

**METHODS FOR THE DIRECT ELECTROLYTIC PRODUCTION OF STABLE, HIGH CONCENTRATION
AQUEOUS HALOSULFAMATE OR HALOSULFONAMIDE SOLUTIONS**

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CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims priority to and the benefit of filing of U.S. Provisional Patent Application Serial No. 62/089,770, entitled "Methods for the Direct Electrolytic Production of Stable, High Concentration Aqueous Halosulfamate or Halosulfonamide Solutions", filed on December 9, 2014, the specification and claims of which are incorporated herein by reference.

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BACKGROUND OF THE INVENTION

Field Of The Invention (Technical Field)

The present invention is related to the *in situ* production of high concentration stable aqueous biocidal solutions comprised of mixtures of free halogens, N-halosulfamic acid compounds, N-halosulfamate compounds, N,N-dihalosulfamic acid compounds and N,N-dihalosulfamate compounds, with or without additional biocidally active components, in any desired compositional mixture and at a desired pH through an electrolysis process, where the nature of the biocidal solution is determined by the nature of the brine used in the electrolysis process as well as the operational parameters of the electrolytic process.

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Background Art

Note that the following discussion may refer to a number of publications and references. Discussion of such publications herein is given for more complete background of the scientific principles and is not to be construed as an admission that such publications are prior art for patentability determination purposes.

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Aqueous free halogen species such as chlorine, bromine, iodine, hypochlorous acid, hypobromous acid, hypiodous acid, hypochlorite, hypobromite, and hypoiodite are known to be very powerful anti-microbial agents and are often used in water disinfection applications. Along with a high

level of biocidal activity, aqueous free halogens are also highly chemically reactive to other species often present in waters undergoing treatment. These species include natural organic matter, synthetic and natural organic chemicals, iron, manganese, hydrogen sulfide, ammonia, arsenic, and other chemicals. The presence of these free halogen demanding substances consume free halogens added to the water that would otherwise be useful in inactivating microorganisms, thus, this process could be considered detrimental to the overall treatment process if the free halogen consuming chemical reaction is not desirable. Reactions between aqueous free halogens and organic material present in the water being treated can also, in some cases, lead to the undesirable products such as the formation of halogenated organic chemicals such as trihalomethanes and haloacetic acids. Therefore, the treatment of waters containing high amounts of these halogen-reactive compounds is often advantageously accomplished through the use of biocides that are less chemically reactive than aqueous free halogen species.

Haloamines, which can broadly be considered as chemical species which contain at least one nitrogen-halogen bond, are often used in place of oxidizing free halogens to provide a disinfectant for water treatment. While haloamines are effective biocidal compounds, they are also much less chemically reactive as compared to free halogens. Thus, in waters containing substantial amounts of free halogen demanding substances, haloamines have the potential to provide a substantial benefit to the overall water disinfection process. Aqueous solutions of haloamines are typically produced through a chemical reaction between an aqueous free halogen species and a compound containing at least one nitrogen-hydrogen bond whereby the chemical reaction produces a compound containing at least one nitrogen-halogen bond. Ammonia or ammonium ions are the most common source of the nitrogen containing compound used in this process, although other nitrogen containing compounds are often utilized as well.

One major deterrent to the use of haloamines, and especially haloamines produced through the reaction of ammonia or ammonium ions with an aqueous free halogen species, is that they are highly unstable, especially at higher concentrations (i.e. greater than 10 mg/L); see for example Audrieth, L. F.; Rowe, R. A. "The Stability of Aqueous Chloramine Solutions" J. Am. Chem. Soc. 1955, 77, 4726-4728. Due to the instability of haloamines, it is typically not possible to produce concentrated haloamine solutions and ship them to a point of application. As a result, haloamines derived from ammonia or ammonium ions are often produced in situ during treatment by the action of aqueous free halogens on ammonia or organic amines naturally present or added to water being treated. Alternatively, it is

sometimes desirable to prepare concentrated aqueous haloamine solutions derived from the reaction between ammonia or ammonium ions at the point of application and then use these formed haloamine solutions as a primary disinfectant. Situations where this could be advantageous include the treatment of waters which have a known or highly variable free halogen demand which would consume free halogens without the benefit of microbial inactivation but which can be effectively treated with a haloamine disinfectant.

Sulfamic acid and its organic compound derivatives, known as sulfonamides (for example, toluenesulfonamide), are chemically distinct from ammonia or other organic amine-containing compounds used to produce haloamines but, like ammonia or many amines, typically contain a nitrogen-hydrogen bond which can react with aqueous halogen species. Products of the reaction between sulfamic acid, having the chemical formula H_3NSO_3 , and an aqueous halogen species are N-halosulfamate compounds (either N-halosulfamate, having the chemical formula HNSO_3X^- , or N-halosulfamic acid, having the chemical formula $\text{H}_2\text{NSO}_3\text{X}$), N,N-dihalosulfamate compounds (N,N-dihalosulfamic acid, having the chemical formula HNSO_3X_2 , or N,N-dihalosulfamate, having the chemical formula NSO_3X_2^-), or combinations thereof, where, in all cases, the letter X represents a halogen (i.e. Cl, Br, I). Products of the reaction between and organic sulfonamide compounds, having the chemical formula of RSO_2NH_2 , and an aqueous halogen species are N-halosulfanamide compounds, having the chemical formula of RSO_2NHX , N,N-dihalosulfonamide compounds, having the chemical formula of RSO_2NX_2 , or combinations thereof, where, in all cases, the letter R represents an organic functional group comprising at least carbon and hydrogen and the letter X represents a halogen (i.e. Cl, Br, I). These compounds can stabilize the electrolyzed halogen species.

