

METHOD AND APPARATUS OF PROVIDING POWER TO IGNITE AND SUSTAIN A PLASMA IN A REACTIVE GAS GENERATOR

FIELD OF THE INVENTION

[0001] The invention relates generally to the field of generating reactive gas containing ions, free radicals, atoms and molecules and to apparatuses for and methods of providing power for igniting and/or sustaining a plasma in a reactive gas generator.

BACKGROUND OF THE INVENTION

[0002] Plasma discharges can be used to excite gases to produce reactive gas containing ions, free radicals, atoms and molecules. Reactive gases are used for numerous industrial and scientific applications including processing solid materials such as semiconductor wafers, powders, and other gases.

[0003] One example of a reactive gas is atomic fluorine, which can be used to clean chemical vapor deposition (CVD) chambers for deposition of thin films onto substrate surfaces. CVD chambers need to be routinely cleaned to remove the deposits that build up on the surfaces of chamber parts other than the substrate surfaces. Wet cleaning of a chamber is labor intensive and hazardous to workers, while cleaning the chamber with atomic fluorine generated by a plasma source allows the deposits to be removed without opening the chamber to atmosphere, improving tool productivity and working conditions. Typical source gases for atomic fluorine include perfluorocompounds (PFCs) such as NF_3 , CF_4 , CHF_3 , C_2F_6 , and C_4F_8 .

[0004] Another example of a reactive gas is atomic oxygen, which can be used for photoresist removal in microelectronics fabrication. After pattern generation, photoresist is removed by

exposing the wafer surface to atomic oxygen generated by a plasma source. Atomic oxygen reacts rapidly and selectively with photoresist, allowing the process to be conducted in a vacuum and at relatively low temperature.

SUMMARY OF THE INVENTION

[0005] Plasma can be generated through inductive coupling of energy from a power supply into a gas that is capable of being transformed into a plasma. Known techniques for igniting a plasma include applying a high voltage or current to spark gaps to generate the initial breakdown of the pre-ionized gas. Known feedback techniques for detecting plasma ignition and sustaining the plasma include use of the plasma current as the feedback signal. In addition, known techniques for igniting and sustaining a plasma include the use of one power train for controlling multi-power train systems. However, such techniques are generally not reliable for the following reasons: arcing outside of the ignition window often occurs, punch through often occurs due to high loop and/or spark voltages, the operation is unreliable due to the use of one power train for control and monitoring, and large mismatches exist between impedances.

[0006] The invention features methods and power supplies that provide power to ignite and sustain a plasma in a reactive gas generator. Any of the particular embodiments described below can realize one or more of the following advantages. Embodiments can provide for a larger ignition space (e.g., a broader range of pressure and/or gas flows capable of igniting) with less complexity. In addition, embodiments can provide for a higher dQ/dt , which can allow for a large change of gas flow rate. Embodiments can eliminate or minimize the risk of anodization breakdown and punch-through. Embodiments can provide for reliable ignition and operation. Embodiments can increase block life. In addition, embodiments can provide for safe drop-out under all gas conditions.

[0007] In one aspect, there is a method of igniting a plasma in a reactive gas generator. The method includes providing power from an ignition power supply to a plasma ignition circuit, measuring a pre-ignition signal of the plasma ignition circuit, adjusting the power provided to the plasma ignition circuit based on the measured pre-ignition signal and an adjustable pre-ignition control signal, and adjusting the adjustable pre-ignition control signal after a period of time has elapsed.

[0008] In another aspect, there is a system of controlling the ignition of a plasma in a reactive gas generator. The system includes a measurement device coupled to a plasma ignition circuit and configured to generate a pre-ignition signal. The system also includes a controller. The controller includes a computing means for adjusting an ignition power supply control signal based on the pre-ignition signal and an adjustable pre-ignition control signal, an outputting means for outputting the ignition power supply control signal to an ignition power supply, and a computing means for adjusting the adjustable pre-ignition control signal after a period of time has elapsed.

[0009] In other examples, any of the aspects above can include one or more of the following features. The ignition power supply can include a switching power source. The ignition power supply can include a half-bridge inverter or a full-bridge inverter. The pre-ignition signal can include a voltage, current, or power of the plasma ignition circuit, or any combination thereof. The pre-ignition signal can include a current between the ignition power supply and the plasma ignition circuit. Measuring the pre-ignition signal can include measuring a peak of the pre-ignition signal during the period of time.

[0010] In some embodiments, adjusting the power provided to the plasma ignition circuit can include adjusting a duty cycle and/or a frequency value of the ignition power supply. Adjusting

the power provided to the plasma ignition circuit can be based on the difference between the measured pre-ignition signal and the adjustable pre-ignition control signal. Adjusting the power provided to the plasma ignition circuit can include providing less power to the plasma ignition circuit if the measured pre-ignition signal is greater than the adjustable pre-ignition control signal, and providing more power to the plasma ignition circuit if the measured pre-ignition signal is less than the adjustable pre-ignition control signal.

