

TIME BASE COMPRISING AN INTEGRATED
MICROMECHANICAL RING RESONATOR

The present invention relates to a time base, i.e. a device comprising a resonator and an integrated electronic circuit for driving the resonator into oscillation and for producing, in response to this oscillation, a signal having a determined frequency.

5 Time bases, or frequency standards, are required in a large variety of electronic devices, ranging from wristwatches and other timepieces to complex telecommunication devices. Such time bases are typically formed by an oscillator including a quartz resonator and an electronic circuit for driving the resonator into oscillation. An additional division chain may be used to divide the frequency of the
10 signal produced by the oscillator in order to obtain a lower frequency. Other parts of the circuit may serve to adjust the frequency, for example by adjusting the division ratio of the division chain. The components of the electronic circuit are advantageously integrated onto a single semiconductor substrate in CMOS technology. Other functions, not directly related to the frequency processing, may be
15 integrated onto the same substrate.

Advantages of quartz resonators are their high quality factor Q leading to good frequency stability and low power consumption as well as their good temperature stability. A disadvantage of typical time bases using quartz resonators however resides in the fact that two components, namely the quartz resonator and the
20 integrated electronic circuit, are required in order to provide a high-precision frequency. A discrete quartz resonator requires board space which is scarce in many cases. For instance, a standard quartz resonator for wristwatch applications requires space of the order of $2 \times 2 \times 6 \text{ mm}^3$. Moreover, additional costs are caused by the assembly and connection of the two components. Yet, space and assembly costs are
25 major issues, especially in the growing field of portable electronic devices.

It is thus a principal object of the present invention to provide a solution to the above-mentioned problems by providing a time base comprising an integrated resonator.

Another object of the present invention is to provide a time base that may be
30 fully integrated on a single substrate, that is suitable for mass production and that is compatible with CMOS technology.

Still another object of the present invention is to provide a time base comprising a resonator having an improved quality factor Q and thereby a greater frequency stability and low power consumption.

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Yet another object of the present invention is to provide such a time base which is low-priced and requires only a very small surface area on a semiconductor chip.

Accordingly, there is provided a time base comprising a resonator and an
5 integrated electronic circuit for driving said resonator into oscillation and for producing, in response to said oscillation, a signal having a determined frequency, characterised in that said resonator is an integrated micromechanical ring resonator supported above a substrate and adapted to oscillate, according to a first oscillation mode, around an axis of rotation substantially perpendicular to said substrate, said ring
10 resonator comprising :

- a central post extending from said substrate along said axis of rotation;
- a free-standing oscillating structure connected to said central post and

including :

- an outer ring coaxial with said axis of rotation; and
- 15 - a plurality of spring elements disposed symmetrically around said central post and connecting said outer ring to said central post;

and

- at least one pair of diametrically opposed electrode structures disposed around said outer ring and connected to said integrated electronic circuit.

20 An advantage of the time base according to the present invention lies in the fact that the micromechanical ring resonator exhibits a high quality factor Q. Quality factors as high as 2×10^5 have been measured. For comparison, tuning-fork quartz resonators usually exhibit values between 5×10^4 and 1×10^5 after laser trimming of the fork tines. Different design features favouring a high quality factor Q are the object of
25 dependent claims and will be described hereinafter in detail.

In addition, for a given resonant frequency, the surface area required on the substrate to form the ring resonator is small in comparison with other resonators.

According to one aspect of the invention, the electronic circuit is advantageously integrated on the substrate together with the micromechanical ring
30 resonator, thereby leading to a low-priced time base. A lower price is also obtained by wafer-level packaging of the resonator using wafer-bonding technology.

It must be pointed out that ring resonators having similar features are known from sensing devices, such as angular rate sensors, accelerometers or gyroscopes. For instance U.S. Patent No. 5,450,751 to Putty et al. and U.S. Patent No. 5,547,093
35 to Sparks both disclose a micromechanical ring resonator for a vibratory gyroscope comprising a plated metal ring and spring system supported above a silicon substrate. U.S. Patent No. 5,872,313 to Zarabadi et al. discloses a variant of the above sensor

which is configured to exhibit minimum sensitivity to temperature variation. U.S. Patent No. 5,025,346 also discloses a ring resonator for use as a micro-sensor in a gyroscope or an angular rate sensor.

None of the above-cited documents however indicates or suggests using such
5 a type of ring resonator in an oscillator circuit to act as a frequency standard or time base. Moreover, a number of design features (e.g. the shape and number of spring elements) of the ring resonators disclosed in these documents are such that they would not be suitable for horological applications where frequency stability and low power consumption are essential. For instance, the resonating structures disclosed in
10 U.S. Patent No. 5,025,346 exhibit a quality factor ranging from 20 to 140 which is too low for being used in a highly precise time base in horological applications, whereas quartz resonators used in horological applications exhibit quality factors of the order of 1×10^4 to 1×10^5 .