U.S. Patent No. 3,776,825 to Vit entitled "Electrolytic Treatment" discloses that a brine comprising a halide ion source and an amine compound both dissolved in water is first pH adjusted through the addition of a base such as sodium hydroxide, and then electrolyzed, thereby producing a solution containing one or more haloamine compound, including N-chlorosulfamates or N-chlorosulfonamides produced from sulfamic acid or organic sulfonamides, respectively. Vit further teaches that when electrolysis is used to make these haloamine solutions they are unstable, and therefore the invention described by Vit is focused entirely on the instantaneous production and immediate subsequent use of the produced haloamines as opposed to the production of stable haloamine solutions. Because Vit discloses

the addition of NaOH to the brine prior to electrolysis, and discloses that the pH of the solution is thus greater than 12, the solution prior to electrolysis no longer comprises sulfamic acid, but instead comprises sulfamate ions.

5 SUMMARY OF THE INVENTION (DISCLOSURE OF THE INVENTION)

The present invention is a method for producing a stable disinfecting solution comprising a plurality of halosulfamate and/or halosulfamic acid species and one or more halogen species, the method comprising preparing an acidic solution comprising desired concentrations of halide ions and sulfamic acid and electrolyzing the solution, wherein the concentrations of the halide ions and the sulfamic acid in
10 the acidic solution and the pH of the acidic solution are chosen to produce the desired concentrations of the halosulfamate species and/or halosulfamic acid species in the stable disinfecting solution. The acidic solution optionally further comprises one or more additional halogen stabilizing compounds. The one or more additional halogen stabilizing compounds are preferably selected from the group consisting of lithium sulfamate, sodium sulfamate, potassium sulfamate, organic sulfonamide, methylsulfonamide, o-
15 toluenesulfonamide, m-toluenesulfonamide, p-toluenesulfonamide, cyanuric acid, a derivative of cyanuric acid, succinimide, a derivative of succinimide, hydantoin, a derivative of hydantoin, and combinations thereof. The stable disinfecting solution can then optionally comprise N-halosulfonamide compounds and/or N,N-dihalosulfonamide compounds. The halosulfamate species preferably comprise N-halosulfamate compounds and/or N,N-dihalosulfamate compounds, and the halosulfamic acid species
20 preferably comprise N-halosulfamic acid compounds and/or N,N-dihalosulfamic acid compounds. The stable disinfecting solution is preferably a high concentration solution. The acidic solution preferably does not comprise a non-amine base.

The preparing step optionally comprises providing a salt blend comprising sulfamic acid and one or more salts comprising the halide ions and diluting the salt blend with water. The salt blend preferably
25 comprises a pellet, briquette, or compacted form, preferably comprises a solid solution, and optionally comprises an anti-caking agent. The method preferably further comprises flowing the acidic solution through an electrolytic cell at a flow rate selected to produce the desired pH of the stable disinfecting solution. The flow rate can optionally be increased, thereby maintaining the acidity of electrolyte in the vicinity of cathodes in the electrolytic cell during the electrolyzing step, which then preferably results in

removing scale from surfaces of the cathodes or preventing the formation of scale on the surfaces of the cathodes. The pH of the acidic solution is preferably less than 4, and more preferably less than 1. The pH of the stable disinfecting solution is optionally greater than 9, or optionally greater than 11, or optionally less than 3.

5 Objects, advantages and novel features, and further scope of applicability of the present invention will be set forth in part in the detailed description to follow, taken in conjunction with the accompanying drawings, and in part will become apparent to those skilled in the art upon examination of the following, or may be learned by practice of the invention. The objects and advantages of the invention may be realized and attained by means of the instrumentalities and combinations particularly pointed out in the appended
10 claims.

BRIEF DESCRIPTION OF THE DRAWINGS

 The accompanying drawings, which are incorporated into and form a part of the specification, illustrate several embodiments of the present invention and, together with the description, serve to explain
15 the principles of the invention. The drawings are only for the purpose of illustrating certain embodiments of the invention and are not to be construed as limiting the invention. In the drawings:

 FIG. 1 is a schematic drawing of a system for the production of stable, concentrated aqueous solutions comprised of free halogen species, N-halosulfamate compounds, N,N-dihalosulfamate compounds, N-halosulfonamide compounds, N,N-dihalosulfonamide compounds from a single, highly
20 concentrated brine source that is diluted into a process water.

 FIG. 2 is a schematic drawing of a system for the production of stable, concentrated aqueous solutions comprised of free halogen species, N-halosulfamate compounds, N,N-dihalosulfamate compounds, N-halosulfonamide compounds, N,N-dihalosulfonamide compounds from a dual, highly
concentrated brine sources that are diluted into a process water.

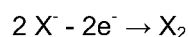
25 FIG. 3 is a schematic drawing of a system for the production of stable, concentrated aqueous solutions comprised of free halogen species, N-halosulfamate compounds, N,N-dihalosulfamate compounds, N-halosulfonamide compounds, N,N-dihalosulfonamide compounds from a single source brine.

DETAILED DESCRIPTION OF EMBODIMENTS OF THE INVENTION

Embodiments of the present invention are simplified electrochemically-driven processes whereby controlled formation and electrolysis of specifically designed aqueous brine blends comprising metal halide salts combined with at least sulfamic acid either alone or in combination with other halogen stabilizing compounds in a single electrolysis step are used to produce stable, high concentration aqueous solutions comprised of at least halogens, N-halosulfamate compounds, N,N-dihalosulfamate compounds, or other stabilized compounds, in any desired compositional blend. Production of these solutions is preferably achieved through precise control of the composition of the brines, used in the electrolysis process as well as electrolytic conditions used to electrolyze the brines.