[0011] In yet other embodiments, adjusting the adjustable pre-ignition control signal can include increasing the adjustable pre-ignition control signal after the period of time has elapsed. The adjustable pre-ignition control signal can be increased linearly with respect to time. Increasing the adjustable pre-ignition control signal can be bounded by a predetermined maximum control signal. The method can further include overriding the adjustment of the power provided to the plasma ignition circuit based on an override signal. The override signal can be based on a predetermined maximum control signal and the measured pre-ignition signal. Overriding the adjustment of the power provided to the plasma ignition circuit can include providing no power to the plasma ignition circuit during a second period of time.

[0012] In some embodiments, after an ignition period of time has elapsed, the method can further include adjusting the adjustable pre-ignition control signal to a reset value, maintaining the adjustable pre-ignition control signal at the reset value for a wait period of time, and adjusting the adjustable pre-ignition control after the wait period of time has elapsed. The plasma ignition circuit can include a transformer and a resonant circuit coupled to a primary winding of the transformer. The pre-ignition signal can include a voltage of the primary winding. The resonant circuit can include one or more inductors and one or more capacitors. The plasma ignition circuit can further include one or more ignition electrodes coupled to a

secondary winding of the transformer. The secondary winding can include a center tap coupled to ground. The transformer can be electromagnetically coupled to a plasma chamber for providing power to a plasma in the plasma chamber.

[0013] In yet other embodiments, the method can further include determining whether the plasma is present in the plasma chamber, using the plasma ignition circuit to provide power from the ignition power supply to the plasma in the plasma chamber, and, if the plasma is determined to be present in the plasma chamber, adjusting the power provided to the plasma ignition circuit based on a plasma control signal. Adjusting the power provided to the plasma can include adjusting a duty cycle and/or a frequency value of the ignition power supply. Adjusting the power provided to the plasma can be based on the difference between the measured pre-ignition signal and the plasma control signal. The method can further include measuring a plasma signal, wherein adjusting the power provided to the plasma is based on the difference between a measured plasma signal and the plasma control signal. The plasma signal can include a current of the primary winding, a power supply signal, a plasma chamber signal, or any combination thereof.

[0014] In some embodiments, the system can further can include the ignition power supply and the plasma ignition circuit coupled to the ignition power supply. The measurement device can be further configured to generate the pre-ignition signal based on a voltage measurement, a current measurement, a power measurement, or any combination thereof, of the plasma ignition circuit. The measurement device can further includes a peak detection unit for measuring a peak of the measurement during the period of time. The computing means for adjusting the ignition power supply control signal can be configured to adjust the ignition power supply control signal based on the difference between the pre-ignition signal and the adjustable pre-ignition control signal.

The computing means for adjusting the adjustable pre-ignition control signal can be configured to increase the adjustable pre-ignition control signal after the period of time has elapsed.

[0015] In yet other embodiments, the system can further include a plasma detection unit for detecting the presence of the plasma in the plasma chamber, and a power controller having a computing means for adjusting, if the plasma is determined to be present in the plasma chamber, power provided to the plasma ignition circuit based on a plasma control signal. The plasma control signal can include a predetermined plasma control value, a current of the primary winding, a power supply signal, a plasma chamber signal, or any combination thereof. The measurement device can be further coupled to one or more other plasma ignition circuits and can be configured to generate the pre-ignition signal based on measurements from the one or more other plasma ignition circuits. The outputting means for outputting the ignition power supply control signal can further include means for outputting the ignition power supply control signal to one or more other ignition power supplies associated with the one or more other plasma ignition circuits.

[0016] In other examples, any of the features above relating to a method can be performed by a system, and/or a controller of the system, configured to or having means for performing the method. In addition, any of the features above relating to a method can be performed by a computer program product including instructions being operable to cause a data processing apparatus to perform the method.

BRIEF DESCRIPTION OF THE DRAWINGS

[0017] The advantages of the invention described above, together with further advantages, will be better understood by referring to the following description taken in conjunction with the

accompanying drawings. The drawings are not necessarily to scale, emphasis instead generally being placed upon illustrating the principles of the invention.

[0018] Fig. 1 is a diagram illustrating a reactive gas generator to which embodiments of the invention may be applied.

[0019] Fig. 2 is a block diagram illustrating a top-level control system for a power train.

[0020] Fig. 3 is a flowchart depicting control of a power supply system to ignite and sustain a plasma in a reactive gas generator.

[0021] Figs. 4A-B are circuit diagrams illustrating a power supply and block ignition circuit according to different embodiments.

[0022] Fig. 5 is a block diagram illustrating a control system for a single power train according to one embodiment.

[0023] Figs. 6A-6C are timing diagrams illustrating inverter and primary current values according to different ignition scenarios.

[0024] Fig. 7 is a block diagram illustrating a top-level control system for two power trains.

DETAILED DESCRIPTION

[0025] The invention features methods and power supplies that provide power to ignite and sustain a plasma in a reactive gas generator. Any of the particular embodiments described below can realize one or more of the following advantages. Embodiments can provide for a larger ignition space (e.g., a broader range of pressure and/or gas flows capable of igniting) with less complexity. In addition, embodiments can provide for a higher dQ/dt , which can allow for a large change of gas flow rate. Embodiments can eliminate or minimize the risk of anodization

breakdown and punch-through within the plasma chamber. Embodiments can provide for reliable ignition and operation. Embodiments can increase block life. In addition, embodiments can provide for safe drop-out under all gas conditions.

