

**CONTROL OF EXPANSION IN CONCRETE
DUE TO ALKALI SILICA REACTION**

Field of the Invention

5 The present invention relates to admixtures for
cement compositions that include spodumene to reduce
expansion. In particular, the present invention
relates to a cement admixture, and the resultant
improved cement composition, capable of inhibiting
cracking of concrete due to the alkali-silica
10 reaction.

Background of the Invention

15 Deterioration of concrete is known to occur due
to chemical reactions between certain hydraulic cement
constituents and those constituents present in the
aggregate of a concrete mix. Certain materials are
known to be reactive with the alkalis in cements.
These materials include various forms of silica, such
as opal, chalcedony, tridymite and cristobalite. For
example, it is known that when hydrated silica which
20 is inherent in aggregate comes into contact with
sodium or potassium at high pH (the high pH being
caused by hydroxyl ions present from alkaline
compounds of cement), alkali silicate is formed.
Alkali may also be derived from external sources such
25 as deicing salts and sea water, as well as from
internal sources such as admixtures, fly ash and
alkali-bearing aggregates. Alkali silicates, which
are the product of this "alkali-silica reaction", form
a water swellable expansive gel deposit within and on
30 the exterior surface of the aggregate particles
contained in concrete. Under moist conditions, the

swelling of this gel can eventually produce sufficient pressure to induce deleterious cracking and expansion of the concrete mass.

5 As a means to combat the "alkali-silica reaction", Japanese Kokai Patent Sho 62-278151 proposes adding Li_2O to the cement during the course of preparing the concrete. Specifically, 0.01 to 5% by weight of Li_2O is added to hydraulic cement that contains aggregates that can cause deleterious
10 reactions. Disclosed sources of lithium include lithia mica, leafy feldspar, lithia pyroxene (i.e. the naturally occurring spodumene mineral, which is alpha-spodumene) containing 4 to 9.5% Li_2O , and petalite. The reference teaches that the lithium source is
15 preferably added as a powder to form a uniform mixture with the cement.

U.S. Patent No. 3,331,695 discloses mortar (cement, sand and water) and paste (cement and water) compositions which can achieve an accelerated
20 hardening rate by adding 0.1 to 20% spodumene ($\text{LiAlSi}_2\text{O}_6$), based on the dry weight of the cement binder, to the cement of such cement compositions. The cement compositions of this '695 patent did not contain aggregate having the type of silica capable of
25 entering into the deleterious alkali-silica reaction to exhibit cracking and expansion.

It is therefore an object of the present invention to provide a cement admixture capable of inhibiting alkali-silica reaction. It is a further
30 object of the present invention to provide an improved concrete composition capable of inhibiting cracking and expansion as a result of alkali-silica reactions.

Summary of the Invention

5 The present invention provides a cement admixture composed of a heat treated spodumene, as fully described hereinbelow, which is capable of inhibiting expansion of the cement due to the alkali-silica reaction and to the resultant improved cement composition. The present invention also provides a method of reducing expansion in cement.

Brief Description of the Drawing

10 Figure 1 is a graph comparing the expansion effects on cement compositions containing untreated versus heat-treated spodumene according to the present invention.

Detailed Description of the Invention

15 The term "cement composition" as used herein and in the appended claims refers to compositions comprising a hydraulic cement binder and at least a sufficient amount of one aggregate having a silica content suitable to cause alkali-silica reaction.
20 Such aggregate may be, for example, fly ash, silica fume, blast furnace slag, coarse aggregate having high silica content and the like. Generally, the cement compositions applicable to the present invention are concretes composed of a hydraulic cement (generally, a
25 portland cement), fine aggregate (e.g. sand), coarse aggregate (e.g. gravel) and water, although mortars composed of a hydraulic cement, fine aggregate having

high silica content in amounts to cause alkali-silica reaction and water are also applicable. Such compositions may additionally include other admixtures such as defoaming agents, air-entraining or detraining agents, set accelerators, set retarders, water reducing agents, superplasticizers, and other components known to those skilled in the art for altering properties of the composition. The cement compositions of the present invention are formed by mixing required amounts of certain materials, e.g., a hydraulic cement, water, and fine and/or coarse aggregate, as may be applicable for the particular cement composition being formed.