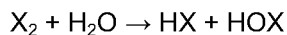
As used throughout the specification and claims, the term "high concentration" means a solution with a total halogen content of at least 2100 mg/L. Total halogen content includes free halogen species, N-halosulfamate compounds, and N,N-dihalosulfamate compounds. As used throughout the specification and claims, the term "stable" means a solution with less than a 5% loss in total halogen content over a 24 hour time period. As used throughout the specification and claims, the term "non-amine base" means any basic compound that does not comprise an amine, such as sodium hydroxide, potassium hydroxide, sodium bicarbonate, or calcium carbonate. The present invention can be used to provide halogen-based disinfectant solutions wherever such solutions can be useful for microbiological control, and will be especially useful in the disinfection of highly challenging waters such as those found in oil and gas production processes, industrial cooling systems, pulp and paper production facilities, and food and beverage production processes. Embodiments of the present invention are directed to electrolysis processes of brines comprising mixtures of sodium chloride, sodium bromide, and sulfamic acid, although other metal halide sources can be used in place of sodium chloride or sodium bromide, and other halogen stabilizing compounds can be used instead of or in addition to sulfamic acid.

Metal halide brines subjected to electrolysis undergo several electrolytic and chemical transformations, starting with the electrolytic oxidation of halide ions to produce halogens:



where X^- is the halide ion and X_2 is the diatomic, molecular halogen. Here, X^- can be Cl^- , Br^- , I^- , or any combination thereof while X_2 can be Cl_2 , Br_2 , I_2 , $BrCl$, Brl , ICl , or any combination thereof. Once the X_2

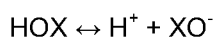
halogen species is formed by the electrolysis process, it will react with water also present in the brine to produce a combination of acids:



where H_2O is water, HX is a hydrohalic acid, and HOX is a hypohalous acid. Here, HX can be HCl , HBr ,

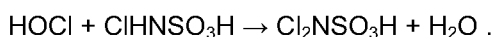
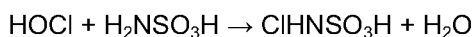
5 HI , or any combination thereof while HOX can be $HOCl$, $HOBr$, HOI , or any combination thereof.

Depending on the pH of the brine during electrolysis and/or the pH of the electrolyzed solution, the hypohalous acid component of the electrolyzed solution can disassociate to yield hypohalite ions according to:



10 where XO^- is the hypohalite ion, such as ClO^- , BrO^- , IO^- , or any combination thereof, depending on the halide ion content of the brine. The relative amount of HOX and XO^- present in the brine during electrolysis and the electrolyzed solution varies according to the acid disassociation constants of the various hypohalous acids. In this process, X_2 , HOX , and XO^- are all considered to be free halogen species.

15 In the presence of sulfamic acid, these chlorine species will participate in a sequence of chemical reactions that will yield N-chlorosulfamic acid, N-chlorosulfamate, N,N-dichlorosulfamic acid, and N,N-dichlorosulfamate. An example of this is the reaction between hypochlorous acid and sulfamic acid:



20 In other words, when sulfamic acid, having a chemical formula of H_3NSO_3 , is present in the brine during electrolysis, it will react with the free halogen species present in the electrolyzed brine to produce N-halosulfamic acids, having chemical formulas of H_2NSO_3X , N-halosulfamates, having chemical formulas of $HNSO_3X^-$, N,N-dihalosulfamic acids, having chemical formulas of $HNSO_3X_2$, and N,N-dihalosulfamates, having chemical formulas of $NSO_3X_2^-$ where, in all cases, X represents halogens such as chlorine (Cl),
 25 bromine (Br), and/or iodine (I). Depending on the composition of the brine used in the present invention, the biocidal composition of the electrolyzed solutions can contain chlorine (Cl_2), bromine (Br_2), iodine (I_2), bromine monochloride ($BrCl$), bromine monoiodide (BrI), iodine monochloride (ICl) hypochlorous acid ($HOCl$), hypobromous acid ($HOBr$), hypoiodous acid (HOI), hypochlorite (ClO^-), hypobromite (BrO^-), hypoiodite (IO^-), N-chlorosulfamic acid (H_2NSO_3Cl), N-bromosulfamic acid (H_2NSO_3Br), N-iodosulfamic

acid ($\text{H}_2\text{NSO}_3\text{I}$), N-chlorosulfamate (HNSO_3Cl^-), N-bromosulfamate (HNSO_3Br^-), N-iodosulfamate (HNSO_3I^-), N,N-dichlorosulfamic acid (HNSO_3Cl_2), N,N-dibromosulfamic acid (HNSO_3Br_2), N,N-diiodosulfamic acid (HNSO_3I_2), N-bromo-N-chlorosulfamic acid (HNSO_3BrCl), N-bromo-N-iodosulfamic acid (HNSO_3BrI), N-chloro-N-iodosulfamic acid (HNSO_3ClI), N,N-dichlorosulfamate ($\text{NSO}_3\text{Cl}_2^-$), N,N-dibromosulfamate ($\text{NSO}_3\text{Br}_2^-$), N,N-diiodosulfamate (NSO_3I_2^-), N-bromo-N-chlorosulfamate ($\text{NSO}_3\text{BrCl}^-$), N-bromo-N-iodosulfamate (NSO_3BrI^-), N-chloro-N-iodosulfamate (NSO_3ClI^-), or any combination of these components thereof.