[0026] Fig. 1 is a diagram illustrating a reactive gas generator **100** to which embodiments of the invention can be applied. As illustrated, the reactive gas generator **100** includes a power supply **110** and a plasma chamber **120**. The plasma chamber **120** includes an inlet **140** for receiving a gas (e.g., Argon) for transformation into a plasma (e.g., Ar⁺). Once generated, a plasma may be used directly, or can be used to excite one or more other source gases into corresponding reactive gases that exit the generator at outlet **142** and into, for example, a process chamber **145**.

[0027] In order to ignite and/or sustain a plasma, the power supply **110** includes a transformer **130**. The transformer primary includes a primary winding **132** wrapped about a portion of a magnetic core **134**. Energy from the power supply **110** is inductively coupled via the transformer primary to the gas traveling through the chamber **120** to ignite, generate, and/or sustain the plasma. The ignited plasma within the plasma chamber **120** serves as the transformer secondary. Specifically, the power supply **110** applies an excitation voltage of high magnitude across the primary winding **132** of the transformer. This high excitation voltage induces high current in the winding **132**, thereby generating an alternating magnetic field through the magnetic core **134** across a path of the gas. As a result, an electric field is induced within the gas, causing its ignition into a plasma and/or providing current to sustain the plasma. Once the plasma is generated, the plasma can be used to excite other source gas, producing a desired reactive gas for specific applications. The inner surface of the plasma chamber **120** can be coated and/or include an anodization layer (e.g., a dielectric material), for electrically isolating the plasma gas from the plasma chamber **120** itself.

[0028] Fig. 2 is a block diagram illustrating a top-level control system **200** for a power train.

The system **200** can include a DC supply **210**, a bridge inverter **220**, a resonant tank **230**, a frequency and duty cycle control unit **240**, a plasma detection unit **250**, and/or a safety and monitoring unit **260**. The DC supply **210** can provide a DC power to the bridge inverter **220**.

The bridge inverter **220**, in turn, can provide power to the resonant tank **230**. The bridge inverter **220** can be a half bridge or a full bridge power converter as known in the art. Alternatively, any adjustable source of alternating current or voltage can be used in place of the DC supply **210** and the bridge inverter **220**. The bridge inverter **220** can provide an alternating source signal having a frequency at or substantially at the resonant frequency of the resonant tank **230**, which can include a resonant circuit. The resonant circuit can include one or more inductors and one or more capacitors. The resonant tank **230** can be inductively coupled via a transformer **232** to a plasma load (not shown) and/or to an plasma ignition unit (not shown). The frequency and duty cycle control unit **240** can control the frequency, duty cycle, and/or amplitude of the source signal provided by the bridge inverter **220** and DC supply **210**. Control of the frequency and/or duty cycle by the unit **240** can be based on one or more signals measured from or provided by the DC supply **210**, the bridge inverter **220**, the resonant tank **230**, the plasma detection unit **250**, predetermined setpoint(s) **242**, and/or any combination thereof. The plasma detection circuit **250** can detect the presence of a plasma based on one or more signals from the resonant tank **230** (e.g., inverter current and/or primary current) and/or one or more other signals from other units in the system (e.g., a plasma current or a power signal from the DC supply **210**). The safety and monitoring unit **260** can provide one or more safety and monitoring functions to one or more of the units of the diagram **200**. For example, in one embodiment, the safety and monitoring unit

260 can provide an override signal to the bridge inverter **220** to prevent the buildup of additional energy in the resonant tank **230**.

[0029] Fig. 3 is a flowchart **300** depicting control of a power supply system to ignite and sustain a plasma in a reactive gas generator. The elements of flowchart **300** are described using the exemplary block diagram **200** of FIG. 2. Control of the power supply system **210** includes measuring a pre-ignition signal by the frequency and duty cycle control unit **240** (**310**), adjusting, by the frequency and duty cycle control unit **240**, a pre-ignition control signal (**320**), adjusting, by the bridge inverter **220**, power provided to the resonant tank **230** (**330**), and/or determining the presence of a plasma by the detection unit **250** (**340**).

[0030] The pre-ignition signal can include, for example, a voltage, current, and/or power of the resonant tank **230**. In one embodiment, the pre-ignition signal is a current (e.g., the inverter current) between the bridge inverter **220** and the resonant tank **230**. In an alternative embodiment, the pre-ignition signal is a voltage (e.g., the voltage of the transformer's primary winding). Measuring the pre-ignition signal (**310**) can include determining a peak of the pre-ignition signal during a period of time (e.g., for every time period based on the time cycle of the alternating power source **220**). In a supplemental or alternative embodiment, measuring the pre-ignition signal (**310**) can include taking an average of the measured signal, filtering the measured signal, and/or other signal processing functions.

[0031] Adjusting the pre-ignition control signal (**320**) can be based on a predetermined pre-ignition control signal profile. In one embodiment, the predetermined pre-ignition control signal profile can include a ramp-up portion followed by a clamped portion. The ramp-up portion can be based on, for example, any monotonically increasing function of time $F(t)$ (e.g., $F(t) = at$, where $a > 0$ is a selected slope value), in which case adjusting the pre-ignition control signal

includes evaluating the function F at a given time. In a supplemental embodiment, the predetermined pre-ignition control signal profile can include a delay period following the clamped portion.