The minimum amount of silica necessary to cause the alkali-silica reaction expansion varies according to the type of silica and size of the silica contained in a cement composition. For example, very fine reactive aggregate (smaller than about 45 microns or - 325 mesh U.S. Standard sieve) is not expansive but is pozzolanic, and thus adds to the cement bonding. On the other hand, opal, a very reactive hydrated silica, can cause expansion when present in about 2% or greater of the total weight of aggregate in cement compositions. Those skilled in the art can readily ascertain whether the type and quantity of silica is sufficient to cause expansion as a result of the alkali-silica reaction, by means of known test methods such as ASTM C-227 or C-441.

The present inventors have found that natural spodumene which has been heat treated, as described hereinbelow to cause it to go through phase transition from α -spodumene to β -spodumene, provides a material

- 5 -

capable of causing a significant reduction of expansion in cement due to the alkali-silica reaction.

5 The spodumene should be heated to at least 1000°C, preferably to about 1100°C. Heating above about 1400°C, and preferably above 1200°C, should be avoided to prevent melting of associated mineral impurities (gangue), which could lead to agglomeration rather than fracture due to phase change. The
10 spodumene should be heated for a time sufficient to allow the entire spodumene mass being heat treated to reach the desired temperature. Thus, the spodumene based cement admixture of the present invention is conventional spodumene which has to be heated to at least 1000°C but not greater than about 1400°C and
15 preferably from about 1100°C to about 1200°C.

 The present heat-treated spodumene product should be in the form of a free-flowing powder prior to incorporation into the cement composition. Preferably the heat-treated spodumene is ground to a particle
20 size ranging from about 1 to about 10 μ m, and is used in an amount of from about 1 to about 10% by weight based on the weight of the dry cement contained in the cement composition, preferably about 2 to 6% by weight of the dry cement. It has been found that the
25 introduction of heat-treated spodumene to cement in these amounts substantially inhibits the expansion occurring as a result of the alkali-silica reaction. For example, limiting of expansion to not more than about 0.075 percent under ASTM C-227 procedure can be
30 readily attained.

 The following is an outline of the procedures used in the example that follows. All parts and

percentages given hereinbelow and in the examples are by weight unless otherwise indicated. The examples are made for illustrative purposes only and are not meant to be a limitation on the invention as defined by the claims appended hereto.

Mortars were prepared in accordance with ASTM method C-109, sec. 10.1.1. The water/cement ratio was 0.485 and the sand/cement ratio was 2.75 with 10% of sand by weight replaced with -20+50 TECOSIL fused silica from CE Minerals. Sodium hydroxide was added and total alkali was expressed as weight percent of cement, including that present in the cement originally.

The mortars were mixed in accordance with ASTM method C-305 requirements. A Hobart mixer was used along with paddle and bowl that meets the required dimensions. The procedure for mixing was as follows:

- Water added to dry mixing bowl
- Cement added to bowl and mixer started at slow speed for 30 seconds
- Sand then added over a 30 second period with mixer on slow speed
- Mixer changed to medium speed for 30 second period
- Turn mixer off for a 1.5 minute period
- Finish mixing at medium speed for 1 minute

The spodumene was heated in a 2 $\frac{3}{4}$ " diameter x 1 $\frac{1}{2}$ " high platinum dish at 1050-1100°C in a muffle furnace for about 1 hour.

Molds were prepared in accordance with ASTM method C-490 sec. 4, except that no mineral oil was

- 7 -

used to coat the inside of the mold. The molds were lined with thick polyethylene film.

5 The storage of the molds, after bars were cast, was in accordance with ASTM method C 227, section 8.1. Bars which were in the molds were stored at 73.4°F in 100% humidity for 24 hours. The bars were then demolded and stored vertically in a metal storage box at 100°F in 100% humidity in accordance with ASTM method C-227, section 8.2. The storage box was not
10 cooled prior to opening. The water level was monitored every 7 days, but the box was not cleaned after every measurement.

Mortar bars were measured with a length comparator as described in ASTM method C 490, section
15 4.5. To simplify readings, the length comparator dial gauge was replaced with a digital dial gauge made by Chicago Instruments, Model #DPX1000. The length calibrator was calibrated with a reference bar in accordance with ASTM method C-490, section 4.5.3. An
20 initial measurement was taken when the bars were demolded and this measurement was used as the reference measurement. Measurements were made every 7 days until the expansion became so great that there was no doubt of failure. When expansions were
25 consistently small, measurements were made at less frequent intervals. Expansion was expressed as a percent change from the initial length measurement.