The relative composition of free halogens, N-halosulfamic acids, N-halosulfamates, N,N-dihalosulfamic acids, and N,N-dihalosulfamates present in the electrolyzed solution will typically be determined by factors including, but not limited to, the relative composition of halide ions and sulfamic acid in the brine, and the pH of the electrolyzed solution. For example, the ratio of halide ion (and therefore eventual halogen content after electrolysis) to sulfamic acid in the brine will impact the relative distribution of free halogen, monohalogenated sulfamate species (N-halosulfamic acid and N-halosulfamate), and dihalogenated sulfamate species (N,N-dihalosulfamic acid and N,N-dihalosulfamate). In brines where there is an excess of sulfamic acid relative to the halide ion, the primary initial product will be monohalogenated sulfamate species; conversely, when the halide ion is in large excess of the sulfamic acid, the primary initial product of electrolysis will primarily be free halogen and dihalogenated sulfamate species. Similarly, the electrolyzed solution's pH can dictate the relative concentration of halosulfamic acids versus halosulfamate species, typically with higher halosulfamic acid composition at lower electrolyzed solution pH. Therefore, by varying the pH of brine prior to electrolysis, for example by varying the relative concentration of sulfamic acid and halides, the composition of the electrolyzed solution can be tailored as desired.

Organic sulfonamide, having a chemical formula of RSO_2NH_2 where R indicates the presence of an organic functional group such as, but not limited to, o-tolyl, m-tolyl, or p-tolyl, will behave in a similar fashion to sulfamic acid, in that N-halosulfonamide compounds having a chemical formula of RSO_2NHX , and N,N-dihalosulfonamide compounds having a chemical formula of RSO_2NX_2 and where X in both formulations represents a halogen, can be produced through this process. Similarly, mixtures of sulfamic acid and various organic sulfonamides can be used to produce mixtures of halosulfamate compounds and halosulfonamide compounds along with free halogen species of any desired composition. As with the

above process, control over the composition of these complex solutions is preferably achieved by controlling the composition of the mixed brines used in the electrolysis process.

Alternatively, this process can utilize other halogen stabilizing chemical compounds besides or in addition to sulfamic acid and its derivatives. Typically, these chemicals comprise a molecule containing at least one nitrogen atom wherein the at least one nitrogen atom has a chemical bond to at least one hydrogen atom and the same nitrogen also has at least one chemical bond to an atom other than nitrogen, hydrogen, or a halogen. Examples of halogen stabilizing compounds that can be used for these purposes include, but are not limited to, cyanuric acid and its derivatives, succinimide and its derivatives, and hydantoin and its derivatives. Another example of a halogen stabilizing compound, phosphoramidic acid (a chemical having a formula of H_4NPO_3), can be used in place of or in addition to sulfamic acid in the practice of the present invention. Electrolysis of solutions containing at least phosphoramidic acid and at least one metal halide ion as described by the practice of the present invention can result in the production of free halogens, N-halophosphoramidic acid compounds (having a chemical formula of $\text{H}_3\text{NPO}_3\text{X}$), N-halophosphoramidate compounds (having a chemical formula of $\text{H}_2\text{NPO}_3\text{X}^-$ or $\text{HNPO}_3\text{X}^{2-}$), N,N-dihalophosphoramidic acid compounds (having a chemical formula of $\text{H}_2\text{NPO}_3\text{X}_2$), N,N-dihalophosphoramidate compounds (having a chemical formula of $\text{HNPO}_3\text{X}_2^-$ or $\text{NPO}_3\text{X}_2^{2-}$), or combinations thereof.

In the practice of the present invention, electrolysis is accomplished using an electrolytic cell comprising at least one cathode and at least one anode, although some embodiments of the present invention will also include several intermediate electrode plates to form a bipolar cell. Electrodes can be of any suitable material, but preferably Dimensionally Stable Anodes (which can be used as both the anode and cathode) are used in the present invention. Voltage applied to the electrolytic cell is preferably approximately 6V.

In the embodiment of the present invention shown in FIG. 1, tank 2 is a brine generator that is charged with a blended salt and water from a source (not shown). Here, the brine generator and a blended salt are used to produce a brine with continuous, near uniform composition which is transferred using pump 4 into line 6, which preferably also contains water. The diluted mixed brine is then transferred into generation system 8, which comprises an electrolytic cell along with a plurality of sensors and controls which monitor and alter the electrochemical process as needed to provide the desired product.

The electrolyzed brine solution is then transferred through line **10** into tank **12**, where the solution is stored until it is transferred to the application point.

Salt blends used in this embodiment of the present invention may include one or more metal halide compounds and at least sulfamic acid, but may also or alternatively include an organic sulfonamide or any other halogen stabilizing compound in any desired combination. Metal halide compounds useful here include, but are not limited to, sodium chloride, potassium chloride, sodium bromide, potassium bromide, sodium iodide, and potassium iodide. In addition to sulfamic acid, the organic sulfonamide component or halogen stabilizing component of the salt blend used in the present invention can include, but is not limited to, methylsulfonamide, o- toluenesulfonamide, m-toluenesulfonamide, p-toluenesulfonamide, cyanuric acid and its derivatives, succinimide and its derivatives, and hydantoin and its derivatives or any combination of these compounds. The ratio of metal halides to halogen stabilizing compounds in the blended salt used to prepare the brines is preferably carefully controlled in order to produce the desired aqueous solution comprising free halogen species, N-halosulfamate compounds, N,N-dihalosulfamate compounds, N-halosulfonamide compounds, N,N-dihalosulfonamide compounds, and any combination thereof in a highly stable, concentrated form.