According to the present invention, various design features are proposed which
15 lead to a high quality factor Q, a high stability of the oscillation frequency against variations in the amplitude of the driving voltage, and tolerance of fabrication process variations. In fact, one of the major objectives for an application as an oscillator is a high quality factor Q. A high quality factor Q results in a stable oscillation with low phase noise and low power consumption, as is required for horological applications.

20 According to other aspects of the present invention, various mechanisms are proposed for substantially compensating for the effect of temperature on the resonant frequency of the ring resonator.

According to another aspect of the present invention, a temperature measuring circuit may further be integrated on the substrate in order to compensate for the effect
25 of temperature on the frequency of the signal produced by the time base. Such compensation of the resonator's temperature dependency may easily be effected since the ring resonator of the present invention has the advantage of exhibiting substantially linear temperature characteristics.

According to still another aspect of the present invention, a second
30 micromechanical ring resonator may be formed on the substrate in order to allow temperature compensation. According to another aspect of the invention, temperature compensation is also achieved by using a single micromechanical ring resonator which is operated simultaneously with two oscillation modes having different resonant frequencies.

35 Other aspects, features and advantages of the present invention will be apparent upon reading the following detailed description of non-limiting examples and embodiments made with reference to the accompanying drawings, in which :

- Figure 1 is a top view illustrating schematically a first embodiment of a time base according to the present invention comprising a micromechanical ring resonator and an integrated electronic circuit;
 - Figure 2 is a detailed view of the central post of the micromechanical ring resonator and its junctions with the spring elements;
 - Figure 3 is a detailed view of a portion of the outer ring with its junctions with the spring elements;
 - Figure 4 is a cross-sectional view of the micromechanical ring resonator of Figure 1 taken along line A-A';
 - Figure 5 shows an idealized straight spring element with a section of the outer ring;
 - Figure 6 shows a top view illustrating schematically a second embodiment of a time base according to the present invention;
 - Figures 7a to 7c show detailed top views of three different designs intended to prevent the ring resonator from sticking on the electrode structures;
 - Figure 8 shows a top view illustrating an improvement of the first embodiment shown in Figure 1;
 - Figure 9 is a cross-sectional view of the embodiment of Figure 8 taken along line A-A';
 - Figures 10a and 10b are two top views illustrating two variants of a mechanism for altering the mass moment of inertia of the ring resonator as a function of temperature, in order to substantially compensate for the effect of temperature on the resonant frequency of the ring resonator;
 - Figures 11a and 11b are respectively top and cross-sectional views illustrating a second mode of oscillation where the resonator performs a tilting oscillation; and
 - Figures 12a and 12b are respectively top and cross-sectional views illustrating another second mode of oscillation where the resonator performs a vertical oscillation perpendicular to the substrate plane.
- Figure 1 schematically shows a top view of a first embodiment of the present invention. There is shown an integrated time base, indicated generally by reference numeral 1, comprising a resonator 4 and an integrated electronic circuit 3 for driving the resonator into oscillation and for producing, in response to this oscillation, a signal having a determined frequency. Figure 4 shows a cross-sectional view of the ring resonator 4 taken along line A-A' as shown in Figure 1.

The integrated electronic circuit 3 is not shown in detail since this circuit may easily be designed by those skilled in the art. Preferably both the integrated electronic

circuit 3 and the resonator 4 are realized and integrated on a same substrate 2 as illustrated in Figure 1. A preferred substrate material is silicon, but other similar materials known by those skilled in the art to be equally suitable for realising the time base of the present invention may be used.

5 According to the present invention, the resonator 4 is realised in the form of a monolithic micromechanical resonating ring, hereinafter referred to as a micromechanical ring resonator, which is essentially supported above the substrate 2 and adapted to oscillate around an axis of rotation O substantially perpendicular to the substrate 2. The ring resonator 4 essentially comprises a central post 5 extending
10 from the substrate 2 along the axis of rotation O and a free-standing oscillating structure, indicated globally by reference numeral 6, connected to the central post 5.

 The free-standing oscillating structure 6 includes an outer ring 60 coaxial with the axis of rotation O, and a plurality of spring elements 62 disposed symmetrically around the central post 5 and connecting the outer ring 60 to the central post 5. The
15 spring elements 62 are essentially formed as curved rod-shaped spring elements. It will be appreciated that the central post 5 constitutes the only mechanical connection of the ring resonator 4 with the substrate 2 and that oscillation of the resonator takes place in a plane substantially parallel to the surface of the substrate 2.