[0032] Adjusting the power provided to the resonant tank **230** (**330**) can be based on the measured pre-ignition signal and the adjusted pre-ignition control signal. In one embodiment, the frequency and duty cycle control unit **240** can control the frequency and/or the duty cycle of the alternating source signal supplied by the bridge inverter **220**. In a supplemental or alternative embodiment, the control unit **240** can also control the amplitude of the power signal using, for example, the DC supply **210**. In another embodiment, adjusting the power (**330**) can be based on the difference between the measured pre-ignition signal and the adjustable pre-ignition control signal, in which less power can be provided if the measured pre-ignition signal is greater than the adjustable pre-ignition control signal and more power can be provided if the measured pre-ignition signal is less than the adjustable pre-ignition control signal.

[0033] Determining the presence of a plasma by the detection unit **250** (**340**) can be based on, for example, the primary current supplied to the transformer by the resonant tank **230**. In an alternative or supplemental embodiment, the presence of a plasma can be based on a power signal from the DC supply **210** or an RF signal from the resonant tank **230**. If a plasma is not detected, then the process can loop back to steps (**310**) and (**320**). If a plasma is detected, then the control unit **240** can enter into a plasma sustainability state, in which case the power provided to sustain the plasma can be adjusted to meet certain operating standards. In one embodiment, one or more elements of block diagram **200** can also be used to operate and provide power to the plasma chamber when a plasma is present.

[0034] Fig. 4A is a circuit diagram **400** illustrating a power supply and block ignition circuit according to one embodiment in which ignition occurs via ignition electrodes. While the circuit diagram **400** includes two modular power trains, other configurations with any number of modular power trains are possible. Each power train includes a power source **420a** and **420b** (e.g., an H-bridge) and a resonant circuit **430a** and **430b**. The power sources **420a** and **420b** can be respectively coupled to, for example, DC sources **422a** and **422b** (e.g., 360VDC). In the circuit diagram **400**, the resonant circuits **430a** and **430b** include three inductors (L_1 , L_2 and L_3) and two capacitors (C_a and C_b), however other resonant configurations can also be used. In one embodiment, the values of the inductors L_1 , L_2 and L_3 can be, respectively, 1.7uH, 1.7uH and 1.05uH, and the values of the capacitors C_a and C_b can be, respectively, 55.6nF and 37.6uF. The resonant circuits **430a** and **430b** are coupled to a magnetic core **425**.

[0035] The magnetic core **425** is coupled to a secondary plasma (not shown) and to a winding **432** wrapped about a portion of the magnetic core **425** of the transformer. When the power supplies **420a** and **420b** provide an excitation voltage across the primary winding, a current is induced within the winding **432** according to a turns ratio. The winding **432** can include a central ground tap, which results in the leads that extend from the winding being bipolar and thus enables the generation of positive and negative ignition electrodes. The leads of the winding **432** are switchably connected to one or more ignition electrodes **440a/440b** and **450a/450b** via, respectively, switches **435a** and **435b**. In addition, one or more capacitors C_7 can be placed between the winding **432** and the ignition electrodes **440a/440b** and **450a/450b**. The capacitors C_7 can have a value, for example, of 200 pF. Generally, the value of the capacitors C_7 can be chosen to limit the current to the ignition electrodes **440a/440b** and **450a/450b** such that charge buildup on the dielectrics is kept below predetermined levels.

[0036] The one or more ignition electrodes **440a/440b** and **450a/450b** can be arranged about or within the plasma chamber **120**. By placing the positive and negative ignition electrodes such that they oppose one another in the plasma chamber **120**, an increase in the amount of electric flux can be realized across the plasma chamber or channel. This can result in less voltage to ground being required to generate the requisite amount of electric flux to ignite the plasma gas. In one embodiment, the electrodes can be configured such that the electric field is generated across a channel of the plasma chamber **120**. When the switches **435a** and **435b** are connected to the ignition electrodes **440a/440b** and **450a/450b**, an electric field is generated between the ignition electrodes **440a/440b**, **450a/450b** and/or ground electrodes **460a** and **460b**, which can initiate breakdown in the gases present in the chamber to thereby ignite a plasma.

[0037] During plasma ignition, one or both of the relays **435a** and **435b** are closed so that the voltage from the leads can be applied to the one or more ignition electrodes **440a/440b** and **450a/450b**. Once the plasma ignites, the relays **435a** and **435b** are opened, disabling the capacitive discharge. A typical arrangement of ignition electrodes can be such that they are positioned about a cross section of a plasma chamber or channel within the chamber. Specifically, ignition electrodes **440a/440b** and **450a/450b** can be positioned on opposing sides of the plasma chamber **120** and are switchably connected to the leads of the winding **432**, resulting in both electrodes having the same polarity. Ground electrodes **460a** and **460b** can also be positioned on opposing sides of the plasma chamber or channel at an offset between the ignition electrodes **440a/440b** and **450a/450b**. Generally, any number of ignition electrodes can be placed throughout a plasma chamber. In one embodiment, the blocks of the plasma chamber **120** can serve as the ignition and ground electrodes.