Control over the brine content is preferably achieved by producing the salt blend as a pellet, briquette, or other compacted form, such that the individual components of the salt pellet or briquette are introduced into the brine at a predictable rate. Here, the salt blend preferably comprises at least one halide-containing salt combined with sulfamic acid and/or other halogen stabilizing agents as desired. The halide containing salt is preferably sodium chloride, although other halide containing salts can be used alone or in combination with sodium chloride. These salts include, but are not limited to, lithium chloride, potassium chloride, lithium bromide, sodium bromide, potassium bromide, lithium iodide, sodium iodide, and potassium iodide. Additional halogen stabilizing compounds that could be used in this embodiment of the present invention in addition to sulfamic acid include, but are not limited to, lithium sulfamate, sodium sulfamate, potassium sulfamate, o- toluenesulfonamide, m-toluenesulfonamide, p-toluenesulfonamide, cyanuric acid and its derivatives, succinimide and its derivatives, and hydantoin and its derivatives. In one embodiment a metal halide salt is preferably combined with sulfamic acid to form a solid solution. The sulfamic acid is preferably no more than approximately 30% by weight of the solid solution and the metal halide is preferably at least approximately 70% by weight of the solid solution. The components are

preferably thoroughly mixed and evenly dispersed throughout the solid solution. Additionally, other components, such as anticaking components, can be added to this mixture. When diluted, this salt blend produces a brine with a predictable and steady composition which can be used to produce, through electrolysis and the subsequent chemical transformations described above, the desired product biocidal solutions.

Alternatively, brines with a desired composition can be formulated and used as an aqueous solution. In such embodiments the brine preferably comprises a halide containing salt and sulfamic acid dissolved in water at the desired concentrations and in the desired ratio of halide ion to sulfamic acid. The halide containing salt is preferably sodium chloride, although any other halide containing salt could be used in this embodiment of the present invention either alone or in combination with sodium chloride. These salts include, but are not limited to, lithium chloride, potassium chloride, lithium bromide, sodium bromide, potassium bromide, lithium iodide, sodium iodide, and potassium iodide. Additionally, other halogen stabilizing compounds can be added to these brines in addition to the sulfamic acid. These halogen stabilizing compounds can include, but are not limited to, lithium sulfamate, sodium sulfamate, potassium sulfamate, o- toluenesulfonamide, m-toluenesulfonamide, p-toluenesulfonamide, cyanuric acid and its derivatives, succinimide and its derivatives, and hydantoin and its derivatives.

The present invention preferably does not require the addition of a non-amine base to produce the desired halosulfamate or halosulfamic acid solution. In U.S. Patent No. 3,776,825, Vit discloses that electrolytically produced aqueous solutions of chloramines having a pH in the range of 8 to 12 require the use of a brine made from a combination of a salt containing at least one halide ion, at least one amine compound and, importantly, a hydroxide compound used in molar excess of the amine compound which is required for pH control. In the examples disclosed by Vit, the pH of the brines used to prepare the desired aqueous organic haloamine solutions were all greater than 12 (calculated from the numbers presented by Vit). In contrast, the present invention preferably is performed with an initial brine pH of less than 12, and more preferably less than 10, and even more preferably less than 7, and even more preferably less than 4, and even more preferably less than 2, and even more preferably less than 1.

An alternative embodiment of the present invention is shown in FIG. 2. In this embodiment of the present invention, tank **20** is a brine generator where the brine formed by the generator comprises metal halide salts substantially without sulfamic and is fed with water from a source (not shown). Similarly, tank

26 is also a brine generator where the brine formed by the generator sulfamic acid substantially without metal halide salts, organic sulfonamide compounds, or combinations thereof. Brine produced in tank **20** is transferred to line **24** through the action of pump **22** while the brine produced in tank **26** is also transferred to line **24** through the action of pump **28**. Line **24** also preferably contains water from a source not shown
5 here, which serves to dilute the brines from tank **20** and tank **24** to the desired concentration. The diluted brine stream then enters generation system **30** wherein the desired biocidal solution is produced and is then transferred through line **32** to tank **34**. The electrolyzed solution is then stored in tank **34** until it is transferred to the application point.

The embodiment depicted in FIG. 2 could optionally utilize a multitude of brine generator tanks
10 and injection pumps to provide a further degree of control over the composition of the brine solution used in this process. For example, separate brine generation tanks could contain singular metal halide salts, sulfamic acid, and organic sulfonamide compounds which could be selectively and individually injected into the brine stream entering generator system **30** in any desired composition, thereby producing a biocidal solution of any desired composition. This embodiment of the present invention would be
15 advantageous in applications where several biocidal solutions or different compositions are required for different water treatment applications within a single facility, with the desired solution being able to be produced on demand by simply varying the amounts of the different components of the brine solution. A plurality of product tanks could optionally be utilized so that each specifically desired biocidal solution could be stored and applied separately.

An alternative embodiment of the present invention is shown in FIG. 3. In this embodiment, brine
20 from a source not shown here is transferred through the action of pump **40** into generation system **42**. In this embodiment, the brine is at a ready-to-use concentration and does not need to be diluted by process water as shown in the other embodiments of the present invention. Once the brine is in generation system **42**, the brine is electrolyzed and transferred out of generation system **42** along line **44** and into
25 tank **46**, where the electrolyzed solution is stored until needed and transferred out of tank **46** using a mechanism not shown here.

The generation systems described above preferably comprise the electrochemical cell(s) in which the electrochemical oxidation of halide ions to aqueous halogens occurs. Once the aqueous halogen species is formed, it is free to react with sulfamic acid, producing the desired biocidal solution containing

a combination of free halogen species, N-halosulfamate, N-halosulfamic acid, N,N-dihalosulfamate, and N,N-dihalosulfamic acid. A plurality of sensors and control systems (not shown) are preferably used by the present invention to ensure that the proper brine composition is utilized by generator system **8** or generator system **30** to produce the desired biocidal solution.

5 In the practice of all embodiments of the present invention, it is possible to control the composition of the electrolyzed solution by varying the composition of the brine used in the production process as well as the overall flow through the electrolytic cell. For example, by varying the molar ratio of the total halide ion content of the brine to the sulfamic acid or total sulfamic acid and other stabilizer component of the brine, it is possible to produce solutions which comprise the desired amount of free
10 halogen and stabilized halogen species. Moreover, it is also possible to achieve control over the pH of the electrolyzed solution by varying this ratio as well, so that low pH oxidant solutions can be produced when the ratio of sulfamic acid to total halide ion content is high enough. Similarly, in cases where a biocidal solution comprising two or more halogen species is desirable, it is possible to control the ratio of halogen in the biocidal solution by varying the ratio of different halide ions in the brine.

