	680
Reactor inlet pressure (MPa)	0.21
Diluent gas flow rate (Nm ³ /H)	989.8
ΣDiluent gas/Σgas to be treated (molar ratio)	3.54
Catalytic bed volume (m ³)	10.18
N ₂ O conversion (%)	>99

INDUSTRIAL APPLICABILITY

As the detailed description given above clearly
5 indicates, the present invention provides a highly useful
method in practice for preventing global warming which makes
it possible to efficiently decompose N₂O at a low temperature
while externally supplying only an extremely small amount of
energy, and an apparatus therefor. The invention achieves
10 remarkable effects as will be shown hereinafter.

That is to say, the invention for preventing global
warming by thermally decomposing N₂O achieves the following
effects.

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1. It exerts remarkably excellent effects such that N_2O can be thermally decomposed at a high decomposition ratio at a relatively low temperature; that the thus formed NO and NO_2 exist at high concentrations and can be economically recovered, if needed; and that only a very small amount of heat energy is supplied externally.

2. The invention can provide an apparatus which is highly useful in practice and has the merits such as having a small reactor volume; the materials of the process instruments thereof being easily selected; only a small heat load being applied on the process instruments thereof; a smaller heat exchanger being usable in heating the gas to be treated; and making it possible to recover NO, etc. at high concentration.

On the other hand, the invention for preventing global warming by catalytically decomposing N_2O achieves the following effects.

1. In the method of decomposing N_2O according to the invention, the N_2O -containing gas to be treated is divided and a portion thereof is preheated to the temperature at which the catalytic decomposition of N_2O can be initiated while the remainder of the divided gas to be treated is supplied into an N_2O catalytic decomposition bed at a temperature lower than the temperature of the preheated gas as described above. Thus, the amount of the heat required

in preheating can be considerably reduced, compared with the case wherein the whole gas to be treated is preheated and then supplied.

2. Therefore, the preheating devices (for example, a heat exchanger) to be used can be considerably reduced in size. When the preheating is carried out by combustion of a fuel supplied externally, the amount of the fuel can be significantly reduced.

3. In the invention, it is also possible that the gas to be treated is mixed with a diluent gas and supplied into the catalytic bed. In this case, the amount of the diluent gas to be used can be largely reduced owing to the effects achieved by supplying the gas to be treated in portions as described above.

4. According to the method of the invention, N_2O is catalytically decomposed by using a catalytic bed. Thus, the heat formed in a large amount in association with the catalytic decomposition of N_2O in the former catalytic bed can be successively given to the catalytic bed located posterior in the longitudinal direction. That is, the heat formed in a large amount by the catalytic decomposition of N_2O can be very efficiently utilized in elevating the temperature of the gas stream to be treated successively supplied in portions.

5. Thus, the temperature of the gas to be supplied into each catalytic bed and the temperature in each catalytic bed can be easily controlled at an appropriate level for the desired catalytic system.

5 6. The apparatus of catalytic decomposition of N_2O according to the invention makes it possible to embody the above-described method for catalytically decomposing N_2O to give the effects as described above. Since the whole apparatus can be molded in a smaller size, various costs
10 thereof can be reduced. Moreover, the amount of a fuel or energy supplied externally can be considerably reduced.

7. By using this apparatus, the temperature of the catalytic decomposition bed can be very easily controlled and a rapid increase in temperature at the catalytic bed or
15 around the same due to the decomposition heat of N_2O can be prevented without fail.

8. Thus, the N_2O catalytic decomposition apparatus of the invention can be operated easily and, moreover, has an excellent durability, thereby being highly useful in
20 practice.

9. In the process for producing adipic acid according to the present invention, N_2O is released into the atmosphere only in a very small amount. Since this process depends on the N_2O -decomposition techniques being highly useful in
25 practice as described above, it largely contributes to the

prevention of global warming. In addition, it can be economically carried out at a low equipment cost.

CLAIM

1 1. A method for preventing global warming comprising,
2 a process of thermally or catalytically decomposing N_2O in an
3 N_2O -containing gas to be treated, by dividing the N_2O -
4 containing gas stream to be treated in portions, preheating
5 a portion thereof so as to exothermally decompose N_2O in said
6 gas stream to form a hot gas stream, and supplying the
7 remainder of the divided gas stream to be treated into said
8 hot gas stream to thereby continuously decompose N_2O , so that
9 global warming is prevented.

1 2. The method for preventing global warming as
2 claimed in claim 1, wherein said exothermic decomposition of
3 N_2O is performed by thermal decomposition without using any
4 catalyst.

1 3. The method for preventing global warming as
2 claimed in claim 2, wherein the remainder of said divided
3 gas to be treated is supplied into plural positions in the
4 flow direction of said hot gas stream.