[0038] Fig. 4B is a circuit diagram **401** illustrating an alternative configuration for coupling the ignition electrodes **440a/440b** and **450a/450b** to the leads of winding **432**. In particular, the ignition voltages are alternatively applied along a plasma channel in the circuit diagram **401**. Generally, the ignition voltages and/or ground electrodes can be applied in any configuration to one or more ignition electrodes along a plasma channel. Based on the configuration, the volume in the plasma chamber that is covered by the applied electric field can be maximized while limiting the voltage of ignition electrodes to ground.

[0039] The dielectric separation between each of the electrodes can be represented as one or more capacitors C_{dielec} **465**. The voltage (denoted as V_{spark}) at one of the leads of winding **432** can be related to the voltage (denoted as V_{dielec}) at one of the ignition electrodes as follows:

$$V_{dielec} = \frac{Z_{dielec}}{Z_{dielec} + Z_{\gamma}} V_{spark},$$

[0040] where $Z_{\gamma} = -j/(\omega C_{\gamma})$ and $Z_{dielec} = -j/(\omega C_{dielec})$.

[0041] Fig. 5 is a block diagram illustrating a control system **500** for a single power train according to one embodiment. The elements of the control system **500** can be implemented, for example, with the circuit **400** of FIG. 4. The system **500** includes a DC supply **510**, a bridge inverter **520** (e.g., a half or full bridge), a resonant circuit **530**, and control components. The resonant circuit **530** is coupled to a magnetic core **532**, which is coupled to a gas or plasma **533**. The magnetic core **532** can also be coupled to a circuit of one or more ignition electrodes, as depicted in Fig. 4, and/or to other ignition circuits. The system also includes detection units **540a** and **540b**. Detection unit **540a** can measure the peak inverter current **535a** and can perform additional signal processing (e.g., filtering, averaging, and/or smoothing) if necessary. Detection unit **540b** can measure the peak primary current **535** and can also perform additional

signal processing if necessary. The output from detection unit **540b** is provided to plasma detection unit **545**. The plasma detection unit **545** can determine whether a plasma **533** has been ignited based on whether, for example, the measured primary current is greater than a predetermined threshold value.

[0042] The plasma detection unit **545** controls switch **550**. In the absence of a plasma (e.g., during pre-ignition), the switch **550** latches to the pre-ignition control unit **555**. The operation of the pre-ignition control unit **555** is described below with reference to Figs. 6A-6C. In the presence of a plasma, the switch **550** latches to the post-ignition control unit **560**. The operation of system **500** will first be described when the system is in the pre-ignition state (i.e., switch **550** is latched to the control unit **555**).

[0043] The outputs from detection unit **540a** and the pre-ignition control unit **555** are provided to comparator **565**, which can take the difference between the two applied signals. The difference is, in turn, provided to a power supply control unit **570**. In one embodiment, the power supply control unit **570** can include a PID control unit and a control chip. The power supply control unit **570** can determine adjustments to the frequency, the duty cycle, and/or other characteristics of the alternating signal supplied by the bridge inverter **520**. For example, if the comparator **565** determines that the measured pre-ignition signal is greater than the pre-ignition control signal from unit **555**, then the duty cycle can be decreased and/or the frequency shifted away from the resonant frequency of the resonant circuit **530**. Likewise, if the comparator **565** determines that the measured pre-ignition signal is less than the pre-ignition control signal from unit **555**, then the duty cycle can be increased and/or the frequency shifted towards from the resonant frequency of the resonant circuit **530**. In a supplemental embodiment, the control unit **570** can be coupled to, or include, a hardware soft-start source **580**.

[0044] The control signal from the control unit **570** can be coupled to the bridge inverter **520** via a programmable logic device **485**. The programmable logic device **485** can be programmed to pass through the control signal in the absence of any override signal from the comparator **590**. The comparator **590** can issue an override signal if it determines that a measurement signal **595** based on the inverter current is greater than a predetermined threshold value **596**. The override mechanism thus established can advantageously provide a protection scheme for the system **500** for preventing unsafe energy levels from building up within the resonant circuit **530**.

[0045] As described above, if a plasma is detected, the switch **550** latches to the post-ignition control unit **560**. In one embodiment, the post-ignition control unit **560** can provide a predetermined inverter current control value based on the desired operating conditions of the plasma system. In this embodiment, the control unit **570** can adjust the power to the resonant circuit **530** such that the measured inverter current tracks the predetermined control value provided by the unit **560**. In another embodiment, the post-ignition control unit **560** can include a PID control that outputs a signal based on the difference between the measured primary current **535b** and a predetermined primary current control value based on the desired operating conditions of the plasma system. In yet another embodiment, the post-ignition control unit **560** can include a PID control that outputs a signal based on the difference between a measured power signal (not shown) and a predetermined power control value based on the desired operating conditions of the plasma system. The measured power signal can be, for example, provided by the DC supply **510** or from the other components of the system **500**.