15 Electrolysis operational parameters can also be used to vary the composition of the electrolyzed solution, primarily through adjusting the flow rate through the electrolytic cell. Under low flow conditions, electrolyzed solutions at high pH and increased combined halogen content are typically produced, while at higher flow rates, the electrolyzed solution is typically produced at low pH and decreased combined halogen content, even though the brine concentration is the same. This unexpected finding can be very
20 useful in the practice of the present invention, for example by providing a method by which the electrolytic cell can be self-cleaned. It is well known in the art that the electrolysis of halide containing brines will result in the formation of scales on the cathode surfaces. These scales typically comprise calcium carbonate, although magnesium hydroxide, iron oxide, and manganese oxide scales can also form on the cathode. Scale formation on the cathodes is primarily driven by the low pH environment at the cathode
25 surface, and it is well known in the art that acid can be used to remove scales from the cathode surfaces. In the practice of the present invention, it is possible to automatically remove the scale from the electrode surface while continuing the production of the desired biocidal solution by simply increasing the flow of the brine through the cell such that an acidic oxidant solution is produced, thereby cleaning the scale from the electrode surfaces. The composition of the electrolyzed product produced during the cleaning cycle

would be different than the composition of the electrolyzed product produced during normal operation of the system.

In general, embodiments of the present invention can produce a solution that has a total halogen content of less than 500 mg/L, more preferably less than 1000 mg/L, even more preferably less than 2100 mg/L, even more preferably more than 2100 mg/L, even more preferably more than 2500, and even more preferably more than 3000. In addition, embodiments of the present invention can be tailored so that the pH of the electrolyzed solution can be quite high even though the pH of the brine prior to electrolysis is very low.

The following examples demonstrate that varying the brine composition as well as the electrolysis operational parameters define the composition of the electrolyzed solution.

Example 1

Using an electrochemical system similar to the one depicted in FIG.3, brines containing a mixture of sodium chloride and sulfamic acid were electrolyzed at an applied plate-to-plate voltage of 6 V to produce solutions comprising free chlorine species, N-chlorosulfamate, N-chlorosulfamic acid, N,N-dichlorosulfamate, and N,N-dichlorosulfamic acid. Brines used in this example were prepared with a sodium chloride content of 30 g/L in every brine along with a sulfamic acid content of between 1 and 12 g/L. All brines prepared for this test had a pH of 2.12 or less. After electrolysis, the free chlorine content (representing only chlorine, hypochlorous acid, and hypochlorite ions) was measured alongside the total chlorine content, which measured free chlorine species as well as N-chlorosulfamate, N-chlorosulfamic acid, N,N-dichlorosulfamate, and N,N-dichlorosulfamic acid. These results are given in Table 1 below. As can be seen, the relative composition of the electrolyzed solution varies as a function of the sulfamic acid content in the initial brine. Moreover, when the sulfamic acid content of the brine was ~12% and higher, the electrolyzed solution primarily comprised N-chlorosulfamate, N-chlorosulfamic acid, N,N-dichlorosulfamate, and N,N-dichlorosulfamic acid, with very few free chlorine species present.

Sulfamic acid content in the brine (%)	Brine pH	Free chlorine content in the electrolyzed solution (mg/L)	Total chlorine content in the electrolyzed solution (mg/L)	Electrolyzed solution pH	Percent free chlorine in the electrolyzed solution (%)	Percent N-chlorosulfamate, N-chlorosulfamic acid, N,N-dichlorosulfamate, and N,N-dichlorosulfamic acid in the electrolyzed solution (%)
3	2.12	2675	3950	11.28	68	32
6	1.81	1650	4025	11.48	41	59
9	1.63	400	3925	11.40	10	90
12	1.53	175	3850	10.48	5	95
14	1.45	190	4000	9.96	5	95
17	1.39	85	4300	9.40	2	98
19	1.33	135	4475	2.39	3	97
21	1.26	115	4825	1.90	2	98
23	1.25	130	4950	1.63	3	97
29	1.19	70	5200	1.48	1	99

Table 1

Example 2

Electrolysis of brines containing mixed halide ions and sulfamic acid can be utilized to produce complex disinfection solutions containing mixed halogen, halosulfamic acid, and halosulfamate compounds. Using an electrochemical system similar to the one depicted in FIG.3, brines containing a mixture of sodium chloride and sulfamic acid were electrolyzed at an applied plate-to-plate voltage of 6 V to produce solutions comprised of free chlorine species, N-halosulfamate, N-halosulfamic acid, N,N-dihalosulfamate, and N,N-dihalosulfamic acid. In this example, N-halosulfamate can be either N-chlorosulfamate or N-bromosulfamate, N-halosulfamic acid can be either N-chlorosulfamic acid or N-bromosulfamic acid, N,N-dihalosulfamate can be N,N-dichlorosulfamate, N,N-dibromosulfamate, or N-bromo-N-chlorosulfamate, and N,N-dihalosulfamic acid can be N,N-dichlorosulfamic acid, N,N-dibromosulfamic acid, or N-bromo-N-chlorosulfamic acid. Brines used in this example were prepared with a sodium chloride content of 24 g/L and a sodium bromide content of 6 g/L in every brine along with a sulfamic acid content of between 0 and 10 g/L, resulting in brines comprising between 0% and 12% by weight sulfamic acid, 18% to 20% by weight sodium bromide, and 71% to 80% by weight sodium chloride. Brines containing sulfamic acid in this example had a pH of 2.04 or less. After electrolysis, the free halogen content, representing the content of chlorine, hypochlorous acid, hypochlorite ions, bromine,