EXAMPLE

30 Mortar bars were made in accordance with the foregoing procedure, and various amounts of heat treated and untreated spodumene were independently

added to the mixing bowls after the sand was added, but before any appreciable mixing of the sand had occurred. The bars were stored in accordance with ASTM method C227 as detailed above, and the expansion was observed . The results are shown in Figure 1.

The addition of 1% heat-treated spodumene reduced the expansion by more than 50%, and 2% and 3% dosage of heat-treated spodumene controlled expansion almost completely. In comparison, the addition of 1%, 2% and 3% (based on cement) of untreated spodumene (-325 mesh) had little effect on expansion.

Figure I graphically shows the results of the present example. Each point on the graph represents an average test result of four (4) bars. The graph clearly shows that the C-109 mortar bars were substantially unaffected when 1, 2 and 3 weight percent untreated spodumene was used and that utilization of the subject heat-treated spodumene caused substantial inhibition to expansion. The samples containing heat-treated spodumene (especially those having 2 and 3 weight percent dosages) exhibited substantially no expansion over a 12-month period of time.



REPLACED SHEETS SG

- ☐ Description : paged to paged
☒ Claim(s) : paged⁹ to paged¹¹
☐ Drawing(s) : paged to paged
☐ Abstract : paged to paged

WHAT IS CLAIMED IS:

1. An improved cement comprising a hydraulic cement having from about 1 to about 10 weight percent of a heat-treated spodumene, wherein said spodumene has been heated to a temperature sufficient to have caused a phase transition from α -spodumene to β -spodumene

2. The admixture of Claim 1 wherein said temperature to which said spodumene is heated to is at least about 1000°C.

3. The admixture of Claim 1 wherein said temperature to which said spodumene is heated to is from about 1100°C to about 1200°C.

4. A cement composition comprising a hydraulic cement binder, an aggregate comprising a sufficient amount of silica to react with alkali present in said composition and cause expansion, and spodumene that has been heated to a temperature sufficient to have caused a phase transition from α -spodumene to β -spodumene, said spodumene being present in an amount effective for reducing said expansion caused by reaction of said silica with said alkali.

5. The cement composition of Claim 4, where said temperature to which said spodumene is heated to is at least about 1000°C.





6. The cement composition of Claim 4, where said temperature to which said spodumene is heated to is from about 1100°C to about 1200°C.

5 7. The cement composition of Claim 4, wherein said spodumene is added in an amount of from about 1% to about 10% by weight based on the hydraulic cement in said composition.

10 8. The cement composition of Claim 4, where said spodumene has a particle size ranging from about 1 to about 10 μ m.

15 9. The cement composition of Claim 4 wherein said spodumene has been subjected to a temperature of at least about 1000°C, is present in from about 2% to about 6% by weight based on the weight of hydraulic cement in said composition, and has a particle size of from about 1 to about 10 μ m.

20 10. The cement composition of Claim 4 wherein the composition is a concrete composed of hydraulic cement, fine aggregate, coarse aggregate and water and at least one of said aggregates contains sufficient amount of silica to react with alkali.

25 11. The cement composition of Claim 4 wherein the composition is a mortar composed of hydraulic cement, fine aggregate and water and said fine aggregate contains sufficient amount of silica to react with alkali.





5 12. A method of reducing expansion of cement compositions caused by the alkali-silica reaction, comprising adding spodumene to cement composition having aggregate with a sufficient amount of silica to
10 react with alkali present in said cement and cause expansion, wherein said spodumene has been heated to a temperature sufficient to have caused a phase transition from α -spodumene to β -spodumene and is added in an amount effective to reduce said expansion caused by reaction of said silica with said alkali.

13. The method of Claim 12, wherein said spodumene is added in an amount of from about 1% to about 10% by weight based on the weight of hydraulic cement.

15 14. The method of Claim 12, wherein said spodumene is heated to a temperature of at least about 1000°C.

20 15. The method of Claim 12, wherein said spodumene has a particle size ranging from about 1 to about 10 μm .

25 16. The method of Claim 12 wherein said spodumene has been subjected to a temperature of at least about 1000°C, is present in from about 2% to about 6% by weight based on the weight of hydraulic cement in the treated composition, and has a particle size of from about 1 to about 10 μm .