1 4. The method for preventing global warming as
2 claimed in claim 2 or 3, wherein said decomposition of N_2O in



3 the gas to be treated is performed in a state of a
4 substantially plug flow.

1 5. The method for preventing global warming as
2 claimed in claim 2 or 3, wherein said preheating is
3 performed by a direct heating system utilizing an oxidative
4 exothermic reaction of a fuel.

1 6. The method for preventing global warming as
2 claimed in claim 5, wherein said fuel is hydrogen or
3 methanol.

1 7. The method for preventing global warming as
2 claimed in claim 1, wherein said exothermic decomposition of
3 N_2O is performed by catalytic decomposition.

1 8. The method for preventing global warming as
2 claimed in claim 7, wherein the remainder of said divided
3 gas to be treated is supplied into plural positions in the
4 flow direction of said hot gas stream and each brought into
5 contact with a catalytic bed respectively.

1 9. The method for preventing global warming as
2 claimed in claim 7 or 8, wherein the gas stream, immediately



3 before contacting the catalytic bed, is a mixture with a
4 diluent gas.

1 10. The method for preventing global warming as
2 claimed in claim 9, wherein said diluent gas is air and/or
3 the gas, which has been subjected to the catalytic
4 decomposition of N_2O in the gas to be treated.

1 11. The method for preventing global warming as
2 claimed in claim 9, wherein the gas having been subjected to
3 the catalytic decomposition of N_2O in the gas to be treated
4 is cooled and then used as the diluent gas.

1 12. The method for preventing global warming as
2 claimed in claim 7, 8, 10 or 11, wherein said preheating is
3 performed by mixing the gas to be treated and/or the diluent
4 gas with steam formed by reacting hydrogen and oxygen using
5 a noble metal catalyst.

1 13. An apparatus for preventing global warming by
2 thermally decomposing N_2O in an N_2O -containing gas,
3 comprising:

4 (a) an introduction portion for the N_2O -containing gas
5 to be treated;



6 (b) a preheating portion for the thus introduced gas
7 to be treated;
8 (c) a thermal decomposition portion adjacent to the
9 preheating portion, said thermal decomposition portion
10 having means for supplying the gas to be treated, said
11 supplying means being provided at one or more positions in
12 the flow direction of a gas stream; and
13 (d) a discharging portion for the thermally decomposed
14 gas.

1 14. The apparatus for preventing global warming as
2 claimed in claim 13, wherein said preheating portion is
3 having means of fuel combustion.

1 15. The apparatus for preventing global warming as
2 claimed in claim 14, wherein the temperature of the gas
3 stream at the outlet of said discharging portion is
4 controlled to a constant level by controlling the amount of
5 the fuel fed into said fuel-combustion means.

1 16. The apparatus for preventing global warming as
2 claimed in claim 13, 14 or 15, wherein said thermal
3 decomposition portion has a porous plate and/or a multi-pipe
4 nozzle in front of and/or at the back of at least one means
5 for supplying the gas to be treated.



1 17. The apparatus for preventing global warming as
2 claimed in claim 13, 14 or 15, wherein said porous plate,
3 multi-pipe nozzle and/or inlet of the gas to be treated are
4 located in such a manner that the gas stream flowing towards
5 the means for supplying the gas to be treated flows as a
6 rotary stream.

1 18. An apparatus for preventing global warming by
2 bringing N_2O in an N_2O -containing gas into contact with a
3 catalytic bed to thereby catalytically decompose N_2O ,
4 comprising:

5 (a) an introduction portion for the gas to be treated
6 and/or a diluent gas;

7 (b) a mixing portion for the gas to be treated and/or
8 the diluent gas;

9 (c) a mixing portion having one or more means for
10 supplying the gas to be treated and/or the diluent gas at
11 different positions in the longitudinal direction of the
12 apparatus;

13 (d) a catalytic decomposition portion having the
14 catalytic bed; and

15 (e) a discharging portion for the catalytically
16 decomposed gas.



1 19. An apparatus for preventing global warming by
2 catalytic decomposition of N_2O in an N_2O -containing gas,
3 comprising:
4 a device which comprises:
5 (a) an introduction portion for the gas to be treated
6 and/or a diluent gas;
7 (b) a mixing portion for the gas to be treated and/or
8 the diluent gas;
9 (c) a catalytic decomposition portion having a
10 catalytic bed; and
11 (d) a discharging portion for the catalytically
12 decomposed gas; and
13 one or more devices each of which comprises:
14 (e) an introduction portion for the discharged gas
15 having been catalytically decomposed, the gas to be treated
16 and/or a diluent gas;
17 (f) a mixing portion for the discharged gas having
18 been catalytically decomposed, the gas to be treated and/or
19 the diluent gas;
20 (g) a catalytic decomposition portion having a
21 catalytic bed; and
22 (h) a discharging portion for the catalytically
23 decomposed gas.