hypobromous acid, and hypobromite ions was measured. The free bromine content, measuring only the presence of bromine, hypobromous acid, and hypobromite ions was also measured along with the total halogen content, which measured all free halogen species along with the N-halosulfamate, N-halosulfamic acid, N,N-dihalosulfamate, and N,N-dihalosulfamic acid content. These results are given in Table 2 below. As can be seen in this data, increasing the amount of sulfamic acid in the brine decreased the free halogen percentage in the electrolyzed brine while the percentage of the N-halosulfamate, N-halosulfamic acid, N,N-dihalosulfamate, and N,N-dihalosulfamic acid content increased correspondingly. Unexpectedly, the bulk of the free halogen content in all brines with added sulfamic acid was found to be free bromine species.

Sodium Chloride content in the brine (%)	Sodium Bromide content in the brine (%)	Sulfamic acid content in the brine (%)	Brine pH	Free halogen content in the electrolyzed solution (mg/L (%))	Free bromine content of the free halogen in the electrolyzed solution (mg/L (%))	Total halogen content in the electrolyzed solution (mg/L (%))	Electrolyzed Solution pH
80	20	0	6.94	3600 (100)	2750 (76)	Not Applicable	9.87
77	19	3	2.04	3200 (85)	2400 (75)	3750 (15)	11.18
75	19	6	1.77	2600 (70)	2400 (92)	3700 (30)	11.23
73	18	9	1.58	1925 (53)	1825 (95)	3625 (47)	11.06
71	18	12	1.48	2125 (53)	1850 (87)	4025 (47)	10.53

Table 2

Example 3

Stability of solutions produced through the electrolysis of brines containing mixed halide ions and sulfamic acid was examined using the same procedure outlined in Example 2. Here, using an electrochemical system similar to the one depicted in Fig. 3, brines containing a mixture of sodium chloride, sodium bromide, and sulfamic acid were electrolyzed at an applied plate-to-plate voltage of 6 V to produce solutions comprised of free chlorine species, N-halosulfamate, N-halosulfamic acid, N,N-dihalosulfamate, and N,N-dihalosulfamic acid. Brines used in this example were prepared with a sodium chloride content of 24 g/L and a sodium bromide content of 6 g/L in every brine along with a sulfamic acid content of between 0 and 6 g/L, giving brines comprised of between 0% and 9% by weight sulfamic acid,

18% to 20% by weight sodium bromide, and 73% to 80% by weight sodium chloride. Brines used in this example had a pH of 2.09 or less. Total halogen content of these solutions was measured immediately after electrolysis as well as after the electrolyzed solutions were stored for 24 hours. These results are shown in Table 3, where it can be seen that the addition of even 3% sulfamic acid to the electrolyzed

5 brine confers a high degree of stability on the total halogen content of the electrolyzed solution compared to solutions where sulfamic acid was not added. Additionally, the compositions of the chlorine and bromine components of the free halogen species of these solutions were also measured both immediately after electrolysis and after storage for 24 hours. These results, given in Table 4, show that for all solutions tested, the relative amount of bromine in the free halogen content of the electrolyzed brines

10 increases during aging, indicating that a continuous oxidation process of bromide ions during storage is occurring.

Sulfamic acid content in the brine (%)	Brine pH	Total halogen content in the electrolyzed solution immediately after electrolysis (mg/L)	Total halogen content in the electrolyzed solution after 24 hours of storage (mg/L)	Percent loss of the total halogen content after storage for 24 hours (%)	Electrolyzed solution pH
0	6.82	3375	450	87	9.91
3	2.09	3400	3400	0	11.12
9	1.62	3350	3200	4	11.13

Table 3

Sulfamic acid content in the brine (%)	Free halogen content in the electrolyzed brine		Free bromine content in the electrolyzed brine		Free bromine content of the free halogen in the electrolyzed brine (%)	
	Immediately after electrolysis	After storage for 24 hours	Immediately after electrolysis	After storage for 24 hours	Immediately after electrolysis	After storage for 24 hours
0	3100	450	2125	375	69	83
3	2850	2975	1925	2350	68	79
9	2050	2275	1825	2175	89	96

Table 4

Example 4

Using an electrochemical system similar to the one depicted in FIG.1, brines containing a mixture of sodium chloride and sulfamic acid were combined with process flow water and electrolyzed at an

applied plate-to-plate voltage of 6 V to produce solutions comprising free chlorine species, N-chlorosulfamate, N-chlorosulfamic acid, N,N-dichlorosulfamate, and N,N-dichlorosulfamic acid. Brines used in this example were prepared with >99% saturated aqueous sodium chloride with sulfamic acid added at a concentration of between 0 and 200 g/L. Brines containing sulfamic acid in this example typically had a pH of less than 1. After electrolysis, the pH of the electrolyzed solution was measured alongside the total chlorine content, which measured free chlorine species as well as N-chlorosulfamate, N-chlorosulfamic acid, N,N-dichlorosulfamate, and N,N-dichlorosulfamic acid. These results are given in Table 5 below. When the brine sulfamic acid content was 150 g/L or lower, the pH of the electrolyzed solution was 9.28 or higher. However, when the sulfamic acid content was increased to above 150 g/L, the pH of the electrolyzed solution rapidly decreased to as low as 2.03. Thus the final composition of the electrolyzed solution can be varied depending on even small changes in the sulfamic acid content of the brine.