[0046] Figs. 6A-6C are timing diagrams illustrating inverter and primary current values over time according to different ignition scenarios for a particular pre-ignition control signal generated by unit **555**. In particular, the predetermined pre-ignition control signal profile

generated by unit **555** is the same for Figs. 6A-6C and corresponds to the signal **610** as described below. Fig. 6A illustrates an ignition failure scenario, in which no plasma ignites. Fig. 6B illustrates plasma ignition after a clamp threshold is reached. Fig. 6C illustrates plasma ignition prior to a clamp threshold being reached. As illustrated in Fig. 6A, the pre-ignition control signal **610** increases linearly during a ramp-up period of time **614**, which can be, in one embodiment, about 20 ms. At time **614**, the pre-ignition control signal **610** is bounded (i.e., clamped) at a threshold value **612**. The threshold value **612** can be chosen to be below, for example, any value in which punch through is likely within the plasma chamber. Punch through can be dependent on choice of dielectric material, thickness of the dielectric material, geometry of the plasma chamber, and/or other characteristics of the plasma chamber and/or ignition circuit. Setting the threshold in such a fashion can therefore protect the anodization layer inside the plasma chamber from punch through. The pre-ignition control unit **555** maintains the signal **610** at the threshold value **612** for a predetermined amount of time **616**, which can be, in one embodiment, about 100 ms. If no plasma is detected prior to time **616**, the signal **610** resets to zero and the ramp up process starts over. In some embodiments, a delay period can be inserted after time **616** before the ramp up process starts again. In one embodiment, the delay period can be 400 ms. The following control values can be variably set and adjusted by the control system during operation based on desired operating conditions (e.g., based on different gas flow rates and/or types of gases): the threshold value **612**, the ramp-up time **614**, the reset time **616**, and/or the delay period.

[0047] The signal **610** in Fig. 6A also can represent the measured inverter current **535a** (or other corresponding pre-ignition signal) from the system, because the control unit **570** uses the feedback from the comparator **565** in order to have the inverter current **535a** track the desired

pre-ignition control profile **610** provided by the pre-ignition control unit **555**. During pre-ignition, the primary current **535b** is substantially zero and therefore is not illustrated in Fig. 6A.

[0048] The signals **620a/620b** and **640a/640b** in Figs. 6B-6C can represent the measured inverter current **535a** (or other corresponding pre-ignition signal), whereas the signals **630a/630b** and **650a/650b** can represent the measured primary current **535b**. Prior to ignition, the primary currents **630a** and **650a** are substantially zero. In Fig. 6B, ignition occurs after time **614**, whereas in Fig. 6C, ignition occurs prior to time **614**.

[0049] As illustrated in Figs. 6B-6C, when plasma ignition occurs, the inverters currents **620a** and **640a** initially drop in value and the primary currents **630a** and **650a** shoot up. In one embodiment, plasma detection occurs after the primary currents **630a** and **650a** have exceeded a detection threshold value for a period of time **618a** and **618b**. Upon plasma detection, the switch **550** latches on to the post-ignition control unit **560** which, in these illustrations, provides a control signal for the current higher than **612** in order to sustain the plasma. The system takes some amount of time before the inverter currents **620b** and **640b** stabilize at this value.

[0050] Fig. 7 is a block diagram illustrating a top-level control system **700** for two power trains that implement any of the above-mentioned features for a single power train system. While only two power trains are illustrated in Fig. 7, other configurations are possible for any number of power trains. The system **700** includes two DC supplies **711** and **712**, two bridge inverters **721** and **722**, two resonant tanks **731** and **732**, one frequency and duty cycle control unit **740**, one plasma detection unit **750**, and/or a safety and monitoring unit (not shown). The control unit **740** is a multiple-input-single-output (MISO) control unit. For example, the output control signals to bridge inverters **721** and **722** are the same. In one embodiment, the output control signals provide frequency and/or duty cycle values for the bridge inverters **721** and **722**. The inputs

provided to the control unit 740 can include, for example, the mean, average, or rms values of the inverter currents (or other pre-ignition signals) from the resonant tanks 731 and 732. For example, detection unit 540a can output a pre-ignition control signal to comparator 565 that represents one or more inverter currents from one or more power trains. Providing a MISO control unit can advantageously decrease the complexity of the control circuitry required for multiple power train systems. In addition, providing a single output control can advantageously provide for greater control and stability of the overall system 700.

[0051] The above-described techniques can be implemented in digital and/or analog electronic circuitry, or in computer hardware, firmware, software, or in combinations of them. The implementation can be as a computer program product, i.e., a computer program tangibly embodied in a machine-readable storage device, for execution by, or to control the operation of, a data processing apparatus, e.g., a programmable processor, a computer, and/or multiple computers. A computer program can be written in any form of computer or programming language, including source code, compiled code, interpreted code and/or machine code, and the computer program can be deployed in any form, including as a stand-alone program or as a subroutine, element, or other unit suitable for use in a computing environment. A computer program can be deployed to be executed on one computer or on multiple computers at one or more sites.