 The ring resonator 4 according to the present invention further comprises pairs
20 of diametrically opposed electrode structures surrounding the outer ring 60, indicated by reference numeral 9 in Figure 1. According to this first embodiment, comb-shaped members 8 are provided on the outer ring 60 of the free-standing oscillating structure 6. These comb-shaped members 8 form a part of the electrode structures of the ring and each include a base member 80 extending radially from the outer ring 60 and first
25 and second lateral members, indicated respectively by reference numerals 82 and 84, that extend substantially perpendicularly from both sides of the base member 80.

 The electrode structures 9 comprise first and second comb-shaped electrode structures 91 and 93 surrounding the outer ring 60 in such a way that they mesh with the comb-shaped members 8 of the free-standing oscillating structures. More
30 particularly, according to this embodiment, the first comb-shaped electrode structure 91 includes first electrodes 92 and meshes with comb-shaped member 8 so that the first electrodes 92 are adjacent to the first lateral members 82. Similarly, the second comb-shaped electrode structure 93 (disposed opposite the first comb-shaped electrode structure 91) includes second electrodes 94 and meshes with comb-shaped
35 member 8 so that the second electrodes 94 are adjacent to the second lateral members 84. As shown in Figure 1, the lateral members 82, 84 and the electrodes 92, 94 of the first and second electrode structures 91, 93 are preferably designed so as to

have the shape of an arc of a circle concentric with the outer ring 60.

In this embodiment, the first comb-shaped electrode structures 91 serve to electrostatically drive the ring resonator 4 into oscillation, and the second comb-shaped electrode structure 93, which are disposed on the other side of the base members 80, serve to capacitively sense the oscillation of the resonator. The first electrode structures 91 surrounding the resonator 4 are connected together via a first conductor 11 formed on the substrate 2, and, similarly, the second electrode structures 93 are connected together via a second conductor 12 formed on the substrate 2. These conductors 11, 12 as well as a third conductor 13 providing an electrical contact to the ring via the central post 5 are connected to appropriate terminals of the electronic circuit 3.

Figure 4 shows a cross-sectional view of the ring resonator 4 taken along line A-A' as illustrated in Figure 1. Thickness and other dimensions are not to scale. There is shown the substrate 2, the central post 5 along the axis of rotation O of the ring resonator, the free-standing oscillating structure 6 including the outer ring 60 and the spring elements 62, the lateral members 82 of the comb-shaped members 8, the electrodes 92 of the first comb-shaped electrode structures 91, and the first and second connectors 11, 12 that respectively connect the electrode structures 91 and 93 surrounding the outer ring 60. Figure 4 further shows a first insulating layer 20, such as a silicon oxide layer, formed above the surface of substrate 2, beneath the ring resonator 4 and onto which are formed the first and second conductors 11, 12. A second insulating layer 21, such as another oxide layer or silicon nitride layer, is formed above the first layer 20 below the ring resonator.

The resonating ring structure is preferably manufactured by means of silicon surface micro-machining techniques which are familiar to those skilled in the art and will therefore not be described here. One such technique makes use of a poly-silicon layer deposited on top of a so-called "sacrificial layer" in order to form the free-standing structures of the resonator. Another technique uses a buried oxide layer, such as e.g. in a silicon on insulator (SOI) wafer, as the sacrificial layer and results in a free-standing structure made of mono-crystalline silicon. Other material and processing techniques, however, may also be used to realise the micromechanical ring resonator according to the present invention.

One of the major objectives for an application as a time base or frequency standard is a high quality factor Q of the resonator. A high quality factor Q results in a stable oscillation with low phase noise and low power consumption as is required for horological applications. The quality factor Q of the micromechanical ring resonator according to the present invention is very high due to a number of advantageous

design features that will be explained below. As already mentioned hereinabove, quality factors as high as 2×10^5 have been measured on these structures. For comparison, tuning-fork quartz resonators usually exhibit values between 5×10^4 and 1×10^5 after laser trimming of the fork tines.

5 The shape of the spring elements 62 connecting the outer ring 60 to the central post 5 is optimised so as to obtain a high quality factor Q. In contrast to the conditions present when using straight spring elements, the tensions along the bending line are, in the present case, homogeneously distributed along the spring element. The curved shape is such that energy losses per oscillation period are kept
10 minimal.