Sulfamic acid content in the brine (g/L)	Total halogen content in the electrolyzed solution (mg/L)	pH of the electrolyzed solution
0	3100	9.28
10	3300	10.79
20	3350	11.14
30	3325	11.41
40	3475	11.46
50	3650	11.55
60	3550	11.59
70	3525	11.62
80	3525	11.69
90	3525	11.64
100	3475	11.44
110	3375	11.18
120	3350	10.99
130	3075	10.43
140	3050	10.16
150	3125	9.76
160	3050	5.34
170	2775	2.33
180	2975	2.68
190	2725	2.16
200	2575	2.03

Table 5

Example 5

Using an electrochemical system similar to the one depicted in FIG.1, brines containing a mixture of sodium chloride and sulfamic acid were combined with process flow water and electrolyzed at an applied plate-to-plate voltage of 6 V to produce solutions comprising free chlorine species, N-chlorosulfamate, N-chlorosulfamic acid, N,N-dichlorosulfamate, and N,N-dichlorosulfamic acid. Brines used in this example were prepared with >99% saturated aqueous sodium chloride with sulfamic acid added to a concentration of 80 g/L, with the brine having a pH of less than 1. In this example, the total flow of water through the system was varied between 19.6 and 44.9 gallons per hour. After electrolysis, the pH of the electrolyzed solution was measured alongside the total chlorine content, which measured free chlorine species as well as N-chlorosulfamate, N-chlorosulfamic acid, N,N-dichlorosulfamate, and N,N-dichlorosulfamic acid. These results are given in Table 6 below. Unexpectedly, the pH of the electrolyzed solution was highly dependent on total flow rate. Under low flow conditions (24.4 gal/hr or lower), the pH of the electrolyzed solution was higher than 10.25. In the transition flow range of 28.5 to 32.0 gal/hr, the pH of the electrolyzed solution was more moderate with a range of 3.90 to 8.86. When the flow was 33.3 gal/hr or higher, the pH of the electrolyzed solution was highly acidic and lower than 2.81, and as low as 2.05.

Water Flow Rate (gal/hr)	pH the electrolyzed solution	Total halogen content in the electrolyzed solution (mg/L)
19.6	11.46	4108
21.5	10.79	3808
24.4	10.25	3400
28.5	8.86	2767
30.9	7.54	2867
32.0	3.90	2667
33.3	2.81	2633
34.3	2.73	2525
36.7	2.13	2392
39.1	2.09	2308
42.0	2.05	2242
44.9	2.06	2042

Table 6

Although the invention has been described in detail with particular reference to the disclosed embodiments, other embodiments can achieve the same results. Variations and modifications of the present invention will be obvious to those skilled in the art and it is intended to cover all such modifications and equivalents. The entire disclosures of all patents and publications cited above are

5 hereby incorporated by reference.

CLAIMS

What is claimed is:

1. A method for producing a stable disinfecting solution comprising a plurality of halosulfamate species and/or halosulfamic acid species and one or more halogen species, the method comprising:

preparing an aqueous acidic solution comprising halide ions and sulfamic acid and having a pH of less than 7; and

electrolyzing said aqueous acidic solution to produce the stable disinfecting solution, wherein the concentrations of the halide ions and the sulfamic acid in said aqueous acidic solution and the pH of said aqueous acidic solution being such as to produce the stable disinfecting solution having a total halogen content of at least 2100 mg/L and exhibiting less than 5% loss of halogen content over a 24 hour time period.
2. The method of claim 1, wherein the aqueous acidic solution further comprises one or more additional halogen stabilizing compounds.
3. The method of claim 2, wherein the one or more additional halogen stabilizing compounds are selected from the group consisting of lithium sulfamate, sodium sulfamate, potassium sulfamate, organic sulfonamide, methylsulfonamide, o-toluenesulfonamide, m-toluenesulfonamide, p-toluenesulfonamide, cyanuric acid, a derivative of cyanuric acid, succinimide, a derivative of succinimide, hydantoin, a derivative of hydantoin, and combinations thereof.
4. The method of claim 3, wherein the stable disinfecting solution comprises N-halosulfonamide compounds and/or N,N-dihalosulfonamide compounds.
5. The method of claim 1, wherein the halosulfamate species comprise N-halosulfamate compounds and/or N,N-dihalosulfamate compounds.
6. The method of claim 1, wherein the halosulfamic acid species comprise N-halosulfamic acid compounds and/or N,N-dihalosulfamic acid compounds.
7. The method of claim 1, wherein the stable disinfecting solution has a total halogen content of at least 2500 mg/L.
8. The method of claim 1, wherein the aqueous acidic solution does not comprise a non-amine base.

9. The method of claim 1, wherein the preparing step comprises:

providing a salt blend comprising sulfamic acid and one or more salts comprising the halide ions;

and

diluting the salt blend with water.
10. The method of claim 9, wherein the salt blend comprises a pellet, briquette, or compacted form.
11. The method of claim 9, wherein the salt blend comprises a solid solution.
12. The method of claim 9, wherein the salt blend comprises an anti-caking agent.
13. The method of claim 1, further comprising flowing the aqueous acidic solution through an electrolytic cell at a flow rate selected to produce the desired pH of the stable disinfecting solution.
14. The method of claim 13, further comprising increasing the flow rate, thereby maintaining the acidity of electrolyte in the vicinity of cathodes in the electrolytic cell during the electrolyzing step.
15. The method of claim 14, further comprising removing scale from surfaces of the cathodes or preventing the formation of scale on the surfaces of the cathodes.
16. The method of claim 1, wherein the pH of the aqueous acidic solution is less than 4.
17. The method of claim 16, wherein the pH of the aqueous acidic solution is less than 2.
18. The method of claim 1, wherein the pH of the stable disinfecting solution is greater than 9.
19. The method of claim 18, wherein the pH of the stable disinfecting solution is greater than 11.
20. The method of claim 1, wherein the pH of the stable disinfecting solution is less than 3.