1 20. The apparatus for preventing global warming as
2 claimed in claim 18 or 19, wherein said mixing portion for
3 the gas to be treated and/or the diluent gas involves a
4 preheating portion for the gas to be treated and/or the
5 diluent gas.

1 21. A process for producing adipic acid with reduced
2 release of N_2O that causes global warming, comprising:

3 (1) a nitric acid-oxidation step in which cyclohexanol
4 and/or cyclohexanone are oxidized with nitric acid to form
5 adipic acid;

6 (2) a nitric acid recovery step in which HNO_3 is
7 recovered from an N_2O -containing gas caused in the nitric
8 acid-oxidation step;

9 (3) a N_2O decomposition step in which the remaining
10 N_2O -containing gas stream to be treated, from which HNO_3 has
11 been recovered, is divided, a portion thereof is preheated
12 to exothermally decompose N_2O in the gas stream to form a hot
13 gas stream, and the remainder of the divided gas stream to
14 be treated is supplied into said hot gas stream to thereby
15 continuously decompose N_2O ; and

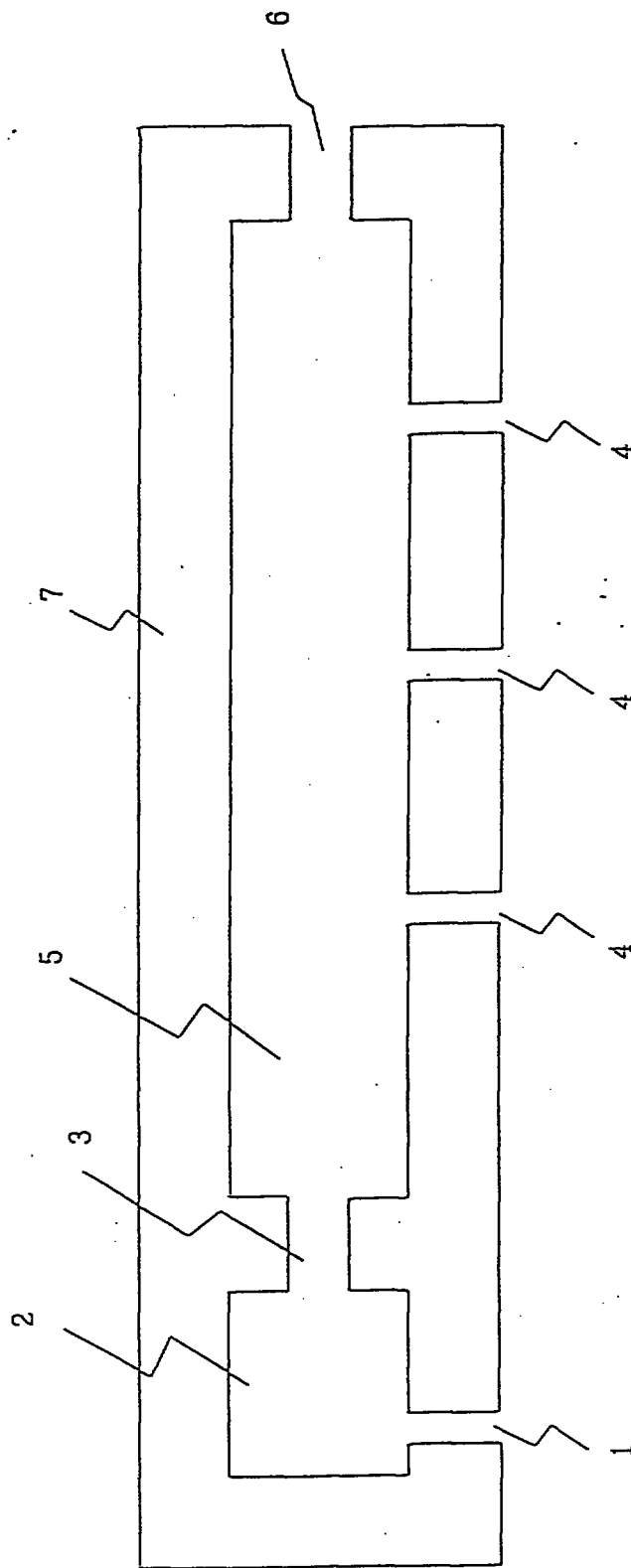
16 (4) a N_2O decomposition heat recovery step in which the
17 N_2O decomposition heat emitted from the N_2O decomposition
18 step is recovered.