 In addition, junctions 63 of the spring elements 62 with the central post 5 are substantially perpendicular, as shown in Figure 2. Preferably, round shapes or fillets 63a are provided at the junctions 63. These fillets 63a prevent notch tensions during oscillation, thereby favouring an elevated quality factor Q, as substantially no energy
15 is dissipated in the central post 5 during oscillation. Furthermore, the central post 5 remains substantially free of tension, which again favours a high quality factor Q. Figure 3 shows the junctions 64 of the spring elements 62 with outer ring 60. Here also, substantially perpendicular junctions 64 and fillets 64a are preferred designs.

 Using a plurality of spring elements 62 rather than the minimum of three
20 required for a well-defined suspension increases the quality factor Q. Due to the fact that minor geometrical variations (e.g. as a result of spatial fluctuations in processing) as well as material inhomogeneities are averaged over the plurality of spring elements, the quality factor Q increases with the number of spring elements. The upper limit is given by geometrical restrictions due to the design rules of the micro-
25 structuring process. The number of spring elements is therefore comprised between four and fifty, and preferably is of the order of twenty.

 Another element favouring a high quality factor Q of the ring resonator is the perfect rotationally symmetrical structure, where the centre of gravity of the entire structure remains motionless. Non-linear effects, present in most other resonator
30 designs, are thereby removed to a large extent.

 The resonant frequency of the ring resonator can be adjusted over a wide range by changing the geometrical dimensions of the device. The ring resonator can be looked at as a plurality of spring elements connected to a segment of the outer ring. In a zero-order approximation, and in order to obtain a close algebraic
35 expression for the resonant frequency, one can study the case of a straight spring element 22 with a segment 27 of the outer ring 60, as shown in Figure 5. The resonant frequency f_r of this structure reads :

$$f_r \approx \frac{1}{2\pi} \sqrt{\frac{3 \cdot E \cdot J}{l^3 (m_r + 0.24 \cdot m_s)}}$$

where $J = d \cdot w^3 / 12$ is the surface moment of inertia of the structure, E is the
 5 elasticity module, d , w and l are the thickness, width and length of the straight spring
 element 22, respectively, and m_r , m_s are the masses of the ring segment 27 and
 spring element 22, respectively. It can be easily seen from the above formula, that the
 resonance frequency can be influenced by varying the width and/or length of the
 spring elements or by varying the mass of the outer ring (including the mass of the
 10 comb-shaped members 8), again via its geometrical dimensions. Scaling of the entire
 structure further widens the accessible frequency range.

It is important for mass production of such ring resonators to keep the resonant
 frequency from one chip to the other within small tolerances. Tolerances in the
 resonant frequency due to slight variations in process parameters can be greatly
 15 reduced by carefully dimensioning the ring and springs. This can again be shown
 using the example of Figure 5. The resonant frequency will be lower than the
 projected frequency if the width of the spring elements 22, indicated by reference
 numeral 26, is smaller after processing, e.g. due to an over-etch, than a desired width
 25. However, if one considers that at the same time the mass of the ring 60 (as well
 as the mass of the base members 80 and lateral members 82, 84) is lowered due to
 the same over-etch, the decrease of the resonant frequency will be compensated for
 by the reduction of the masses. Openings in the ring and the bars (not shown in the
 Figures), which may be necessary for processing the structure, favour this effect.

The surface area required by the micromechanical ring resonator according to
 25 the present invention is very small with respect to the resonant frequency obtained.
 For instance, a ring resonator according to the present invention designed for a rather
 low frequency of 32 kHz requires a surface of well below 1 mm^2 . Conventional
 structures require relatively large structures in order to obtain such a low frequency.
 For a given geometrical layout, the dimensions and frequency are inversely related,
 30 i.e. the larger the geometrical dimensions, the lower the frequency. For comparison,
 EP 0 795 953 describes a silicon resonator requiring a surface of about 1.9 mm^2 for a
 higher frequency of 1 MHz. It is obvious that the substrate surface area required by
 the resonator is directly related to the price of the integrated time base.

The resonant frequency of the ring resonator is, within the temperature range
 35 of 0 to 60°C , in good approximation, a linear function of temperature. At a resonant
 frequency of 45 kHz, it has been observed that the thermal coefficient of the resonant

frequency is of the order of $-25 \text{ ppm}/^{\circ}\text{C}$. It is thus desirable to incorporate, in the same substrate 2, a temperature measuring circuit having an output signal which may be used to compensate for the frequency variation by adequately adjusting the frequency of the signal produced by the time base.

5 To this effect, the time base according to the present invention may advantageously comprise an integrated temperature measuring circuit (not shown). An example of such a temperature measuring circuit is described in the article "Smart Temperature Sensor in CMOS Technology" by P. Krümenacher and H. Oguey, in "Sensors and Actuators", A21-A23 (1990), pages 636 to 638. Here, temperature
10 compensation is achieved by acting on the division ratio of the division chain, for instance using an inhibition technique well known to those skilled in the art.