[0052] Method steps can be performed by one or more processors executing a computer program to perform functions of the invention by operating on input data and/or generating output data. Method steps can also be performed by, and an apparatus can be implemented as, special purpose logic circuitry, e.g., a FPGA (field programmable gate array), a FPAA (field-programmable analog array), a CPLD (complex programmable logic device), a PSoC

(Programmable System-on-Chip), ASIP (application-specific instruction-set processor), or an ASIC (application-specific integrated circuit). Subroutines can refer to portions of the computer program and/or the processor/special circuitry that implement one or more functions.

[0053] Processors suitable for the execution of a computer program include, by way of example, both general and special purpose microprocessors, and any one or more processors of any kind of digital or analog computer. Generally, a processor receives instructions and data from a read-only memory or a random access memory or both. The essential elements of a computer are a processor for executing instructions and one or more memory devices for storing instructions and/or data. Memory devices, such as a cache, can be used to temporarily store data. Memory devices can also be used for long-term data storage. Generally, a computer also includes, or is operatively coupled to receive data from or transfer data to, or both, one or more mass storage devices for storing data, e.g., magnetic, magneto-optical disks, or optical disks. A computer can also be operatively coupled to a communications network in order to receive instructions and/or data from the network and/or to transfer instructions and/or data to the network. Information carriers suitable for embodying computer program instructions and data include all forms of volatile and non-volatile memory, including by way of example semiconductor memory devices, e.g., DRAM, SRAM, EPROM, EEPROM, and flash memory devices; magnetic disks, e.g., internal hard disks or removable disks; magneto-optical disks; and optical disks, e.g., CD, DVD, HD-DVD, and Blu-ray disks. The processor and the memory can be supplemented by and/or incorporated in special purpose logic circuitry.

[0054] To provide for interaction with a user, the above described techniques can be implemented on a computer in communication with a display device, e.g., a CRT (cathode ray tube), plasma, or LCD (liquid crystal display) monitor, for displaying information to the user and

a keyboard and a pointing device, e.g., a mouse, a trackball, a touchpad, or a motion sensor, by which the user can provide input to the computer (e.g., interact with a user interface element). Other kinds of devices can be used to provide for interaction with a user as well; for example, feedback provided to the user can be any form of sensory feedback, e.g., visual feedback, auditory feedback, or tactile feedback; and input from the user can be received in any form, including acoustic, speech, and/or tactile input.

[0055] The above described techniques can be implemented in a distributed computing system that includes a back-end component. The components of the computing system can be interconnected by a transmission medium, which can include any form or medium of digital or analog data communication (e.g., a communication network). The transmission medium can include one or more packet-based networks and/or one or more circuit-based networks in any configuration. Packet-based and/or circuit-based networks can include wireline and/or wireless networks.

[0056] One skilled in the art will realize the invention may be embodied in other specific forms without departing from the spirit or essential characteristics thereof. The foregoing embodiments are therefore to be considered in all respects illustrative rather than limiting of the invention described herein. Scope of the invention is thus indicated by the appended claims, rather than by the foregoing description, and all changes that come within the meaning and range of equivalency of the claims are therefore intended to be embraced therein.

What is claimed:

1. A method of igniting a plasma in a reactive gas generator, comprising:
providing power from an ignition power supply to a plasma ignition circuit;
measuring a pre-ignition signal of the plasma ignition circuit;
5 adjusting the power provided to the plasma ignition circuit based on the measured pre-ignition signal and an adjustable pre-ignition control signal; and
adjusting the adjustable pre-ignition control signal after a period of time has elapsed.
2. The method of claim 1 wherein the ignition power supply comprises a switching power source.
- 10 3. The method of claim 1 wherein the ignition power supply comprises a half-bridge inverter or a full-bridge inverter.
4. The method of claim 1 wherein the pre-ignition signal comprises a voltage, current, or power of the plasma ignition circuit, or any combination thereof.
5. The method of claim 1 wherein the pre-ignition signal comprises a current between the
15 ignition power supply and the plasma ignition circuit.
6. The method of claim 1 wherein measuring the pre-ignition signal comprises measuring a peak of the pre-ignition signal during the period of time.
7. The method of claim 1 wherein adjusting the power provided to the plasma ignition circuit comprises adjusting a duty cycle and/or a frequency value of the ignition power supply.
- 20 8. The method of claim 1 wherein adjusting the power provided to the plasma ignition circuit is based on the difference between the measured pre-ignition signal and the adjustable pre-ignition control signal.

9. The method of claim 8 wherein adjusting the power provided to the plasma ignition circuit comprises:

providing less power to the plasma ignition circuit if the measured pre-ignition signal is greater than the adjustable pre-ignition control signal; and

5 providing more power to the plasma ignition circuit if the measured pre-ignition signal is less than the adjustable pre-ignition control signal.

10. The method of claim 1 wherein adjusting the adjustable pre-ignition control signal comprises increasing the adjustable pre-ignition control signal after the period of time has elapsed.

10 11. The method of claim 10 wherein the adjustable pre-ignition control signal is increased linearly with respect to time.

12. The method of claim 10 wherein increasing the adjustable pre-ignition control signal is bounded by a predetermined maximum control signal.

15 13. The method of claim 1 further comprising overriding the adjustment of the power provided to the plasma ignition circuit based on an override signal.