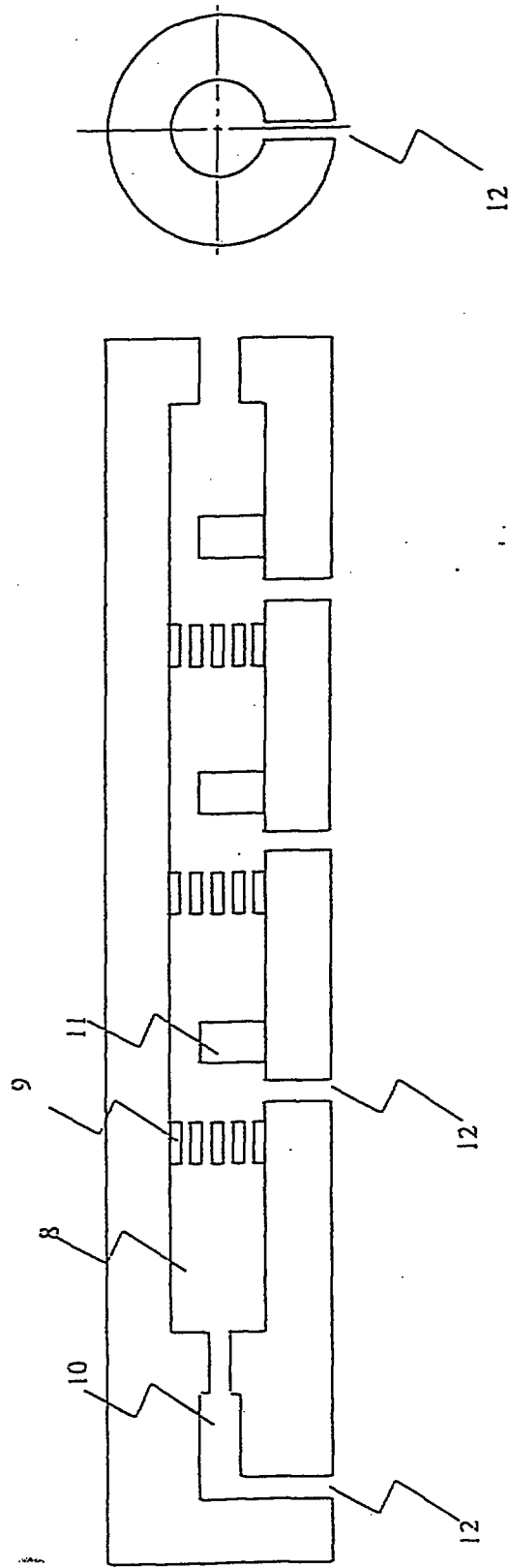
ABSTRACT

A low-cost and practically useful method for preventing global warming by decomposing N_2O wherein N_2O contained in an N_2O -containing gas to be treated can be decomposed at a relatively low temperature; and an apparatus therefor. That is, a method for preventing global warming comprising, in a process of thermally or catalytically decomposing N_2O in an N_2O -containing gas to be treated, dividing the N_2O -containing gas stream to be treated in portions, preheating a portion thereof so as to exothermally decompose N_2O in said gas stream to form a hot gas stream, and supplying the remainder of the divided gas stream to be treated into said hot gas stream to thereby continuously decompose N_2O , so that global warming is prevented; and an apparatus therefor.