Alternatively, two ring resonators with different resonant frequencies may be integrated onto the same chip, such arrangement allowing the chip temperature to be precisely determined by measuring the frequency difference of the two resonators
15 (both ring resonators have the same temperature coefficient since they are made from the same material).

The advantage of using integrated time bases according to the present invention is twofold: Firstly, the temperature dependency of the ring resonator is linear which facilitates the electronic signal treatment necessary to compensate for the
20 temperature. Secondly and more importantly, the small size and monolithic integration of the ring resonator allows a second resonator to be provided with only a slight increase in chip size and without further external connections.

Alternatively, according to a particularly advantageous embodiment of the invention, it is possible to use a single ring resonator which operates simultaneously
25 with two oscillation modes. A first of these modes is the above described rotational mode. A second oscillation mode may be a tilting oscillation mode, wherein the free-standing structure 6 performs a tilting oscillation against the substrate plane. This tilting oscillation mode may be excited electrostatically and sensed capacitively by using further electrodes on the substrate under the ring area. The two modes are
30 selected to have different frequencies so that temperature compensation may be achieved by measuring the frequency difference. A schematic illustration of the above mentioned tilt mode is shown in Figures 11a and 11b. As shown in these figures, two sets of electrodes 100 and 120 (in this case four) having substantially the shape of arcs of circles are disposed on the substrate under the ring 60 so that the first set of
35 electrodes 100 drives the structure 6 into a tilting oscillation and the second set of electrodes 120 senses this tilting oscillation. The set of driving electrodes 100 and the set of sensing electrodes 120 are disposed on opposite sides of the structure 6 with

respect to the central post 5 (respectively on the left and right sides in Figure 11a).

A second oscillation mode may be a vertical oscillation mode, wherein the free-standing structure 6 performs a vertical oscillation perpendicular to the substrate plane, i.e. the free-standing structure 6 oscillates in a direction parallel to the axis of rotation O. A schematic illustration of the above mentioned perpendicular mode is shown in Figures 12a and 12b. As shown in these figures, two sets of electrodes 130 and 150 are disposed on the substrate under the ring 60 so that the first set of electrodes 130 drives the structures 6 into an oscillation perpendicular to the substrate plane and the second set of electrodes 150 senses this oscillation. In contrast to the tilting mode, the set of driving and sensing electrodes 130, 150 are disposed symmetrically around the central post 5, i.e. the sets of electrodes each comprise diametrically opposed electrodes.

As already mentioned, the comb-shaped electrode structures 91 shown in the embodiment of Figure 1 serve to electrostatically drive the ring resonator into oscillation and the opposite comb-shaped electrode structures 93 serve to capacitively sense this mechanical oscillation. An alternating voltage signal is applied to electrode structures 91 resulting in electrostatic forces on the ring and oscillation thereof, which, in turn, induces an alternating signal on the opposite set of electrode structures 93, when the resonator operates. It will be understood that electrode structures 91 and 93 are interchangeable.

Since there is a parabolic relationship between the voltage applied on the electrodes and the resulting force on the ring and, it is desirable to add a constant direct voltage to the alternating voltage so as to obtain a substantially linear force-voltage relationship. In the schematic representation of Figure 1, there are shown three signal lines or conductors 11 to 13 that are respectively connected to electrode structures 91, electrode structures 93 and central post 5. These lines serve to drive the ring resonator into oscillation and to sense this oscillation via the respective electrode structures.

According to a first variant, conductor 13 may be used to apply the direct voltage component to the ring resonator via the central post 5, while the alternating voltage component is applied to electrode structures 91 via conductor 11, conductor 12 being used to sense the resulting signal. According to a second variant, the alternating driving voltage and the direct voltage component may be superposed on electrode structures 91 via conductor 11 while the ring resonator is tied to a fixed potential, such as e.g. ground, via conductor 13. Conductor 12 is used to sense the signal in this case. It will be appreciated that electrode structures 91 and 93 are interchangeable and that electrode structures 93 may alternatively be used for driving,

electrode structures 91 being used for sensing.

Alternatively, sensing may be done by detecting a change in impedance at resonance. As represented in Figure 6, such a solution requires only two conductors, 11 and 13, and an electrode structure 9* comprising a single set of comb-shaped electrode structures 91 connected to conductor 11 (the comb-shaped members 8* are modified accordingly and only comprise first lateral members 82). According to a first variant, the alternating driving voltage is applied, via conductor 11, to the single set of electrode structures 91, and the direct voltage component is applied to the ring via conductor 13. According to another variant, the sum of alternating and direct driving voltages can be applied to electrode structures 91 via conductor 11, the ring being in this case tied via conductor 13 to a fixed potential such as e.g. ground.