14. The method of claim 13 wherein the override signal is based on a predetermined maximum control signal and the measured pre-ignition signal.

15. The method of claim 13 wherein overriding the adjustment of the power provided to the plasma ignition circuit comprises providing no power to the plasma ignition circuit during a
20 second period of time.

16. The method of claim 1, after an ignition period of time has elapsed, further comprising:
adjusting the adjustable pre-ignition control signal to a reset value;

maintaining the adjustable pre-ignition control signal at the reset value for a wait period of time; and

adjusting the adjustable pre-ignition control after the wait period of time has elapsed.

17. The method of claim 1 wherein the plasma ignition circuit comprises a transformer and a resonant circuit coupled to a primary winding of the transformer.

18. The method of claim 17 wherein the pre-ignition signal comprises a voltage of the primary winding.

19. The method of claim 17 wherein the resonant circuit comprises one or more inductors and one or more capacitors.

20. The method of claim 17 wherein the plasma ignition circuit further comprises one or more ignition electrodes coupled to a secondary winding of the transformer.

21. The method of claim 20 wherein the secondary winding comprises a center tap coupled to ground.

22. The method of claim 17 wherein the transformer is electromagnetically coupled to a plasma chamber for providing power to a plasma in the plasma chamber.

23. The method of claim 22 further comprising:
determining whether the plasma is present in the plasma chamber;
using the plasma ignition circuit to provide power from the ignition power supply to the plasma in the plasma chamber; and

if the plasma is determined to be present in the plasma chamber, adjusting the power provided to the plasma ignition circuit based on a plasma control signal.

24. The method of claim 23 wherein adjusting the power provided to the plasma comprises adjusting a duty cycle and/or a frequency value of the ignition power supply.

25. The method of claim 23 wherein adjusting the power provided to the plasma is based on the difference between the measured pre-ignition signal and the plasma control signal.

26. The method of claim 23 further comprising measuring a plasma signal, wherein adjusting the power provided to the plasma is based on the difference between a measured plasma signal and the plasma control signal.

27. The method of claim 26 wherein the plasma signal comprises a current of the primary winding, a power supply signal, a plasma chamber signal, or any combination thereof.

28. A system of controlling the ignition of a plasma in a reactive gas generator, the system comprising:

a measurement device coupled to a plasma ignition circuit and configured to generate a pre-ignition signal;

a controller having:

(i) a computing means for adjusting an ignition power supply control signal based on the pre-ignition signal and an adjustable pre-ignition control signal;

(ii) an outputting means for outputting the ignition power supply control signal to an ignition power supply; and

(iii) a computing means for adjusting the adjustable pre-ignition control signal after a period of time has elapsed.

29. The system of claim 28 further comprising:

the ignition power supply; and

the plasma ignition circuit coupled to the ignition power supply

30. The system of claim 29 wherein the ignition power supply comprises a half-bridge inverter or a full-bridge inverter.

31. The system of claim 28 wherein the measurement device is further configured to generate the pre-ignition signal based on a voltage measurement, a current measurement, a power measurement, or any combination thereof, of the plasma ignition circuit.
32. The system of claim 31 wherein the measurement device further comprises a peak
5 detection unit for measuring a peak of the measurement during the period of time.
33. The system of claim 28 wherein the computing means for adjusting the ignition power supply control signal is configured to adjust the ignition power supply control signal based on the difference between the pre-ignition signal and the adjustable pre-ignition control signal.
34. The system of claim 28 wherein the computing means for adjusting the adjustable pre-
10 ignition control signal is configured to increase the adjustable pre-ignition control signal after the period of time has elapsed.
35. The system of claim 34 wherein the increase in the adjustable pre-ignition control signal is bounded by a predetermined maximum control signal.
36. The system of claim 29 wherein the plasma ignition circuit comprises a transformer and a
15 resonant circuit coupled to a primary winding of the transformer.
37. The system of claim 36 wherein the resonant circuit comprises one or more inductors and one or more capacitors.
38. The system of claim 36 wherein the plasma ignition circuit further comprises one or more ignition electrodes coupled to a secondary winding of the transformer.
- 20 39. The system of claim 38 wherein the secondary winding comprises a center tap coupled to ground.
40. The system of claim 36 wherein the transformer is electromagnetically coupled to a plasma chamber for providing power to a plasma in the plasma chamber.

41. The system of claim 28 further comprising:

a plasma detection unit for detecting the presence of the plasma in the plasma chamber;

and

a power controller having a computing means for adjusting, if the plasma is determined

5 to be present in the plasma chamber, power provided to the plasma ignition circuit based on a plasma control signal.

42. The system of claim 41 wherein the plasma control signal comprises a predetermined plasma control value, a current of the primary winding, a power supply signal, a plasma chamber signal, or any combination thereof.

10 43. The system of claim 28 wherein the measurement device is further coupled to one or more other plasma ignition circuits and is configured to generate the pre-ignition signal based one measurements from the one or more other plasma ignition circuits.

44. The system of claim 43 wherein the outputting means for outputting the ignition power supply control signal further comprises means for outputting the ignition power supply control
15 signal to one or more other ignition power supplies associated with the one or more other plasma ignition circuits.