—第1图—
Fig. 1



第2图
Fig. 2



~~Fig. 3~~ Fig. 3

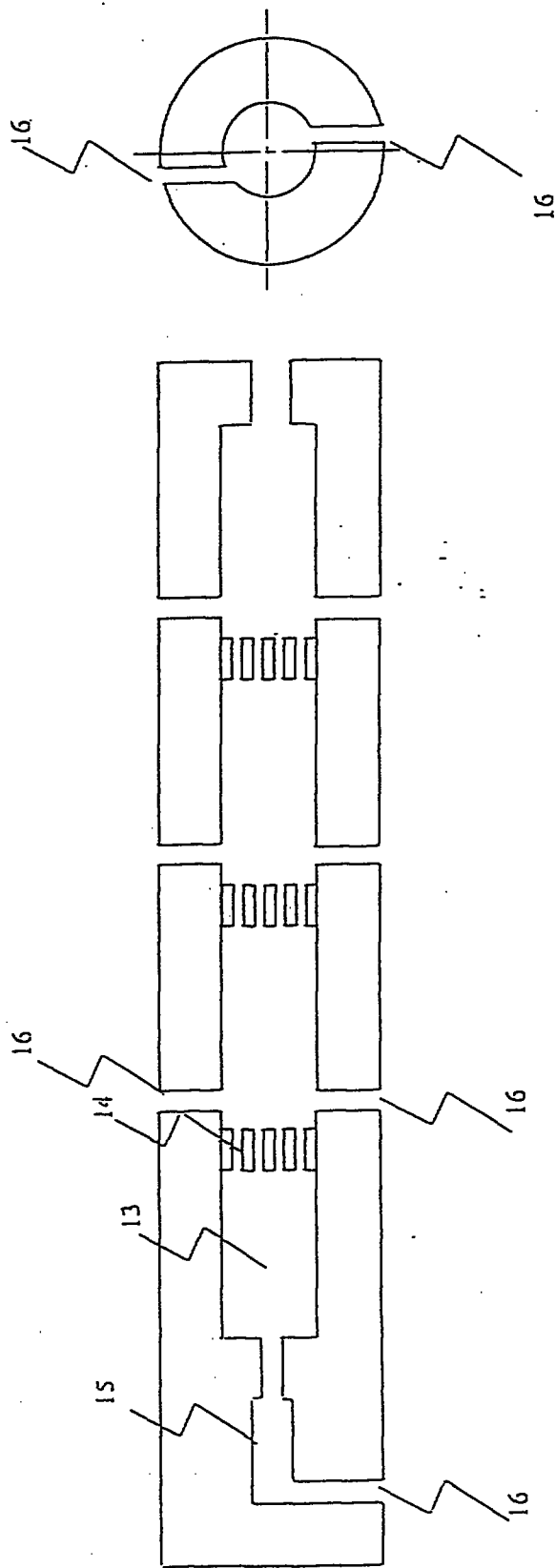
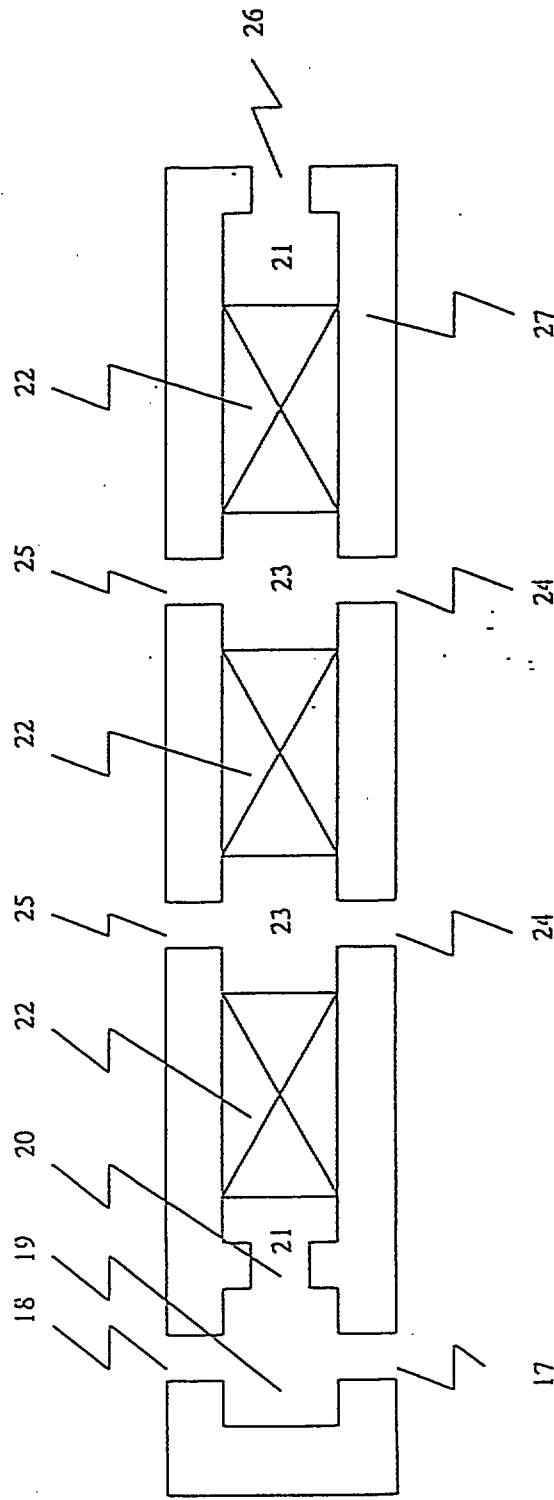
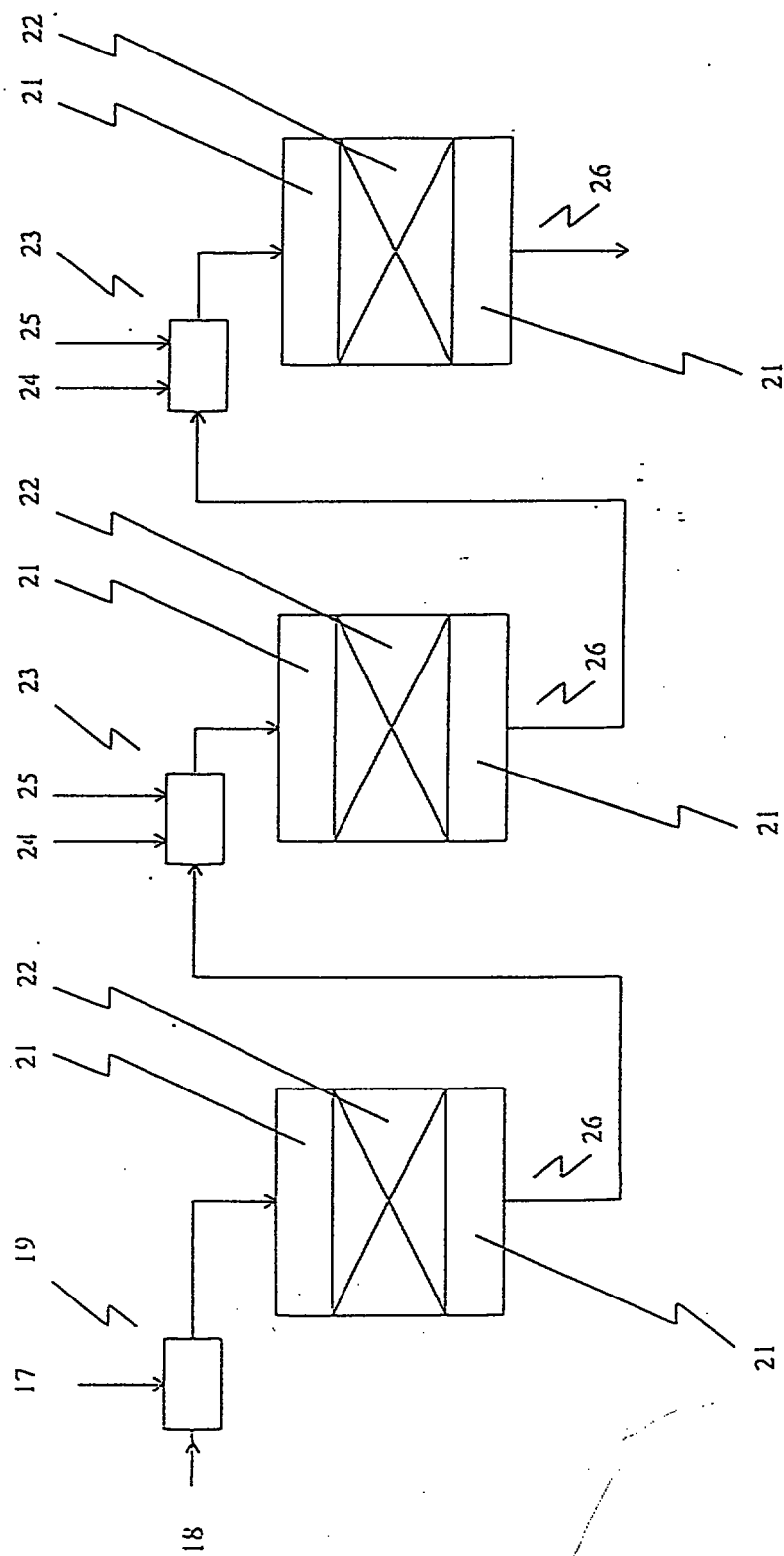