The two-conductor option provides two advantages, namely (i) a reduction in the diameter of the entire structure since a second conductor and a second set of electrode structures surrounding the ring is no longer required, and (ii) the possibility of providing a larger number of comb-shaped electrode structures 91 along the periphery of the outer ring 60, resulting in an enhanced signal.

The different modes of operation of the ring resonator are summarized in the following table. It will be appreciated that, in any of the above-mentioned variants, the signals applied to the driving electrodes and the ring, namely the alternating driving voltage and the direct voltage component, are perfectly interchangeable.

	Electrodes 91	Ring	Electrodes 93	Remarks
3 Conductors	AC-driving	DC-bias	Sensing	Electrodes 91 and 93 are interchangeable
	AC-driving + DC bias	Fixed potential, e.g. ground	Sensing	
	DC-bias	AC-driving	Sensing	
	Fixed potential, e.g. ground	AC-driving + DC-bias	Sensing	
2 Conductors	AC-driving	DC-bias	-	Sensing is done by detecting a change in impedance at resonance
	AC-driving + DC bias	Fixed potential, e.g. ground	-	
	DC-bias	AC-driving	-	
	Fixed potential, e.g. ground	AC-driving + DC-bias	-	

The fact that the lateral members 82, 84 and the electrodes 92, 94 are of

curved shape and concentric with outer ring 60 reduces non-linearities in the electro-mechanical coupling, resulting in a high quality factor Q on the one hand and a resonant frequency of the ring resonator which is essentially independent of the amplitude of alternating and direct driving voltages on the other hand. Furthermore,
5 the micromechanical ring resonator according to the present invention can be driven with voltages as low as 1.5 V, which is a major advantage for portable electronic applications.

In addition, due to electrostatic driving and capacitive sensing, and due to the high quality factor Q determined by the design, the power consumption of the ring
10 resonator is ten to hundred times lower than that of a quartz, which is of particular interest for portable electronics applications.

Figures 7a to 7c show three different advantageous design features intended to prevent the ring resonator from sticking in case of a shock. According to a first variant shown in Figure 7a, stop structures 28 disposed on the substrate 2 are
15 provided at outer ends 80a of the base members 80. These stop structures 28 are designed so as to limit the angular movement of the ring structure 6 and therefore prevent the free-standing oscillating structure 6 from sticking on the electrode structures 9 when excessive angular movements take place due, for instance, to mechanical shocks.

Alternatively, as shown in Figure 7b, extremities 82a, 84a of the lateral
20 members 82, 84 and/or extremities 92a, 94a of the electrodes 92, 94 may be designed so as to exhibit a pointed shape or at least a suitably small surface area so as to prevent sticking.

Finally, as shown in the variant of Figure 7c, one 82*, 84* of the lateral
25 members 82, 84 can be made longer than the others, thereby reducing the adhesion forces when the comb-shaped members 8 and the comb-shaped electrode structures 91, 93 get into mechanical contact with each other. Obviously, the same effect may be obtained when one of electrodes 92 and 94 is longer than the others.

Figures 8 and 9 show an improvement of the micromechanical ring resonator 4
30 according to the present invention which is illustrated in Figure 1. Figure 9 shows a cross-sectional view of Figure 8 taken along line A-A'. A conductive pattern 31 is provided on (or below) the surface of the substrate 2 under at least part of the free-standing oscillating structure 6, i.e. spring elements 62, outer ring 60, as well as comb-shaped members 8, the shape of this conductive pattern 31 being essentially a
35 projection of the free-standing oscillating structure 6 on the surface of the substrate 2. Connecting this conductive pattern 31 to the same potential as the free-standing oscillating structure 6 suppresses forces perpendicular to the substrate 2 between the

ring resonator 4 and the surface of the substrate 2 leading to a resonant frequency which is independent of the direct voltage component.

Figures 10a and 10b show further improvements of the micromechanical ring resonator 4 according to the present invention which allow the temperature coefficient of the resonant frequency to be reduced to a value close to zero. Two main factors determine the temperature characteristics of the ring resonator. Firstly, Young's modulus E of the material used to realize the vibrating structure decreases with increasing temperature resulting in a reduced stiffness of the spring elements 62 and therefore a lower resonant frequency. Secondly, due to thermal expansion, the diameter of the ring will increase with increasing temperature resulting in an increased mass moment of inertia of the structure, which, in turn, also reduces the resonant frequency.