Fig. 4



第5圖 Fig. 5



eliminated before supplying into the N_2O decomposition apparatus or a gas which has been mixed with other gases, etc.

The present invention is not restricted by the kind of the catalyst for decomposing N_2O . To achieve the objects of the invention, however, it is preferable to use those containing copper, nickel, iron, cobalt, palladium, or oxides or complex oxides of these metals. It is preferable that the catalyst is carried on a carrier. As the carrier, those having appropriate pores and showing a high heat stability may be selected. Preferred examples of the catalyst carrier to be used in the invention include oxides and complex oxides of aluminum, ~~silica~~^{silicon}, titanium, magnesium and zirconium. As aluminum oxides among these carriers, it is still preferable to use α -alumina, β -alumina or γ -alumina. As the silica/alumina complex oxides, it is still preferable to use zeolite such as ZSM5. As the titanium oxides, it is still preferable to use those of the anatase and rutile types. It is also preferable to use zirconia which has a high heat resistance. Furthermore, it is preferable to use a carrier obtained by mixing these carriers as cited above. In the invention, the catalyst may be carried on the carrier by a well-known method. For example, the carrier is impregnated with an aqueous solution of a water-soluble salt of a metal catalyst and then baked.

decomposed as in Example 1 but the flow rate of hydrogen supplied into the preheating portion being 2.9 Nm³/hr; and the flow rates of the gas to be treated supplied into the preheating portion and the second and third reaction chambers being respectively 40.4 Nm³/hr, 76.5 Nm³/hr and 163.1 Nm³/hr.

The pressure within the furnace was 1.25 kg/cm². The temperature of the gas stream discharged from the thermal decomposition reaction furnace was 1173°C and N₂O contained in the supplied gas to be treated had been thus thermally decomposed at a ratio of 99% or more.

The pressure within the furnace was 1.25 kg/cm². The gas stream mixture in the preheating portion and at the inlets of the second, third and fourth reaction chambers had each a temperature of 830°C. The temperature of the gas stream discharged from the thermal decomposition reaction furnace was 1173°C and N₂O contained in the supplied gas to be treated had been thus thermally decomposed at a ratio of 99% or more.

Example 6

The inside of the thermal decomposition reaction furnace as in Example 1 was divided in series into first and second chambers, having a space of almost the same volume, with a porous plate made of heat resistant bricks (thickness: 200 mm). The inlets of the gas to be treated and the baffle plates were arranged as in Example 1. The preheating portion had the same volume as in Example 1. N₂O contained in a gas to be treated was thermally decomposed as in Example 1 but the flow rate of hydrogen supplied into the preheating portion being 6.9 Nm³/hr; and the flow rates of the gas to be treated supplied into the preheating portion and the second reaction chamber being respectively 96.6 Nm³/hr and 183.4 Nm³/hr.

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heat. The gas to be treated was supplied at a rate of 32.6 Nm³/H to the mixing chamber in front of the fourth reaction chamber. After mixing, the gas showed an N₂O concentration of 6.5% by mol and a temperature of 443°C. The gas at the outlet of the fourth reaction chamber was a hot gas at 603°C due to the N₂O decomposition heat. The gas to be treated was supplied at a rate of 57.4 Nm³/H to the mixing chamber in front of the fifth reaction chamber. After mixing, the gas showed an N₂O concentration of 6.5% by mol and a temperature of 426°C. The temperature of the decomposed gas at the outlet of the fifth reaction chamber was 587°C. Thus, N₂O contained in the supplied gas to be treated had been catalytically decomposed at a ratio of 99% or more.

The total amount of the gas to be treated in this Example amounts to 130.6 m³/H. Since the gas to be treated is supplied in portions, a 12.5 m³/H portion alone in 130.6 m³/H is preheated to the initiation temperature of the reaction of 430°C before supplying. Thus, the heat load on the heat exchanger required for preheating is 908 kcal/h. The remainder of the divided gas to be treated can be supplied without preheating. Although the remainder of the gas to be treated is supplied without preheating, the ^{inlet}~~outlet~~ temperature of each catalytic bed can be maintained at 430°C (i.e., the initiation temperature of the reaction) or higher

and N_2O can be catalytically decomposed continuously, as this Example clearly shows.

Example 10

N_2O contained in a gas to be treated discharged from an adipic acid plant having the composition and flow rate as given in Table 4 was catalytically decomposed by using a catalyst. The same catalyst as that of Example 9 was employed.

The catalytic decomposition reactor employed was a cylindrical container of 2700 mm in inner diameter and 5000 mm in length. The inside of the reactor was divided into two catalytic decomposition reaction chambers in opposition to the flow direction of the hot gas stream. A mixing chamber partitioned with porous plates was located between these reaction chambers. The first and second reaction chambers had respectively 3.90 m³ and 6.04 m³ of the catalyst.

The preheated gas to be treated was fed into the first together with a diluent gas reaction chamber, while the remainder of the divided gas to be treated was introduced into the mixing chamber in front of the second reaction chamber from two positions perpendicular to the hot gas stream flow direction in such a manner as to form a rotary stream.

The pressure at the inlet of the reactor was adjusted to 0.21 MPa. 114.8 Nm³/H of the gas to be treated at 30°C and 406.7 Nm³/H of a diluent gas at 230°C were mixed together

heated by the N_2O decomposition heat. Thus, N_2O contained in the supplied gas to be treated had been catalytically decomposed at a ratio of 99% or more. In this Comparative Example 3, the heat load required in preheating was ~~9.623~~^{9.623} kcal/h. Accordingly, use should be made in this case of a large-scaled heat exchanger with which 11 times as much heat can be subjected to heat-exchange as compared to the case of Example ~~6~~⁹.

Comparative Example 4

10 The same catalyst and gas to be treated as employed in Example ~~9~~¹⁰ were used. The catalytic decomposition reactor employed was a cylindrical container of 2700 mm in inner diameter and 5000 mm in length composed of a single reaction chamber. The reaction chamber had 10.18 m^3 of the catalyst.