Different thermal expansion coefficients of different materials can be used to introduce a compensation mechanism 65, as sketched in Figure 10a or 10b. As shown in Figures 10a and 10b, a plurality of thermally compensating members 65 (only one is shown in the Figures) are attached to the outer ring 60. These thermally compensating members 65 are designed to alter the mass moment of inertia of the free-standing oscillating structure 6 as a function of temperature so as to substantially compensate for the effect of temperature on the resonant frequency of the resonator 4. To this effect, the members 65 include a weight member 66 connected to the outer ring 60 by means of a connecting member 67 comprising first and second layers 68, 69 made respectively of first and second materials having different thermal coefficients. The materials are chosen so that the thermal expansion coefficient α_{th1} of the first layer 68 is smaller than the thermal expansion coefficient α_{th2} of the second layer 69. In a preferred embodiment, the first material is silicon and the second material is a metal, preferably aluminium.

The design of the mechanism 65 according to Figure 10a is such that, with increasing temperature, the connecting member 67 straightens due to the different thermal expansion of the first and second layers 68, 69. As a consequence, the weight members 66 move towards the centre of the ring, i.e. closer to the axis of rotation O of the oscillating structure 6, thereby reducing the mass moment of inertia of the ring resonator, resulting in an increase of the resonant frequency which substantially counteracts the effect of the Young's modulus and the thermal expansion of the ring on the resonant frequency. Such thermal compensation mechanisms can alternatively be attached to the outer side of the ring 60, as shown in Figure 10b, or to some other part of the free-standing oscillating structure 6 so as to alter its mass moment of inertia as a function of temperature. The layout and fabrication of the members 65

have to be realized so that the weight members 66 move towards the axis of rotation O of the ring resonator when temperature increases.

Having described the invention with regard to certain specific embodiments, it is to be understood that these embodiments are not meant as limitations of the
5 invention. Indeed, various modifications and/or adaptations may become apparent to those skilled in the art without departing from the scope of the annexed claims.



CLAIMS

1. Time base comprising a resonator (4) and an integrated electronic circuit (3) for driving said resonator (4) into oscillation and for producing, in response to said oscillation, a signal having a determined frequency, characterised in that said resonator is an integrated micromechanical ring resonator (4) supported above a substrate (2) and adapted to oscillate, according to a first oscillation mode, around an axis of rotation (O) substantially perpendicular to said substrate (2), said ring resonator (4) comprising :
- 10 - a central post (5) extending from said substrate (2) along said axis of rotation (O);
- a free-standing oscillating structure (6) connected to said central post (5) and including :
- an outer ring (60) coaxial with said axis of rotation (O); and
- 15 - a plurality of spring elements (62) disposed symmetrically around said central post (5) and connecting said outer ring (60) to said central post (5);
- and
- at least one pair of diametrically opposed electrode structures (9; 9*) disposed around said outer ring (60) and connected to said integrated electronic
- 20 circuit (3).
2. Time base according to claim 1, characterised in that said electronic circuit (3) is integrated on said substrate (2) together with said micromechanical ring resonator (4).
3. Time base according to claim 1, characterised in that said spring
- 25 elements (62) have a curved shape and are connected substantially perpendicularly to said central post (5) by first junctions (63).
4. Time base according to claim 3, characterised in that said spring elements (62) are connected substantially perpendicularly to said outer ring (60) by second junctions (64).
- 30 5. Time base according to claim 3 or 4, characterised in that said junctions (63, 64) are provided with round fillets (63a, 64a).
6. Time base according to claim 1, characterised in that the number of spring elements (62) is comprised between four and fifty, and preferably is of the order of twenty.
- 35 7. Time base according to claim 1, characterised in that said free-standing oscillating structure (6) further comprises at least one pair of diametrically opposed comb-shaped members (8) disposed around said outer ring (60) and including :