15 The preheated mixture of the gas to be treated and the diluent gas was fed into the reaction chamber. The pressure at the inlet of the reactor was adjusted to 0.21 MPa. $280.0 \text{ Nm}^3/\text{H}$ of the gas to be treated at 30°C and $989.8 \text{ Nm}^3/\text{H}$ of the gas to be treated at 230°C were mixed together to give an N_2O concentration of 7.5% by mol. Further, the gas mixture was subjected to indirect heat-exchange with the outlet gas of the reactor to attain a temperature of 500°C followed by supplying.

The above-described diluent gas was one obtained by
25 heat-recovery with the use of a boiler from the reaction

Table 5: Reaction conditions and results

	Ex.10	Ex.11	Ex.12	Ex.13
No. of stages supplying gas to be treated	2	3	4	5
Supplying temp. (°C)	500 30	35 30	35 30	35 30
Diluent gas temp. (°C)	230	230	230	230
Inlet temp. at each stage (°C)	500	500	500	500
Outlet temp. at each stage (°C)	680	680	680	680
Pressure at reactor inlet (MPa)	0.21	0.21	0.21	0.21
Feed of gas to be treated (Nm ³ /H)				
Stage 1	114.8	62.0	37.4	23.7
Stage 2	165.2	89.3	53.8	34.2
Stage 3	-	128.7	77.4	49.2
Stage 4	-	-	111.4	70.9
Stage 5	-	-	-	102.0
Σ	280.0	280.0	280.0	280.0
Feed of diluent gas (Nm ³ /H)				
Stage 1	406.7	219.2	131.6	83.8
Stage 2	44.1	23.8	14.3	9.1
Stage 3	-	34.2	20.5	13.1
Stage 4	-	-	29.6	18.9
Stage 5	-	-	-	27.2
Σ	450.8	277.2	196.0	152.1
Σ Diluent gas/Σ gas to be treated (molar ratio)	1.61	0.99	0.70	0.54
Catalytic bed volume (m ³)				
Stage 1	3.90	2.07	1.24	0.78
Stage 2	6.04	3.08	1.81	1.14
Stage 3	-	4.70	2.69	1.67
Stage 4	-	-	4.07	2.48
Stage 5	-	-	-	3.73
Σ	9.93	9.85	9.82	9.80
N ₂ O conversion (%)	>99	>99	>99	>99

Table 6: Reaction conditions and results of Comparative Example 4

	Compara. Example. 4
Discharged gas: Feed Stage number	1
Ditto : Feed temp. (°C)	55 30
Diluent gas temp. (°C)	230
Inlet temp. (°C)	500
Outlet temp. (°C)	680
Reactor inlet pressure (MPa)	0.21
Diluent gas flow rate (Nm ³ /H)	989.8
ΣDiluent gas/Σgas to be treated (molar ratio)	3.54
Catalytic bed volume (m ³)	10.18
N ₂ O conversion (%)	>99

INDUSTRIAL APPLICABILITY

As the detailed description given above clearly
 5 indicates, the present invention provides a highly useful
 method in practice for preventing global warming which makes
 it possible to efficiently decompose N₂O at a low temperature
 while externally supplying only an extremely small amount of
 energy, and an apparatus therefor. The invention achieves
 10 remarkable effects as will be shown hereinafter.

That is to say, the invention for preventing global
 warming by thermally decomposing N₂O achieves the following
 effects.

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decomposed as in Example 1 but the flow rate of hydrogen supplied into the preheating portion being 2.9 Nm³/hr; and the flow rates of the gas to be treated supplied into the preheating portion and the second and third reaction chambers being respectively 40.4 Nm³/hr, 76.5 Nm³/hr and 163.1 Nm³/hr.

~~The pressure within the furnace was 1.25 kg/cm². The temperature of the gas stream discharged from the thermal decomposition reaction furnace was 1173°C and N₂O contained in the supplied gas to be treated had been thus thermally decomposed at a ratio of 99% or more.~~

The pressure within the furnace was 1.25 kg/cm². The gas stream mixture in the preheating portion and at the inlets of the second, ^{and} third ~~and fourth~~ reaction chambers had each a temperature of 830°C. The temperature of the gas stream discharged from the thermal decomposition reaction furnace was 1173°C and N₂O contained in the supplied gas to be treated had been thus thermally decomposed at a ratio of 99% or more.

Example 6

The inside of the thermal decomposition reaction furnace as in Example 1 was divided in series into first and second chambers, having a space of almost the same volume, with a porous plate made of heat resistant bricks (thickness: 200 mm). The inlets of the gas to be treated and the baffle plates were arranged as in Example 1. The preheating portion had the same volume as in Example 1. N₂O contained in a gas to be treated was thermally decomposed as in Example 1 but the flow rate of hydrogen supplied into the preheating portion being 6.9 Nm³/hr; and the flow rates of the gas to be treated supplied into the preheating portion and the second reaction chamber being respectively 96.6 Nm³/hr and 183.4 Nm³/hr.