- a base member (80) extending radially from said outer ring (60);
 - at least a first lateral member (82) extending substantially perpendicularly from a first side of said base member (80); and
 - at least a second lateral member (84) extending substantially perpendicularly from a second side of said base member (80) opposite said first side;
- 5 and in that each of said electrode structures (9) comprises :
- a first comb-shaped electrode structure (91) meshing with said comb-shaped member (8) and comprising first electrodes (92) adjacent to said first lateral members (82); and
- 10 - a second comb-shaped electrode structure (93) meshing with said comb-shaped member (8) and comprising second electrodes (94) adjacent to said second lateral members (84).
8. Time base according to claim 7, characterised in that :
- said first comb-shaped electrode structures (91) are used to drive said ring resonator (4) into oscillation;
- 15 - said free-standing oscillating structure (6) is tied via said central post (5) to a fixed potential; and
- said second comb-shaped electrode structures (93) are used to sense a signal resulting from the oscillation of said ring resonator (4),
- 20 a constant direct voltage component being added to one or both of said first comb-shaped electrode structures (91) or free-standing oscillating structure (6).
9. Time base according to claim 1, characterised in that said free-standing oscillating structure (6) further comprises at least one pair of diametrically opposed comb-shaped members (8*) disposed around said outer ring (60) and including :
- 25 - a base member (80) extending radially from said outer ring (60); and
- at least a first lateral member (82) extending substantially perpendicularly from a first side of said base member (80);
- and in that each of said electrode structures (9*) comprises :
- a comb-shaped electrode structure (91) meshing with said comb-shaped member (8) and comprising first electrodes (92) adjacent to said first lateral members (82).
- 30
10. Time base according to claim 9, characterised in that :
- said comb-shaped electrode structures (91) are used to drive said ring resonator (4) into oscillation; and
- 35 - said free-standing oscillation structure (6) is tied via said central post (5) to a fixed potential,
- a constant direct voltage component being added to one or both of said comb-



shaped electrode structures (91) or free-standing oscillating structure (6), and sensing being done by detecting a change in impedance at resonance.

11. Time base according to claim 7 or 9, characterised in that said lateral members (82, 84) and said electrodes (92, 94) have a shape of an arc of a circle
5 concentric with said outer ring (60).

12. Time base according to claim 7 or 9, characterised in that at least one stop structure (28) is provided on said substrate (2) adjacent to an outer end (80a) of at least one base member (80) in order to limit angular and/or tilt movements and prevent said free-standing oscillating structure (6) from sticking in case of a shock.

10 13. Time base according to claim 7 or 9, characterised in that extremities (82a, 84a) of said lateral members (82, 84) and/or extremities (92a, 94a) of said electrodes (92, 93) are pointed or have a suitably small surface area so as to prevent said free-standing oscillating structure (6) from sticking in case of a shock.

14. Time base according to claim 7 or 9, characterised in that at least one of
15 said lateral members (82, 84) and/or one of said electrodes (92, 94) is longer than the others so as to prevent said free-standing oscillating structure (6) from sticking in case of a shock.

15. Time base according to claim 1, characterised in that a conductive pattern (31) having substantially the shape of said free-standing oscillating structure
20 (6) is provided on a surface of said substrate (2) under at least a part of said free-standing oscillating structure (6), said free-standing oscillating structure (6) and said conductive pattern being put at a same potential.

16. Time base according to claim 1, characterised in that said free-standing oscillating structure (6) further comprises at least a first pair of diametrically opposed
25 thermally compensating members (65) disposed around said outer ring (60), said thermally compensating members (65) being adapted to alter a mass moment of inertia of said free-standing oscillating structure (6) as a function of temperature so as to compensate for the effect of temperature on the resonant frequency of the ring resonator (4).

30 17. Time base according to claim 16, characterised in that each of said thermally compensating members (65) comprises a weight member (66) connected to said outer ring (60) by means of a connecting member (67) comprising first and second layers (68, 69) made respectively of first and second materials having different thermal coefficients, said connecting member (67) being adapted to gradually bring
35 said weight member (66) closer to said axis of rotation (O) when temperature increases, thereby reducing the mass moment of inertia of said free-standing oscillating structure (6).



18. Time base according to claim 1, characterised in that it further comprises an integrated temperature measuring circuit intended to compensate for the effect of temperature on the frequency of the signal produced by said time base.

19. Time base according to claim 1, characterised in that it further comprises
5 a second micromechanical ring resonator supported above said substrate (2) and adapted to oscillate at a resonant frequency which is different from the resonant frequency of the other resonator, a frequency difference between both resonant frequencies being used for compensating for the effect of temperature on the frequency of the signal produced by said time base.

10 20. Time base according to claim 1, characterised in that electrodes (100, 120; 130, 150) are positioned under said free-standing oscillating structure (6) in such a way as to drive and sense a second oscillation mode having a resonant frequency which is different from the resonant frequency of said first oscillation mode, a
15 frequency difference between the resonant frequencies of both oscillation modes being used for compensating for the effect of temperature on the frequency of the signal produced by said time base.

21. Time base according to claim 20, characterised in that said second oscillation mode is a tilting oscillation mode.

22. Time base according to claim 20, characterised in that said second
20 oscillation mode is a vertical oscillation mode parallel to said axis of rotation (O).

23. Time base according to claim 1, characterised in that said substrate (2) and said ring resonator (4) are made of silicon material.